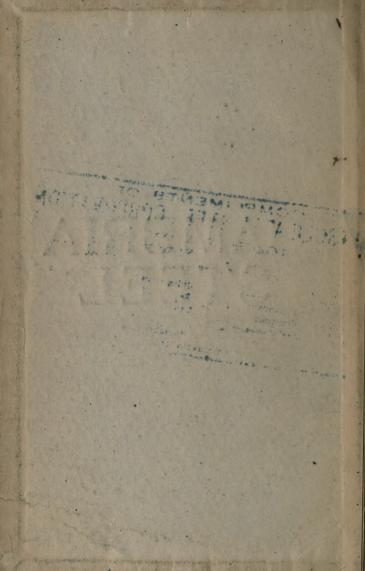


# CAMBRIA STEEL



77 S/A77

CONSOLIDATED STEEL CORPORATION
TORONTO, ONT.

# CAMBRIA STEEL COMPANY'S WORKS JOHNSTOWN, PA.

# CAMBRIA PLANT



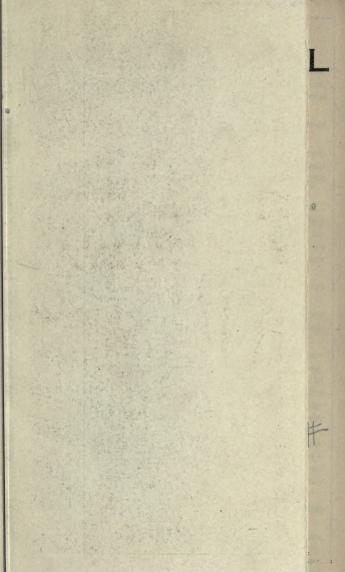
BLAST FURNACES 1-4

PAINT, CAR REPAIR AND PATTERN SHOPS

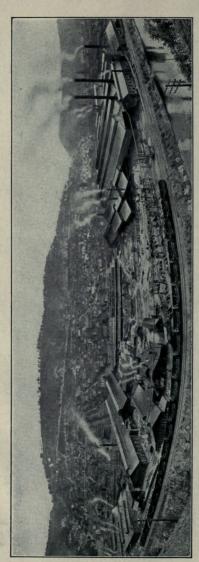
ROLL SHOP

AXLE SHOP
RAIL AND SHAPE MILLS
COAL STORAGE

BLAST FURNACES 5 AND BLOOMING, BILLET AND BEAM MILLS SESSEMER STEEL WORKS 0. H. STEEL WORKS



# GAUTIER PLANT



COLD ROLL SHOP
9" MILL
BAR MILL

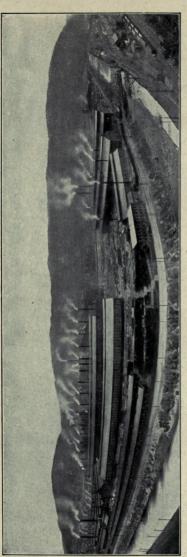
RAKE SHOP MACHINE SHOP

DISC SHOP

UNIVERSAL PLATE MILL 14" 1

LL 14" MILL 8" MILL

# FRANKLIN PLANT



BLAST FURNACES 7 AND 8 COKE PLANT BLOOMING MILLS SLABBING MILL

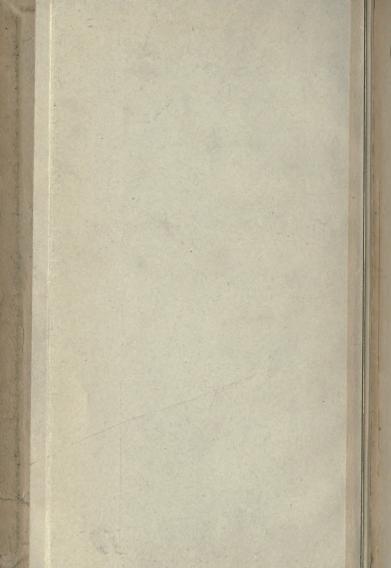
O. H. STEEL WORKS 134" PLATE MILL

STRUCTURAL SHOP CAR SHOP FORGE SHOP BOLT SHOP

POWER PLANT

BEAM YARD

GENERAL SALES OFFICES: PHILADELPHIA, PA., U. S. A.



# CAMBRIA STEEL

A HANDBOOK OF INFORMATION RELATING TO

## STRUCTURAL STEEL

MANUFACTURED BY THE

### CAMBRIA STEEL COMPANY

CONTAINING USEFUL TABLES, RULES, DATA, AND FORMULÆ FOR THE USE OF

ENGINEERS, ARCHITECTS, BUILDERS AND MECHANICS

GEORGE E. THACKRAY, C. E.

SPECIAL ENGINEER, CAMBRIA STEEL CO.

GENERAL OFFICES: PHILADELPHIA, PA.
WORKS AT JOHNSTOWN, PA.
U. S. A.

2 1919

CAMBRIA STEEL

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Price, \$1.50



### PREFACE TO TWELFTH EDITION.

This edition introduces much new matter thought useful, and revises, to a considerable extent, the data of the prior edition, to conform to current practice and a wider range of structural products.

The table of steel ingots is greatly amplified by the addition of more sizes and styles.

Cuts and properties of many new sections are introduced, among which are bulb angles, top-guard bulb angles, 3-inch and 4-inch channels for cars, 12-inch ship channels, and some seventeen T-bars of considerable range in dimensions.

Three sizes of rolled steel car stakes are also included.

Drawings and tabulations of standard ship sections including ship channels, bulb angles and one Z-bar hatch section, together with the equal leg and unequal leg angles selected as standards for ship building, which were adopted on November 20, 1918, are now given.

Rolled safety floor plates and buckle plates are newly listed in most convenient sizes.

In view of well-recognized practice, the standard connection angles formerly shown have been superseded by new standards and all tables relating thereto are correspondingly modified.

Additional new tables believed of value have been incorporated. These refer to Flat and Corrugated Steel Sheeting; Roof Truss Dimensions and Stresses; Moments of Inertia of Rectangles; Sizes of Wrought Spikes and Wood Screws; Wire Gauges shown in Combined Table; Decimal Equivalents of Non-Binary Fractions; Square Roots and Cube Roots of Fractions; Weights of Circular Steel Plates; Trigonometrical Formulæ; Squares and Cubes of Numbers and Fractional Intervals; Combinations and Factors of  $\pi$ ; Relations in Circular Segments; Volumes and Surfaces of Solids; Minutes and Seconds expressed in Decimals of a Degree and vice versa; Metric and Customary Measure Conversions, etc.

The tables of weights for various substances and materials have been considerably augmented.

Specifications for Structural and Boiler Steel have undergone slight revision to bring these up to date.

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(For Complete details of Contents, see Index)

### GENERAL INFORMATION.

Our products are principally steel, made by the Bessemer or Open Hearth process, as required, and of all qualities from the softest rivet stock to high carbon special spring material.

Our Beams and Channels are made to conform to the American Standards, adopted January, 1896, in which the flanges have a uniform slope of one to six, and the dimensions, proportions and weights are determined by a regular schedule, as shown on the diagrams on pages 28 and 29. The standard proportions of

beams and channels are further shown on page 27.

The principal structural angles now made are limited in number to conform to the American Standards, as revised May 21, 1910, and include eight base, or a total of fifty-four sizes for equal leg angles, and nine base, or a total of fifty-seven sizes of unequal leg angles, all varying in thickness by one-sixteenth inch, as shown on pages 17 and 18 and tables herein. It is believed that these standard angles include a sufficient range of sizes to meet all usual structural requirements, but, at the same time, we will continue the manufacture of angles of special sizes and proportions for those who require them, as shown on page 19.

The weights of angles, now given, are those adopted as Amer-

ican Standards in May, 1910.

The standard ship sections adopted November 20, 1918, comprising ship channels, bulb angles and one Z-bar hatch section are now shown and tabulated herein for the first time, and these standards also include certain equal leg and unequal leg angles, which were adopted on the same date, as standards for ship building, all of which are shown and indicated herein by a dagger. Although the drawings of standard structural sections herein show the minimum sizes, the drawings of standard bulb angles and ship channels are made to indicate the sizes of the British standard sections, which form the basis of these ship section standards.

During the time when rolls are being prepared for the new ship channels and bulb angles, our older sections of these shapes shown herein will be furnished, but as the new rolls become ready, the standard sections will be supplied and the prior shapes will be obsolete.

The method of increasing the sectional area of shapes from the minimum or base sizes to intermediate and maximum sizes, is shown approximately on page 26. For beams and channels the increase from the minimum adds equally to the web thickness and flange width, the weight of the increase being equal to that of a plate of the same depth as the section, and of a thickness equal to the increase of the dimensions stated.

The method of increasing the thickness of angles from the minimum has the effect of adding to the length of the legs, as shown on page 26, so that for intermediate and maximum sizesthe legs will be somewhat longer than the minimum or nominal dimensions, except in the cases for which we have finishing grooves. The plates of drawings of sections, pages 2 to 26 inclusive, show the minimum or base sizes of the various shapes, except in cases of standard ship channels and bulb angles as heretofore noted. Sections shown on the plates or lists for which more than one weight is stated can be rolled of different thicknesses to produce the stated weights. Others for which only one weight is given cannot be varied. Each section shown herein is numbered, both in the plates and tables, for convenience in reference and ordering.

I-Beams and Channels should be ordered of weights shown in the tables. Orders and inquiries concerning 12 in. 40 lb., 15 in. 60 lb., and 15 in. 80 lb. I-Beams should also specify these by

Section Number.

Orders for angles and plates should specify either the thickness or the weight, but not both.

Orders for universal or edged plates should specify the width and thickness in inches and the length in feet and inches, whereas orders for sheared plates should give all the dimensions in inches.

All weights are stated in pounds per lineal foot of section, except in the table of rails on page 214, in which the weights are given in pounds per yard, as is customary. Weights of rolled sections are calculated on the basis of 489.6 pounds per cubic foot of steel, and 3.4 times the sectional area in square inches equals the weight in pounds per lineal foot. In calculating the weights, areas, and properties of I-Beams, Channels, and Angles for the lists and tables herewith, the fillets and smaller rounded corners were not considered.

The dimensions of all steel material herein are theoretical, as

they are subject to customary rolling variations.

Structural Angles, I-Beams and Channels, unless otherwise ordered, will be cut to length with variation not to exceed \(\frac{3}{6}\) inch more or less than that specified. For cutting to exact lengths, or with less variation than \(\frac{3}{6}\) inch, an extra price will be charged.

All sections shown herein are steel.

# OFFICES FOR SALE OF CAMBRIA STEEL COMPANY PRODUCTS.

### GENERAL OFFICES: WIDENER BUILDING, PHILADELPHIA, PA., U. S. A.

ATLANTA	Candler	Building,	129 Peachtr	ee Street.
Boston	Scollay	Building,	40 Court St	reet.
-				

CHICAGO.......McCormick Building, Corner of Michigan
Avenue and Van Buren Street.

CINCINNATI...... Union Trust Building, Corner of Fourth and Walnut Streets.

CLEVELAND.......Swetland Building, 1010 and 1012 Euclid Avenue.

Detroit......Penobscot Building, 45 Fort Street, West.

NEW YORK.....City Investing Building, 165 Broadway.

PHILADELPHIA......Widener Building, Chestnut and Juniper
Streets.

PITTSBURGH.....Oliver Building, Smithfield Street.

St. Louis.......Chemical Building, Corner of Eighth and Olive Streets.

SALT LAKE CITY.... Newhouse Building, Corner of Main Street and Exchange Place.

SAN FRANCISCO.... Monadnock Building, 681 Market Street.

SEATTLE......Colman Building, Corner of First Avenue and Marion Street.

Washington, D. C. Woodward Building, Corner of Fifteenth and H Streets, N. W.

WORKS AT JOHNSTOWN, PA. U. S. A.

### CAMBRIA STEEL COMPANY PRODUCTS.

### STRUCTURAL STEEL WORK.

Finished Steel Work for Buildings, including Beams, Girders, Columns, Roof Trusses, etc., fitted complete and ready for erection.

### STEEL CARS.

Gondola, Hopper-Gondola, Hopper, Flat, Tank, Mine, etc., Underframes and Trucks. Freight, Passenger, Electric and Industrial Car Wheels. Draft Gears, Forged and Pressed Steel Car Parts.

### STEEL RAILS.

Steel T-Rails, 12 lbs. to 150 lbs. per yard. Angle, Plain and Special Type Splice Bars. Standard and Special Track Bolts and Nuts. For detailed information, see Rail and Splice Catalogue.

### STEEL AXLES.

Passenger Car, Freight Car, Tender Truck, Engine Truck, Driving, Electric Car, Street Car, Mine Car, etc.

### CRANK PINS, PISTON RODS, BRIDGE PINS.

Made to any requirement.

## MACHINE BOLTS, NUTS, RIVETS, AND PIPE OR TANK BANDS WITH ROLLED THREADS.

### FORGINGS.

Axles, Crank Pins, Piston Rods and Forgings in general furnished of carbon steel, annealed, or treated by our Coffin toughening process (patented) as specified.

Crank Pins and Piston Rods also furnished oil-tempered and annealed; other small Forgings will be, if desired.

For small car forgings and pressed steel parts, see list on pages 30 and 31 herein.

### ANNULAR ROLLED SECTIONS.

Car Wheels, Crane Track Wheels, Blanks for Cylindrical Wheels, Gears, Sprockets, Band Wheel Flanges, Pipe Flanges, Bevel Rollers, and Automobile Fly Wheels, etc.

### MERCHANT BAR STEEL.

Including Tire, Toe Calk, Machinery, Automobile Spring, Carriage Spring, Baby Carriage Spring, Railroad Spring, Hoe, Rake, Fork, Forging, Bolt, Rivet, etc. Special Sections.

Automobile and Motor Truck Rim Sections.

### STEEL SPECIALTIES.

Mine Ties, Fence Posts, Reinforcing Bars, etc.

### AGRICULTURAL STEEL AND SHAPES.

Finger Bars, Knife Backs, Rake Teeth, Bundle Carrier Teeth, Tedder Forks and Springs, Spring Harrow Teeth, Harrow (Drag) Teeth, Seat Springs, etc.

### PLOW STEEL.

Bars and Slabs (Pen and Pernot), Flat Plow Shapes, Digger Blades, Hammered Lay, Rolled Lay, etc.

### COLD ROLLED AND COLD DRAWN STEEL.

Rounds, Squares, Hexagons, Flats, Shafting and Special Shapes.

### STEEL DISCS WITH ROLLED BEVEL.

 $10^{\prime\prime}$  to  $20^{\prime\prime}$  diameter dished for Harrows, Drills, Cultivators, etc.

23" to 28¾" diameter dished for Plows. 8" to 26" diameter flat for Rolling Coulters.

### PRESSED STEEL SEATS FOR AGRICULTURAL IMPLEMENTS.

### WIRE RODS, WIRE AND WIRE PRODUCTS.

Wire Rods. Bolt, Screw and Rivet Wire. Bright and Annealed Wire. Galvanized Coiled Steel Spring Wire.

Barbed Wire, Galvanized or Painted.
Wire Nails, Bright or Galvanized.

Cement Coated Nails.

Fence Wire and Wire Fence. Fence and Poultry Netting Staples.

Bale Ties-Single Loop.

### NON-STEEL PRODUCTS.

Cinder, Slag and Coal Derivatives. Limestone Ballast and Screenings.

FOR PRODUCTS NOT LISTED HEREIN, SEE SPECIAL CATALOGUES.

# SECTIONS

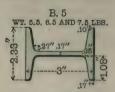
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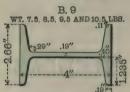
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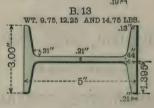
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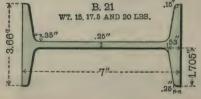
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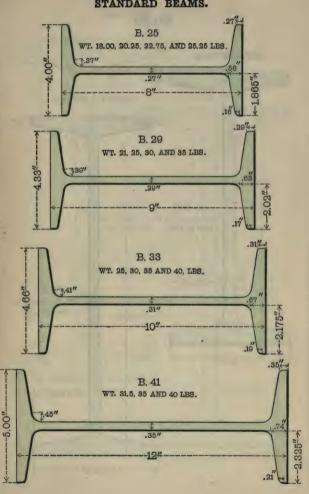






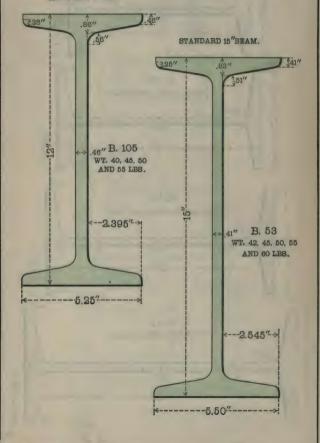


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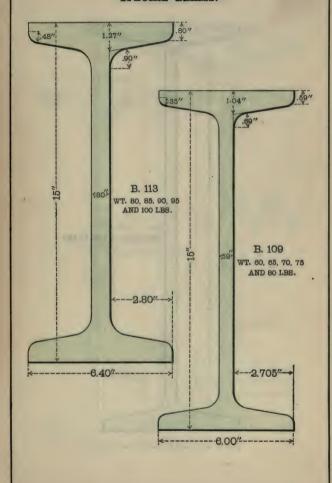


### BEAWS.

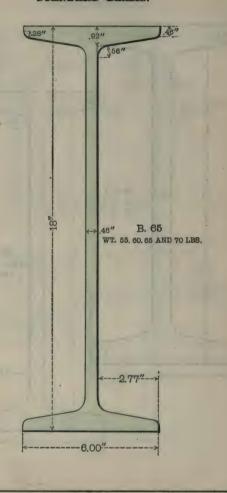
SPECIAL 12"BEAM.



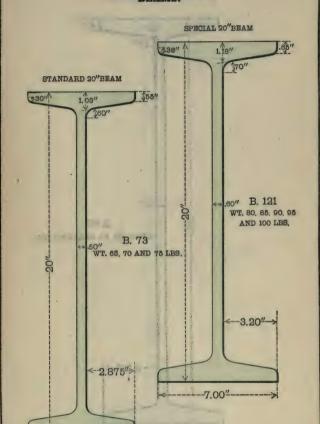
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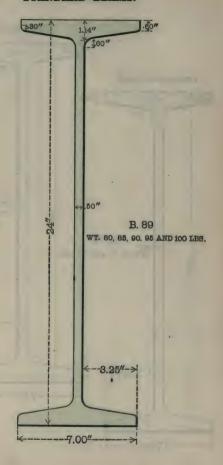
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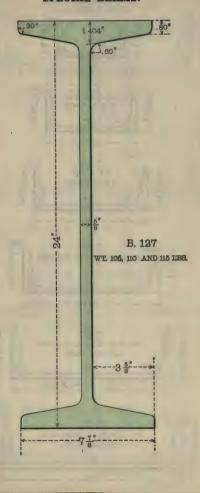
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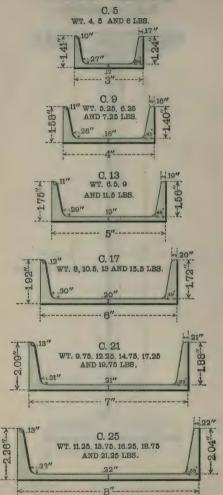
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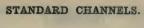


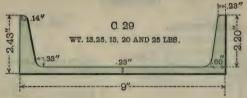
SPECIAL BEAMS.

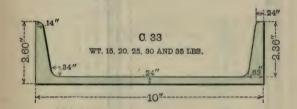


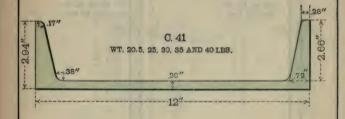
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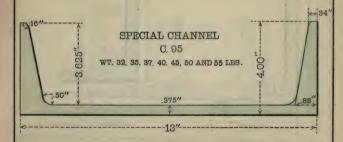




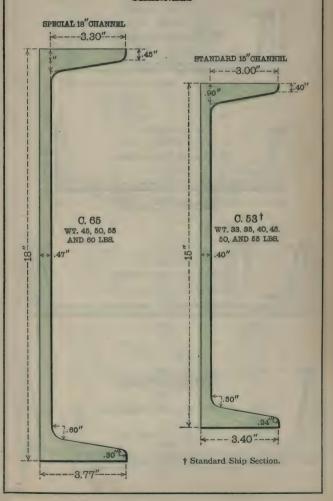




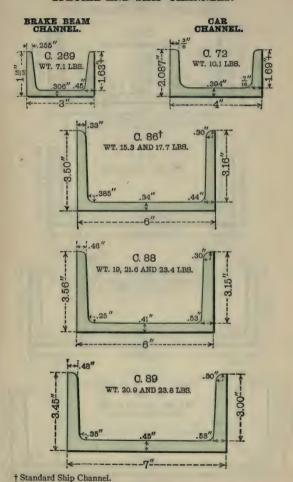




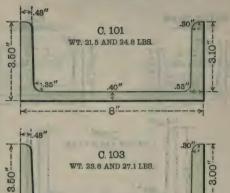
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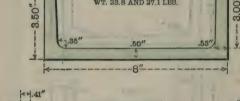


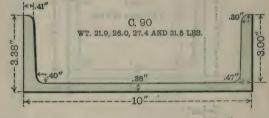
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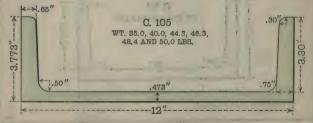


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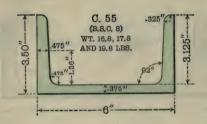


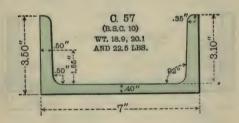


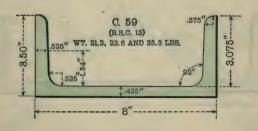




### STANDARD SHIP CHANNELS.



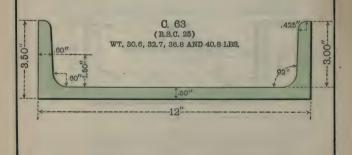




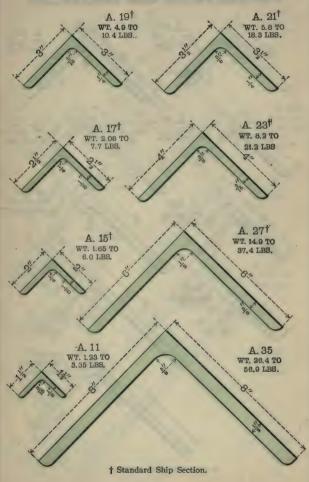
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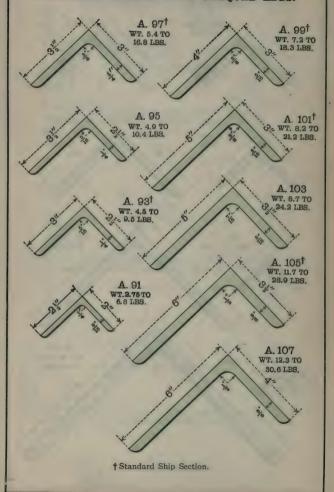




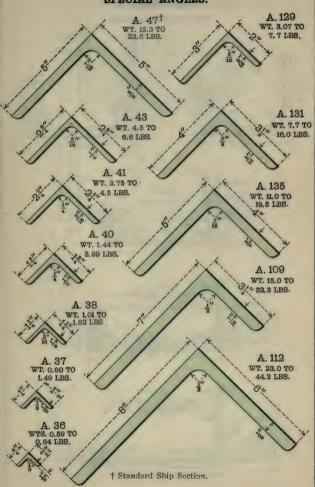
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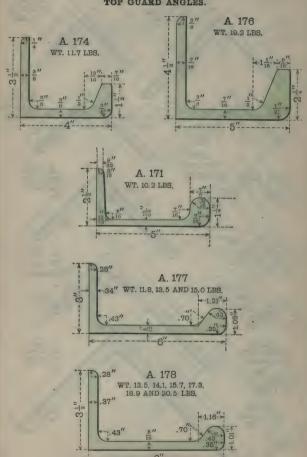
### STANDARD ANGLES WITH UNEQUAL LEGS.



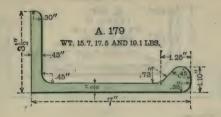




# BULB ANGLES. TOP GUARD ANGLES.

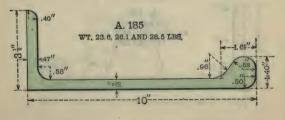


### BULB ANGLES.

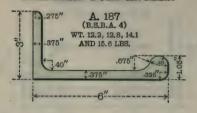


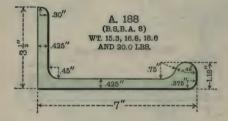


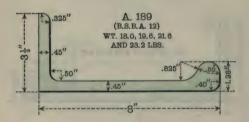


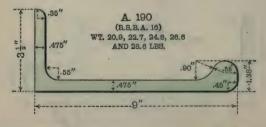


### STANDARD BULB ANGLES.

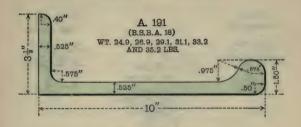








### STANDARD BULB ANGLES.

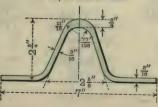


### Z-BAR HATCH SECTION. STANDARD SHIP SECTION.



### CAR SIDE STAKE SECTIONS.

L. 2 WT. 7.2, 8.7 AND 11.7 LBS.



### T-BARS WITH EQUAL LEGS.

T. 5 WT. .89 LBS.



T. 181 WT. 1,37 LBS.



T. 183 WT. 1.51 LBS.



T. 187 WT. 1.60 LBS.



T. 188



T. 191 WT. 1.94 LBS.



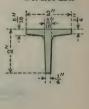
T. 193 WT. 2,47 LBS.



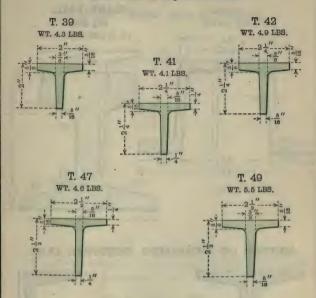
T. 194



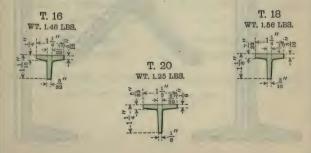
T. 37 WT. 3,56 LBS.



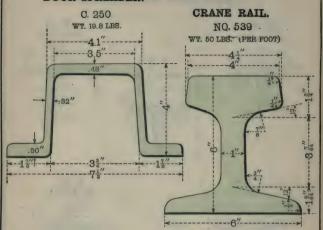
### T-BARS WITH EQUAL LEGS.



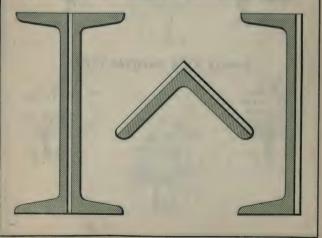
### T-BARS WITH UNEQUAL LEGS.



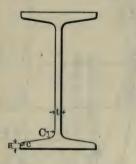
### DOOR-SPREADER.



### METHOD OF INCREASING SECTIONAL AREA.



### STANDARD BEAMS AND CHANNELS.





The following data are common to all Standard I-Beams and Channels, with the exceptions stated:

 $c = \frac{6}{10}$  Minimum Web.

 $C = Minimum Web + \frac{1}{10} inch.$ 

8 = Minimum Thickness of Web = t Minimum for all Channels and Beams, except 20" I and 24" I.

For 20" Standard I, s = .55", t Minimum = .50".

For 24" Standard I, s = .60", t Minimum = .50".

The Slope of Flange of all Standard Beams and Channels is  $16\frac{2}{3}\%$ 

$$= 9^{\circ} - 27' - 44'' = 2''$$
 per foot.

### STANDARD BEAMS.

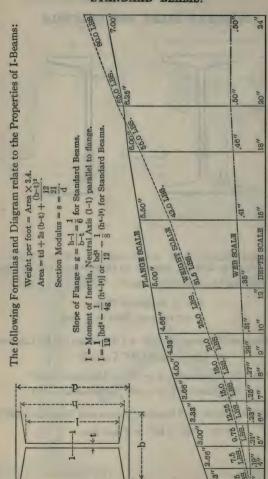


DIAGRAM FOR MINIMUM STANDARD BEAMS.

### STANDARD CHANNELS

The following Formulas and Diagram relate to the Properties of Channels:

Weight per foot = Area  $\times 3.4$ .

Area = td + 2s (b-t) +  $\frac{(b-t)^2}{6}$ .

Section Modulus =  $s = \frac{21}{d}$ .

Slope of Flange =  $g = \frac{h-1}{2(b-t)}$ , or  $\frac{1}{6}$  for Standard Channels.

I = Moment of Inertia, Neutral Axis (1-1) parallel to flange.

I =  $\frac{1}{12}$  [bd<sup>3</sup> -  $\frac{1}{8g}$  (h+1)) or  $\frac{bd^3}{12}$  -  $\frac{h^4-1^4}{16}$  for Standard Channels.



# DIAGRAM FOR MINIMUM STANDARD CHANNELS

### PRESSED STEEL OR FLANGED CAR PARTS

Truck Bolsters

Side Sills.

Center Sills.

End Sills.

Draft Sills.

Draft Lugs.

Sub-Side Sills.

Side Stakes.

End Stakes.

Corner Stakes.

Outside Hopper Plates.

Inside Hopper Plates.

Side Plates.

End Plates.

Floor Plates. Longitudinal Ridge Plates.

Cross-Ridge Plates.

End-Plate Stiffeners.

Hopper Doors.

Drop Doors.

Longitudinal Ridge Stiffeners.

Cross Ridge Supports.

Cross Body Ties.

Diagonal Braces.

Door Spreaders.

Air Reservoir Supports.

Push Pole Pockets.

Body Corner Caps.

Door Hinge Butts.

Bolster Diaphragms.

Wheel Diaphragms.

Cross Bearer Diaphragms.

Hopper Diaphragms.

Door Diaphragms.

Center Diaphragms.

Center Sill Diaphragms.

Bolster Center Diaphragms.

### FORGINGS FOR CAR WORK.

Air Cylinder Push Rod.

Air Reservoir Release Rod.

Arch Bars.

Bottom Follower Guide.

Bottom Side Bearing.

Bracket for Brake Shaft.

Brake Beam Hanger.

Brake Beam Hanger Carrier.

Brake Connection Rod Carrier.

Brake Levers.

Brake Mast.

Brake Mast Yoke.

Brake Pins.

Brake Rods with Clevises.

Brake Step Bracket.

Chain Hook.

Chain Link. Corner Bands

Column Bolt Nut Lock.

Coupler Yokes.

Coupling Links.

Coupling Pins.

Cylinder Lever Connecting Rod.

Cylinder Lever Fulcrum.

Door Chain U-Bolt.

Door Hinge.

Door Hinge Pins.

Door Operating Lever.

### FORGINGS FOR CAR WORK (CONTINUED).

Door Safety Chain Support.
Door Shaft Pawl.
Door Tumbling Link.
Draft Cylinder Support.
Draw Bar Carrier.
Draw Bar Liner.
Draw Bar Yoke.
Door Clevises.

Door Tumbling Lever. End Sill Pipe Clamp.

Eye-Bolts.
Floating Lever.
Floating Lever Carrier.
Floating Lever Connecting
Rod.

Floating Lever Fulcrum. Grab Irons.

Hand Brake Lever Carrier.
Hand Brake Lever Fulcrum.
Hand Brake Lever Guide.

Hand Brake Rod. Hand Brake Rod Guide.

Hand Brake Rod Stop.
Hand Brake Rod with Threaded
Connection for Malleable

Stop.
Hook Bolts.
Inside Body Step.

Journal Bearing Wedges. King Bolt.

King Pin Support.

Lever Guides.

Live Truck Lever Guide.

Main Follower Sprocket Wheel Shaft.

Operating Shaft.
Operating Shaft Cam.

Operating Shaft Cam Stops. Operating Ratchet Pawl.

Operating Ratchet Pawl Guard.

Pipe Clamp.

Pipe Clamp and Support.

Pushrod Carrier. Ratchet Wrench Dog.

Roping Staple. Sheave and Link Pin. Side Stake Pockets.

Sill Step Suspension Spring.

Suspension Spring.
Suspension Spring Hanger.

Tie Bars with Upset Ends or

Top Body Tie Angle.
Top Side Bearing.

Truck and Body Center Plates.

Truck Bolster Tie Bar.

Truck Door Stop, Chain Clamp Hooks.

Truck Levers.

Truck Side Bearing.

U-Bolt Clamp for Angle Valve.

Uncoupling Lever.

A large variety of small forgings not listed above can be furnished to order.

### STEEL INGOTS.

Style of	Me	old Dimensions		Approximate	
Mold	Bottom	Тор	Height	Ingot Weight	Grade
(See Foot-note)	Inches	Inches	Ft.—Ins.	Pounds	
O,X. O,F. O,F. B,F.S. O,F. I,F,S. O,F. O,F. O,F. O,X. O,X. O,X. O,X. O,F. I,F,S. C,G. C,G. C,G. C,G. G,R. B,F. K,G,S.	2018 x 238 21 x 21 x 21 x 21 x 21 x 21 x 21 16½ x 20½ 16½ x 20½ x 20½ x 30 x	18½ x 20½ 19 x 19 19 x 19 25 x 25 20½ x 23½ 20½ x 23½ 20½ x 23½ 20½ x 24½ 28 x 28 30 x 30 23 x 35 22½ x 35½ 23 x 51½ 23 x 50½ 24 x 50 30 x 54 25 x 25 30 x 30 20 diam. 23½ " 26 " 34 " 16 x 28 20 x 36 19 { short diam.	6-1½ 6-3 6-3 6-5 2 6-2 6-2 6-2 6-2 6-2 6-2 6-3 6-0 6-2 8-0 8-0 18-0 18-0 18-0 18-0 18-0 18-0 1	7300 7300 7300 7300 7300 7300 7300 7800 7900 10400 13500 15500 20500 25500 19500 20400 25000 25000 25000 25000 30000 10200 15700 23800 29100 33800 41800 55000 36500 8300	Open Hearth or Bessemer Open Hearth

B = Bottle-Necked; C = Circular; F = Ingot Sides Flat; G = Corrugated; I = Inverted; K = Octagonal; O = Open Top; R = Rectangular or Slab Style; V = Ingot Sides Concave; X = Ingot Sides Rounded or Convex; S = With Sinkhead; \* = Irregular Taper.

Sizes of Hot and Cold Ingots will vary slightly from above

dimensions.

### STEEL SQUARES.

All sizes from  $\frac{3}{16}$ " to  $2\frac{1}{16}$ " increasing by  $\frac{4}{64}$ ". All sizes from  $2\frac{1}{16}$ " to  $3\frac{1}{26}$ " increasing by  $\frac{3}{32}$ ". All sizes from  $3\frac{1}{2}$ " to  $5\frac{1}{2}$ " increasing by  $\frac{1}{32}$ ". Planished squares from  $\frac{3}{32}$ " to  $2\frac{1}{2}$ "

### STEEL HAND ROUNDS.

All sizes from  $1\frac{1}{6}$ " to  $2\frac{7}{8}$ " increasing by  $\frac{1}{64}$ " All sizes from  $2\frac{7}{8}$ " to  $3\frac{7}{8}$ " increasing by  $\frac{1}{16}$ " All sizes from  $3\frac{1}{4}$ " to  $7\frac{1}{4}$ " increasing by  $\frac{1}{8}$ " All sizes from  $7\frac{1}{4}$ " to 8" increasing by  $\frac{1}{4}$ ".

### STEEL GUIDE ROUNDS.

All sizes from  $\frac{1}{4}$ " to  $2\frac{5}{16}$ " increasing by  $\frac{1}{64}$ "

### LARGE STEEL ROUNDS.

DIAMETER Inches	MINIMUM LENGTHS Sheared with Rough Ends. Inches	MAXIMUM LENGTH Feet
11	6 to 36	25
15	6 to 36	10½
16	6 to 36	9½

Other lengths shorter than maximum can only be furnished by special arrangement.

### REGULAR FLATS.

WIDTH	THICKNESS.	WIDTH	THICKNESS
Inches	Inches	Inches	Inches
1 to 1 1 to 1 1 8 1 1 to 1 1 2 1 1 2 to 2 1	36 to 96 36 to 3 36 to 3 36 to 7 36 to 14	2½ to 3 3 to 4 4 to 4½ ½ to 6	16 to 21 16 to 23 16 to 23 16 to 116 16 to 216

Variation for intermediate widths less than  $1'' = \frac{1}{64}i''$ . Variation for intermediate widths over  $1'' = \frac{1}{16}i'$ , or less by special arrangement.

### THIN FLATS OR LIGHT BANDS.

WIDTH	THIOKNESS						
$\frac{3}{8}$ " to $\frac{1}{2}$ " increasing by $\frac{1}{16}$ " $\frac{1}{2}$ " to 12" increasing by $\frac{1}{16}$ "	$\frac{1}{16}$ " (.125") to $\frac{5}{32}$ " (.156") $\frac{1}{16}$ " (.063") to $\frac{5}{32}$ " (.156")						

### MAXIMUM LENGTHS OF

					_																
								WI	DT	H 1	N	INC	HE	B.							
Thickness in Inches.	41/2	5	51/2	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23
	LENGTE IN FEET.																				
2	ı				10	30	30	30	30	30			ľ			I	ı	I			
21/2			п	10	30	30	30	30	3,0	30	30	30	30	30	30	30	30	30	30	30	30
3	н			30	30	30	-	-	30		30			30		-	-	30	30	30	30
3 1/2			п	30	30	30	30	30			30		30	_	30	_		30	30	30	30
4		30	30		30	30	30	30			30		_	_	30	_	30	30	_		30
41/2	30	30	30		30	30	30	30		30	_	200	30	_	30	_		30	30		30
5		30	-	-	30	30	30	30			30		30				30	-	30		30
51/2			30		30	30	30	30			30		30	_	30	_		30	_		30
6				30	30	30	30	30	30	30			30		30	_		30			30
7					30	30	30	30		30	-		_	30			-	30		30	28
8						30	30	30	30	30	_	30	_	30				28	27	26	25
9							30			30	30			30	30	-		25	24	23	22
10								30		30	30			30	30		-	23	21	20	20
11									30	30			30	30	30				19	19	18
12										30			30	30	28		25		18		16
13											30	0.0	30	28	26	25	23	17	16		15
14												30	28	26	24		22	16	15		14
15					ш						П		26	24	23	21	20		14		13
16											ш			22	21	20	19		13		12
17											80				20		18		13	12	12
18											и					18		12	12	11	11
20																	16				11
21																		11	10		10
22						ı													10	10	9
22														1						0	0

Minimum Length for sizes included by heavy lines =  $1\frac{1}{2}$  feet. Minimum Length other sizes = 3 feet.

Under certain conditions other sizes than those listed

### BILLETS, BLOOMS AND SLABS.

	WIDTH IN INCHES.																				
Thickness in Inches	51	50	49	48	47	46	45	37	36	35	34	33	32	31	30	29	28	27	26	25	24
	-							т.	EE	N F	I	TE	ENG	LE					-		
2								П				ı									
2:	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30	30
3	30	27	27	28	29	30	00	27	28	29	30	29	29	30	30	30	30	30	30	30	30
4	28	24	24	25	25	30		24	24	25	30	25	26	27	27	28	30	30	30	30	30
4	25	21	21	22	22	30		21	22	22	30	22	23	24	24	25	30	30	30	30	30
5	22	19	19	19	20	30	30	19	19	20	30	20	20	21	22	23	30	30	30	30	30
5	20	17	17	18	18	28	28	17	18	18	30	18	19	19	20	21	29	30	30	30	30
В	18	16	16	16	16	25	26	16	16	17	27	16	17	18	18	19	27	28	29	30	30
7	16	13	13	14	14	21	22	13	14	14	23	14	14	15	15	16	23	24	25	26	27
8	14	12	12	12	12	19	19	12	12	12	20	12	13	13	13	14	20	21	22	23	24
9	12	10	10	11	11	17	17	10	11	11	18	11	11	11	12	12	18	19	19	20	21
10	11	9	9	10	10	15	15	9	9	10	16	10	10	10	11	11	16	17	17	18	19
11	10	8	8	9	9	14	14	8	9	9	14	9	9	9		10	15			16	17
12	9	8	8	8	8	12	13	8	8	8	13	8	8	9	9	9	13		-	15	15
13	8	7	7	7	7	11	12	7	7	7	12	7	8	8	8	8	12		13	13	14
14 15	8	6	6	7 6	7 6	11 10	11	6	7	7	11	7	7	7	8	8	11		12	13	13
16	7	6	6	6	6	9	10	6	6	6	11 10	6	6	7 6	7	7	11 10	11	11	12	12 12
17	6	5	5	6	8	9	9	5	6	6	9	6	6	6	6	7	9	9	10	11	11
18	6	5	5	5	5	8	9	5	5	5	9	5	6	6	6	6	9	9	9	10	10
19	.								0	0			-	V	U	U	8	8	9	10	10
20																	8	8	8	9	9
21																	8	8	8	9	9
22																	7	7	8	8	8

Minimum Length = 3 feet.

herein might be furnished by special arrangement.

SQUARE BILLETS. WITH ROUND CORNERS.

Size.	Maximum Length.	Minimum Length.
Inches.	Feet.	Feet
13 x 13	30	24
2 x 2	30	24
2½ x 2½ 3° x 3	30	24
3 x 3	30	24
4 x 4	16	11/2
$4\frac{1}{2} \times 4\frac{1}{2}$	16	11
5 x 5	16	11/3
$5\frac{1}{2} \times 5\frac{1}{2}$	16	11/2
6 x 6	16	11

### SHEET AND TIN BARS.

Width.	Weight per Foot Length.	Maximum Length,	Minimum Length.	
Inches.	Pounds.	Feet.	Feet.	
8	8	30	25	
8	9	30	25	
8	10	30	25	
8	11	30	203	
8	12	30	201	
.8 .8	13	30	$20\frac{1}{2}$	
8	14	30	$16\frac{1}{2}$	
8	15	30	161	
8 8 8	16	30	161	
8	17	30	161	
8	18	30	13	
8	19	30	13	
8	20	30	13	
8	21	30	13	
8	22	30	13	
8	23	30	13	
8	24	30	91	
8	25	30	91	

### EDGED PLATES.

															-
		THICKNESS IN INCHES.													
Width in Inches.	3 16	14	5 16	38	7	1/2	9 16	15/00	34	7 8	1	11/4	1 1/2	134	2
	MAXIMUM LENGTH IN FEET.														
$\begin{array}{c} 6\frac{1}{8} - 25\\ 26 - 27\\ 28\\ 29\\ 30\\ 31\\ 32\\ 33\\ 34 \end{array}$	85 60 60 60 60	85 85 85 60 60 60 60	85 85 85 85 85 85 85 85	85 85 85 85 85 85 85 85 85	85 85 85 85 85 85 85 85 85	85 85 85 85 85 85 85 85 85	85 85 85 85 85 85 85 85 85	85 85 85 85 85 85 85 85 85 85 85 85	85 85 85 85 85 85 85 85 85 85	85 85 85 85 85 84 81 79	85 85 85 85 78 75 73 71 69	68 68 67 64 62 60 58 57 55	56 56 56 54 52 50 49 47 46	48 48 48 46 44 43 42 40 39	42 42 42 40 39 37 36 35 34
35 36		60	85 85	85 85	85 85	85 85	85 85	85 85	85 85	76 74	67 65	53 52	44 43	38 37	33 32

### THIN SHEARED PLATES.

	THICKNESS IN GAUGE AND INCHES.											
Width in Inches.	No. 16	No. 15 .072	No. 14 .083	No. 13 .095	No. 12 .109	No. 11 .120	No. 10 .134	No. 9	No. 8			
- 22			N	MUMIXAI	LENGTH	IN FEE	T.					
8	12	12	14	16	20	20	20	20	20			
9	10	12	14	16	20	20	20	20	20			
10	10	12	14	15	20	20	20	20	20			
11 12	10	12 12	14 14	15 15	19 19	20	20	20	20			
13, 14	10	11	13	14	18	19 19	20 20	20 20	20 20			
15, 14	10	11	13	14	17	19	20	20	20			
16	10	11	12	13	17	18	20	20	20			
17, 18	10	11	12	13	16	18	20	20	20			
19				13	15	18	20	20	20			
20				12	15	17	20	20	20			
21					14	16	20	20	20			
22					14	15	20	20	20			
23					13	14	18	20	20			
24					13	14	18	18	20			
25							18	18	18			
26, 27							16	16	18			
28									16			

SHEARED PLATES.

Width	THICKNESS IN INCHES.											
in Inches.	3 16	14	5 16	ස)්ත	7 16	1/2	9 16	5/8	11			
moues.	MAXIMUM LENGTE IN INCHES											
24	400	525	575	600	600	600	600	600				
25- 30	375	525	500	600	600	625	625	625				
31- 36	375	475	525	550	550	575	575	575	575			
37- 42	450	525	550	575	610	600	600	600	575			
· 43- 48	450	525	575	600	600	600	600	600	600			
49- 54	450	525	550	600	600	625	625	625	600			
55- 60	400	525	550	600	600	625	625	625	600			
61- 66	350	475	500	575	575	600	600	600	600			
67- 72	325	450	500	540	550	575	575	575	575			
73- 78		425	475	440	540	540	540	540	540			
79- 84		400	475	440	540	540	540	540	540			
85- 90		350	375	400	450	450	450	450	450			
91- 96		300	325	350	400	400	400	400	400			
97-102		275	300	325	375	375	375	375	375			
103-108		250	275	300	350	350	350	350	350			
109-114		175	200	225	275	275	275	300	300			
115-120			175	200	250	250	250	250	250			
121-126				180	180	180	180	180	180			
Maximum Diam. of Heads.	72	115	124	127	127	127	127	127	127			

Minimum Diameter of Heads (Circular Plates) = 30 inches.

### SHEARED PLATES.

-	THICKNESS IN INCHES.													
34	13 16	7/8	15 16	1	11/8	11/4	1½	134	2	Width in Inches.				
			MAXIM	UM LEN	GTH IN	INCHES.								
										24				
										25- 30				
550	525	500	475	475	450	425	400	375	350	31- 36				
575	525	500	500	500	475	425	400	375	350	37- 42				
575	550	550	525	525	500	450	400	375	350	43- 48				
575	550	550	525	525	500	450	400	375	350	49- 54				
575	550	550	525	525	475	425	400	375	325	55- 60				
575	550	550	525	525	475	425	375	350	325	61- 66				
575	550	525	500	500	475	425	375	350	300	67- 72				
525	500	475	450	450	425	375	325	300	280	73- 78				
500	450	450	425	425	375	350	325	300	280	79- 84				
425	400	400	375	375	350	325	280	270	260	85- 90				
400	375	375	350	325	300	275	260	260	250	91- 96				
375	350	350	325	300	275	250	250	240	240	97-102				
350	325	325	300	275	250	250	180	175	160	103-108				
300	275	275	250	250	225	200	175	160	150	109-114				
275	250	250	225	225	200	200	175	160	150	115-120				
180	200	200	175	175	160	160	150	144	144	121-126				
127	126	126	126	126	126	125	125	125	125	Maximum Diam. of Heads.				

Larger sizes up to 4 inch thickness, finished weight not exceeding 12,000 pounds, will be considered.

### WEIGHTS AND DIMENSIONS OF STANDARD I-BEAMS.

Section Number.	Depth of Beam.	Weight per Foot.	Area of Section.	Thickness of Web.	Width of Flange.	Page Number of
Number,	Inches.	Pounds.	Sq. In.	Inch.	Inches.	Section.
B 5 "	3 "	5.5 6.5 7.5	1.63 1.91 2.21	.17 .26 .36	2.33 2.42 2.52	2 "
B 9 "	4 " " " " " " " " " " " " " " " " " " "	7.5 8.5 9.5 10.5	2.21 2.50 2.79 3.09	.19 .26 .34 .41	2.66 2.73 2.81 2.88	2 u u
B 13	5 "	9.75 12.25 14.75	2.87 3.60 4.34	.21 .36 .50	3.00 3.15 3.29	2 "
B 17	6	12.25 14.75 17.25	3.61 4.34 5.07	.23 .35 .47	3.33 3.45 3.57	2 "
B 21 "	7 "	15.0 17.5 20.0	4.42 5.15 5.88	.25 .35 .46	3.66 3.76 3.87	2 "
B 25 "	66 66 18	18.0 20.25 22.75 25.25	5.33 5.96 6.69 7.43	.27 .35 .44 .53	4.00 4.08 4.17 4.26	3 " "
B 29	9 " "	21.0 25.0 30.0 35.0	6.31 7.35 8.82 10.29	.29 .41 .57 .73	4.33 4.45 4.61 4.77	
B 33 " "	10 "	25.0 30.0 35.0 40.0	7.37 8.82 10.29 11.76	.31 .45 .60 .75	4.66 4.80 4.95 5.10	8 « «
B 41 "	12	31.5 35.0 40.0	9.26 10.29 11.76	.35 .44 .56	5.00 5.09 5.21	3 "
B 53 "	15 "	42.0 45.0 50.0 55.0	12.48 13.24 14.71 16.18	.41 .46 .56 .66	5.50 5.55 5.65 5.75	4 " " "
и	"	60.0	17.65	.75	5.84	66

Orders and inquiries concerning 12 in, 40 lb., 15 in, 60 lb., and 15 in, 80 lb. I-Beams should also specify by Section Number.

### WEIGHTS AND DIMENSIONS OF STANDARD I-BEAMS.

Section	Depth of Beam.	Weight per Foot.	Area of Section.	Thickness of	Width of Flange.	Page Number of
Number.	Inches.	Pounds.	Sq. In.	Inch.	Inches.	Section.
B 65	18	55.0	15.93	.46	6.00	6
66	66	60.0	17.65	.56	6.10	EC.
и	66	65.0	19.12	.64	6.18	66
66	cc	70.0	20.59	.72	6.26	ш
B 73	20	65.0	19.08	.50	6.25	7
"	"	70.0	20.59	.58	6.33	"
ži.	44	75.0	22.06	.65	6.40	"
B 89	24	80.0	23.32	.50	7.00	8
"	46	85.0	25.00	.57	7.07	"
66	"	90.0	26.47	.63	7.13	66
66	66	95.0	27.94	.69	7.19	66
66	66	100.0	29.41	.75	7.25	"

### WEIGHTS AND DIMENSIONS OF SPECIAL I-BEAMS.

Section Number.	Depth of Beam. Inches.	Weight per Foot. Pounds.	Area of Section. Sq. In.	Thickness of Web. Inch.	Width of Flange. Inches.	Page Number of Section.
B 105  " " B 109  " "	12 « « 15 « «	40.0 45.0 50.0 55.0 60.0 65.0 70.0 75.0 80.0	11.84 13.24 14.71 16.18 17.67 19.12 20.59 22.06 23.53	.46 .58 .70 .82 .59 .69 .78 .88	5.25 5.37 5.49 5.61 6.00 6.10 6.19 6.29 6.39	4      
B 113	15 " "	80.0 85.0 90.0 95.0 100.0	23.57 25.00 26.47 27.94 29.41	.80 .90 .99 1.09 1.19	6.40 6.50 6.59 6.69 6.79	5   
B 121	20 " " "	80.0 85.0 90.0 95.0 100.0	23.73 25.00 26.47 27.94 29.41	.60 .66 .74 .81	7.00 7.06 7.14 7.21 7.28	7  
B 137	24 "	105.0 110.0 115.0	30.98 32.48 33.98	.63 .69 .75	7.88 7.94 8.00	9 "

Orders and inquiries concerning 12 in. 40 lb., 15 in. 60 lb., and 15 in. 80 lb. I-Beams should also specify by Section Number.

### WEIGHTS AND DIMENSIONS OF STANDARD CHANNELS.

Section Number.	Depth of Channel.	Weight per Foot.	Area of Section.	Thickness of Web.	Width of Plange.	Page Number of Section.
artimor;	Inches.	Pounds.	Sq. In.	Inch.	Inches.	Section.
C 5	8 "	4.0 5.0 6.0	1.19 1.47 1.76	.17 .26 .36	1.41 1.50 1.60	10
C 9	4 "	5.25 6.25 7.25	1.55 1.84 2.13	.18 .25 .33	1.58 1.65 1.73	10
C 13	5 "	6.50 9.00 11.50	1.95 2.65 3.38	.19 .33 .48	1.75 1.89 2.04	10
C 17	6 "	8.00 10.50 13.00 15.50	2.38 3.09 3.82 4.56	.20 .32 .44 .56	1.92 2.04 2.16 2.28	10
C 21	7  	9.75 12.25 14.75 17.25 19.75	2.85 3.60 4.34 5.07 5.81	.21 .32 .42 .53	2.09 2.20 2.30 2.41 2.51	10
C 25	8   	11.25 13.75 16.25 18.75 21.25	3.35 4.04 4.78 5.51 6.25	.22 .31 .40 .49	2.26 2.35 2.44 2.53 2.62	10
C 29	9 "	13.25 15.00 20.00 25.00	3.89 4.41 5.88 7.35	.23 .29 .45 .61	2.43 2.49 2.65 2.81	11
C 33	10 "	15.0 20.0 25.0 30.0 35.0	4.46 5.88 7.35 8.82 10.29	.24 .38 .53 .68	2.60 2.74 2.89 3.04 3.18	11
C 41	12 "	20.5 25.0 30.0 35.0 40.0	6.03 7.35 8.82 10.29 11.76	.28 .39 .51 .64	2.94 3.05 3.17 3.30 3.42	11

### WEIGHTS AND DIMENSIONS OF STANDARD CHANNELS.

Section	Depth of Channel.	Weight per Foot.	Area of Section.	Thickness of Web.	Width of Flange.	Page Number of
Number.	Inches.	Pounds.	Sq. Ins.	Inch.	Inches.	Section.
C 53	15	33 †	9.90	.40	3.40	12
"	"	35 1	10.29	.43	3.43	46
"	"	40 1	11.76	.52	3.52	66
a	"	45 1	13.24	.62	3.62	"
"	u	50 1	14.71	.72	3.72	"
а	"	55 †	16.18	.82	3.82	"

### WEIGHTS AND DIMENSIONS OF SHIP AND SPECIAL CHANNELS.

Section Number	Depth of Channel.	Weight per Foot.	Area of Section.	Thickness of Web.	Width of Flange.	Increase in Web and Flange for each Pound Increase of Weight.	Page Number of Section.
	Inches.	Pounds.	Sq. In.	Inch.	Inches.	Inch.	
C 269	3	7.1	2.07	.306	1 15	.098	13
C 72	4	10.1	2.95	.394	2.09	.074	13
C 86	6 "	15.3† 17.7	4.47 5.19	.34	3.50 3.62	.049	13
C 88	6	19.0 21.6	5.58 6.36	.41	3.56	.049	13
а	"	23.4	6.87	.63	3.78	žt.	Ei
C 89	7 "	20.9 23.8	6.15 6.99	.45 .57	3.45 3.57	.042	13
C 101	8 "	21.5 24.8	6.30 7.26	.40 .52	3.50 3.62	.037	14
C 103	8 "	23.8 27.1	7.00 7.96	.50 .62	3.50 3.62	.037	14
C 90	10	21.9 26.0	6.44	.38	3.38 3.50	.029	14
"	ш	27.4	8.04	.54	3.54	44	ш
"	"	31.5	9.24	.66	3.66	c	ĸ
C 105	12	35.0	10.30	.47	3.77	.0245	14
"	"	40.0	11.76	.60	3.90	"	и
"	"	44.3	13.02	.70	4.00	"	и
"	ш	46.3	13.62	.75	4.05	u	и
u	H "	48.4	14.22	.80	4.10	46	EZ EZ
66	" "	50.0	14.70	.84 rd Ship S	4.14		1 "
		T	Standal	d comb	Jection 1		

# WEIGHTS AND DIMENSIONS OF STANDARD SHIP CHANNELS.

Dimensions of standard 6-inch, 15.3 lb. ship channel on page 43.

Section' Number.	Depth of Channel.	Weight per Foot.	Area of Section,	Thickness of Web.	Width of Flange.	Increase in Web and Flange for each Pound increase of Weight.	Page Number of Section.
	Inches.	Pounds.	Sq. Ins.	Inch.	Inches.	Inch.	
C 55	6	16.8	4.92	.325	3.45	.049	15
" (BSC 8)	EE.	17.8	5.22	.375	3.50	66	"
"	ш	19.8	5.82	.475	3.60	"	"
		-				1	
C 57	7	18.9	5.55	.350	3.45	.042	15
" (BSC 10)	ш	20.1	5.90	.400	3.50	4	u
"	п	22.5	6.60	.500	3.60	66	ш
C 59	8	21.2	6.23	.375	3.45	.037	15
" (BSC 13)	"	22.6	6.63	.425	3.50	"	ш
"	"	25.3	7.43	.525	3.60	"	"
C 60	.9	23.7	6.96	.400	3.45	.033	16
" (BSC 17)	ш	25.2	7.41	.450	3.50	"	"
"	ш	28.3	8.31	.550	3.60	"	и
H	"	31.3	9.21	.650	3.70	4	ж
				1			
C 61	10	24.6	7.23	.375	3.40	.029	16
66	u	26.3	7.73	.425	3.45	ш	ш
" (BSC 20)	"	28.0	8.23	.475	3.50	44	24
"	211	31.4	9.23	.575	3.60	4	u
u	"	34.8	10.23	.675	3.70	"	"
						9	
C 63	12	30.6	9.00	.450	3.45	.0245	16
" (BSC 25)	- 66	32.7	9.60	.500	3.50	at	"
"	EL.	36.8	10.80	.600	.3.60	ш	"
"	66	40.8	12.00	.700	3.70	"	"

General slope of flange, 2° = .035.

### WEIGHTS AND DIMENSIONS OF SHIP AND SPECIAL CHANNELS.—Continued.

Section' Number.	Depth of Channel.  Inches.	Weight per Foot.	Area of Section, Sq. Ins.	Thickness of Web.	Width of Flange.	Increase in Web and Flange for each Pound increase of Weight.	Page Number of Section.
C 95	13	32	9.30	.38	4.00	.023	11
"	66	35 37	10.29	.45	4.08 4.12	"	«« ««
и	66	40	11.76	.56	4.19	46	u
44	a	45	13.24	.68	4.30	"	"
u	α	50	14.71	.79	4.42	"	"
"	"	55	16.18	.90	4.53	. "	ш
C 65	18	45	13.25	.47	3.77	.016	12
ш	"	50	14.71	.55	3.85	"	44
u	"	55	16.18	.63	3.93	«	"
"	"	60	17.65	.72	4.02	EZ	66

### WEIGHTS AND DIMENSIONS OF BULB ANGLES.

Section	Size	Weight per Foot	Area of Section	Thickness Plain Leg	Thickness Bulb Leg	Length of Bulb	Width of Bulb	Page Number
Number	Inches	Pounds	Sq. Ins.	Inches	Inches	Inches	Inches	of Section
A174	4 x 3½	11.7	3.42	3 8	38	57	11/2	20
A176	5 x 4½	19.2	5.64	7 16	7 16	1 9 3 2	21/4	ш
A171	5 x 2½	10.2	3.00	$\frac{9}{32} - \frac{13}{32}$	1964	7 8	11/4	cc
A177	6 x 3	11.8	3.47	.34	5 16 3 8 7	1.21	1.08	"
"	"	13.5	3.95	.39	38	"	1.14	"
"	"	15.0	4.41	.43	7 16	u,	1.20	66
A178	6 x 3½	12.5	3.66	.37		1.16	1.01	66
66	"	14.1	4.13	.41	30	66	1.08	ш
ш	"	15.7	4.60	.45	7	"	1.14	66
66	"	17.3	5.07	.49	1/2	"	1.20	"
"	"	18.9	5.53	.53	16	"	1.26	"
66	44	20.5	6.02	.58	58	"	1.33	66
A179	7 x 3½	15.7	4.61	.43	3	1.25	1.10	21
"	"	17.5	5.13	.46	78	ii ii	1.16	66
66	"	19.1	5.60	.48	1 2	ш	1.23	66
A181	8 x 3½	17.4	5.09	.42	3	1.35	1.18	«
KE	"	19.3	5.64	.44	7	"	1.24	u
"	ш	21.5	6.30	.50	යි. සින්නද (රිද්යා ක්රියාන ක්නද රිද්යානය ක්නද (රිද්යා	"	1.30	66
A183	9 x 3½	20.3	5.96	.44	13 32 15 32 17 32	1.48	1.29	п
46	"	22.6	6.62	.48	15	66	1.35	46
"	"	24.8	7.27	.52	17	"	1.41	46
A185	10 x 3½	23.6	6.91	.47	3.	1.61	1.40	cc
"	"	26.1	7.64	.51	16	"	1.46	ш
"	и	28.5	8.35	.55	$\frac{7}{16}$ $\frac{1}{2}$ $\frac{9}{16}$	"	1.53	ш
		-		1	20 1			

# WEIGHTS AND DIMENSIONS OF STANDARD BULB ANGLES.

Section Number	Size.	Weight per Foot.	Area of Section.	Plain Leg.		Width of Bulb.	Page Number of
· ·	Ins.	Lbs.	Sq. In.	Ins.	Ins.	Ins.	Section.
A 187 " (BSBA 4) "	6 x 3	12.2 12.8 14.1 15.6	3.58 3.76 4.14 4.58	.375	.350 .375 .425 .475	1.025 1.050 1.100 1.150	22 u u
A 188 " (BSBA 8) " "	7 x 3½	15.3 16.8 18.6 20.0	4.50 4.94 5.46 5.90	.425	.375 .425 .475 .525	1.125 1.175 1.225 1.275	22 "
A 189 "(BSBA 12,	8 x 3½ «	18.0 19.6 21.6 23.2	5.29 5.78 6.34 6.83	.450	.400 .450 .500 .550	1.225 1.275 1.325 1.375	22 " "
A 190 "(BSBA 16) " " " "	9 x 3½	20.9 22.7 24.8 26.6 28.6	6.14 6.68 7.29 7.82 8.41	.475	.425 .475 .525 .575 .625	1.325 1.375 1.425 1.475 1.525	22 " "
A 191 "(BSBA 18) " " " " " "	10 x 3½	24.9 26.9 29.1 31.1 33.2 35.2	7.32 7.90 8.55 9.14 9.77 10.35	.525	.475 .525 .575 .625 .675 .725	1.450 1.500 1.550 1.600 1.650 1.700	23 " " " " " " " " " " " " " " " " " " "

### WEIGHTS AND DIMENSIONS OF CAR SIDE STAKES.

Section	Extreme Width.	Depth.	Weight per Foot.	Area of Section.	Base Thickness.	Apex Thickness.	Groove Width.	Page Number of
Number.	Ins.	Ins.	Lbs.	Sq. In.	Ins.	Ins.	Ins.	Section.
L 2	7 " "	$\begin{array}{c} 2\frac{3}{4} \\ 2\frac{13}{16} \\ 2\frac{15}{16} \end{array}$	7.2 8.7 11.7	2.10 2.54 3.42	3 16 1 4 3 8	3 8 7 16 9 16	25 «	23

# WEIGHTS AND DIMENSIONS OF REGULAR T-BARS. EQUAL LEGS.

Section Number.	Width of Flange.	Depth, of Bar.	Thickness of Flange.	Thickness of Stem.	Weight per Foot.	Area of Section.	Page Number of
	Inches.	Inches.	Inch.	Inch.	Pounds.	Sq. Ins.	Section.
T 5	1	1	1 to 5 32	1 to 5 32	.89	.26	24
T 181	11/8	118	3 " 7 32	5 " 7 32	1.37	.40	"
T 183	13	13	3 " 1 16 4	5 4 7 32 32	1.51	.44	"
T 187	11/4	11/4.	3 " 1	5 " 7 32 32	1.60	.47	«
T 188	11/4	114	8 " 7 16 32	3 " 9 16 32	1.70	.50	ш
T 191	11/2	11/2	3 4 7 32	3 " 7 16 32	1.94	.57	ú
T 193	11/2	11/2	1 " 9 32	1 " 9 32	2.47	.73	"
T 194	134	134	1 " 5 16	1 " 5 16	3.09	.91	и
T 37	2	2	1 " <u>5</u>	1 " 5 16	3.56	1.05	ш
T 39	2	2	5 4 3	5 " <u>3</u> 16 8	4.3	1.26	- 25
T 41	21	21	1 4 5	1 " 5 16	4.1	1.19	"
T 42	21/4	21	5 4 <u>3</u> 16 8	5 4 <u>3</u> 16	4.9	1.43	ш
T 47	21/2	21/2	1 " <u>5</u>	1 " 5 4 16	4.6	1.33	«
T 49	21/2	21/2	5 " 3 16 8	<u>5</u> " 3 8	5.5	1.60	ш

# WEIGHTS AND DIMENSIONS OF REGULAR T-BARS. UNEQUAL LEGS.

Section Number.		Width Depth of Flange. Bar. Inches.		Thickness of Flange. Inch.	Thickness of Stem.	Weight per Foot. Pounds.	Area of Section.	Page Number of Section.	
Т	16	11/4	116	3 to 1	$\frac{5}{32}$ to $\frac{7}{32}$	1.48	.43	25	
T	18	11/4	11/8	3 " <del>7</del> 16 32	3 " 1	1.56	.46	ш	
T	20	11/2	11/4	1 " 5 32	1 4 5	1.25	.37	a	

# WEIGHTS AND DIMENSIONS OF STANDARD ANGLES. EQUAL LEGS.

Sizes not specially marked were adopted as standard, May 21, 1910, by the Association of American Steel Manufacturers, for bridge, car, ship and general building construction. Sizes marked \* are of special thickness and age not A. A. S. M. Standard.

Section Num- ber.	Dimensions,	Thick-	Weight per Foot. Pounds.	Area of Section.	Section Num- ber.	Dimensions.	Thick- ness.	Weight per Foot.	Area of Section. Sq. Ins.
A 11  " " *A 15  " " " " " " " " "	11 12 12 12 12 12 12 12 12 12 12 12 12 1	1683 1-1466 638 1836 1836 1836 1646 176 187 16 12 188 16 148 176 188 16 188 16 188 16 188 16 188 16 188 16 188 16 188 16 188 16 188 16 188 16 188 16 188 16 188 16 188 16 188 16 188 16 188 188	1.23 1.80 2.34 2.86 3.35 1.65 2.44 3.19 3.92 4.7 5.3 6.0	.98 .48 .72 .94	A 23  ""  ""  ""  ""  ""  ""  ""  ""  ""	4 x 4 4 x 4	5 16 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8.2 9.8 11.3 12.8 14.3 15.7 17.1 18.5 19.9 21.2	2.40 2.86 3.31 3.75 4.18 4.61 5.03 5.44 5.84 6.23
*A 17  " " " " " " " " " " " " " " " " " "	2.12.12.12.12.12.12.12.12.12.12.12.12.12	16 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.08 3.07 4.1 5.0 5.9 6.8 7.7 4.9 6.1 7.2 8.3	.61 .90 1.19 1.47 1.73 2.00 2.25 1.44 1.78 2.11 2.43	A 27 w	6 x 6 6 x 6	387767 + + + + + + + + + + + + + + + + + +	14.9 17.2 19.6 21.9 24.2 26.5 28.7 31.0 33.1 35.3 37.4	4.36 5.06 5.75 6.43 7.11 7.78 8.44 9.09 9.73 10.37 11.00
* "A 21 "" " " " " " " " " " " " " " " " " "	30 X 30 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	123-14-15-15-15-15-15-15-15-15-15-15-15-15-15-	9.4 10.4 5.8 7.2 8.5 9.8 11.1 12.4 13.6 14.8 16.0 17.1 18.3	2.75 3.06 1.69 2.09 2.48 2.87 3.25 3.62 3.98 4.34 4.69 5.03	A 35	8 x 8 8 x 8	1239 155 8 1 16 1 1 16 1 16 1 16 1 16 1 18 1 16 1 18 1 16 1 18 1 1	26.4 29.6 32.7 35.8 38.9 42.0 45.0 48.1 51.0 54.0 56.9	7.75 8.68 9.61 10.53 11.44 12.34 13.23 14.12 15.00 15.87 16.73

Standard Angles vary only by  $\frac{1}{16}$  inch. Sections shown on page 17.  $\dagger$  Standard Ship Section.

# WEIGHTS AND DIMENSIONS OF STANDARD ANGLES. UNEQUAL LEGS.

Sizes not specially marked were adopted as standard, May 21, 1910, by the Association of American Steel Manufacturers, for bridge, car, ship and general building construction. Sizes marked \* are of special thickness and are not A. A. S. M. standard.

Section Num-	Dimensions.	Thick- ness.	Weight per Foot.	Area of Section.	Section Num-	Dimensions.	Thick- ness.	Weight per Foot.	Area of Section.
ber.	Inches.	Inch.	Pounds.	Sq. Ins.	ber.	Inches.	Inch.	Pounds.	Sq. Ins.
A 91 " " " " " " " " " "	2½ x 2 2½ x 2	3 16 16 38 7 16 12	2.75 3.62 4.5 5.3 6.1 6.8	.81 1.06 1.31 1.55 1.78 2.00	A 99 " " " " "	4 x 3 4 x 3 4 x 3 4 x 3 4 x 3 4 x 3 4 x 3	5 16 1 38 7 16 1 12 9 16 5 8 11 16	7.2 8.5 9.8 11.1 12.4 13.6 14.8	2.09 2.48 2.87 3.25 3.62 3.98 4.34
A 93	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1 †	4.5 5.6 6.6 7.6	1.31 1.62 1.92 2.22	* "	4 x 3 4 x 3 4 x 3	3 13 16 7 8	16.0 17.1 18.3	4.69 5.03 5.36
* " * " A 95	$   \begin{array}{ccccccccccccccccccccccccccccccccccc$	1 2 9 16	8.5 9.5	2.50 2.78	A101	5 x 3 5 x 3 5 x 3 5 x 3	5 16 3 8 7 16 1 2 9 16 5 8 11 16	8.2 9.8 11.3 12.8	2.40 2.86 3.31 3.75
A 30 " " " " " " " " " "	3 2 X 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	145 16 38 7 16 12 9	4.9 6.1 7.2 8.3 9.4 10.4	1.44 1.78 2.11 2.43 2.75 3.06	# " * "	5 x 3 5 x 3 5 x 3 5 x 3 5 x 3 5 x 3	9 16 58 11 16 34 13 16 7 8	14.3 15.7 17.1 18.5 19.9 21.2	4.18 4.61 5.03 5.44 5.84 6.23
*A 97 "" "" "" "" "" "" "" "" "" "" "" "" ""	3 ½ x 3 3 ½ x 3	9 16 5 8 11 16	5.4 6.6 7.9 9.1 10.2 11.4 12.5 13.6 14.7	1.56 1.93 2.30 2.65 3.00 3.34 3.67 4.00 4.31	A103 "" "" "" * ""	5 x 3 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5 16 3 8 7 16 12 9 16 5 8 11 16 3 4 13 16	8.7 10.4 12.0 13.6 15.2 16.8 18.3 19.8	2.56 3.05 3.53 4.00 4.47 4.92 5.37 5.81
* "	$3\frac{1}{2} \times 3$ $3\frac{1}{2} \times 3$	13	15.8 16.8	4.62 4.92	* "	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	16 7 8 15 16	21.3 22.7 24.2	6.25 6.67 7.09

Standard Angles vary only by  $\frac{1}{16}$  inch. Sections shown on page 18. † Standard Ship Section.

# WEIGHTS AND DIMENSIONS OF STANDARD ANGLES. UNEQUAL LEGS.—CONTINUED.

Sizes not specially marked were adopted as standard, May 21, 1910, by the Association of American Steel Manufacturers, for bridge, car, ship and general building construction. Sizes marked \* are of special thickness and are not A. A. S. M. standard.

Section Num- ber.	Dimensions.	Thick- ness.	Weight per Foot.	Area of Section.	Section Num- ber.	Dimensions.	Thick-	Weight per Foot.	Area of Section.
	inches.	IHCH.	Pounus.	Sq. Ins.		Inches.	Inch.	Pounds.	Sq. Ins.
A105	$6 \times 3\frac{1}{2}$	3 1	11.7	3.42	A107	6 x 4	3 8 7 16	12.3	3.61
	$6 \times 3\frac{1}{2}$	7	13.5	3.97		6 x 4	16	14.3	4.18
"	$6 \times 3\frac{1}{2}$	1 T	15.3	4.50	п	6 x 4	1/2	16.2	4.75
"	$6 \times 3\frac{1}{2}$	9 1	17.1	5.03	66	6 x 4	9	18.1	5.31
"	$6 \times 3\frac{1}{2}$	1 † † † † † † † † † † † † † † † † † † †	18.9	5.55	66	6 x 4	5	20.0	5.86
"	6 x 3½	116	20.6	6.06	66	6 x 4	11	21.8	6.40
"	6 x 3\frac{3}{2}	3 †	22.4	6.56	66	6 x 4	12 9 16 5 8 11 16 34	23.6	6.94
66	$6 \times 3\frac{1}{2}$	13	24.0	7.06	22	6 x 4	13	25.4	7.47
66	$6 \times 3\frac{1}{2}$	7	25.7	7.55	66	6 x 4	7/8	27.2	7.98
* 4	6 x 3½	13 16 7 8 15 16	27.3	8.03	* "	6 x 4	15	28.9	8.50
# "	$6 \times 3\frac{1}{2}$	1	28.9	8.50	* "	6 x 4	1	30.6	9.00

# WEIGHTS AND DIMENSIONS OF SPECIAL ANGLES. EQUAL LEGS.

Section Num- ber.	Dimensions.	Thick- ness.	Weight per Foot.	Area of Section.	Section Num- ber.	Dimensions.	Thick-	Weight per Foot.	Area of Section.
	Inches.	Inch.	Pounds.	Sq. Ins.		Inches.	Inch.	Pounds.	Sq. Ins.
A 36	3 x 3	18 3 16	.59 .84	.17 .25	A 41	$\begin{array}{c} 2\frac{1}{4} \times 2\frac{1}{4} \\ 2\frac{1}{4} \times 2\frac{1}{4} \\ 2\frac{1}{4} \times 2\frac{1}{4} \end{array}$	3 16 1 5 16	2.75 3.62 4.5	.81 1.06 1.31
и А 38	1 x 1 1 x 1 1 4 x 1 4 1 4 x 1 4	16 14	1.16 1.49 1.01 1.48	.34 .44 .30 .43	A. 43	$\begin{array}{c} 2\frac{3}{4} \times 2\frac{3}{4} \\ 2\frac{3}{4} \times 2\frac{3}{4} \\ 2\frac{3}{4} \times 2\frac{3}{4} \end{array}$	14 5 16 38	4.5 5.6 6.6	1.31 1.62 1.92
40 A 40	$1\frac{1}{4} \times 1\frac{1}{4}$	16 18 3 16 14 5 16 3 8	1.44 2.12 2.77 3.39 3.99	.56 .42 .62 .81 1.00 1.17	A 47	5 x 5 5 x 5 5 x 5 5 x 5 5 x 5 5 x 5 5 x 5	36776 16129 165814 11034	12.3 14.3 16.2 18.1 20.0 21.8 23.6	3.61 4.18 4.75 5.31 5.86 6.40 6.94

Standard Angles vary only by 1/8 inch. Sections shown on pages 18 and 19. † Standard Ship Section.

# WEIGHTS AND DIMENSIONS OF SPECIAL ANGLES. UNEQUAL LEGS.

Section Num- ber	Dim	ensions	Thick- ness	Weight per Foot		Section Num- ber	Dim	ensions	Thick-ness	Weight per Foot	Area of Section
	I	nches	Inch	Pounds	Sq. Ins.		I	nches	Inch	Pounds	Sq. Ins.
A129	3	x 2	3 16	3.07	.90	A109	7	$x 3\frac{1}{2}$	7 16	15.0	4.40
"	3	x 2	1/4	4.1	1.19	"	7	$x 3\frac{1}{2}$	1/2	17.0	5.00
ш	3	x 2	5 16	5.0	1.47	и	7	$x 3\frac{1}{2}$	9 16	19.1	5.59
u	3	x 2	38	5.9	1.73	ш	7	$x 3\frac{1}{2}$	5/8	21.0	6.17
ш	3	x 2	7 16	6.8	2.00	66	7	$x 3\frac{1}{2}$	11 16	23.0	6.75
"	3	x 2	1/2	7.7	2.25	ш	7	x 3½	14	24.9	7.31
						"	7	x 3½	13 16	26.8	7.87
A131	4	$x 3\frac{1}{2}$	16	7.7	2.25	"	7	$x 3\frac{1}{2}$	7	28.7	8.42
EE.	4	x 3½	38	9.1	2.67	ш	7	x 3½	15 16	30.5	8.97
ex .	4	$x 3\frac{1}{2}$	7 16	10.6	3.09	zz	7	x 3½	1	32.3	9.50
"	4	$x 3\frac{1}{2}$	1/2	11.9	3.50						
"	4	$x 3\frac{1}{2}$	9 16	13.3	3.90	A112	8	x 6	1	23.0	6.75
«	4	$x 3\frac{1}{2}$	5/00	14.7	4.30	MIII	8			25.7	7.56
и	4	$x 3\frac{1}{2}$	11 16	16.0	4.68	"		x 6	9 16		
							8	x 6	5/00	28.5	8.36
A135	5	x 4	38	11.0	3.23	"	8	x 6	11/16	31.2	9.15
а	5	x 4	7 16	12.8	3.75	ш	8	x 6	34	33.8	9.94
"	5	x 4	1/2	14.5	4.25	ш	8	x 6	13	36.5	10.72
ш	5	x 4	9 16	16.2	4.75	ш	8	x 6	7 8	39.1	11.48
и	5	x 4	50	17.8	5.23	EE	8	x 6	15 16	41.7	12.25
и	5	x 4	11 16	19.5	5.72	ш	8	<b>x</b> 6	1	44.2	13.00
									-		

Sections shown on page 19.

### BEAM TABLES.

Tables of safe loads for beams and channels and spacings of I-Beams for floors are given with explanatory notes on pages 100 to 135.

### BEAMS AS GIRDERS.

In some cases two or more beams may be bolted together side by side to form a girder, in which case cast iron separators with bolts should be used to hold the various members together. Separators should be placed at each end of the girder, at points of concentrated loading, and for uniform loading should be located at distances apart not greater than twenty times the width of the smallest beam flange, in order to laterally support the upper flanges which are in compression and prevent their failure by buckling. The separators should preferably fit closely between the beam flanges so as to unite the beams forming the girder and thereby cause them to act together in resisting the load. Tables of Standard and Special Separators are given on pages 66 and 67.

### CONNECTION ANGLES.

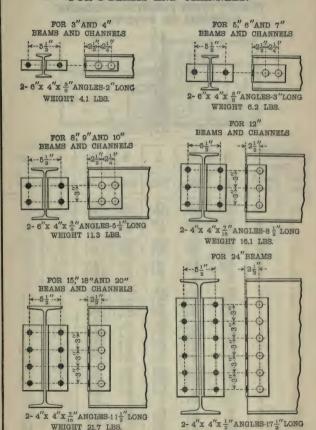
When beams are coped or fitted together at right angles, connection angles are generally used, standards for which, covering usual cases, are shown on pages 53, 54 and 55. Explanations and tables of limiting spans for which these standards may be used are given on pages 56 to 59. Beams may be fitted together thus with flush tops or bottoms or in intermediate positions, as required in cases where the girder or trimmer beam is the larger. In cases where the girder or trimmer beam is the smaller, special stirrups or other connections are required.

### LIVE LOADS FOR FLOORS.

The following loads per square foot, exclusive of weight of floor materials, show the range assumed in usual practice:

On page 328 are given in detail the safe loads for which floors should be designed in accordance with the building laws of various cities.

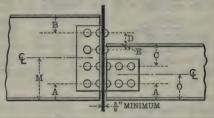
# STANDARD CONNECTION ANGLES FOR I-BEAMS AND CHANNELS.



All rivets and bolts to be 3/4" diameter; all open holes 13" diameter.

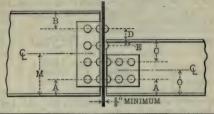
WEIGHT 37.4 LBS.

LOCATION OF CONNECTION ANGLES FOR STANDARD BEAMS OF THE SAME OR DIF-FERENT SIZES FRAMING OPPOSITE, BOTTOMS OR TOPS FLUSH,



In	ches	M	0	A	В	C	D	E
Main Beam	Opposite Beam	Inches	Inches	Inches	·Inches	Inches	Inches	Inche
8	8	11/2	11/2	1½	1½	1½		
4	3 4	21/2	11/2	11/2	21/2	11/2		
5	4 5	21/8	21/8 21/2	21/8 21/2	27/8	1 1/8 21/2		
6	4 5 6	23/8 21/2 3	23/8 21/2 3	23/8 21/2 3	35/8 31/2 3	15/8 21/2 8		
7777	4 5 6 7	23/8 23/2 23/2 33/2	23/8 21/2 21/2 21/2 31/2	23/8 21/2 21/2 31/2	45/8 41/2 41/2 81/2	15/8 21/2 31/2 31/2		
80000000	4 5 6 7 8	35/8 4 4 4	21/8 21/2 21/2 21/2 4	21/8 21/2 21/2 21/2 21/2	27/8 21/2 21/2 21/2 21/2 21/2	17/8 21/2 31/2 41/2 21/2	1½8 ½	 1/2 1/2
99999	56789	4 4 4 4 4 1/2	2½ 2½ 2½ 2½ 4 4½	2½ 2½ 2½ 2½ 2½ 3	3½ 3½ 3½ 3½ 3½ 3½	2½ 3½ 4½ 2½ 2½	1/2	11/2
10 10 10 10 10	5 6 7 8 9	44445	2½ 2½ 2½ 4 4 5	2½ 2½ 2½ 2½ 2½ 2½ 3½	4½ 4½ 4½ 4½ 4½ 4½ 3½	2½ 3½ 4½ 4½ 3½ 3½ 3½	1/2	1 1/2

## LOCATION OF CONNECTION ANGLES FOR STANDARD BEAMS OF THE SAME OR DIF-FERENT SIZES FRAMING OPPOSITE, BOTTOMS OR TOPS FLUSH.



	of Beams	M	0	A	В	C	D	E
Main Beam	Opposite Beam	Inches	Inches	Inches	Inches	Inches	Inches	Inches
12 12 12 12 12	8* 9* 10 12	5 %4 5 %4 5 %4 6	4¼ 4¼ 4¼ 6	284 284 284 284 30	3¼ 3¼ 3¼ 3 3	2¼ 3¼ 4¼ 8	3/4	11/4
15 15 15 15 15	8* 9* 10 12* 15	7¼ 7¼ 7¼ 7½ 7½	4¼ 4¼ 4¼ 6 7½	234 234 234 33	31/4 31/4 31/4 31/4 3	21/4 31/4 41/4 3 3	2 <sup>3</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>4</sub> 0	114
18 18 18 18 18	8* 9* 10 12* 15	7¼ 7¼ 7¼ 7½ 7½ 9	4¼ 4¼ 4¼ 6 7½ 9	2¾ 2¾ 2¾ 3 4½	614 614 614 6 6 41/2	21/4 31/4 31/4 31/4 31/4 31/4 41/2	234 134 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
20 20 20 20 20 20 20	8* 9* 10* 12* 15 18 20	7% 7½ 8 7½ 7½ 7½ 9	43% 4½ 5 6 7½ 9	21/8 31/2 31/2 31/2 51/2	81/8 8 71/2 8 61/2 51/2	21/8 31/2 31/2 41/2 51/2	0 % 21/2 0	0 1/2 0
24 24 24 24 24 24 24 24 24	8* 9* 10* 12* 15* 18 20 24	103/8 101/2 11 101/2 101/2 12 131/2 12	43% 41/2 5 6 71/2 9 101/2 12	21/8 31/2 3 41/2 6 41/2	61/8 6 51/2 6 6 41/2 41/2	2½ 3½ 3½ 3 4½ 4½ 4½	0 % 0 % 0 % 0 % 0 % 0 % 0 % 0 % 0 % 0 %	0 1/2 0 0 11/2 2

<sup>\*</sup>Opposite beam must be set back one inch to clear rivet heads.

## STANDARD CONNECTION ANGLES FOR I-BEAMS AND CHANNELS.

Standard connection angles for all sizes of beams and channels are shown on page 53. These are of sufficient strength for all usual connections of the various sizes shown, figured on the basis of 34 inch rivets or bolts and the following allowable unit stresses in pounds per square inch.

Stress.	Shop Rivets.	Field Rivets or Tarned Bolts.	Field Rough Bolts.
Single Shear	12000	10000	8000
	24000	20000	16000
	30000	20000	16000

In cases where beams frame opposite, the web between outstanding legs of standard connection angles should not be less than % inch thick.

When beams of very short spans are loaded to their full capacity, the end shear or reaction which has to be transmitted through the connections becomes so great that stronger connections than the standard should be used.

The following tables give the limits of length below which the standard connections do not apply and for which special designs should be made. For all lengths greater than those given in the tables the standard connections are sufficiently strong.

# MINIMUM SPANS OF CHANNELS FOR LIMITING VALUES OF STANDARD CONNECTION ANGLES.

-	hannel		Web Connec-	Outstanding Legs Connection.					
-	, manne		tion.	Field R	ivets.	Field B	olts.		
Section Number.	Depth.	Weight per Foot.	Enclosed Bearing Shop Rivets.	Single Shear Rivets or Turned Bolts.	Minimum Span.	Single Shear Rough Bolts.	Minimum Span.		
	Inches.	Pounds.	Pounds.	Pounds.	Feet.	Pounds.	Feet.		
C 5 "	3 "	4.0 5.0 6.0	7650 11700 16200	8840 "	.8 .8	7070	.9 1.0 1.1		
C 9	4 «	5.25 6.25 7.25	8100 11250 14850	8840 "	1.3 1.3 1.4	7070	1.5 1.6 1.8		
C 13	5 " "	6.5 9.0 11.5	8550 14850 21600	8840	1.9 2.2 2.6	7070	2.3 2.7 3.2		

# MINIMUM SPANS OF CHANNELS FOR LIMITING VALUES OF STANDARD CONNECTION ANGLES.

	hannel	JE 24	Web Connec-	Outsta	nding L	egs Conne	ction.
	*************		tion.	Field R	ivets.	Field I	Bolts.
Section Number.	Depth.	Weight per Foot.	Enclosed Bearing Shop Rivets.	Single Shear Rivets or Turned Bolts.	Minimum Span.	Single Shear Rough Bolts.	Minimum Span.
	Inches.	Pounds.	Pounds.	Pounds.	Feet.	Pounds.	Feet.
C 17	6 "	8.0 10.5 13.0 15.5	9000 14400 19800 25200	8840	2.7 3.1 3.5 4.0	7070	3.3 3.8 4.4 5.0
C 21	7 " "	9.75 12.25 14,75 17.25 19.75	9450 14400 18900 23850 28350	8840 "	3.7 4.2 4.7 5.2 5.8	7070 "	4.6 5.3 5.9 6.5 7.2
C 25 " "	8 " " "	11.25 13.75 16.25 18.75 21.25	19800 27900 36000 44100 52200	17670	2.5 2.8 3.1 3.4 3.6	14140	3.1 3.4 3.8 4.2 4.5
C 29	9 " "	13.25 15.00 20.00 25.00	20700 26100 40500 54900	17670	3.2 3.5 4.1 4.8	14140	4.0 4.3 5.1 6.0
C 33 " " "	10 « «	15.0 20.0 25.0 30.0 35.0	21600 34200 47700 61200 73800	17670	4.1 4.8 5.5 6.3 7.0	14140	5.1 6.0 6.9 7.8 8.8
C 41 " "	12 u u	20.5 25.0 30.0 35.0 40.0	18900 26320 34420 43200 51300	26510	6.1 4.9 5.5 6.0 6.6	21210	6.1 6.1 6.8 7.6 8.3
C 53 " " "	15 "" ""	33.0 35.0 40.0 45.0 50.0 55.0	36000 38700 46800 55800 64800 73800	35340	6.3 6.5 7.0 7.6 8.1 8.7	28280	7.9 8.1 8.8 9.5 10.2 10.9

# MINIMUM SPANS OF I-BEAMS FOR LIMITING VALUES OF STANDARD CONNECTION ANGLES.

	I-Beam		Web Connec-	Outsta	nding L	egs Conne	ction.
	I-Deam	•	tion.	Field R	ivets.	Field 1	Bolts.
Section Number.	Depth.	Weight per Foot.	Enclosed Bearing Shop Rivets.	Single Shear Rivets or Turned Bolts.	Minimum Span.	Single Shear Rough Bolts.	Minimum Span.
	Inches.	Pounds.	Pounds.	Pounds.	Feet.	Pounds.	Feet.
B 5 "	3	5.5 6.5	7650 11700	8840	1.2	7070	1.3
u	12	7.5	16200	u	1.2	ш	1.5
В 9	4 "	7.5 8.5	8550 11700	8840	1.8	7070	2.3
ec m	"	9.5 10.5	15300 18450	4	2.1 2.2	er er	2.6 2.7
B 13	5 "	9.75	9450 16200	8840	3.0	7070	3.7
B 17	6 "	14.75 12.25 14.75 17.25	22500 10350 15750 21150	8840	3.7 4.4 4.9 5.3	7070	4.6 5.5 6.1 6.6
B 21	7 8 4	15.00 17.50 20.00	11250 15750 20700	8840	6.3 6.8 7.3	7070	7.9 8.5 9.1
B 25	8 " " " " " " " " " " " " " " " " " " "	18.00 20.25 22.75 25.25	24300 31500 39600 47700	17670	4.3 4.6 4.9 5.2	14140 ""	5.4 5.7 6.1 6.5
B 29	9 "	21.0 25.0 30.0 35.0	26100 36900 51300 65700	17670	5.7 6.2 6.9 7.5	14140 "	7.2 7.8 8.6 9.4
B 33 ""	10 "	25.0 30.0 35.0 40.0	27900 40500 54000 67500	17670	7.4 8.1 8.9 9.6	14140	9.3 10.2 11.1 12.0
B 41	12	31.5 35.0 40.0	23625 29700 37800	26510	8.2 7.7 8.3	21210	9.1 9.6 10.4
B 105	12	40.0 45.0	31050 39150	26510	9.1 9.6	21210	11.3 12.0
44 .	66	50.0 55.0	47250 48600	er er	10.2 10.8	"	12.8

# MINIMUM SPANS OF I-BEAMS FOR LIMITING VALUES OF STANDARD CONNECTION ANGLES.

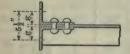
	I-Beam		Web Connec-	Outsta	nding L	egs Conne	ction.
	I-Deam	•	tion.	Field R	ivets.	Field I	Bolts.
Section Number.	Depth.	Weight per Foot.	Enclosed Bearing Shop Rivets.	Single Shear Rivets or Turned Bolts.	Minimum Span.	Single Shear Rough Bolts.	Minimum Span.
	Inches.	Pounds.	Pounds.	Pounds.	Feet.	Pounds.	Feet.
B 153	15 "	42.0 45.0 50.0 55.0	36900 41400 50400 59400	35340	8.9 9.2 9.8 10.3	28280	11.2 11.5 12.2 12.9
"	ш	60.0	67500	и	10.9	и	13.6
B 109	15 " "	60.0 65.0 70.0 75.0	53100 62100 70200 79200	35340	12.3 12.8 13.4 14.0	28280 ""	15.4 16.0 16.7 17.4
и	а	80.0	88200	ш	14.5	"	18.1
В 113	*15	80.0 85.0	72000 81000	35340	15.9 16.5	28280	19.9
u	u u	90.0	89100 98100	ec ec	17.0 17.6	ш	21.3 22.0
B 65	18	100.0	107100	35340	18.1	28280	22.6
"	"	60.0	50400	u	14.2	"	17.7
u	"	65.0	57600 64800	"	14.8 15.5	"	18.5
B 73	20	65.0	45000	35340	17.7	28280	22.1
u	"	70.0 75.0	52200 58500	"	18.5 19.2	"	23.0
B 121	20	80.0 85.0	54000 59400	35340	22.2 22.8	28280	27.7 28.5
"	ш	90.0	66600	и	23.6	"	29.4
"	"	95.0	72900 79200	"	24.3 25.0	u	30.3
B 89	24	80.0	67500	53020	17.6	42410	21.9
u u	ш	85.0	76950 85050	44	18.2 18.8	44	22.8
"	и	95.0	93150	ш	19.4	и	23.5
"	ш	100.0	101250	ш	20.0	ш	25.0
B 127	24	105.0	85050	53020	23.6	42410	29.5
"	HE .	110.0	93150 101250	"	24.2 24.8	at at	30.3

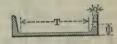
\*Interior web edges of standard connection angles must be chamfered to avoid interference with beam web fillets.

STANDARD SPACING OF RIVET AND BOLT HOLES THROUGH FLANGES AND CONNECTION ANGLES OF I-BEAMS, AND TANGENT DISTANCES BE-TWEEN FILLETS MEASURED ALONG THE WEB.

	20 X					15			P		不 业
Depth of Beam	Wt. per Ft.	n	g	q	T	Depth of Beam	Wt. per Ft.	n	g	q	T
Ins.	Lbs.	Ins.	Ins.	In.	Ins.	Ins.	Lbs.	Ins.	Ins.	In.	Ins.
3 u	5.5 6.5 7.5	1 1/2	2 <sup>21</sup> / <sub>32</sub> 2 <sup>5</sup> / <sub>8</sub> 2 <sup>19</sup> / <sub>32</sub> 2 <sup>21</sup> / <sub>32</sub>	1/4 u	1 13 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	15	42.0 45.0 50.0 55.0 60.0	3 u u	2 ½ 2½ 2½ 2½ 2 ½ 2 ½ 2 ½ 2 ½ 2 ½ 2 ½ 2	5/8	12 76 44 44 44 44 44 44 44 44 44 44 44 44 44
# # B	9.5 10.5 9.75	13/4	25/8 2 19/32 2 17/32 2 5/8	# # # # # # # # # # # # # # # # # # #	3 9 16 4	15	50.0 55.0 70.0 75.0	31/4	2 <sup>15</sup> / <sub>32</sub> 2 <sup>13</sup> / <sub>32</sub> 2 <sup>3</sup> / <sub>8</sub> 2 <sup>5</sup> / <sub>16</sub> 2 <sup>1</sup> / <sub>4</sub>	7/8	113/4
6	12.25 14.75		2½ 2½ 25/8	и	и	15	80.0 80.0 85.0	33/4	21/4 2 1/1 2 1/1 2 5/16	1 1 3 2	10 15
44	14.75 17.25	2	2½ 2½	8/8	4 7 16 4	u u	90.0 95.0 100.0	# # # # # # # # # # # # # # # # # # #	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ec ec
. 7	15.00 17.50 20.00	21/4	2 ½ 2½ 2½	3/8	5 16 4	18	85.0 60.0	31/4	2 17	11	15 3 16
2 4	18.00 20.25 22.75	21/4	25/8 2 16 2 17 2 17	7 16 4	6 3 4	4	70.0	u	2 15 2 3 2 2 3 8	ш	-
9 "	25.25 21.0 25.0	21/2	2½ 2½ 2½ 2½	1/2	7 1 1 8	20	70.0 75.0	31/2	2½ 2½ 2½ 2½	13 16 4	167/8
"	30.0 35.0	4	23/8	u	4	20	80.0 85.0	4	2 13 2 16	15	16,76
10	25.0 30.0 35.0 40.0	25/8 u	$\begin{array}{c} 2 \frac{19}{32} \\ 2 \frac{17}{32} \\ 2 \frac{7}{16} \\ 2 \frac{7}{16} \end{array}$	1/2 "	7 15 u	u	90.0 95.0 100.0	44 44 M	2 11 2 3/8 2 5 16	# # # # # # # # # # # # # # # # # # #	4 4
12 "	31.5 35.0 40.0	23/4	2 ½ 2 ½ 2 ½ 2 ½ 2 ½ 2 ½ 2 ½ 2 ½ 2 ½ 2 ½	1/2	9 11 16 11	24 u	80.0 85.0 90.0 95.0 100.0	<i>u u u</i>	$\begin{array}{c} 2\frac{1}{2} \\ 2\frac{15}{32} \\ 2\frac{7}{16} \\ 2\frac{13}{32} \\ 2\frac{3}{8} \end{array}$	7/8	20 11 4 4 4 4 4
12 u u	40.0 45.0 50.0 55.0	3 "	2 ½ ½ 2 ½ 2 ½ 2 ½ 2 ½ 2 ½ 2 ½ 2 ½ 2 ½ 2	1/2 u u	9 5 16 u	<b>94</b> u	105.0 110.0 115.0	d u u	2 ½ 2 ½ 2 ½ 2 ½ 2 3 ½ 2 3 %		201/8

STANDARD SPACING OF RIVET AND BOLT HOLES
IN FLANGES AND CONNECTION ANGLES OF
CHANNELS, AND TANGENT DISTANCES BETWEEN FILLETS MEASURED ALONG THE WEB.





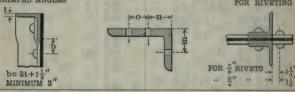
Depth of Channel	Wt. per Ft.	m	g	q	T	Depth of Channel	Wt. per Ft.	m	g	R	T
Ins.	Lbs.	Ins.	Ins.	In.	Ins.	Ins.	Lbs.	Ins.	Ins.	In.	Ins.
3 4 4	4.0 5.0 6.0 6.25 6.25 7.25	1 4 4	2 <sup>21</sup> / <sub>32</sub> 2 <sup>5</sup> / <sub>8</sub> 2 <sup>2</sup> / <sub>16</sub> 2 <sup>2</sup> / <sub>32</sub> 2 <sup>5</sup> / <sub>8</sub> 2 <sup>19</sup> / <sub>32</sub>	33	1 13 16 H	10 "	15.0 20.0 25.0 20.0 35.0	4	25/8 2 1/6 2 1/2 2 1/3 2 1/2 2 1/3 2 1/2	## ## ## ## ## ## ## ## ## ## ## ## ##	8 16 u
5 "	6.5 9.0 11.5	1 11/4	2 31/2 2 19/2 2 1/2	16 u	35/8 «	« «	25.0 30.0 35.0 40.0	13/4	25/8 21/2 23/8	1/2 u u	9 15
<b>6</b> u u	8.0 10.5 13.0 15.5	1½8 1¾8	2 <sup>2</sup> / <sub>3</sub> <sup>2</sup> / <sub>2</sub> 2 <sup>1</sup> / <sub>3</sub> <sup>2</sup> / <sub>2</sub> 2 <sup>1</sup> / <sub>3</sub> <sup>2</sup> / <sub>3</sub>	8/8	41/2	13 « «	32.0 35.0 37.0 40.0	23/4	$\begin{array}{c} 2\frac{?}{16} \\ 2\frac{17}{32} \\ 2\frac{1}{2} \\ 2\frac{15}{32} \end{array}$	16 4	103/8
# # # # # # # # # # # # # # # # # # #	9.75 12.25 14.75 17.25 19.75	1½ = 1½ "	25/8 2 13/2 2 1/2 2 1/2 2 7/16	3/8 = = =	5 7 16 a	a a	45.0 50.0 55.0	es es	2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	es es	es es
<b>8</b> u u	11.25 13.76 16.25 18.75 21.25		25/8 2 1/8 2 1/8 2 1/2 2 1/2 2 1/2 2 1/2	# # # # # # # # # # # # # # # # # # #	6 1 6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 4 4	33.0 35.0 40.0 45.0 50.0 55.0		2 17 2 17 2 1/2 2 1/2 2 1/6 2 3/8 2 11 2 1/2	5/8 u u u	123/8
9 "	13.25 15.00 20.00 25.00	13/8 13/4	2 <sup>5</sup> / <sub>8</sub> 2 <sup>13</sup> / <sub>32</sub> 2 <sup>17</sup> / <sub>16</sub>	7 16 4 4	71/4	18 "	45.0 50.0 65.0 60.0	21/4	2 \\ 2 \\ \ 2 \\ \ \ 2 \\ \ \ \ \ \ \ \	7/8	15 

# MAXIMUM SIZE OF RIVETS IN FLANGES OF BEAMS AND CHANNELS.

		I-BEA	CHANNELS.					
Depth of Beam.	Weight.	Diameter of Rivets.	Depth of Beam.	Weight.	Diameter of Rivets.	Depth of Channel.	Weight,	Diameter of Rivets.
Inches.	Lbs. per Ft.	Inch.	Inches.	Lbs.perFt.	Inch.	Inches.	Lbs. per Ft.	Inch.
8 4 5 6 7 8 9 10 12 19	5.50 7.50 9.75 12.25 15.00 18.00 21.00 25.00 31.50 40.00	8/20/20/20/20/20/20/20/20/20/20/20/20/20/	15 15 15 18 20 20 24 24	42.0 60.0 80.0 55.0 65.0 80.0 80.0 105.0	3/4 44 7/8 44 66 66 64	84 56 78 99 102 15	4.00 5.25 6.50 8.00 9.75 11.25 13.25 15.00 20.50 33.00	% % % % % % % % % % % % % % % % % % %

# STANDARD SPACING OF RIVET AND BOLT HOLES IN ANGLES, WITH MAXIMUM

RIVETS IN SIZE OF RIVETS TO BE USED. CLEARANCE FOR RIVETING



#### ANGLES.

Length of Leg.	m	Diam. of Rivet.	Length of Leg.	m	Diam, of Rivet.	Length of Leg.	m	n	0	Diam. of Rivet.
Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.
1 11/4 13/8 11/2 13/4	1/2 5/8 8/4 7/8	1/4 61 8/8 61 61 1/2	21/4 21/2 23/4 31/2 31/2	11/8 11/4 13/8 15/8 13/4	5/8 8/4	441/2 5 6 7 8	2½ 3 3½ 4 4½	2.1/2 3.1/2	1½ 1¾ 2¼ 3	

#### BEARING PLATES FOR SHAPES USED AS REAMS

Shapes used as beams resting on masonry walls or piers will generally require bearing plates of steel or their equivalents, set in or upon the masonry to properly distribute the load thereon with due regard to the allowable safe pressures

for the class of stonework or brickwork in question.

A table of bearing plates is given on page 65, which gives the bearing values in pounds for plates of various sizes based on the safe unit pressure allowable for different classes of masonry. As the strength of masonry varies largely according to the qualities of the material used, the workmanship and age, it is impossible to give absolute figures for safe unit pressures for all classes of work, but the values given on page 64 are believed to fairly represent these for the usual kinds of ordinary architectural masoury. The strength of ordinary masoury generally depends upon the crushing value of the mortar or cement used and does not bear any fixed relation to the ultimate strength of the brick or stone entering into the construction.

The table of bearing plates gives the bearing values of various sizes of plates when used with different classes of masonry, but the thickness of the plate

should be computed for each case.

For a plate of given length and breadth the thickness depends upon the allowable load and unit stress, and the width of the flange of the beam or channel resting upon it.

The thickness may be determined by the following formula

$$t = .866 (1-b) \sqrt{\frac{R}{pb'l}}$$

= thickness of plate in inches.

1 = length of plate in inches, in a direction perpendicular to the axis of the beam or channel.

b = width of flange of beam or channel in inches.

R = reaction at point of support in pounds.

For uniformly distributed loads, R = one-half of the load given in Tables of Safe Loads, pages 106 to 123 inclusive.

= allowable stress in pounds per square inch on extreme fibre of plate.

b' = width of plate in the direction of the axis of the beam or channel; i. e., bearing on wall in inches.

If p = 16000 lbs, for steel we have

$$t = .00685 (1 - b) \sqrt{\frac{R}{b'l}}$$

#### EXAMPLE.

What is the proper size of steel bearing plate to be used in a wall of brick laid in cement mortar to support the end of a 10-inch standard I-Beam, weighing 40 pounds per foot, of 10 foot span, subjected to its safe load uniformly distributed? On page 109 in the Table of Safe Loads Uniformly Distributed for Cambria I-Beams, the total load is found to be 33 850 pounds, and half of this, or 16 925

pounds, will be the reaction at each end.

On referring to the Table of Bearing Plates, on page 65, the proper size for this load on the class of masonry in question is found to be 6" x 10". The width of flange of a 10-inch 40 lb. standard beam is 5.10 inches.

Substituting these values in the formula for thickness gives

$$t = .00685 (10 - 5.10) \sqrt{\frac{16925}{6 \times 10}} = .562$$

The nearest commercial size above this is inch, which is the thickness required.

If a shorter plate would suit the location better it may be seen from the table that a plate 8" x 8" will give the necessary bearing value and the thickness of this would be

$$t = .00685 (8 - 5.10) \sqrt{\frac{16925}{8 \times 8}} = .323$$

and the nearest commercial size above this is 3%", which is the thickness required.

# STANDARD BEARINGS AND BEARING PLATES.

Size		Bearing Plate.						
f Beams and Channels.	Bearing.	Dimensions.	Weight.	Area.				
Inches.	Inches.	Inches.	Pounds.	Sq. Inches				
3	6	6 x 6 x 3/8	3.9	36				
4	6	6 x 6 x 3/8	и	36				
5	6	6 x 6 x 3	ш	36				
6	6	6 x 6 x 3/8	ш	36				
7	8	8 x 8 x ½	9.1	64				
8	8	8 x 8 x ½	"	64				
9	8	8 x 8 x ½	и	64				
10	12	12 x 12 x 3	30.6	144				
12	12	12 x 12 x 3	ш	144				
15	12	$12 \times 15 \times \frac{3}{4}$	38.3	180				
18	15	15 x 15 x 7	55.8	225				
20	15	15 x 18 x 1	76.5	270				
24	15	15 x 18 x 1	и	270				

# SAFE BEARING VALUES OF WALL PLATES FOR VARIOUS STYLES OF MASONRY.

Material.	Pounds per Sq. In.	Tons per Sq. Ft.	
Rubble Masonry in Cement Mortar	250	18.0	
Brickwork " " "	300	21.6	
First Class Sandstone (Dimension Stone).	400	28.8	
" Limestone	500	36.0	
" " Granite	600	43.2	
Portland Cement Concrete 1:2:4	600	43.2	
" " 1:2:5	500	36.0	

# BEARING PLATES FOR I-BEAMS AND CHANNELS.

	0:	Safe Bearing Value of Plate in 1000 Pounds.									
Bearing on Wall.	Size of Plate.	Mortar.	Brick in Cement Mortar.	Sand- stone.	Lime- stone.	Granite.	Concrete. 1:2:4.	Concrete. 1:2:5.			
Ins.	Ins.	250 lbs. per sq. in.	300 lbs. per sq. in.	400 lbs. per sq. in.	500 lbs. per sq. in.	600 lbs. per sq. in.	600 lbs. per sq. in.	500 lbs, per sq. in.			
4 4 4	4 x 4 4 x 6 4 x 8	4.0 6.0 8.0	4.8 7.2 9.6	6.4 9.6 12.8	8.0 12.0 16.0	9.6 14.4 19.2	9.6 14.4 19.2	8.0 12.0 16.0			
6 6	6 x 6 6 x 8 6 x 10	9.0 12.0 15.0	10.8 14.4 18.0	14.4 19.2 24.0	18.0 24.0 30.0	21.6 28.8 36.0	21.6 28.8 36.0	18.0 24.0 30.0			
8 8	8 x 8 8 x 10 8 x 12	16.0 20.0 24.0	19.2 24.0 28.8	25.6 32.0 38.4	32.0 40.0 48.0	38.4 48.0 57.6	38.4 48.0 57.6	32.0 40.0 48.0			
10 10 10	10 x 10 10 x 12 10 x 14	25.0 30.0 35.0	30.0 36.0 42.0	40.0 48.0 56.0	50.0 60.0 70.0	60.0 72.0 84.0	60.0 72.0 84.0	50.0 60.0 70.0			
12 12 12 12 12	12 x 12 12 x 14 12 x 15 12 x 16 12 x 18	36.0 42.0 45.0 48.0 54.0	50.4 54.0 57.6 64.8	57.6 67.2 72.0 76.8 86.4	72.0 84.0 90.0 96.0 108.0	86.4 100.8 108.0 115.2 129.6	86.4 100.8 108.0 115.2 129.6	72.0 84.0 90.0 96.0 108.0			
14 14 14 14	14 x 14 14 x 16 14 x 18 14 x 20	49.0 56.0 63.0 70.0	58.8 67.2 75.6 84.0	78.4 89.6 100.8 112.0	98.0 112.0 126.0 140.0	117.6 134.4 151.2 168.0	117.6 134.4 151.2 168.0	98.0 112.0 126.0 140.0			
15 15	15 x 15 15 x 18	56.2 67.5	67.5 81.0	90.0 168.0	112.5 135.0	125.0 162.0	135.0 162.0	112.5 135.0			
16 16 16 16	16 x 16 16 x 18 16 x 20 16 x 22	64.0 72.0 80.0 88.0	76.8 86.4 96.0 105.6	102.4 115.2 127.0 139.8	128.0 144.0 160.0 176.0	153.6 172.8 192.0 211.2	153.6 172.8 192.0 211.2	128.0 144.0 160.0 176.0			
18 18 18 18	18 x 18 18 x 20 18 x 22 18 x 24	81.0 90.0 99.0 108.0	97.2 108.0 118.8 129.6	129.6 144.0 158.4 172.8	162.0 180.0 198.0 216.0	194.4 216.0 237.6 259.2	194.4 216.0 237.6 259.2	162.0 180.0 198.0 216.0			
20 20 20 20 20	20 x 20 20 x 22 20 x 24 20 x 26	100.0 110.0 120.0 130.0	120.0 132.0 144.0 156.0	160.0 176.0 192.0 208.0	200.0 220.0 240.0 260.0	240.0 264.0 288.0 312.0	240.0 264.0 288.0 312.0	200.0 220.0 240.0 260.0			

Safe Bearing Value of Plate = Area of Plate (in square inches)  $\times$  Allowable Safe Bearing Value (per square inch) on the Masonry.

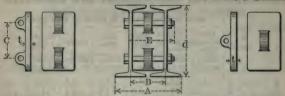
Beams.

25.0

B 41 12 31.5

B 105 | 12 | 40.0

# STANDARD CAST IRON SEPARATORS FOR I-BEAMS.



Separators.

Bolts, Square Heads

								-	amo	L.He.	k. Nut	В.
Section Num- ber.	P. Depth.	Weight per Foot.	Out to Out of Flanges of Beams.	COHOOL	Thiokness.	Weight.	Increase of Weight for each inch additional spread of beams.	Diameter.	Center to Cen-	I length.	Weight of Bolts and Nuts.	Increase of Weight of Bolts for each in, addi- tional spread of Beams,
J. P.	Ins.	Pounds.	Inches.	Inches.	In.	Pounds.	Pounds.	In.	Ins.	Ins.	Pounds.	Pound.
		SE	PARA'	CORS	W S	/ITH	ONI	E E	OL	T.		
B 5 B 9 B 13 B 17 B 21 B 25 B 29	3 4 5 6 7 8 9	5.5 7.5 9.75 12.25 15.0 18.0 21.0		3 141 2 4 44 1/2 5	3 8 4 4 1 2 4 4	1.0 1.3 1.8 3.0 3.3 3.8 5.0	.17 .26 .36 .59 .65 .72	3 4 4 4 4 4 4 4 4		4 4 4 4 4 4 4 5 5 5 6	.95 1.01 1.04 1.11 1.14 1.17 1.23	.123

# SEPARATORS WITH TWO BOLTS.

7.5

7.0

7.5

.98

1.14

1.14

7 1.32 "

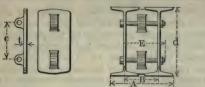
44

1.38

73 44	40			1		1	1	1 -	1	1	1	1
B 41	12	31.5	103	534	1/2	7.8	1.20	34	61/2	7	2.64	.246
B 105	12	40.0	111	6	66	7.8	1.20	ü	n"	71	2.76	44
B 53	15	42.0	113	61/4	II	11.5	1.50	44	7	73	2.82	"
B 109	15	60.0	121	6½ 6¾ 6¾	46	11.5	1.50	"	66	81	2.95	"
B 113	15	80.0	13	63	EE.	11.5	1.50	66	66	9	3.13	66
B 65	18	55.0	123	63	584	16.5	2.28	66	9	81	2.95	66
B 73	20	65.0	131	7		17.5	2.60	"	10	81/2	3.01	46
B 121	20	80.0	141/8	74	66	17.5	2.60	66	66	91	3.19	"
B 89	24	80.0	143	73	"	25.5	3.25	66	12	91	3.19	"
B 127	24	105.0	16	81	66	25.5	3.25	66	IX	$9\frac{1}{2}$	3.26	"

Lengths and weights of separator bolts in above table are for girders composed of two beams of minimum section as shown. Lengths of bolts for intermediate and maximum sizes of beams may be obtained by adding twice the increase of web thickness to the lengths given.

## SPECIAL CAST IRON SEPARATORS FOR I-BEAMS.





Rasms Sanarators Bolts, Square Heads												
		Beam	15.		8	eparat	ors.	B	and	Squ He:	are H	eads
Section Num- ber.	D Depth.	Weight per Foot.	Out to Out of Flanges of Beams.	общия	Thickness.	Weight.	ncrease of Weight for each inch additional spread of Beams.	Diameter.	Center to Cen-	H Length.	Weight of Bolts and Nuts.	Increase of Weight of Bolts for each in. addi- tional spread of Beams.
	Ins.	Pounds.	Inches.	Inches.	In.	Pounds.	Pounds.	In.	Ins.	Ins.	Pounds.	
-		SE	PARA'	TORS	V	/ITH	ONI	B E	BOL	T.		
B 5 B 9 B 13 B 17 B 21 B 25 B 29 B 33 B 41 B 105	3 4 5 6 7 8 9 10 12 12	5.5 7.5 9.75 12.25 15.0 18.0 21.0 25.0 31.5 40.0	$\begin{array}{c} 7\frac{5}{16} \\ 7\frac{7}{8} \\ 8\frac{1}{2} \\ 9\frac{5}{16} \\ 9\frac{7}{8} \\ 10\frac{3}{4} \\ 11\frac{1}{4} \end{array}$	8 14 12 4 14 12 5 5 14 3 4 5 6	3 8 4 4 1 2 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1.1 1.6 2.0 3.3 3.9 4.7 5.9 6.8 8.8 8.9	.29 .38 .49 .78 .92 1.06 1.20 1.33 1.61 1.58	3 4 4 4 4 4 8 8 8 4 4 4 4 4 4 4 4 4 4 4		4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	.95 1.01 1.04 1.11 1.14 1.17 1.23 1.26 1.32 1.38	.123
			PARAT		W	ITH	TWO	-	OL	rs.		
B 41 B 105 B 53 B 109 B 113 B 65 B 73 B 121 B 89 B 127	12 12 15 15 15 18 20 20 24 24	31.5 40.0 42.0 60.0 80.0 55.0 65.0 80.0 80.0	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	534 6 14341434 7 7 3 4 3 4 5 8 7 8 8	12 u u u 558 u u u u	9.5 9.5 12.5 13.0 13.2 19.8 22.9 24.6 30.3 32.5	1.61 1.58 2.02 1.97 1.91 2.41 3.37 3.34 4.07 4.07		6½ "7" "9 10" "12"	7 7 2 3 4 1 4 1 2 1 4 1 4 1 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	2.64 2.76 2.82 2.95 3.13 2.95 3.01 3.19 3.19 3.26	.246

Lengths and weights of separator bolts in above table are for girders composed of two beams of minimum section as shown. Lengths of bolts for intermediate and maximum sizes of beams may be obtained by adding twice the increase of web thickness to the lengths given.

#### FIREPROOF CONSTRUCTION.

Buildings of fireproof construction consist essentially of a steel frame or skeleton to support the floors, and in the case of high buildings, the outside walls also are carried by the steel framing. All parts of the steel work are enclosed and protected by some fire-resisting material, which should be of such quality and arrangement as not to disintegrate or fall away when heated to high temperatures and at the same time exposed to a stream of cold water. The fireproofing for the floors, in addition to its ability to afford a fireproof protection to the steel beams, must be capable of supporting the load and distributing it to the floor beams, which in turn transmit it to the columns and thence to the foundations.

One of the earlier forms of floors consists of brick arches built between and supported by the bottom flanges and lower portions of the web of iron or steel I-Beams, but this style has considerable dead weight and, as ordinarily constructed, does not provide fireproof protection for the bottom flanges of the beams. Another of the earlier forms of floor is composed of sheets of corrugated iron arched between the beams, on which a concrete filling is placed, and this also, as ordinarily constructed, does not provide protection for the bottom flanges of the beams, besides, it is quite heavy.

A later style of floor is the hollow tile system, which is composed of flat or segmental arches constructed of moulded blocks of hard burned clay, specially shaped, and of various depths to suit different loads and the sizes of the I-Beams supporting them. In the hollow tile system, the blocks may also be of porous terracotta which is lighter than hard clay.

Various other systems of fireproofing are now in use, the most usual forms of which consist of cement, concrete or other material used alone or deposited or arranged about a strengthening or supporting framework of steel shapes, bars, rods, wire, wire-cloth, etc.

Column or girder fireproofing may be accomplished by the use of hard clay or porous terra-cotta blocks shaped to fit and enclose the steel work, or the steel may be wrapped with wire, wire-cloth, metal lath, etc., and a concrete or plastered coating applied to it.

Fireproof partitions may be constructed of hollow tile composed of hard clay or porous terra-cotta to which the plaster finish may be directly applied, or they may be composed of suitable metal studding on which is secured the wire-cloth or metal lath that serves to support the concrete or other fireproofing, the surface then being plastered in the usual manner.

The dead weights of fireproof floors vary between wide limits dependent upon the system employed, the load to be carried and the distance between the supporting beams.

## WEIGHTS OF HOLLOW TILE FLOOR ARCHES AND FIREPROOF MATERIALS.

#### END CONSTRUCTION, FLAT ARCH.

Width of Span between Beams.	Depth of Arch.	Weight per Square Foot		
5 feet to 6 feet.	8 inches.	27 pounds.		
6 " 7 "	9 "	29 "		
7 " 8 "	10 "	33 "		
8 " 9 "	12 "	38 "		

#### HOLLOW BRICK FOR FLAT ARCHES.

(SIDE CONSTRUCTION.)

	Width of Span between Beams.							Depth of Arch.		Weight	Weight per Square Foot		
3 1	feet	6	inches	to 4	feet	0	inches.	6	inches.	27	pounds.		
4	"	0	46	4	46	6	"	7	"	29	- "		
4	46	6	66	ŧ	a	0	ш	8	"	32	ш		
5	46	6	ec	. (	46	0	"	9	u	36	u		
6	66	0	44	(	66	6	«,	10	u	39	u		
6	23	6	. 4	7	66	0	"	12	"	44	"		

#### PARTITIONS.

				Thick	ness.	Weight	per Square Foot.
Hollow	Brick	(Clay)	Partitions.	2 inc	ches.	11	pounds.
"	"	"	"	3	"	14	- "
"	44	66	"	4	44	15	4
"	"	"	"	5	66	19	ш
"	46	44	66	6	"	20	44
"	46	u	"	8	66	27	44
Porous	Terra-	Cotta	Partitions.	3	"	16	ш
66	"	ш	4	4	"	19	"
"	4	"	и	5	"	22	"
66	"	66	"	6	44	23	"
44	44	"	u	8	"	33	"

#### FURRING, ROOFING AND CEILING.

				Thic	kness.	Weight	per Square Foot.
Porous	Terra-	Cotta F	urring.	2 in	ches.	8	pounds.
"	4		oofing.	2	4	12	"
66	"	"	"	3	"	14	"
« · · ·	ш	. 66	66	4	"	18	"
ec.	"	" Ce	eiling.	2	"	11	«
44	ш	4	"	3	a	14	"
α	44	44	"	4	"	18	"

6-inch Segmental Arches,  $26\frac{1}{2}$  pounds per square foot.

2- "Porous Terra-Cotta Partition, 8 pounds per square foot. 8" x 3\frac{3}{4}" x 2\frac{1}{4}" Hollow Brick, 3000 lbs. per 1000.

# TABLES OF SAFE LOADS—TERRA COTTA FLOOR ARCHES.

The Table of Safe Loads for Flat Arches, page 71, is applicable to all shapes of blocks. The areas given are obtained by passing a plane through the blocks at right angles to all the webs and are the areas for 1-foot width of arch. Generally speaking, end construction blocks of various shapes, but of the same depth and cross sectional area, have equal strength. The weight of the arch has not been deducted in Table of Safe Loads for Flat Arches. Therefore, this and other dead loads must be deducted to obtain the net safe live load for any arch and span.

EXAMPLE.—What load will an 8-inch arch carry (using a Factor of Safety of 5), for a span of 5 feet 6 inches, the blocks having a sectional area parallel to the beams, of 44.25 square inches?

Area of 8-inch block in Table = 37 sq. ins.

 $44.25 \div 37 = 1.19$ , Ratio of Actual Area to Tabular Area. Safe Load in Table = 228,  $\times 1.19 = 271$  pounds = Safe

Load for Actual Area.

Weight of Arch =  $44.25 \times 12 = 531$  cu. in.  $\times .06 = 32$  lbs. per sq. ft.

271 - 32 = 239 lbs. = Safe Load in lbs. per sq. ft. for

S. F. of 7.  $271 \times 7 \div 5 = 379$ , -32 = 347 lbs., Safe Load for S. F. of 5.

Tables of Safe Loads for Segmental Arches in spans up to 10 feet are given on pages 72 and 73. The areas of the blocks for which the safe loads are given are the areas per foot of arch parallel with beams. The weight of the arch blocks has been deducted in the Table, so that only the dead load of concrete fill, plastering, etc., must be deducted to obtain net live load.

Segmental arch construction is cheaper than flat arch construction, and is the stronger of the two. Where for any reason a flat arch is not deemed necessary, this is an admirable floor

construction to use.

Even with this type of construction, the flat ceiling may be secured by suspending a metal lath ceiling below the arch from the bottom of the beams. To do this, however, adds so much to the cost that it is generally cheaper to use the Flat Arch.

Segmental Arches can also be built with a raised skew. This flattens the arch and reduces the amount and consequently the expense of the cinder concrete fill, but it also reduces the strength

of the arch.

In Segmental Arches, the thrust on the beams (particularly at the bottom of beams) is very great, and where there is any doubt of the beams' sustaining the thrust, it is desirable to use steel tie rods. These tie rods may be fireproofed or left unprotected, the best practice being to protect them.

## SAFE LOADS FOR FLAT FLOOR ARCHES OF SEMI-POROUS TERRA COTTA.

As given by manufacturers of this material.

Safety Factor 7.

	-										
ARCHES.	6 ins.	7 ins.	8 ins.	9 ins.	10 ins.	12 ins.	15 ins.				
ARMAS.			Squ	are Inc	hes.						
	31	34	37	40	48	49	58				
SPANS.		Pounds per Square Foot.									
1 Ft. 6 In.	1928	2468	3069	3733	4459	6097	9022				
2 " 0 "	1085 694	1388 888	1726 1104	2100 1344	2508 1605	3430 2195	5075 3248				
3 " 0 " 8 " 8 " 8 " 8 " 8 " 8 " 8 " 8 " 8	482 410 354 308	617 525 453 394	767 650 563 491	938 795 685 597	1114 950 819 713	1524 1299 1120 975	2255 1922 1657 1443				
4 " 0 " 4 " 8 " 4 " 6 "	271 240 214 192	347 307 274 246	481 382 341 306	525 465 414 372	627 555 495 444	857 759 677 608	1268 1124 1002 900				
5 " 0 " 5 " 3 " 5 " 6 " 5 4 9 "	173 157 143 131	222 201 183 168	276 250 228 208	336 304 277 254	401 364 331 303	548 497 453 415	812 736 671 614				
6 " 0 " 6 " 8 " 6 " 6 "	120 111	154 142 131 121	191 176 163 151	233 215 198 184	278 256 237 220	381 351 324 301	568 519 480 445				
7 " 0 "		113	140 122	171 149	204 178	280 243	414 860				
8 " 0 "			107	131 116	156 138	214 190	317 281				
9 " 0 "				108	128 111	169 152	250 225				
10 " 0 " 10 " 6 "					100	137 124	208 184				
11 " 0 "	Maj.					113 103	167 153				
12 " 0 "	da i a alu d	la suri alt	-f			95	141				

Above Safe Loads include weight of arch blocks and other dead load. Average weight of arch blocks (lbs. per sq. ft. of arch)=Sectional Area  $\times$  12  $\times$ .06. Below heavy lines, spans should be used for ceiling arches only.

# SAFE LOADS FOR TERRA COTTA SEGMENTAL FLOOR ARCHES.

As given by manufacturers of this material.

Weight of Arch Blocks not included.

Factor of Safety 7.

ARO	HES.	4 ins.	6 ins.	8 ins.	10 ins.					
			Square	Inches.						
ARE	AS,	28	36	43	47					
SPANS.	RISE.	Pounds per Square Foot.								
Ftins.	Inches.									
4-0	11/4 11/4 11/4 13/4 2	702 920 1155 1353 1545 1736	902 1148 1485 1740 1986 2288	1078 1414 1774 2079 2878 2667	1178 1545 1989 2272 2598 2915					
4-6	11/4 11/4 11/2 13/4	616 812 1020 1196 1381 1586	792 1044 1313 1539 1775 1975	946 1247 1568 1888 2121 2359	1084 1363 1713 2009 2318 2578					
5-0	3/4 11/4 11/2 13/4 2	551 744 911 1072 1238 1379	709 951 1172 1379 1592 1773	847 1143 1400 1647 1902 2118	926 1249 1530 1800 2078 2315					
5-6	3/4 11/4 11/4 11/4 13/4 2	499 672 826 984 1119 1258	641 864 1062 1266 1439 1619	766 1082 1269 1512 1719 1933	837 1128 1387 1652 1879 2113					
6-0	1 11/4 11/2 13/4 2	455 612 753 898 1022 1148	585 788 969 1154 1815 1476	699 941 1157 1379 1570 1763	764 1028 1265 1507 1716 1927					
6-6	1 11/4 11/2 13/4	428 562 701 828 947 1055	551 724 902 1058 1218 1358	658 864 1077 1264 1455 1622	719 944 1177 1382 1590 1772					
7-0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	520 648	508 669 884	606 799 996	662 878 1089					

# SAFE LOADS FOR TERRA COTTA SEGMENTAL FLOOR ARCHES.

As given by manufacturers of this material.

Weight of Arch Blocks not included.

Factor of Safety 7.

ARC	HES.	4 ins.	6 ins.	8 ins.	10 ins.						
			Square	Inches.							
ARI	EAS.	28	86	48	47						
SPANS.	RISH.	Pounds per Square Foot.									
Ptins.	Inches.	Founds per square root.									
7-0	1½ 1¾ 2	762 876 988	981 1127 1264	1171 1346 1510	1280 1471 1650						
7-6	1 1 1 1 1 1 2 1 8	866 482 602 715 815 915	471 621 774 920 1049 1176	568 741 925 1099 1253 1405	615 810 1011 1201 1369 1536						
8-0	1 1 1 1 1 1 1 2 2	341 457 562 668 767 854	439 588 724 859 987 1099	525 703 864 1026 1179 1812	578 768 944 1122 1288 1484						
8-6	1 1 1 1 1 1 1 2 1 3 2	819 428 527 626 719 807	411 551 678 806 926 1087	491 658 810 963 1106 1239	536 719 885 1052 1208 1354						
9-0	1 1 1 1 1 1 2 2	300 403 501 590 677 759	386 518 645 758 871 977	461 619 770 906 1041 1167	504 677 842 990 1137 1275						
9-6	34 1 11/4 11/2 13/4 2	283 380 472 561 639 717	364 489 608 721 828 923	485 584 726 862 983 1102	475 638 793 942 1074 1204						
10-0	34 1 114 114 134 2	267 359 447 581 610 683	844 462 576 683 784 879	411 552 688 816 987 1050	449 603 751 892 1024 1147						

#### TESTS OF FLOOR ARCHES.

A summary of the principal data and results of tests which were the subject of a paper entitled "Tests of Fire-proof Flooring Material," published in the Transactions of the American Society of Civil Engineers, Vols. xxxiv and xxxv, is given in the following table:

## BREAKING LOAD OF HOLLOW TILE ARCHES.

Depth				Total	Load	Total Hori-	Hori-	В	LOCKS.	Character	Manner
of Arch.	Rise.	Span.	Length.	Load.	per Sq. Foot.	zontal	Thrust per Ft.		Material.	of	of Laying
						Thrust.	of of	Style.	ate	Load.	Joints.
Ins.	Ins.	Ins.	Ins.	Lbs.	Lbs.	Lbs.	Arch.	20	×		
6.	3.5	60	48.	13750	688	29474	7369	E	Hard	Dis.	Port.
7.5	5.	46	11.5	9000	2452	10367	10818	66	66	u	N.M.
7.5	5.	60	35.2	11250		33750	11505	u	и	Cen.	Port.
7.5	5.	60	36.5	13000		39000	12822	"	Porous	"	"
8.	7.	60	38.25	14500		31071	9747	"	"	"	"
8.	7.	60	38.25	15750		33750	10588	EL.	Hard	"	"
12.	10.	60	41.	16400		24600	7200	24	"	"	"
12.	8.75	60	10.	3100		5314	6377	66	"	"	N.M.
12.	9.	60	10.	5000		8333	10000	KK	"	66	"
12.	9.	60	10.	15100	3630	12583	15100	EZ.	M	Dis.	"
12.	9.5	60	10.	2500		3947	4736	KK :	KK	Cen.	
8.	5.5	46	11.5	2500	681	2614	2727	S	"	Dis.	N.M.
8.	5.	45	11.5	1300	362	1463	1526	"	66	"	"
8.	6.	60	36.	10000		25000	8333	K	и	Cen.	Port.
8.	5.	60	36.	5700	380	8550	2850	X	124	Dis.	"
8.	5.	60	12.	3500	700	5250	5250	"	86	"	N.M.
8.	5.5	60	12.	10000	2000	13636	13636	XX.	"	"	"
8.	5.5	60	12.	2500		6818	6818	66	W.	Cen.	"
8.	5.5	60	24.	9950	995	13568	6784	74	a	Dis.	"
8.	5.5	60	24.	2500		6818	3209	"	ш	Cen.	и
10.	7.5	60	36.	13500	900	13500	4500	"	a	Dis.	Port.
10.	8.	60	37.	14500	940	13594	4408	"	u	"	

Note.—In the above table the following abbreviations are used: "E," End Construction; "S," Side Construction; "Hard," Hard Clay; "Porous," Porous Terra-Cotta; "Dis.," Distributed Load; "Cen.," Concentrated Load at Center; "Port.," Portland Cement, and "N. M.," No Mortar.

The Loads per Sq. Foot in the above table were obtained in all cases by dividing the Total Load by the superficial area of the arch in square feet. The Horizontal Thrust for Distributed and Central Loads was obtained

by formulæ similar to those given therefor on the following page, and for Central Loads this is double that for a Distributed Load of the same weight.

#### THRUST OF ARCHES.

The horizontal thrust of segmental floor arches, on the assumption of uniform loading, may be found by the following formula:

$$T = \frac{3WL^2}{2R}$$

in which

T = pressure or thrust in pounds per lineal foot of arch.

W = load on arch in pounds per square foot, uniformly distributed.

L = span of arch in feet.

R = rise of segmental arch in inches.

For a concentrated load at the center, of weight P, the thrust

$$T = \frac{3PL}{R}$$

For arches with flat tops and bottoms, such as are used in floors, the voussoir joints on each side of the central key are usually laid out on parallel lines, and in these cases the thrust may be determined approximately by using for R, in the above formula, the effective depth of the arch, which is somewhat less than the nominal depth, as indicated on page 77.

For segmental arches the rise R is the vertical distance from the highest part of the intrados to the plane of the springing line. If the radius of the intrados for segmental arches is r, the rise may be obtained from the following formula:

$$R=r-\sqrt{r^2-\frac{L^2}{4}}$$
 conversely, 
$$r=\frac{R}{2}+\frac{L^2}{8R}$$

## TIE RODS.

Although in the completed structure the horizontal thrusts of adjoining arches may counterbalance each other, the tie rods should be so proportioned and spaced as to withstand the entire thrust of the arches, thus tying the structure together and facilitating the construction.

#### SPACING OF TIE RODS FOR TILE ARCHES.

The table on the next page was computed from the following formula, which was obtained from that giving the thrust of arches on page 75.

$$B = \frac{A \times R \times 10000}{WL^2}$$

in which

B = spacing of tie rods in feet.

A = net area of rod in square inches.

R = rise of arch in inches.

W = load in pounds per square foot of the arch.

L = span of arch in feet.

The above formula gives the spacing of tie rods corresponding to a tensile stress in the rods of 15 000 pounds per square inch, without considering the flexure of the beams.

In spacing tie rods, the lateral strength of beams, for flexure due to the thrust of the arches, should be taken into consideration, explanations for which are given on pages 78 to 81 inclusive.

Spacings for other loads than that of the table may be found by proportion, thus:

Required spacing =

 $\frac{100 + \text{weight of arch in pounds per square foot}}{\text{New load in lbs. per sq. ft.} + \text{weight of arch in lbs. per sq. ft.}} \times \text{spacing from table.}$ 

Weights of tile arches per square foot are given on page 69.

As noted under the heading "Lateral Strength of Beams," on pages 82 and 83, care should be taken that the spacing of tie rods is not greater than twenty times the least flange width, otherwise the safe loads should be reduced to compensate for the strains produced by flexure of the upper flange considered as a column in compression.

# SPACING OF TIE RODS FOR TILE ARCHES IN FEET.

For a uniform load of 100 lbs. per square foot in addition to the weight of the arch.

			Nominal Depth of Arch. Inches.								
Span of Arch.	Diameter of Tie Rods.	6	7	8	9	10	12				
			Effecti		h or Ris	e of Arc	h.				
Feet.	Inch.	3.6	4.6	5.6	6.6	7.6	9.6				
. 3	() () () () () () () () () () () () () (	6.4 9.5 13.2	8.0 12.0 16.6	9.5 14.2 19.8	10.9 16.3 22.6	12.3 18.3 25.5	15.0 22.4 31.1				
4 "	00-19-100 00-01	3.6 5.4 7.4	4.5 6.7 9.4	5.4 8.0 11.1	6.1 9.2 12.7	6.9 10.3 14.3	8.4 12.6 17.5				
5 "	col-2 p-(co colcs	2.3 3.4 4.8	2.9 4.3 6.0	3.4 5.1 7.1	3.9 5.9 8.1	4.4 6.6 9.2	5.4 8.0 11.2				
6 u	usion original residence		2.0 3.0 4.2	2.4 3.6 4.9	2.7 4.1 5.7	3.1 4.6 6.4	3.7 5.6 7.8				
7 u u	s)@@ #7 @				2.0 3.0 4.2	2.3 3.4 4.7	2.8 4.1 5.7				
8 "	5)003)417-80				••	1.7 2.6 3.6	2.1 3.1 4.4				

Spacings below heavy lines apply to greater spans than are recommended for that depth of arch.

# LATERAL STRENGTH OF BEAMS TO RESIST FLEXURE DUE TO THRUST OF ARCHES, ETC.

In special cases where the thrust of a floor arch is exerted against a beam, channel, angle or other shape without other lateral support than the tie rods, or braces, this will produce lateral flexure and stresses in addition to those caused by the vertical loading. Throughout the body of the floor the thrusts of the adjoining arches, when completed, will usually counterbalance each other, but in the outer beams around shafts or elsewhere, if unsupported sideways, the stresses due to the lateral forces should be considered.

The total allowable stress per square inch for the extreme fibres of beams has been placed at 16 000 pounds per square inch, and in order that this may not be exceeded owing to lateral stresses, the stress due to vertical loading should be correspondingly reduced so that the resultant intensity shall not exceed the allowable limit. This may be calculated by considering the beam as continuous and laterally supported at intervals by the tie rods, the spans being equal to the spacing of the rods.

In this case the fibre stress due to the lateral forces is:

$$p' = \frac{wx_1B^2}{I'} \qquad (1)$$

in which

p' = fibre stress in pounds per square inch due to lateral forces.

w = lateral load or thrust in pounds per lineal foot of section used

 $x_1$  = distance of the extreme fibre from the neutral axis in inches.

B = distance between tie rods or lateral supports in feet.

I' = moment of inertia about the vertical axis of the section or that one at right angles to the line of application of the lateral forces.

For I-Beams with the web placed vertically, as usual,  $x_1$  becomes equal to  $\frac{b}{2}$ , where b is the width of the flange in inches.

In this case the above formula for intensity of unit stress due to lateral load becomes:

$$p' = \frac{wbB^2}{2 I'}$$
 (2)

In order that the total resultant intensity of unit stress shall not exceed the allowable limit of 16 000 pounds per square inch, the stress due to vertical loading must be reduced by the amount of the intensity of stress due to the horizontal thrust of the arch, as determined by formula (2).

If p' represents the intensity of unit stress due to the horizontal thrust of the arch, and p the corresponding allowable intensity of unit stress due to the vertical loading, then

$$p = 16000 - p'$$

Having thus obtained the reduced vertical stress p, the safe vertical load of the tables corresponding to this stress should ac-

cordingly be reduced by multiplying it by the ratio  $\frac{p}{16000}$  and

similarly for other stresses and corresponding loads, thus making proper allowance for the additional stresses produced by the lateral forces.

If the reduction of the safe loads on this account is a considerable proportion of the original amount due to vertical loading only, it would be more economical to provide lateral braces or tie rods at shorter intervals, thus avoiding the use of an excessive amount of material in the beam.

As the stresses due to vertical forces for usual cases of loading are a maximum at the center of the span it will ordinarily be sufficient to space the tie rods or braces at shorter intervals near the center in order to allow for the combined stresses due to vertical loading and horizontal thrusts.

The above method of calculation is not exact when considering the lateral thrust of arches, or loads from similar materials which do not exert a uniform pressure throughout their surfaces of contact with the sustaining beam on account of the friction and bond of their component parts, but this analysis of the stresses may serve as a guide in designing.

The above formulæ should be used in connection with the tables and formula given on pages 82 and 83 relating to the lateral strength of beams, due to compression of the upper flange figured as a column between points of lateral support.

\* This method of treatment gives approximate results which are on the side of safety.

The correct determination can be secured by the use of the section modulus polygon. (See Transactions of the American Society of Civil Engineers, Vol. LVI, 1906, page 169, et seq.)

#### EXAMPLE.

What is the proper size of I-Beam without other lateral support than the usual tie rods, corresponding to a total fibre stress of 16 000 pounds per square inch under the following conditions? The beam is 18 feet between end supports and carries a tile arch on one side having a nominal depth of 9 inches, effective depth of 6.6 inches, a span of 5 feet, designed to carry a superimposed load of 75 pounds per square foot in addition to the weight of the arch and other floor materials. The hollow tile arch weighs 36 pounds per square foot and the other materials, including plastering, weigh 14 pounds, making a total load, exclusive of the weight of the beam, equal to 125 pounds per square foot.

For tie rods of  $\frac{3}{4}$ " diameter the spacing between them would be 5.9 feet, as shown by the table of Spacing of Tie Rods on page 77 in which the safe stresses in the rods only are considered.

Substituting the proper values in the formula for lateral thrust of arches, given on page 75, this will be

$$T = \frac{3 \times 125 \times 5^2}{2 \times 6.6} = 710$$
 lbs. per lineal foot.

Substituting this value for w in formula (2) page 78 and assuming a 10" beam 25 lbs. per foot, the moment of inertia of which is 6.89, as given in the Tables of Properties of I-Beams, page 182, we have

$$p' = \frac{710 \times 4.66 \times 5.9^2}{2 \times 6.89} = 8358$$
 lbs. per sq. in.

Therefore  $p = 16\,000 - 8\,358 = 7\,642$  lbs. per sq. in.

Hence the safe load as determined by the consideration of

vertical loads only, should be reduced to  $\frac{7642}{16000}$ , or approximately

.48 of the amount given by the Tables of Safe Loads in case the spacing of the tie rods is not changed.

The safe vertical load for a 10" beam, weighing 25 lbs. per foot, 18 feet long between supports, for fibre stress of 16 000 lbs. per square inch, is 14 470 lbs. uniformly distributed, including the weight of the beam as given in the Tables of Safe Loads, on page 109, or 14 020 exclusive of the weight of the beam, and .48 of this is 6 730 lbs., which is the vertical load it can safely carry in order that the total stress due to it and the lateral thrust shall not exceed 16 000 lbs. per square inch.

The actual vertical load on the beam under consideration is as follows:

$$\frac{5}{2} \times 18 \times 125 = 5625$$
 lbs.,

which is less than the allowable amount, 6 730 lbs., as figured above, so that a smaller beam may suffice.

Therefore, assume a 9-inch beam, weighing 21 lbs. per foot, the moment of inertia of which about an axis coincident with center line of web is found in the Table of Properties, on p. 182, to be 5.16.

In this case

$$p' = \frac{710 \times 4.33 \times 5.9^2}{2 \times 5.16} = 10370$$
 lbs. per sq. in.

Substituting this in the formula for p we have

$$p = 16000 - 10370 = 5630$$
 lbs. per sq. in.

Therefore the safe vertical load will be  $\frac{5630}{16000}$ , or approximately .35 of the tabular safe load.

The safe vertical load for a 9" 21 lb. beam, 18 feet long, for a fibre stress of 16 000 lbs. per square inch is 11 180 lbs., as given in the Table of Safe Loads, on page 109, and .35 of this, after deducting weight of the beam, is 3 781 lbs., which is less than the actual amount, 5 625 lbs., as calculated above, so that the 9" 21 lb. beam will not suffice.

If the spacing of the tie rods at the center be reduced from 5.9 feet to 3.25 feet, it may be found, in a manner similar to that used in the above calculations, that the safe vertical load for an 8" I-Beam, weighing 18.0 lbs. per foot, is reduced to .74 of its tabular value of 8 430 lbs., or 6 328 lbs., and as this amount is greater than the actual load as above, namely, 5 625 lbs., the 8" beam would answer the purpose, under the changed conditions as to spacing of tie rods. As this beam might deflect beyond the limit for plastered ceilings, it should be examined in accordance with the rule or formula given for obtaining safe deflections in the explanation of the Tables of Safe Loads, and elsewhere herein.

Calculating this by the rule given on page 102, the safe load for the allowable limit of deflection is

$$W = \frac{9480 \times 16^2}{18^2} = 7491 \text{ lbs.,}$$

which is greater than the actual amount, 5 625 lbs., so that the 8" beam is sufficient and proper if the spacing of central tie rods be changed to 3.25 feet, as assumed in the last case.

# LATERAL STRENGTH OF BEAMS, WITHOUT LATERAL SUPPORT

The Tables of Safe Loads for Cambria I-Beams and Channels and Tables of Spacing of Cambria I-Beams, on pages 106 to 135, are calculated on the assumption that proper provision is made for preventing lateral deflection by means of tie rods or other braces. In order to prevent undue strains in the compression flange, considered as a column, the beams should be supported laterally at distances not exceeding twenty times the flange width, this ratio being determined by the following formula, which gives the safe load for solid columns of soft steel:

$$p = \frac{18000}{1 + \frac{l^2}{3000b^2}}$$

in which

p = allowable stress in pounds per square inch.

1 = length between lateral supports in inches.

b = width of flange in inches.

Substituting 16 000 for p in the above formula, which is the allowable unit stress of the safe load tables, it is found that the ratio  $\frac{1}{b}=19.37$ , from which it may be seen that the compression flange should be supported laterally at distances not exceeding twenty times the flange width as stated above.

Beams which are not thus supported laterally should not be loaded to their full transverse capacity. The allowable fibre stresses and proportions of their full loads which they can safely carry when laterally supported at various distances is given in the following table:

## REDUCTION IN VALUES OF ALLOWABLE FIBRE STRESS AND SAFE LOADS FOR SHAPES USED AS BEAMS DUE TO LATERAL FLEXURE.

Ratio of Span or Distance between Lateral Supports to Flange Width.	Allowable Unit Stress for Direct Flexure in Extreme Fibre.	Proportion of Tabular Safe Load	Ratio of Span or Distance between Lateral Supports to Flange Width.	Allowable Unit Stress for Direct Flexure in Extreme Fibre.	Proportion of Tabular Safe Load
1 b	р	to be Used.	1 6	р	to be Used.
19.37 20 25 30 35	16000 15882 14897 13846 12781	1.0 .99 .93 .87	65 70 75 80 85	7474 6835 6261 5745 5281	.47 .43 .39 .36
40 45 50 55 60	11739 10746 9818 8963 8182	.73 .67 .61 .56 .51	90 95 100 105 110	4865 4491 4154 3850 3576	.30 .28 .26 .24 .22

The above table should be used in connection with the Tables of Safe Loads Uniformly Distributed for Cambria I-Beams and Channels, on pages 106 to 123 inclusive, and limits the values found therein under the conditions given above.

#### EXAMPLE.

Required the safe load for a 15-inch standard I-Beam weighing 42 pounds per foot for a span of 30 feet without lateral supports:

From the data the ratio 
$$\frac{1}{b} = \frac{30 \times 12}{5.5} = 65$$
.

From the above table the proportion of the safe load which the beam can safely support under these conditions is .47. From the Table of Safe Loads for I-Beams, page 111, the safe load for this beam when properly supported laterally is 20 940 pounds, which multiplied by .47 gives 9 842 pounds as the safe load uniformly distributed under the conditions given, including the weight of the beam, or 8 582 pounds superimposed load.

# APPROXIMATE WEIGHTS OF VARIOUS ROOF COVERINGS.

In Pounds per Square Foot.

Copper Sheeting, B. W. G. No. 22
Corrugated Iron, B. W. G. Nos. 26 to 16 1-31/4
Felt, two Layers
Felt, two Layers. Felt and Asphalt.
Felt and Gravel, % inch thick
Galvanized Iron, B. W. G. Nos. 26 to 16.
Lath and Plaster Ceiling, Ordinary
Sheathing, 1 inch thick, Hemlock
" " Yellow Pine
Shingles, 16 inch, laid 5½ inch to weather
Skylight Glass, $\frac{1}{16}$ to $\frac{1}{2}$ inch thick
Slates, 1/8 to 18 inch thick, 3 inch double lap 4-7
Slag Roofing, 4-ply, with cement and sand
Steel Sheeting (See next page)
Tiles (See Page 69)
Tin
Tin. %-1 Zinc, B. W. G. No. 20. 1½
Zinc, B. W. G. No. 20
Zinc, B. W. G. No. 20. 1½  APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:
Zinc, B. W. G. No. 20. 1½  APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:
Zinc, B. W. G. No. 20. 1½  APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:  Corrugated Sheets. 8-10
Zinc, B. W. G. No. 20. 1½  APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:  Corrugated Sheets. 8–10 Shingle. 6–10
Zinc, B. W. G. No. 20. 11/2  APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:  Corrugated Sheets. 8-10 Shingle. 6-10 Slate 12-15
Zinc, B. W. G. No. 20       1½         APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:       8-10         Corrugated Sheets       8-10         Shingle       6-10         Slate       12-15         Tar and Gravel       10-12
Zinc, B. W. G. No. 20. 1½  APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:  Corrugated Sheets 8-10 Shingle 6-10 Slate 12-15 Tar and Gravel 10-12 Tin 6-8
Zinc, B. W. G. No. 20       1½         APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:       8-10         Corrugated Sheets       8-10         Shingle       6-10         Slate       12-15         Tar and Gravel       10-12         Tin       6-8         Tile       20-30
Zinc, B. W. G. No. 20. 1½  APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:  Corrugated Sheets 8-10 Shingle 6-10 Slate 12-15 Tar and Gravel 10-12 Tin 6-8
Zinc, B. W. G. No. 20. 1½  APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:  Corrugated Sheets. 8-10 Shingle. 6-10 Slate. 12-15 Tar and Gravel. 10-12 Tin. 6-8 Tile. 20-30 If roof is plastered underneath, add to values given above. 6
Zinc, B. W. G. No. 20       1½         APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:       8-10         Corrugated Sheets       8-10         Shingle       6-10         Slate       12-15         Tar and Gravel       10-12         Tin       6-8         Tile       20-30
Zinc, B. W. G. No. 20.       1½         APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:       8-10         Corrugated Sheets       8-10         Shingle       6-10         Slate       12-15         Tar and Gravel       10-12         Tin       6-8         Tile       20-30         If roof is plastered underneath, add to values given above       6         Weight of Roof Truss with span of 75 feet or less       5
Zinc, B. W. G. No. 20.       1½         APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:       8-10         Corrugated Sheets.       8-10         Shingle.       6-10         Slate.       12-15         Tar and Gravel.       10-12         Tin.       6-8         Tile.       20-30         If roof is plastered underneath, add to values given above.       6         Weight of Roof Truss with span of 75 feet or less.       5         Snow Load—25 lbs. per horizontal square foot of roof for all slopes
Zinc, B. W. G. No. 20.       1½         APPROXIMATE WEIGHT OF ROOFS INCLUDING FRAMING:       8-10         Corrugated Sheets       8-10         Shingle       6-10         Slate       12-15         Tar and Gravel       10-12         Tin       6-8         Tile       20-30         If roof is plastered underneath, add to values given above       6         Weight of Roof Truss with span of 75 feet or less       5

## WIND PRESSURE ON ROOFS.

Based on 20 Lbs. per Sq. Ft. on a Vertical Plane.

 $1.84 \cos a - 1.$ 

FORMULA.—Normal Pressure per sq. ft. = P sin a

Pitch	Angle of Slope (a) with Horizontal.	Rise of Roof per Foot.	Normal Wind Pressure
Roof	Degrees. Minutes.	Inches.	Pounds per Sq. Ft.
1 6 1	18 - 25 26 - 33	4	8.4 11.9
1 1 1	33 - 41 $45 - 0$	8	14.6 18.1
22433374	53 - 7 56 - 20	16 18	19.4 19.7
ī	63 - 27	24	20.0

#### STEEL SHEETING.

Weights given (U. S. Standard) are based on 480 lbs, per cu. ft.

Gange	Thickness		Weight—Ll	Spacing of Supports			
Number Thickness		Flat		Corrug	gated	Roof	Sides
U. S. Std.	Inch	Black	Galvanized	BlackPainted	Galvanized	Not Over Ft.—Ins.	Not Over Ft.—Ins.
16 28 20 22	.0625 .05 .0375	2.50 2.00 1.50	2.66 2.16 1.66	2.75 2.20 1.65	2.81 2.36 1.82	5-9	7 - 8
22 24 26	.03125 .025 .01875	1.25 1.00 .75	1.41 1.16 .91	1.38 1.11 .84	1.54 1.27 .99	$\begin{array}{c} 4 - 9 \\ 3 - 9 \\ 2 - 9 \end{array}$	6 - 8 5 - 8 3 - 10
28	.015625	.63	.79	.69	.86	2 - 8	

Standard Flat and Corrugated Sheets furnished in lengths 48, 60, 72, 84, 96, 108 and 120 inches.

Standard Flat Sheets in widths 24, 26, 28, 30 and 32 inches.

Standard Corrugated Sheets in widths as follows:

For	Width of Sheet Flat	f Sheet of Sheet Corrugation Corrugation Ins. Ins. Ins. Ins. Ins.  30 27½ 2½ 5%	Depth of Corrugation	Corrugation in	Edges Laid			
	Ins.	Ins.	Ins.	Ins.	Lap	Up	Down	
Roofing Roofing Siding	28		21/2	5/8 u	1½ 2 1	1	1 2 2	

Sheets should preferably be ordered in even ft. lengths to span 2 purlin spaces.

End Lap:

6 inches for Roofing, roof pitch 6 inches.

8 inches for Roofing, roof pitch 4 inches.

8 inches for Roofing, roof pitch less than 4 inches, when laid with slater's cement.

4 inches for Roofs in snowless climates and for Siding.

Ridge Roll:-No. 24 Gauge; 96-inch lengths; 3-inch end lap, standard diameter 2½ inches; apron 6 inches. Flashing:—No. 24 Gauge; 30-inch lengths; 3-inch end lap.

Corner Capping: -48-inch lengths: 4-inch end lap.

#### FASTENINGS.

Straps:—No. 18 U. S. Gauge Steel 3/-inch wide; 1 strap and 2 rivets or bolts for each lineal foot of purlin or girts; 1 bundle (400 lin. ft.) straps weighs 50 pounds; 1000 rivets weigh 6 pounds.

Clinch Rivets:-Should clinch at least 1 inch; 2 rivets to each lineal foot of

purlin or girt. Purlin leg 2 inches; 2½ to 3 inches: 3½ inches; 4 to 4½ inches. Length 4 inches: 5 inches: 6 inches; 7 inches. Number per pound 48 38 33

Clips and Bolts:-For fastening sheeting to purlins other than angle purlins when asbestos lining is used under sheeting. No. 16 steel slightly crimped. 2 clips and 2 bolts for each lineal foot of purlin or girt; 500 clips in one box. Hole for bolt  $\frac{2}{16}$ " x 1". Closing Rivets:  $\frac{2}{16}$ -inch diameter;  $\frac{2}{16}$ ,  $\frac{1}{16}$  and  $\frac{2}{16}$ -inch lengths;  $\frac{1}{1600}$  = 6 lbs.

For side laps, 1 rivet for each lineal foot. For fastening flashing, etc., to

sheeting, 2 for each lineal foot.

Nails:-For fastening sheeting to wooden purlins: 10d. clinch nails for roofing. one for each lineal foot (for both end and side laps), 50=1 pound. 8d. clinch nails for siding, one for each lineal foot (for both end and side laps), 70 = 1 pound. For sheeting on wooden sheathing in end laps and in the body of the sheets in rows about 3 or 4 feet apart, same as if purlins or girts occurred at these lines. For fastening flashing, etc., to wood use tinner's nails, 2 per foot. For fastening flashing, etc., to brick wall use 8d. nails, 2 per foot.

(PRATT.)



 $n=S+H=2 \cot \alpha$ **P**=Panel Load.



Heavy lines in diagrams indicate Compression Members.

#### I-4 Panels.

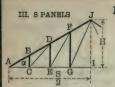
	Length	Stress=P	n =								
Member		X	3	24 7	2 cot 30°	4	24 5	5	6		
AB, BD AC CE BC CD	S sec $\alpha \div 4$ S ÷ 4 S ÷ 2 H ÷ 2 $\sqrt{S^2 + 16 H^2} \div 4$	3/4 n 1/2 n 1	2.70 2.25 1.50 1.00 1.25	2.57 1.71 1.00	2.60 1.73 1.00	3.00 2.00 1.00	3.60 2.40	3.75 2.50 1.00	4.50 3.00 1.00		

## II-6 Panels.

	Length	Stress = P	n =								
Member		II.	3	24 7	2 cot 30°	4	24 5	5	8		
AB, BD	S sec $\alpha \div 6$	$5/4\sqrt{n^2+4}$	4.51	1.96	5.00	5.59	6.50	6.73	7.91		
DF	S sec $\alpha \div 6$	$\sqrt{n^2+4}$	3.61	3.97	4.00	4.47	5.20	5.39	6.32		
AC	S ÷ 6	5/4 n	3.75	4.29	4.33	5.00	6.00	6.25	7.50		
CE	S ÷ 6	n	3.00	3.43	3.46	4.00	4.80	5.00	6.00		
EG .	S ÷ 3	3/4 n	2.25	2.57	2.60	3.00	3.60	3.75	4.50		
BC	H ÷ 3	1	1.00	1.00	1.00	1.00	1.00	1.00	1.00		
DE	2H ÷ 3	3/2	1.50	1.50	1.50	1.50	1.50	1.50	1.50		
CD	$\sqrt{S^2 + 16 H^2 \div 6}$		1.25	1.32	1.32	1.41	1.56	1.60	1.80		
EF	$\sqrt{S^2 + 36 H^2} \div 6$	$\sqrt{1/4} \sqrt{n^2 + 36}$	1.68	1.73	1.73	1.80	1.92	1.95	2.12		

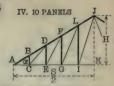
## COEFFICIENTS FOR CALCULATING TRUSS MEMBERS.

n	3	24	2cot 30°	4	24	5	6
ot	33°41.4	30°15.4′	30°	26°33.9′	22°37.2′	21°48.1′	18°26.1′
Sec α	1.2018	1.1577	1.1547	1.1180	1.0833	1.0770	1.0541
Sec² α	1.4444	1.3403	1.3333	1.2500	1.1736	1.1600	1.1111
Sec \alpha tan \alpha	.8012	.6753	.6667	.5590	.4514	.4308	.3514
Sec $\alpha\sqrt{9}\sec^2\alpha-8$	2.6874	2.3334	2.3094	2.0156	1.7342	1.6824	1.4907



 $n=S \div H=2 \cot \alpha$ . **P**=Panel Load.

Heavy lines in diagrams indicate compression members.



#### III-8 Panels.

			TO MID !							
		Stress = P	n =							
Member	Length	X	3	7	2 cot 30°	4	24 5	5	6	
AB, BD	S sec α÷8	$7/4\sqrt{n^2+4}$	6.31	6.95	7.00	7.83	9.10	9.40	11.07	
DF	S sec α÷8	$3/2 \sqrt{n^2 + 4}$	5.41	5.95	6.00	6.71	7.80	8.08	9.49	
FJ	S sec $\alpha \div 8$	$5/4\sqrt{n^2+4}$	4.51	4.96	5.00	5.59	6.50	6.73	7.91	
AC	S÷8	7/4 n	5.25	6.00	6.06	7.00	8.40	8.75	10.50	
CE	S÷8	3/2 n	4.50	5.14	5.20	6.00	7.20	7.50	9.00	
EG	S÷8	5/4 n	3.75	4.29	4.33	5.00	6.00	6.25	7.50	
GI	S÷4	IX	3.00	3.43	3.46	4.00	4.80	5.00	6.00	
BC	H÷4	1	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
DE	H÷2	3/2	1.50	1.50	1.50	1.50	1.50	1.50	1.50	
FG	3H+4	2	2.00	2.00	2.00	2.00	2.00	2.00	2.00	
CD	$\sqrt{S^2 + 16 H^2 \div 8}$	$\frac{1}{4}\sqrt{n^2+16}$	1.25	1.32	1.32	1.41	1.56	1.60	1.80	
EF	$\sqrt{S^2 + 36 H^2 \div 8}$	1/4 V n2 + 36	1.68	1.73	1.73	1.80	1.92	1.95	2.12	
GJ	$\sqrt{S^2 + 64  H^2 \div 8}$	$\frac{1}{4}\sqrt{n^2+64}$	2.14	2.18	2.18	2.24	2.33	2.36	2.50	

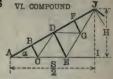
## IV-10 Panels.

		Stress = P				n =			
Member	Length	X X	3	7	2 cot 30°	4	<u>24</u> <u>5</u>	ã	6
AB, BD	S sec $\alpha \div 10$	$9/4\sqrt{n^2+4}$	8.11	8.93	9.00	10.06	11.70	12.12	14.23
DF	S sec α÷10	$2 \sqrt{n^3 + 4}$	7.21	7.94	8.00	8.94	10.40	10.77	12.65
FL	S sec $\alpha \div 10$	$7/4 \sqrt{n^2 + 4}$	6.31	6.95	7.00	7.83	9.10	9.42	11.07
LJ	S sec α÷10	$3/2 \sqrt{n^3 + 4}$	5.41	5.95	6.00	6.71	7.80	8.08	9.49
AC	S÷10	9/4 n	6.75	7.71	7.79	9.00	10.80	11.25	13.50
CE	S+10	2 n	6.00	6.86	6.93	8.00	9.60	10.00	12.00
EG	S÷10	7/4 n	5.25	6.00	6.06	7.00	8.40	8.75	10.50
GI	S÷10	3/2 n	4.50	5.14	5.20	6.00	7.20	7.50	9.00
IK	S ÷ 5	5/4 n	3.75	4.29	4.33	5.00	6.00	6.25	7.50
BC	H÷5	1	1.00	1.00	1.00	1.00	1.00	1.00	1.00
DE	2H÷5	3/2	1.50	1.50	1.50	1.50	1.50	1.50	1.50
FG	3H÷5	2	2.00	2.00	2.00	2.00	2.00	2.00	2.00
LI		5/2	2.50	2.50	2.50	2.50	2.50	2.50	2.50
CD	$\sqrt{S^2+16 H^2+10}$	$\frac{1}{4}\sqrt{n^2+16}$	1.25	1.32	1.32	1.41	1.56	1.60	1.80
EF	$\sqrt{S^2+36 H^2+10}$		1.68	1.73	1.73	1.80	1.92	1.95	2.12
GL	$\sqrt{S^2+64 H^2+10}$		2.14		2.18	2.24	2.33	2.36	2.50
IJ	√S²+100H³÷10	$\sqrt[1/4]{\sqrt{n^2+100}}$	2.61	2.64	2.65	2.69	2.77	2.80	2.92



 $n=S \div H = 2 \cot \alpha$ P=Panel Load.

Heavy lines in diagrams indicate compression members.

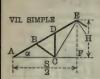


V-Simple.

	Length	Stress = P	n=							
Member		X	3	7	2 cot 30	4	24 5	5	6	
AB	S sec $\alpha \div 4$	$\sqrt[3]{\sqrt{n^2+4}}$	2.70	2.98	3.00	3.35	3.90	4.04	4.74	
BD	S sec a + 4	$\frac{3 \text{ n}^2 + 4}{4 \sqrt{n^2 + 4}}$	2.15	2.47	2.50	2.91	3.52	3.67	4.43	
AC	S sec3 a + 4	3/4 n	2.25	2.57	2.60	3.00	3.60	3.75	4.50	
CE	S (1 — ½ sec² α)	1/2 n	1.50	1.71	1.73	2.00	2.40	2.50	3.00	
BC	$S \sec \alpha \tan \alpha \div 4$	$\frac{n}{\sqrt{n^2+4}}$	0.83	0.86	0.87	0.89	0.92	0.93	0.95	
CD	S $\sec^2 \alpha \div 4$	1/4 n	0.75	0.86	0.87	1.00	1.20	1.25	1.50	

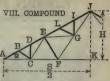
## VI-Compound.

		Stress = P	n =						
Member	Length	X X	3	7	2 cot 30°	4	24 5	5	6
AB	S sec $\alpha \div 8$	$7/4\sqrt{n^2+4}$	6.31	6.95	7.00	7.83	9.10	9.42	11.07
BD	S sec α + 8	$\frac{7 n^{2} + 20}{4 \sqrt{n^{2} + 4}}$	5.76	6.44	6.50	7.38	8.72	9.05	10.75
DF	S sec a + 8	$\frac{7 \text{ n}^2 + 12}{4 \sqrt{\text{n}^2 + 4}}$	5.20	5.94	6.00	6.93	8.33	8.68	10.44
FJ	S sec a + 8	$\frac{7  n^2 + 4}{4 \sqrt{n^2 + 4}}$	4.65	5.43	5.50	6.48	7.95	8.31	10.12
AC	S sec² a + 8	7/4 n	5.25	6.00	6.06	7.00	8.40	8.75	10.50
CE	S sec2 a + 8	3/2 n	1 1	_	5.20		_	_	
EI	$S(1-\frac{1}{4}\sec^2\alpha)$	n		_	3.46		_	_	
BC, FG		$\frac{\pi}{\sqrt{n^2+4}}$	0.83	0.86	0.87	0.89	0.92	0.93	0.95
DE	S $\sec \alpha \tan \alpha \div 4$	$\frac{2 n}{\sqrt{n^2 + 4}}$	1.66	1.73	1.73	1.79	1.85	1.86	1.90
CD, DG	S sec <sup>2</sup> $\alpha \div 8$	1/4 n	0.75	0.86	0.87	1.00	1.20	1.25	1.50
EG	S sec² a ÷ 8	1/2 n	1.50	1.71	1.73	2.00	2.40	2.50	3.00
GJ	S sec <sup>2</sup> \( \alpha \div 8 \)	34 n	2.25	2.57	2.60	3.00	3.60	3.75	4.50



 $n=S+H=2 \cot \alpha$ . **P**=Panel Load.

Heavy lines in diagrams indicate compression members.



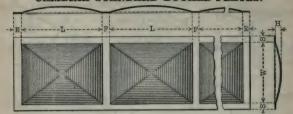
## VII—Simple.

		C4 D	n =						
Member	Length	Stress=P	3	7	2 cot 30°	4	24 5	5	6
AB	S sec α÷6	$5/4\sqrt{n^2+4}$	4.51	4.96	5.00	5.59	6.50	6.73	7.91
BD	S sec $\alpha \div 6$	$\frac{13 (n^2 + 36)}{12 \sqrt{n^3 + 4}}$	3.54	3.96	4.00	4.55	5.38	5.59	6.64
DE	S sec $\alpha \div 6$	$\frac{5 n^2 + 4}{4 \sqrt{n^2 + 4}}$	3.40	3.95	4.00	4.70	5.73	5.99	7.27
AC		5/4 n		4.29				6.25	
CF	$S(1-\frac{1}{2}\sec^2\alpha)$		2.25					3.75	
	Ssec a V9 sec2 a -8				1.00				
CE	Ssec <sup>2</sup> $\alpha \div 4$ [ $\div$ 12	$\frac{1}{2}$ n $[6\sqrt{n^2+4}]$	1.50	1.71	1.73	2.00	2.40	2.50	3.00

## VIII-Compound.

		Stress=P n =							
Member	Length	Length x 3		7	2 cot 30°	4	24 5	5	6
AB	S sec $\alpha \div 12$	$11/4\sqrt{n^2+4}$	9.92	10.92	11.00	12.30	14.30	14.81	17.39
BD	S sec $\alpha \div 12$	$\frac{31 \text{ n}^3 + 108}{12 \sqrt{n^2 + 4}}$	8.95	9.92	10.00	11.26	13.18	13.66	16.13
DE	S sec $\alpha \div 12$	$\frac{11 \text{ n}^2 + 28}{4 \sqrt{n^2 + 4}}$	8.81	9.91	10.00	11.40	13.53	14.07	16.76
EL	S sec a+12	$\frac{11  n^2 + 20}{4  \sqrt{n^2 + 4}}$	8.25	9.40	9.50	10.96	13.15	13.70	16.44
LI	S sec α+12	$\frac{31  n^2 + 36}{12  \sqrt{n^2 + 4}}$	7.28	8.41	8.50	9.91	12.02	12.55	15.18
IJ	S sec α ÷ 12	$\frac{11  n^2 + 4}{4 \sqrt{n^2 + 4}}$	7.14	8.40	8.50	10.06	12.38	12.95	15.81
AC CF FK	S $\sec^2 \alpha \div 8$ S $\sec^2 \alpha \div 8$ S $(1 - \frac{1}{2} \sec^2 \alpha)$	11/4 n 9/4 n 3/2 n	8.25 6.75 4.50	7.71	7.79	9.00	10.80	13.75 11.25 7.50	13.50
BC,CD) GL, GI)	S sec $\alpha \sqrt{9 \sec^2 \alpha - 8}$ [ $\div 24$	$n\sqrt{\frac{n^2+36}{n^2+4}}$	0.93	1.00	1.00	1.08	1.18	1.21	1.34
EF	S sec α tan α+4	$\frac{3 \text{ n}}{\sqrt{\overline{n^2 + 4}}}$	2.50	2.59	2.60	2.68	2.77	2.79	2.85
CE, EG FG GJ	S sec² a ÷ 8	1/2 n 3/4 n 5/4 n	2.25	1.71 2.57 4.29		3.00	2.40 3.60 6.00	3.75	4.50

#### CAMBRIA STANDARD BUCKLE PLATES.



No.		Side (W).	RISE OF BUCKLE (H).	PLATE THICKNESS. Ins.	NUMBER OF BUCKLES PER PLATE.	
1 2 3 4 5 0 7 8 9 10 11 12	2-8 2-8 3-8 3-1 3-2 3-1 3-9 4-0 4-6 3-11	2-8 3-8 2-8 3-2 3-1 3-9 3-1 4-0 3-11 4-6 5-6 3-6	2 2 2 3 5 5 5 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	1/4, 5 OT 3/8	1 to 10 1 a 10 1 a 8 1 a 9 1 a 9 1 a 8 1 a 7 1 a 6 1 a 7 1 a 8	fr wgl pl

#### WIDTH OF FLANGES AND FILLETS.

END FLANGES (E)
Preferably made alike,
from 2 to 18 ins. wide. If
wider than 18 ins., use angles riveted across the
plates for stiffeners.
SIDE FLANGES (S)

Preferably made alike, from 2 to 6 ins. wide. Best not to exceed 4 ins.

FILLETS (F)
From 2 to 6 ins. wide.
Best not to exceed 4 ins.

# ROLLED STEEL SAFETY FLOOR PLATES.



WIDTH (W).	THICKNESS (T).	MAXIMUM LENGTH.
Inches.	Inches.	Feet.
18 to 25 25 " 36	\$ to \$\frac{3}{4}\$ \\ \frac{5}{16} \times \frac{4}{1/2}\$	50 50

#### FIREPROOFING-REINFORCED CONCRETE.

The actual fire tests of reinforced concrete have been limited. but experience, together with the results of tests so far made, indicates that concrete may be safely used for fireproofing purposes. It is in itself incombustible and proof against ordinary fire when composed of the best materials properly mixed, applied and anchored in place. For a fireproof filling or deadening layer in floors, these same materials without reinforcement may be used or clean hard burned cinders may be substituted for this purpose. The low rate of heat conductivity is one reason of its value for fireproofing and the concrete actually affected by fire. remains in position and affords protection to the concrete beneath it. The thickness of protective coating required, depends upon the probable duration of a fire, which is likely to occur in the structure. However, for ordinary conditions, it is recommended, as a general rule, that the metal in girders and columns be protected by a minimum of 2 inches, beams 11 inches. and floor slabs, the different minimum values, as indicated in the accompanying table.

A properly designed combination of protected steel framework with reinforced concrete floor slabs, if well executed is particularly safe and effective in fireproof building construction, and the use of concrete and steel in the floor slab is especially advan-

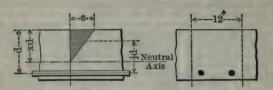
tageous, affording both strength and rigidity.

In reinforced concrete design, the following assumptions are recommended and considered by almost all authorities, and are, therefore, used as the basis for the formulæ and tables of pages 92 and 93, but it must be noted that all these ideal conditions cannot be had in practice and if possible allowance should be made accordingly.

- (1) Calculations should be made with reference to working stresses and safe loads, rather than to ultimate strengths and ultimate loads.
  - (2) A section, plane before bending remains plane after bending.
- (3) The modulus of concrete in compression within the usual limits of working stresses is constant. The distribution of compressive forces in slabs is therefore rectilinear.
- (4) The tensile stresses in the concrete shall be neglected in calculating the reinforced slab resistance.
- (5) Perfect adhesion between concrete and reinforcement is assumed.
- (6) Initial stresses in the reinforcement due to contraction or expansion in the concrete may be neglected.

These above assumptions, while not entirely borne out by experimental data, are recommended and used by various authorities on this subject in the interest of simplicity and uniformity.

### REINFORCED CONCRETE FLOOR SLABS.



#### NOTATION.

w = Total weight in lbs. per sq. ft. including slab weight.

L = Span in feet c. to c. of beam supports.

M = Bending Moment for 12" width of slab (inch pounds).

Ec = Modulus of Elasticity for concrete.

Es = " " " steel.

r = Ratio. Es ÷ Ec.

C = Extreme fibre stress of concrete in compression.

S = " " steel in tension.

K = Constant for a given steel and concrete.

d = Effective depth of slab in inches.

n = Patie of steel area to effective eleb

p = Ratio of steel area to effective slab area.
 x = Distance. Top of slab to Neutral Axis ÷ d.

i = "between centers of stress + d.

V = Maximum Shear, 12" width of slab.

v = Unit shear.

u = Unit bond stress.

 $\Sigma$ o = Sum of perimeters of bars (in 12" width of slab).

### FORMULE.

 $M = 1.5 \text{ wL}^2$ —for slabs freely supported.

= 1.2 wL<sup>2</sup>— " continuous over supports.

$$p = \frac{C^2r}{2 \text{ S (Cr+S)}} \qquad x = rp \left(\sqrt{1 + \frac{2}{rp}} - 1\right)$$

$$K = \frac{Sp}{3} \left(\frac{2Cr + 3S}{Cr + S}\right) \qquad j = 1 - \frac{x}{3}$$

$$d = \sqrt{\frac{M}{12 \text{ K}}}$$
 Steel Area (12" width of slab) = 12 dp

 $v = \frac{V}{12 \text{ id}}$  (not to exceed 60 lbs. for stone or 25 lbs. for cinder concrete).

 $u = \frac{V}{jd \Sigma o}$  (not to exceed 60 lbs. for stone or 30 lbs. for cinder concrete).

For Square and Round Bars, refer to pages 451-457.

NOTE.—Best practice indicates that Spans of Floor Slabs should not exceed seven feet between steel beams or steel girders. Generally speaking, the span should in no case exceed 10 feet for ordinary work.

#### REINFORCED CONCRETE FLOOR SLABS.

Values deduced from formulæ, page 92, using unit stresses based on modern safe practice.

Concrete.	Weight per cu. ft. Pounds.	C	s	r= E <sub>s</sub> ÷E <sub>o</sub>	p	K		3
Stone. 1:2:4.	150	500	16000	15	.0050	71.5	.320	.893
Cinder. 1:2:4.	110	185	16000	30	.0015	21.8	.258	.914

#### THICKNESS OF CONCRETE BELOW STEEL.

Depth of Slab "d" (inches).	2½ to 4	4½ to 8½	9 to 12	13 to 18	19 to 20	Above 20
Thickness of Concrete below Lower Surface of Steel Rods (inches).	3 4	1	114	11/2	134	2

#### SPACING OF REINFORCING BARS.

The lateral spacing of parallel bars should not be less than two and one-half diameters, center to center, nor greater than  $2\frac{1}{2} \times$  thickness of slab; nor should the distance from edge of slab to center of nearest bar be less than one and one-half diameters. The clear spacing between two layers of bars should not be less than one-half inch.

Cross reinforcement of steel rods of small diameter (¼") laid parallel to the principal beams upon which the slab rests, should be used to prevent shrinkage and temperature cracks and to give added strength. They should be spaced about two feet, center to center.

#### DISTRIBUTION OF LOAD FOR SLABS OF FOUR SIDES SUPPORT.

Where length of slab exceeds 1.5 width, the entire load should be carried by transverse reinforcement. Slabs of smaller ratio of dimension may well be reinforced in both directions. Distribution of the load may be determined by use of the formula

$$r = \frac{1^4}{1^4 + b^4}$$

in which r = proportion of load carried by transverse reinforcement, l = length and b = breadth of slab.

Using values thus determined, each set of reinforcement is to be calculated as in slabs having two supports only.

NOTE.—In all cases of two-way reinforcement, intersections of rods should be securely tied with heavy wire.

### LIMITING SPANS AND MAXIMUM LOADS OF I-BEAMS AND CHANNELS DUE TO CRIPPLING OF THE WEB.

I-Beams and Channels, when used as beams for very short spans in which the ratio of length of span to depth of beam is small, should be examined for safe strength of the web considered as a column, subjected to crippling due to the shearing strains.

The Tables of Safe Loads of Beams and Channels are computed with regard to the safe unit stresses due to flexure, and, with one or two exceptions, as indicated by dotted lines and accompanying foot-notes, the lengths of spans tabulated are such that the limitation due to web crippling does not appear. The shearing stresses acting in the web of a beam may be considered to consist of two stresses of equal intensity acting at right angles to each other, and at angles of 45 degrees with the neutral axis. The intensity of each of these stresses is equal to the intensity of the vertical shear, which is a maximum at the points of support for uniform loading, and uniform throughout from the point of loading to the supports for a superimposed concentrated load at the center.

The vertical shears for different systems of loading may be obtained by the use of moments in the usual way, and these are given for various cases on pages 162 to 165 inclusive.

The shearing stresses which act at angles of 45 degrees with the neutral axis are equivalent to compressive and tensile forces, and the former will tend to buckle the web, which should therefore be figured as composed of a series of columns of a length equal to its diagonal depth. If c is the vertical depth of the web in the clear between the fillets which connect it with the flanges, the square of the length of the column to be considered will be 2c<sup>2</sup>.

Substituting this value for l2 in the formula for long columns

$$\mathbf{p} = \frac{12000}{1 + \frac{1^2}{3000 \ \mathbf{t}^2}}$$

we have

$$\mathbf{p} = \frac{12000}{1 + \frac{c^2}{1500 \, t^2}}$$

in which

p = intensity of vertical shear, in pounds per square inch =

Total shear in pounds dt.

c = depth of web in clear between fillets in inches.

t = thickness of web in inches.

d = depth of beam in inches.

This formula is also applicable for computing the safe shearing stress in the webs of plate girders, in which case the length, l, is the vertical distance between centers of upper and lower rows of rivet holes connecting the webs and flanges.

The webs of plate girders should be reinforced by stiffening angles at points of support and concentrated loading, and in cases where the intensity of shear exceeds that given by the above formula the web should be provided with stiffeners.

The following tables have been prepared based upon the above formula for safe unit shearing stress in the webs of beams and channels.

#### MAXIMUM SAFE LOADS FOR I-BEAMS OF ANY LENGTH AND CORRESPONDING MINIMUM SAFE SPANS BASED UPON CRIPPLING OF THE WEB.

For loads in pounds uniformly distributed including weight of beam.

Section Num-	Depth of Beam.	Weight per Foot.	Maximum Safe Load.	Mini- mum Span.	Section Num-	Depth of Beam.	Weight per Foot.	Maximum Safe Load.	Mini- mum Span.
ber.	Inches.	Pounds.	Pounds.	Feet.	ber.	Inches.	Pounds.	Pounds.	Feet.
B 5	3	5.5	10900	1.7	B 53	15	42	86530	7.3
		6.5	17790	1.1			45	106100	6.2
		7.5	25230	.9			50	146260	4.8
B 9	4	7.5	15330	2.1	2 1		55	186740	4.0
		8.5	22670	1.6		35	60	222970	3.6
		9.5	30820	1.2	B109	15	60	-160940	5.5
		10.5	37820	1.1			65	201330	4.6
B 13	5	9.75	20050	2.6			70	237380	4.1
20	-	12.25	39730	1.5			75	276990	3.7
		14.75	57400	1.2			80	316160	3.4
B 17	6	12.25	25130	3.1	B113	15	80	247900	4.6
DI	U	14.75	44320	2.0			85	287290	4.2
		17.25	62890	1.6			90	322350	3.9
D 04	-						95	361780	3.6
B 21	7	15 17.5	30510 49320	3.7			100	399220	3.4
		20	69540	1.9	B 65	18	55	109040	8.8
7 01	_						60	155580	6.6
B 25	8	18	36310	4.2			65	194040	5.5
		20.25	53560 72760	3.1			70	232870	4.9
	-	25.25	91590	2.1	B 73	20	65	129150	9.6
D 00		_	-			4 1 1	70	169980	7.3
B 29	9	21	42450	4.8			75	206910	6.7
		25 30	71530 109620	3.1	B121	20	80	182710	8.7
		35	146670	1.9	DIGI	20	85	214600	7.7
700	40		-		100		90	257610	6.6
B 33	10	25	48960	5.4			95	295400	6.0
		80 35	86630 126460	3.4			100	333150	5.5
		40	165320	2.2	D 00	94	20	127540	14.7
D 44	40				B 89	24	80 85	166820	11.8
B 41	12	31.5 35	62890	6.2			90	202450	10.1
		40	91730 130540	4.5 3.5			95	239330	8.8
710	40						100	277070	7.9
B105	12	40	99380	4.9	DAON	0.4	405	909900	10.0
		45	138110	3.8	B127	24	105	203800	12.3
		50 55	176250 213760	3.2			110 115	243290 281900	10.6
		00	210100	1 2.0	1 1		110	201000	0.4

### MAXIMUM SAFE LOADS FOR STANDARD CHAN-NELS OF ANY LENGTH AND CORRESPOND-ING MINIMUM SAFE SPANS BASED UPON CRIPPLING OF THE WEB.

For loads in pounds uniformly distributed including weight of channel.

Section Num-	Depth of Channel	Weight per Foot.	Maximum Safe Load.	Mini- mum Span.	Section Num-	Depth of Channel	Weight par Foot,	Maximum Safe Load.	Mini- mum Span.
ber.	Inches.	Pounds.	Pounds.	Feet.	ber.	Inches.	Pounds.	Pounds.	Feet.
C 5	3	4 5 6	10970 17830 25260	1.1 0.8 .6	C 25	8	18.75 21.25	83150 101800	1.5 1.3
C 9	4	5.25 6.25 7.25	14300 21660 29830	1.4 1.1 .9	C 29	9	13.25 15 20 25	28120 42250 80980 118810	4.0 2.9 1.8 1.4
C 13	5	6.5 9 11.5	17390 35900 54920	1.6 1.1 .9	C 33	,10	15 20 25	30570 67420 107670	4.7 2.6 1.9
C17	6	8 10.5 13 15.5	20280 39580 58300 76540	2.3 1.4 1.1 1.0	C 41	12	30 35 20.5 25	147010 182940 41390 75440	1.6 1.4 5.5 3.5
C 21	7	9.75 12.25 14.75	22950 43660 62200	2.8 1.7 1.4			30 35 40	114230 156000 193920	2.6 2.1 1.9
702		17.25 19.75	82110 99880	1.2	C 53	15	33 35 40	83430 95070 130940	5.4 4.9 4.3
C 25	8	11.25 13.75 16.25	25560 44800 64140	3.4 2.2 1.7		T.	45 50 55	171400 211750 251710	3.2 2.8 2.5

#### COEFFICIENTS FOR DEFLECTION IN INCHES FOR CAMBRIA SHAPES, USED AS BEAMS SUBJECTED TO SAFE LOADS UNIFORMLY DISTRIBUTED.

Distance between Supports in Feet.	Coefficient for Fibre Stress of 16 000 lbs. per Square Inch.	Coefficient for Fibre Stress of 12 500 lbs. per Square Inch.	Distance between Supports in Feet.	Coefficient for Fibre Stress of 16 000 lbs. per Square Inch.	Coefficient for Fibre Stress of 12 500 lbs. per Square Inch.
L	H	H'	L	H	H'
4	.265	.207	23	8.756	6.841
5	.414	.323	24	9.534	7.448
6	.596	.466	25	10.345	8.082
7	.811	.634	26	11.189	8.741
8	1.059	.828	27	12.066	9.427
9	1.341	1.047	28	12.977	10.138
10	1.655	1.293	29	13.920	10.875
11	2.003	1.565	30	14.897	11.638
12	2.383	1.862	31	15.906	12.427
13	2.797	2.185	32	16.949	13.241
14	3.244	2.534	33	18.025	14.082
15	3.724	2.909	34	19.134	14.948
16	4.237	3.310	35	20.276	15.841
17	4.783	3.737	36	21.451	16.759
18	5.363	4.190	37	22.659	17.703
19	5.975	4.668	38	23.901	18.672
20	6.621	5.172	39	25.175	19.668
21	7.299	5.703	40	26.483	20.690
22	8.011	6.259		-	

The above coefficients are for use in obtaining the deflection of steel shapes subjected to transverse strain, under their uniformly distributed safe loads for extreme fibre stresses of 16 000 pounds and 12 500 pounds per square inch; the modulus of elasticity being 29 000 000.

To find the deflection of any shape that is symmetrical about its neutral axis under the above conditions of loading when used as a beam, such as I-Beams, Channels, etc., divide the coefficient in the table corresponding to the given span and fibre stress, by the depth of the beam in inches. The result will be the deflection in inches.

To find the deflection of any shape that is unsymmetrical about its neutral axis when used as a beam, under the above conditions of loading, such as Angles, etc., divide the coefficient in the table corresponding to the given span and fibre stress by twice the distance of the most remote fibre from the neutral axis, expressed in inches.

If, in construction, the beam is placed in position in the usual manner upon its end supports without special scaffolding or falsework between them, it will deflect somewhat by reason of its own weight, and upon the addition of external loading a further deflection will occur.

The deflections obtained as above described are the total deflections due to the weight of the beam itself and the superimposed safe load uniformly distributed.

Thus, to find, from the preceding table, the deflection in inches for Cambria shapes used as Beams under their safe loads uniformly distributed including the weight of the beam:

Let D = deflection in inches.

L = length between supports in feet.

H = coefficient for deflection from table for fibre stress of 16 000 pounds per square inch.

H' = coefficient for deflection from table for fibre stress of 12 500 pounds per square inch.

d = depth of beam in inches for symmetrical sections.

x<sub>1</sub> = distances in inches from neutral axis to most remote fibre for unsymmetrical sections.

#### FOR SYMMETRICAL SECTIONS.

For fibre stress of 16 000 pounds per square inch D =

For fibre stress of 12 500 pounds per square inch D =

FOR UNSYMMETRICAL SECTIONS.

For fibre stress of 16 000 pounds per square inch D =

For fibre stress of 12 500 pounds per square inch D =

#### EXAMPLES.

Case I.—To find the deflection of a 9" I-Beam weighing 30 pounds per foot, for a span of 15 feet and a maximum fibre stress of 16 000 pounds per square inch, under its safe load uniformly distributed.

From the above table the deflection coefficient for this case is found to be 3.724 which divided by 9, the depth of the beam in inches, gives

.414, which is the required deflection in inches.

The safe load for this beam under the conditions named is 16 100 pounds including the weight of the beam itself as stated in the Tables of Safe Loads for Cambria I-Beams on page 109.

Case II.—To find the deflection of a  $6'' \times 4'' \times \frac{1}{2}''$  angle, supported at the ends on its short leg as a horizontal base, for a span of 9 feet and a maximum fibre stress of 16 000 pounds per square inch under

its safe load uniformly distributed including its own weight.

From the table of "Properties of Angles" on page 207 the distance x' from the neutral axis to the back of the shorter leg is found to be 1.99 inches, which subtracted from the length of long leg, 6 inches, gives 4.01 as the distance x<sub>1</sub> from the neutral axis to the most remote fibre. From the above table the deflection coefficient for this case is found to be 1.341, which divided by 8.02, twice x<sub>1</sub>, gives .167, which is the required deflection in inches.

NOTE.—For deflections of Beams and Channels due to any central or uniform load see coefficients of deflection N and N' in the Tables of Properties relating to these sections and the accompanying explanations.

For deflections of any symmetrical beams due to various systems of loading,

see general formulæ and diagrams on pages 160 to 165 inclusive.

### TABLES OF SAFE LOADS FOR CAMBRIA SEC-TIONS USED AS BEAMS, AND SPACING FOR CAMBRIA I-BEAMS.

Pages 106 to 159 inclusive.

#### TABLES OF SAFE LOADS AND SPACINGS.

The Tables of Safe Loads for Cambria I-Beams, Channels, and Angles, give the safe loads in pounds uniformly distributed for all usual spans based upon extreme fibre stresses of 16 000 pounds per square inch.

These loads include the weight of the steel shape itself, which should be deducted in order to obtain the external load that it will safely carry. In case the shape is used to support a floor, the weight of the steel, together with that of the other portions of the floor construction, must be deducted in order to obtain the net live load which can be safely sustained. Weights of hollow tile floor arches and fireproofing material are given on page 69. to which should be added the weight of plastering, filling on top of arches and the weight of the material forming the surface of the floor, in order to obtain the dead load of materials in figuring fireproof floors, in addition to the weight of the steel.

A table of superimposed loads per square foot, exclusive of the weights of materials, in accordance with the usual practice for different classes of buildings, is given on p. 52.

The Tables of Safe Loads for Cambria sections used as beams and the Tables for Spacing of Cambria I-Beams are calculated on the assumption that proper provision has been made for preventing lateral deflection by means of tie-rods or other braces spaced at suitable distances apart; which for beams and channels should not exceed twenty times the flange width. In cases where intermediate lateral support is not provided, the safe loads shown in the tables must be reduced, and for beams and channels the

amount of this reduction can de determined by reference to the explanations and tables therefor on pages 82 and 83.

The thrust of floor arches, which is considerable, particularly in the case of long spans or distances between tie-rods, should be taken into account where it tends to produce lateral flexure of the floor beams.

Explanations of this and a formula for reducing the unit stresses from vertical loading, on account of the additional stresses caused by horizontal forces, are given on pages 78 to 81 inclusive.

In some instances the allowable deflection will govern the design rather than the transverse strength, as in the case of beams carrying plastered ceilings, in which the deflection should be limited to  $\frac{1}{30}$  inch per foot of span, or  $\frac{1}{300}$  of the distance between supports in order to avoid cracking the plaster.

This limit of deflection is indicated in the tables by full horizontal lines, the figures below which correspond to loads or spacings for the given spans that will produce greater deflections than the allowable limit for plastered ceilings.

The deflection limits of the Tables of Safe Loads have been calculated for the total loads, including the weight of the section used as a beam. The superimposed live load will not produce all of this deflection, and therefore the deflection limit of the tables includes an element of safety for the reason that the beams will be deflected, after being put in place, by their own weight and that of the floor materials before the plastering is applied.

In cases where the deflection limits the use of the beam for the safe loads corresponding to the fibre stresses of the tables, the beam may be used with a less load such as to produce only the allowable deflection. The lesser load corresponding to the limit of deflection may be obtained for any span from the Table of Safe Loads as follows:

$$W = \frac{W_8 \times L^2}{L_1^2}$$

in which

- W = safe load in pounds for the limit of deflection for plastered ceilings =  $\frac{1}{\pi k \pi}$  of the span.
- W<sub>s</sub> = safe load of tables next above the line giving the limit of
- L = length of span in feet corresponding to Ws from the table
- $L_1$  = length of span for the case under consideration.

This may also be expressed by the following-

#### RULE.

Multiply the safe load next above the heavy line of the tables by the square of the corresponding span in feet and divide the product by the square of the required span. The result will be the required load corresponding to the limit of allowable deflection for plastered ceilings.

A Table of Deflections for Cambria shapes used as beams, subjected to their safe loads uniformly distributed, and accompanying explanations with examples, are given on pages 98 and 99.

#### TABLES OF SAFE LOADS FOR I-BEAMS AND CHANNELS.

Tables of Safe Loads for all sizes and weights of Cambria I-Beams and channels for the usual spans, expressed in feet, are given on pages 106 to 123 inclusive.

#### TABLES FOR SPACING OF CAMBRIA I-BEAMS.

Tables for Spacing of Cambria I-Beams for a total load of 100 pounds per square foot including the weight of the beam, corresponding to spans from 4 to 48 feet, are given on pages 124 to 135 inclusive.

For any given size of beam the spacing or distances from centers to centers for different intensities of loading varies inversely as the load, so that the spacing for any intensity of loading may be found from the tabular spacing by proportion as stated in the notes at the foot of the tables.

### TABLES OF SAFE LOADS FOR ANGLES.

Tables of uniformly distributed safe loads for the usual sizes of angles, are given on pages 138 to 159. In these tables the safe loads for equal leg angles are given on the assumption that one of the legs of the angle is horizontal and the other leg vertical. In the case of angles with unequal legs the safe loads are given for both positions, that is, with the long leg vertical and with the short leg vertical.

# EXAMPLES OF APPLICATION OF TABLES OF SAFE LOADS AND TABLES OF SPACING.

#### EXAMPLE I.

What is the proper size of beam with a clear span of 24 feet to carry a superimposed load of 30 000 pounds uniformly distributed, the deflection to be such as not to crack a plastered ceiling?

From the Tables of Safe Loads for Cambria I-Beams, page 111, it is found that a 15-inch standard beam of this length, weighing 60 pounds per foot, will carry a gross load of 31 910 pounds, and the weight of the beam itself is  $60 \times 24 = 1440$  pounds. Thus the net load may be 30 470 pounds, so that this is the proper size for the conditions named, as its deflection is within the allowable limit, which is shown to be at a span of 30 feet as indicated by the horizontal line on the table.

Similarly it may be found from page 112, that a 15-inch special beam, of 60 pounds per foot, will more than suffice, but as this section is not regularly kept in stock the standard 15-inch 60-pound beam should be ordered if prompt delivery is wanted.

It may also be found from page 114, that an 18-inch 55-pound beam will amply suffice, and as this is both stiffer and lighter than the 15-inch 60-pound beams, it could be used with economy if otherwise suitable for the location.

### EXAMPLE II.

What is the safe load for an 8-inch standard I-Beam weighing 18.0 pounds per foot for a span of 20 feet, the deflection to be such as not to crack a plastered ceiling?

From the Tables of Safe Loads, page 108, it is found that the safe load for the beam in question is 7 580 pounds, but this value is below the line which indicates the span corresponding to the allowable limit of deflection.

Substituting the proper values in the formula for obtaining the reduced load corresponding to the allowable deflection, as given on page 101, we have

$$W = \frac{W_8 \times L^2}{L_1^2} = \frac{9480 \times 16^2}{20^2} = 6067$$
 pounds.

which is the safe load required.

### EXAMPLE III.

Required the best arrangement of beams for the floor system of a building 40 feet wide x 88 feet deep to safely support a live load of 100 pounds per square foot, using 10-inch tile arches resting on 12-inch I-Beams.

The weight of the floor materials will be about 50 pounds per square foot, allowing 39 pounds for the arch and 11 pounds for the other materials, or a total load of 150 pounds per square foot to be carried by the beams.

From the Table of Spacing for I-Beams for a uniform load of 100 pounds per square foot, page 128, it is seen that 12" standard I-Beams weighing 31½ pounds per foot and spaced 9.6 feet apart from center to center can be used with a span of 20 feet, and for a load of 150 pounds per square foot the spacing will be

$$\frac{9.6 \times 100}{150} = 6.4$$
 feet.

This will require one row of interior columns lengthwise of building.

To support the beams at the center of the building will require a line of girder beams resting on the columns. Assume the columns 22 feet apart, thus dividing the building into 8 bays, four on each side of the center.

The load on each girder will be

$$\frac{40}{2} \times 22 \times 150 = 66\,000$$
 pounds.

From the Table of Safe Loads, page 111, it is found that this will require two 15-inch standard I-Beams, each weighing 60 pounds per foot.

On account of the advisability of spacing the floor beams equally, the arrangement outlined above would reduce their distances to 22

 $\frac{22}{4}$  = 5.5 feet center to center, so that 10-inch I-Beams, weighing

40 pounds per foot, might be used for the body of the floor, as may be determined by referring to the Table of Spacings of Cambria I-Beams, page 127, and calculating as before, with the result that the allowable spacing for these conditions is found to be 5.7 feet. The 10-inch 40-pound beam under these conditions, will, however, deflect almost to the allowable limit for plastered ceilings, besides, they are heavier than the 12-inch 31.5-pound beams first considered, so that the latter will be the stiffer and more economical.

Although the load on the girder is not uniformly distributed, but concentrated at three points between the supports, the bending moment in this case will be the same as if the load were figured to be distributed uniformly, and for similar cases with different spacings the moments would be very nearly identical.

### TABLES OF MAXIMUM BENDING MOMENTS.

The Tables of Maximum Bending Moments for beams and channels given on pages 136 and 137 are useful in determining the proper section required to support one or more irregularly located concentrated loads or various arrangements of loads to which the tables of safe loads uniformly distributed will not apply.

The method used consists in computing the maximum bending moment in foot pounds resulting from the specified loading, the proper section corresponding to a fibre stress of 16 000 or 12 500 lbs. per square inch, being taken directly from the tables without further computation.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

Distance	STANDARD I-BEAMS.										
between supports	3 In	ch No.	B 5.		4 Inch	No. B 9.					
in feet.	5.5 lbs.	6.5 lbs.	7.5 lbs.	7.5 lbs.	8.5 lbs.	9.5 lbs.	10.5 lbs.				
4 5	4410 3530	4780 3830	5180 4140	7950 6360	8470 6780	9000 7200	9520 7610				
6 7 8 9	2940 2520 2210 1960 1770	3190 2730 2390 2130 1910	3450 2960 2590 2300 2070	5300 4540 3980 3530 3180	5650 4840 4240 3770 3390	6000 5140 4500 4000 3600	6350 5440 4760 4230 3810				
11 12 13 14 15	1600 1470 1360 1260 1180	1740 1590 1470 1370 1280	1880 1730 1590 1480 1380	2890 2650 2450 2270 2120	3080 2820 2610 2420 2260	3270 3000 2770 2570 -2400	3460 3170 2930 2720 2540				
16 17 18 19	1100 1040 980 930 880	1200 1130 1060 1010 960	1290 1220 1150 1090 1040	1990 1870 1770 1670 1590	2120 1990 1880 1780 1690	2250 2120 2000 1890 1800	2380 2240 2120 2000 1900				
21	840	910	990	1510	1610	1710	1810				

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{100}$  span.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

Distance		STA	NDARI	I-BEA	MS.	,
between	5 In	ch No. I	3 13.	6 In	ch No. I	3 17.
in feet.	9.75	12.25	14.75	12.25	14.75	17.25
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
4 5	12900	14520	16160	19370	21320	23280
	10320	11620	12930	•15490	•17050	18620
6	8600	9680	10770	12910	14210	•15520
7	7370	8300	9230	11070	12180	13300
8	6450	7260	8080	9680	10660	11640
9	5730	6460	7180	8610	9470	10350
10	5160	5810	6460	7750	8530	9310
11	4690	5280	5880	7040	7750	8460
12	4300	4840	5390	6460	7110	7760
18	3970	4470	4970	5960	6560	7160
14	3680	4150	4620	5530	6090	6650
15	3440	3870	4310	5160	5680	6210
16	3220	3630	4040	4840	5330	5820
17	3030	3420	3800	4560	5020	5480
18	2870	3230	3590	4300	4740	5170
19	2720	3060	3400	4080	4490	4900
20	2580	2900	3230	3870	4260	4660
21	2460	2770	3080	3690	4060	4430
22	2340	2640	2940	3520	3880	4230
23	2240	2530	2810	3370	3710	4050
24	2150	2420	2690	3230	3550	3880
25	2060	2320	2590	3100	3410	3720
26 27 28	1980 1910	2230 2150	2490 2390	2980 2870 2770	3280 3160 3050	3580 3450 3330

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span. Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

Distance	STANDARD I-BEAMS.										
between	7 In	ch No.	B 21.	8 Inch No. B 25.							
supports in feet.	15 lbs.	17.5 lbs.	20 lbs.	18.00 lbs.	20.25 lbs.	22.75 lbs.	25.25 lbs.				
4 5	27600 22080	29850 23880	32140 25710	30330	32100	34190	86290				
6 7 8 9	18400 •15770 13800 12270 11040	19900 •17060 14930 13270 11940	21430 18370 •16070 14280 12860	25280 21670 18960 16850 15170	26750 22930 20060 17830 16050	28500 24420 21370 19000 17100	• 30240 25920 22680 20160 18140				
11 12 13 14 15	10040 9200 8490 7890	10860 9950 9190 8530	11690 10710 9890 9180 8570	13790 12640 11670 10830 10110	14590 13380 12350 11470 10700	15540 14250 13150 12210 11400	16490 15120 13960 12960 12100				
16 17 18 19 20	6900 6490 6130 5810 5520	7460 7020 6630 6280 5970	8030 7560 7140 6770 6430	9480 8920 8430 7980 7580	10030 9440 8920 8450 8030	10690 10060 9500 9000 8550	11340 10670 10080 9550 9070				
21 22 23 24 25	5260 5020 4800 4600 4420	5690 5430 5190 4980 4780	6120 5840 5590 5360 5140	7220 6890 6590 6320 6070	7640 7300 6980 6690 6420	8140 7770 7430 7120 6840	8640 8250 7890 7560 7260				
26 27 28 29	4250 4090 3940 3810	4590 4420 4260 4120	4940 4760 4590 4430	5830 5620 5420 5230	6170 5940 5730 5530	6580 6330 6110 5900	6980 6720 6480 6260				

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{3600}$  span. Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

Distance			STAN	DARD	I-BE	AMS.		
between	9	Inch N	To. B 2	9.	10	Inch I	No. B 3	3.
in feet.	21 lbs.	25 lbs.	30 lbs.	35 lbs.	25 lbs.	SO lbs.	85 lbs.	40 lbs.
8 9 10	25160 22370 20130	27240 24210 21790	30180 26830 24150	33120 29440 26500	26050	28620	31240	33850
11 12 13	18300 16770 15480 14380	19810 18160 16760 15570	21950 20120 18570 17250	24090 22080 20380 18930	23680 21710 20040 18610	26020 23850 22020 20450	28400 26030 24030 22310	30780 28210 26040 24180
15 16 17 18 19	13420 12580 11840 11180 10590	13620 12820 12110 11470	15090 14200 13410 12710	17670 16560 15590 14720 13950	17360 16280 15320 14470 13710	17890 16840 15900 15070	19520 18380 17350 16440	22570 21160 19910 18810 17820
20 21 22 23 24	9590 9150 8750 8390	10900 10380 9910 9480 9080	12070 11500 10980 10500 10060	13250 12620 12050 11520 11040	13020 12400 11840 11320 10850	13630 13010 12450 11930	15620 14880 14200 13580 13020	16120 15390 14720 14110
25 26 27 28 29 30	7740 7460 7190 6940 6710	8720 8380 8070 7780 7510 7260	9660 9290 8940 8620 8330 8050	10600 10190 9810 9460 9140 8830	10420 10020 9650 9300 8980 8680	11450 11010 10600 10220 9870 9540	12500 12020 11570 11160 10770 10410	13540 13020 12540 12090 11670 11280
31 32 33	6490	7030	7790	8550	8400 8140 7890	9230 8950 8670	10080 9760 9470	10920 10580 10260

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{380}$  span.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

Distance		ANDAI BEAM		1115		CIAL AMS.				
supports	12 In	ch No.	B 41.	12 Inch No. B 105.						
in feet.	31.5	35	40	40	45	50	55			
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.			
10	38370	40580	43720	47810	50790	53930	57070			
11	34880	36890	39740	43470	46180	•49030	• 51880			
12	31970	33820	36430	39840	42330	44940	47560			
13	29510	31220	33630	36780	39070	41480	43900			
14	27400	28990	31230	34150	36280	38520	40760			
15	25580	27050	29140	31880	33860	35950	38040			
16	23980	25360	27320	29880	31750	33710	35670			
17	22570	23870	25720	28130	29880	31720	33570			
18	21310	22540	24290	26560	28220	29960	31700			
19	20190	21360	23010	25160	26730	28380	30040			
20	19180	20290	21860	23910	25400	26960	28530			
21 22 23 24 25	18270 17440 16680 15990	19320 18450 17640 16910 16230	20820 19870 19010 18220 17490	22770 21730 20790 19920	24190 23090 22080 21160	25680 24510 23450 22470 21570	27170 25940 24810 23780			
26	14760	15610	16810	18390	19540	20740	21950			
27	14210	15030	16190	17710	18810	19970	21140			
28	13700	14490	15610	17080	18140	19260	20380			
29	13230	13990	15070	16490	17510	18600	19680			
30	12790	13530	14570	15940	16930	17980	19020			
31	12380	13090	14100	15420	16380	17400	18410			
32	11990	12680	13660	14940	15870	16850	17830			
33	11630	12300	13250	14490	15390	16340	17290			
34	11280	11940	12860	14060	14940	15860	16780			
35	10960	11590	12490	13660	14510	15410	16300			

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{800}$  span. Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

		STAN	DARD I-	BEAM.					
Distance between supports	15 Inch No. B 53.								
in feet.	42	45	50	55	60				
	lbs.	lbs.	lbs.	lbs.	lbs.				
10	62830	64830	68750	72670	76600				
11	57120	58940	62500	•66070	•69630				
12	52360	54030	57290	60560	63830				
13	48330	49870	52890	55900	58920				
14	44880	46310	49110	51910	54710				
15	41880	43220	45840	48450	51060				
16	39270	40520	42970	45420	47870				
17	36960	38140	40440	42750	45060				
18	34900	36020	38200	40370	42550				
19	33070	34120	36190	38250	40310				
20	31410	32420	34380	36340	38300				
21	29920	30870	32740	34610	36470				
22	28560	29470	31250	33030	34820				
23	27320	28190	29890	31600	33300				
24	26130	27010	28650	30280	31910				
25	25130	25930	27500	29070	30640				
26	24160	24940	26440	27950	29460				
27	23270	24010	25460	26920	28370				
28	22440	23150	24550	25960	27360				
29	21660	22360	23710	25060	26410				
30	20940	21610	22920	24220	25530				
31	20270	20910	22180	23440	24710				
32	19630	20260	21490	22710	23940				
33	19040	19650	20830	22020	23210				
34	18480	19070	20220	21370	22530				
35	17950	18520	19640	20760	21880				

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span. Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

		SPE	CIAL I-B	EAM.	•				
Distance between supports	15 Inch No. B 109.								
in feet.	60	65	70	75	80				
	lbs.	lbs.	lbs.	lbs.	lbs.				
10	86610	90470	94390	98310	102230				
11	78740	82240	85810	89370	92940				
12	72180	75390	78660	81920	85190				
13	• 66630	• 69590	72610	75620	78640				
14	61870	64620	• 67420	• 70220	73020				
15	57740	60310	62920	65540	68150				
16	54130	56540	58990	61440	63890				
17	50950	53220	55520	57830	60140				
18	48120	50260	52440	54620	56790				
19	45590	47610	49680	51740	53810				
20	43310	45230	47190	49150	51120				
21	41240	43080	44950	46810	48680				
22	39370	41120	42900	44690	46470				
23	37660	39330	41040	42740	44450				
24	36090	-37690	39330	40960	42600				
25	34650	36190	37750	39320	40890				
26	33310	34790	36300	37810	39320				
27	32080	33510	34960	36410	37860				
28	30930	32310	33710	35110	36510				
29	29870	31200	32550	33900	35250				
80	28870	30160	31460	32770	34080				
31	27940	29180	30450	31710	32980				
32	27070	28270	29500	30720	31950				
33	26250	27410	28600	29790	30980				
34	25470	26610	27760	28910	30070				
35	24750	25850	26970	28090	29210				

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span. Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

		SPEC	CIAL I-B	EAM.	
Distance between supports		15 I	nch No. I	3 113.	
in feet.	80	85	90	95	100
	lbs.	lbs.	lbs.	lbs.	lbs.
10	112230	116030	119960	123880	127800
11	102030	105490	109050	112620	116180
12	93520	96700	99960	103230	106500
13	86330	89260	92270	95290	98310
14	80160	82880	85680	88480	91280
15	74820	77360	79970	82580	85200
16	• 70140	72520	74970	77420	79870
17	66020	• 68260	• 70560	72870	75180
18	62350	64460	66640	•68820	71000
19	59070	61070	63130	65200	•67260
20	56110	58020	59980	61940	63900
21	53440	55250	57120	58990	60860
22	51010	52740	54530	56310	58090
23	48800	50450	52150	53860	55560
24	46760	48350	49980	51620	53250
25	44890	46410	47980	49550	51120
26	43170	44630	46140	47650	49150
27	41570	42980	44430	45880	47330
28	40080	41440	42840	44240	45640
29	38700	40010	41360	42720	44070
30	37410	38680	39990	41290	42600
31	36200	37430	38700	39960	41230
32	35070	36260	37490	38710	39940
33	34010	35160	36350	37540	38730
34	33010	34130	35280	36430	37590
35	32070	33150	34270	35390	36510

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{3 \cdot 60}$  span. Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

Distance	33.5		STAND	ARD I-	BEAMS	3.	
between	1	8 Inch	No. B 6	5.	20 Iz	nch No.	В 73.
in feet.	55	60	65	70	65	70	75
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
14	67350	71260	74620	77990	89110	92940	96670
15	62860	•66510	•69650	72790	83170	86740	90230
16	58930	62360	65300	•68240	77970	81320	84590
17	55460	58650	61460	64220	73380	76540	79610
18	52380	55430	58040	60660	•69310	72280	75190
19	49630	52510	54990	57460	65660	•68480	71230
20	47140	49880	52240	54590	62370	65060	•67670
21	44900	47510	49750	51990	59400	61960	64450
22	42860	45350	47490	49360	56700	59140	61520
23	40990	43380	45420	47470	54240	56570	58840
24	39290	41570	43530	45490	51980	54210	56390
25	37720	39910	41790	43670	49900	52040	54140
26	36260	38370	40180	41990	47980	50040	52050
27	34920	36950	38690	40440	46200	48190	50130
23	33670	35630	37310	38990	44550	46470	48340
29	32510	34400	36030	37650	43020	44870	46670
30	31430	33260	34820	36390	41580	43370	45110
31	30420	32180	33700	35220	40240	41970	43660
32	29460	31200	32650	34120	38980	40660	42290
33	28570	30230	31660	33080	37800	39430	41010
34	27730	29340	30730	32110	36690	38270	39810
35	26940	28510	29850	31190	35640	37170	38670
36	26190	27710	29020	30330	34650	36140	37590
37	25480	26960	28240	29510	33720	35160	36580
38	24810	26250	27490	28730	32830	34240	35620
39	24180	25580	26790	27990	31990	33360	34700
40	23570	24940	26120	27290	31190	32530	33830

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span. Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

	Lugar.	SPEC	IAL I-B	EAM.					
Distance between supports	20 Inch No. B 121.								
in feet.	80	<b>85</b>	90	95	100				
	lbs.	lbs.	lbs.	lbs.	lbs.				
16	97750	100570	103840	107100	110370				
17	92000	94650	97730	100800	103880				
18	86890	89390	92300	95200	98110				
19	82320	84690	87440	90190	92950				
20	78200	80460	83070	85680	88300				
21	74480	76620	79110	81600	84090				
22	71090	73140	75520	77890	80270				
23	• 68000	•69960	72230	74510	76780				
24	65170	67050	•69220	71400	73580				
25	62560	64360	66460	68550	•70640				
26	60160	61890	63900	65910	67920				
27	57930	59600	61530	63470	65410				
28	55860	57470	59340	61200	63070				
29	53930	55490	57290	59090	60900				
30	52140	53640	55380	57120	58870				
31	50450	51910	53590	55280	56970				
32	48880	50280	51920	53550	55190				
33	47400	48760	50350	51930	53510				
34	46000	47330	48860	50400	51940				
35	44690	45970	47470	48960	50460				
36	43450	44700	46150	47600	49050				
37	42270	43490	44900	46320	47730				
38	41160	42340	43720	45100	46470				
39	40100	41260	42600	43940	45280				
40	39100	40230	41530	42840	44150				

Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

Distance	STANDARD I-BEAM.								
between supports	24 Inch No. B 89.								
in feet.	80	85	90	95	100				
	lbs.	lbs.	lbs.	lbs.	lbs.				
18	103070	107050	110540	114020	117510				
19	97650	•101420	•104720	108020	111330				
20	92770	96350	99480	•102620	•105760				
21	88350	91760	94750	97740	100720				
22	84330	87590	90440	93290	96140				
23	80670	83780	86510	89240	91960				
24	77300	80290	82900	85520	88130				
25	74210	77080	79590	82100	86410				
26	71360	74110	76530	78940	81350				
27	68720	71370	73690	76020	.78340				
28	66260	68820	71060	73300	.75540				
29	63980	66450	68610	70770	.72940				
30	61840	64230	66320	68410	.70510				
31	59850	62160	64180	66210	68230				
32	57980	60220	62180	64140	66100				
33	56220	58390	60290	62200	64100				
34	54570	56680	58520	60370	62210				
35	53010	55060	56850	58640	60430				
36	51540	53530	55270	57010	58760				
37	50140	52080	53780	55470	57170				
38	48820	50710	52360	54010	55660				
39	47570	49410	51020	52630	54240				
40	46380	48170	49740	51310	52880				
41	45280	47000	48530	50060	51590				
42	44170	45880	47370	48870	50360				
43	43150	44810	46270	47730	49190				
44	42170	43790	45220	46650	48070				
45	41230	42820	44220	45610	47000				
46	40330	41890	43250	44620	45980				
47	39470	41000	42330	43670	45000				
48	38650	40140	41450	42760	44070				

Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

Distance	SPECIAL I-BEAM.						
between supports	24	Inch No. B 127	7.				
in feet.	105	110	115				
	lbs.	lbs.	lbs.				
18	138840	142390	145950				
19	131530	134890	138270				
20	124950	128150	131350				
21	119000	122050	125100				
22	113590	116500	119410				
23	108660	111440	114220				
24	104130	106790	109460				
25	99960	102530	105080				
26	96120	98580	101040				
27	92560	94930	97300				
28	89250	91540	93830				
29	86170	88380	90590				
30	83300	85440	87570				
31	80620	82680	84740				
32	78100	80100	82100				
33	75730	77670	79610				
34	73500	75380	77270				
35	71400	73230	75060				
36	69420	71200	72970				
37	67540	69270	71000				
38	65770	67450	69130				
39	64080	65720	67360				
40	62480	64080	65680				
41	60950	62510	64080				
42	59500	61030	62550				
43	58120	59610	61090				
44	56800	58250	59710				
45	55530	56960	58380				
46	54330	55720	57110				
47	53170	54530	55890				
48	52060	53400	54730				

Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

			S	TAND	ANDARD CHANNELS.						
Distance	3Inc	h No	. C 5.	4 In	ch No.	C 9.	5 Inc	h No.	C 13.		
in feet.	4 lbs.	<b>5</b> lbs.	6 lbs.	5.25 lbs.	6.25 lbs.	7.25 lbs.	6.5 Ibs.	9 lbs.	11.5 lbs.		
4 5	2910	3290	3680	5060	5570	6090	7910	9460	11100		
	2330	2630	2940	4050	4450	4870	6330	7570	8880		
6 7 8 9	1940 1660 1450 1290 1160	2190 1880 1640 1460 1310	2450 2100 1840 1630 1470	3370 2890 2530 2250 2020	3710 3180 2780 2470 2230	4060 3480 3050 2710 2440	5270 4520 3960 3520 3160	6310 5410 4730 4210 3790	7400 6340 5550 4930 4440		
11	1060	1190	1340	1840	2020	2210	2880	3440	4040		
12	970	1100	1230	1690	1860	2030	2640	3150	3700		
13	890	1010	1130	1560	1710	1870	2430	2910	3410		
14	830	940	1050	1440	1590	1740	2260	2700	3170		
15	780	880	980	1350	1480	1620	2110	2520	2960		
16	730	820	920	1260	1390	1520	1980	2370	2770		
17	680	770	870	1190	1310	1430	1860	2230	2610		
18	650	730	820	1120	1240	1350	1760	2100	2470		
19	610	690	770	1060	1170	1280	1670	1990	2340		
20	580	660	740	1010	1110	1220	1580	1890	2220		
21	550	630	700	960	1060	1160	1510	1800	2110		
22	530	600	670	920	1010	1110	1440	1720	2020		
23	510	570	640	880	970	1060	1380	1650	1930		
24	480	550	610	840	930	1020	1320	1580	1850		
25	470	530	590	810	890	970	1270	1510	1780		

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{180}$  span.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

	STANDARD CHANNELS.										
Distance between	6 I	6 Inch No. C 17.				7 Inc	h No.	C 21.			
supports in feet.	8	10.5	18	15.5	9.75	12.25	14.75	17.25	19.75		
36	lbs.	lbs.	lbs.	Ibs.	lbs.	lbs.	Ibe.	lbs.	lbs.		
4 5	11550 9240	13440 10750	15400 12320	17360 13890	16070 12850	18410 •14730	20700 16560	22990 18390	25280 20220		
6	7700	8960	10270	11570	10710	12280	13800	•15330	•16850		
7 8	6600 5780	7680 6720	8800 7700	9920 8680	9180 8030	10520 9210	11830 10350	13140 11490	14440 12640		
ĝ	5130	5970	6840	7720	7140	2180	9200	10220	11230		
10	4620	5380	6160	6940	6430	7370	8280	9200	10110		
					W0.10	0000	WWOO	0000	0400		
11 12	4200	4890	5600	6310 5790	5840 5360	6700 6140	7530 6900	8360 7660	9190 8430		
13	3850	4480	5130	5340	4940	5670	6370	7070	7780		
14	3300	3840	44400	4960	4590	5260	5910	6570	7220		
15	3080	3580	4110	4630	4280	4910	5520	6130	6740		
10	0000	9900	4110	4000	2200	4010	0000	0100	01.20		
16	2890	3360	3850	4340	4020	4600	5180	5750	6320		
17	2720	3160	3620	4080	3780	4330	4870	5410	5950		
18	2570	2990	3420	3860	3570	4090	4600	5110	5620 5320		
19 20	2430 2310	2830 2690	3240	3650	3380 3210	3880 3680	4360 4140	4600	5060		
20	2010	2000	0000	9210	0210	9000	3130	4000	0000		
21	2200	2560	2930	3310	3060	3510	3940	4380	4810		
22	2100	2440	2800	3160	2920	3350	3760	4180	4600		
23	2010	2340	2680	3020	2790	3200	3600	4000	4400.		
24 25	1930 1850	2240 2150	2570 2460	2890 2780	2680 2570	3070 2950	3450 3310	3830 3680	4210 4040		
20	1000	2100	200	2100	2010	2000	0010	0000	1 2020		

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{300}$  span. Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

			STAI	NDARI	O CHA	NNE	is.		
Distance between	102	8 Inc	ch No.	C 25.	13	9 1	nch l	No. C	29.
supports	11.25	13.75	16.25	18.75	21.25	18.25	15	20	25
in feet.	lbs.	lbs.	lbs.	lbs.	lbs.	Ibs.	lbs.	lbs.	lbs.
4 5	21530	24000	26610	29230	31840	28040	30130	36020	41900
	17230	19200	21290	23380	25470	22430	24110	28810	33520
6	14360	16000	17740	19480	21230	18690	20090	24010	27930
7	12310	13710	15210	16700	18200	16020	17220	20580	23940
8	10770	12000	13310	14610	15920	14020	15070	18010	20950
9	9570	10670	11830	12990	14150	12460	13390	16010	18620
10	8610	9600	10650	11690	12740	11220	12050	14410	16760
11	7830	8730	9680	10630	11580	10200	10960	13100	15240
12	7180	8000	8870	9740	10610	9350	10040	12010	13970
13	6630	7380	8190	8990	9800	8630	9270	11080	12890
14	6150	6860	7600	8350	9100	8010	8610	10290	11970
15	5740	6400	7100	7790	8490	7480	8040	9600	11170
16	5380	6000	6650	7310	7960	7010	7530	9000	10470
17	5070	5650	6260	6880	7490	6600	7090	8470	9860
18	4790	5330	5910	6490	7080	6230	6700	8000	9310
19	4530	5050	5600	6150	6700	5900	6340	7580	8820
20	4310	4800	5320	5850	6370	5610	6030	7200	8380
21	4100	4570	5070	5570	6070	5340	5740	6860	7980
22	3920	4360	4840	5310	5790	5100	5480	6550	7620
23	3750	4170	4630	5080	5540	4880	5240	6260	7290
24	3590	4000	4440	4870	5310	4670	5020	6000	6980
25	3450	3840	4260	4680	5090	4490	4820	5760	6700

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{3} \frac{1}{60}$  span. Above single dot, safe loads are too great for standard connections.

Safe loads below are figured for fibre stress of  $16\,000$  pounds per square inch and include weight of channel.

	STANDARD CHANNEL.								
Distance between supports	10 Inch No. C 33.								
in feet.	15	20	25	30	35				
	lbs.	lbs.	lbs.	lbs.	lbs.				
10	14270	16790	19410	22020	24640				
11	12970	15270	17640	20020	22400				
12	11890	14000	16170	18350	20530				
13	10980	12920	14930	16940	18950				
14	10190	12000	13860	15730	17600				
15	9510	11200	12940	14680	16430				
16	8920	10500	12130	13760	15400				
17	8390	9880	11420	12950	14490				
18	7930	9330	10780	12240	13690				
19	7510	8840	10220	11590	12970				
20	7130	8400	9700	11010	12320				
21	6790	8000	9240	10490	11730				
22	6490	7630	8820	10010	11200				
23	6200	7300	8440	9580	10710				
24	5940	7000	8090	9180	10270				
25	5710	6720	7760	8810	9860				
26	5490	6460	7460	8470	9480				
27	5280	6220	7190	8160	9130				
28	5100	6000	6930	7870	8800				
29	4920	5790	6690	7590	8500				
30	4760	5600	6470	7340	8210				

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

		STAND	ARD CH.	ANNEL.					
Distance between supports in feet.	12 Inch No. C 41.								
	20.5 lbs.	25 lbs.	30 lbs.	85 lbs.	40 lbs.				
10	22780	25600	28740	31870	35010				
11 12 13 14 15	20700 18980 17520 16270 15180	23270 21330 19690 18290 17070	26120 23950 22110 20530 19160	28980 26560 24520 22770 21250	31830 29180 26930 25010 23340				
16 17 18 19 20	14230 13400 12650 11990 11390	16000 15060 14220 13470 12800	17960 16900 15970 15120 14370	19920 18750 17710 16780 15940	21880 20600 19450 18430 17510				
21 22 23 24 25	10850 10350 9900 9490 9110	12190 11640 11130 10670 10240	13680 13060 12490 11970	15180 14490 13860 13280 12750	16670 15910 15220 14590 14000				
26 27 28 29 30	8760 a 8440 8130 7850 7590	9850 9480 9140 8830 8530	11050 10640 10260 9910 9580	12260 11810 11380 10990 10620	13470 12970 12500 12070 11670				

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{3}$  span.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

Distance	STANDARD CHANNEL.									
between	15 Inch No. C 53.									
in feet.	38	<b>25</b>	40	45	50	55				
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.				
10	44450	45500	49420	53350	57270	61190				
11	40410	41370	44930	48500	52060	55630				
12	37040	37920	41190	44460	47720	50990				
13	34190	35000	38020	41040	44050	47070				
14	31750	32500	35300	38100	40910	43710				
15	29630	30340	32950	35560	38180	40790				
16	27780	28440	30890	33340	35790	38240				
17	26150	26770	29070	31380	33690	35990				
18	24700	25280	27460	29640	31820	33990				
19	23400	23950	26010	28080	30140	32210				
20	22230	22750	24710	26670	28630	30590				
21	21170	21670	23540	25400	27270	29140				
22	20210	20680	22470	24250	26030	27810				
23	19330	19780	21490	23190	24900	26600				
24	18520	18960	20590	22230	23860	25500				
25	17780	18200	19770	21340	22910	24480				
26	17100	17500	19010	20520	22030	23530				
27	16460	16850	18310	19760	21210	22660				
28	15880	16250	17650	19050	20450	21850				
29	15330	15690	17040	18400	19750	21100				
30	14820	15170	16470	17780	19090	20400				

### SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams.

Maximum fibre stress 16 000 pounds per square inch.

Distance	STANDARD I-BEAMS.										
between	3 In	ch No.	B 5.		4 Inch	No. B 9.					
in feet.	5.5 lbs.	6.5 lbs.	7.5 lbs.	7.5 lbs.	8.5 lbs.	9.5 lbs.	10.5 lbs.				
4 5	11.0 7.1	12.0 7.7	12.9 8.3	19.9 12.7	21.2 13.6	22.5 14.4	23.8 15.2				
6 7 8 9 10 11 12 13 14 15	4.9 3.6 2.8 2.2 1.8 1.5 1.2 1.0	5.3 3.9 3.0 2.4 1.9 1.6 1.3 1.1 1.0	5.8 4.2 3.2 2.6 2.1 1.7 1.4 1.2 1.1	8.8 6.5 5.0 3.9 3.2 2.6 2.2 1.9 1.6 1.4	9.4 6.9 5.3 4.2 3.4 2.8 2.4 2.0 1.7 1.5	10.0 7.3 5.6 4.4 3.6 3.0 2.5 2.1 1.8 1.6	10.6 7.8 5.9 4.7 3.8 3.1 2.6 2.3 1.9 1.7				
16 17 18 19 20				1.2 1.1 1.0	1.3 1.2 1.0	1.4 1.2 1.1 1.0	1.5 1.3 1.2 1.1 1.0				

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{340}$  span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

 $\label{eq:Required_spacing} \begin{aligned} & \text{Required spacing} = & \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times & \text{Computed spacing from table.} \end{aligned}$ 

### SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance between supports in feet.	STANDARD I-BEAMS.									
	5 In	ch No. I	3 13.	6 Inch No. B 17.						
	9.75 lbs.	12.25 lbs.	14.75 lbs.	12.25 lbs.	14.75 lbs.	17.25 lbs.				
4 5	32.2 20.6	36.3 23.2	40.4 25.9	48.4 •31.0	53.3 •34.1	58.2 37.2				
6 7 8 9 10	14.3 10.5 8.1 6.4 5.2	16.1 11.9 9.1 7.2 5.8	18.0 13.2 10.1 8.0 6.5	21.5 15.8 12.1 9.6 7.7	23.7 17.4 13.3 10.5 8.5	•25.9 19.0 14.5 11.5 9.3				
11 12 13 14 15	4.3 3.6 3.1 2.6 2.3	4.8 4.0 3.4 3.0 2.6	5.3 4.5 3.8 3.3 2.9	6.4 5.4 4.6 4.0 3.4	7.0 5.9 5.0 4.4 3.8	7.7 6.5 5.5 4.8 4.1				
16 17 18 19 20	2.0 1.8 1.6 1.4 1.3	2.3 2.0 1.8 1.6 1.5	2.5 2.2 2.0 1.8 1.6	3.0 2.7 2.4 2.1 1.9	3.3 3.0 2.6 2.4 2.1	3.6 3.2 2.9 2.6 2.3				
21 22 23 24 25	1.2 1.1 1.0	1.3 1.2 1.1 1.0	1.5 1.3 1.2 1.1 1.0	1.8 1.6 1.5 1.3 1.2	1.9 1.8 1.6 1.5 1.4	2.1 1.9 1.8 1.6 1.5				
26 27 28			1.0	1.1 1.1 1.0	1.3 1.2 1.1	1.4 1.3 1.2				

For spacings above single dot the safe loads are too great for standard connections.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings  $= \frac{1}{\pi}\delta_0$  span. Spacings for other intensities of loading may be obtained from those in tables

as follows:

Intensity of loading from table. Required spacing=

## SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance	STANDARD I-BEAMS.									
between supports in feet.	7 Inch No. B 21.			8 Inch No. B 25.						
	15 lbs.	17.5 lbs.	20 lbs.	18.00 lbs.	20.25 lbs.	22.75 lbs.	25.25 lbs.			
4 5	69.0 44.2	74.6 47.8	80.3 51.4	60.7	64.2	68.4	72.6			
6 7 8 9	30.7 •22.5 17.3 13.6 11.0	33.2 •24.4 18.7 14.7 11.9	35.7 26.2 •20.1 15.9 12.9	42.1 31.0 23.7 18.7 15.2	44.6 32.8 25.1 19.8 16.1	47.5 34.9 26.7 21.1 17.1	•50.4 37.0 28.3 22.4 18.1			
11 12 13 14	9.1 7.7 6.5 5.6	9.9 8.3 7.1 6.1	10.6 8.9 7.6 6.6	12.5 10.5 9.0 7.7	13.3 11.1 9.5 8.2	14.1 11.9 10.1 8.7	15.0 12.6 10.7 9.3			
15 16 17 18 19 20	4.9 4.3 3.8 3.4 3.1 2.8	5.3 4.7 4.1 3.7 3.3 3.0	5.7 5.0 4.4 4.0 3.6 3.2	5.9 5.2 4.7 4.2 3.8	7.1 6.3 5.6 5.0 4.4 4.0	7.6 6.7 5.9 5.3 4.7 4.3	8.1 7.1 6.3 5.6 5.0 4.5			
21 22 23 24 25	2.5 2.3 2.1 1.9 1.8	2.7 2.5 2.3 2.1 1.9	2.9 2.7 2.4 2.2 2.1	3.4 3.1 2.9 2.6 2.4	3.6 3.3 3.0 2.8 2.6	3.9 3.5 3.2 3.0 2.7	4.1 3.7 3.4 3.1 2.9			
26 27 28	1.6 1.5 1.4	1.8 1.6 1.5	1.9 1.8 1.6	2.2 2.1 1.9	2.4 2.2 2.0	2.5 2.3 2.2	2.7 2.5 2.3			

For spacings above single dot the safe loads are too great for standard connections.

For spacing above the dotted line the safe load for bending is greater than the For spacing above the dotted line the sale load for belong is greater than the safe load for web crippling, as explained and shown on pages 82 to 84 inclusive. For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{16}\pi$  span. Spacings for other intensities of loading may be obtained from those in tables

as follows:

Intensity of loading from table. Computed spacing from table. Required spacing=

### SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER SOUARE FOOT.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance	STANDARD I-BEAMS.							
between supports	9	Inch l	No. B 2	9.	10 Inch No. B 33.			
in feet.	21 lbs.	25 lbs.	30 lbs.	<b>35</b> lbs.	25 lbs.	30 lbs.	85 lbs.	40 lbs.
8 9 10	31.5 24.9 20.1	34.1 26.9 21.8	37.7 29.8 24.1	41.4 32.7 26.5	26.0	28.6	31.2	33.9
11 12 13 14 15	16.6 14.0 11.9 10.3 8.9	18.0 15.1 12.9 11.1 9.7	20.0 16.8 14.3 12.3 10.7	21.9 18.4 15.7 13.5 11.8	21.5 18.1 15.4 13.3 11.6	23.7 19.9 16.9 14.6 12.7	25.8 21.7 18.5 15.9 13.9	28.0 23.5 20.0 17.3 15.0
16 17 18 19 20	7.9 7.0 6.2 5.6 5.0	8.5 7.5 6.7 6.0 5.4	9.4 8.4 7.5 6.7 6.0	10.4 9.2 8.2 7.3 6.6	10.2 9.0 8.0 7.2 6.5	11.2 9.9 8.8 7.9 7.2	12.2 10.8 9.6 8.7 7.8	13.2 11.7 10.4 9.4 8.5
21 22 23 24 25	4.6 4.2 3.8 3.5 3.5	4.9 4.5 4.1 3.8 3.5	5.5 5.0 4.6 4.2 3.9	6.0 5.5 5.0 4.6 4.2	5.9 5.4 4.9 4.5 4.2	6.5 5.9 5.4 5.0 4.6	7.1 6.5 5.9 5.4 5.0	7.7 7.0 6.4 5.9 5.4
26 27 28 29 30	3.0 2.8 2.6 2.4 2.2	3.2 3.0 2.8 2.6 2.4	3.6 3.3 3.1 2.9 2.7	3.9 3.6 3.4 3.2 2.9	3.9 3.6 3.3 3.1 2.9	4.2 3.9 3.7 3.4 3.2	4.6 4.3 4.0 3.7 3.5	5.0 4.6 4.3 4.0 3.8
31 32 33	2.1	2.3	2.5	2.8	2.7 2.5 2.4	3.0 2.8 2.6	3.3 3.1 2.9	3.5 3.3 3.1

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{380}$  span. Spacings for other intensities of loading may be obtained from those in tables as follows:

Intensity of loading from table. Required spacing=

### SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER. SQUARE FOOT.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance between		ANDA BEAI		SPECIAL I-BEAM.			
supports	12 In	ch No.	B 41.	12	Inch I	No. B 10	)5.
in feet.	31.5 lbs.	35 lbs.	40 lbs.	40 lbs.	45 lbs.	be.	bs.
10	38,4	40.6	43.7	47.8	50.8	53.9	57.1
11 12 13 14 15	31.7 26.6 22.7 19.6 17.1	33.5 28.2 24.0 20.7 18.0	36.1 30.4 25.9 22.3 19.4	39.5 33.2 28.3 24.4 21.3	42.0 35.3 30.1 25.9 22.6	•44.6 37.5 31.9 27.5 24.0	*47.2 39.6 33.8 29.1 25.4
16 17 18 19 20	15.0 13.3 11.8 10.6 9.6	15.9 14.0 12.5 11.2 10.1	17.1 15.1 13.5 12.1 10.9	18.7 16.5 14.8 13.2 12.0	19.8 17.6 15.7 14.1 12.7	21.1 18.7 16.6 14.9 13.5	22.3 19.7 17.6 15.8 14.3
21 22 23 24 25	8.7 7.9 7.3 6.7	9.2 8.4 7.7 7.0 6.5	9.9 9.0 8.3 7.6	10.8 9.9 9.0 8.3	11.5 10.5 9.6 8.8	12.2 11.1 10.2 9.4	12.9 11.8 10.8 9.9
26 27 28 29 30	5.7 5.3 4.9 4.6 4.3	6.0 5.6 5.2 4.8 4.5	6.5 6.0 5.6 5.2 4.9	7.1 6.6 6.1 5.7 5.3	8.1 7.5 7.0 6.5 6.0 5.6	8.6 8.0 7.4 6.9 6.4 6.0	9.1 8.4 7.8 7.3 6.8 6.3
31 32 33 34 35	4.0 3.7 3.5 3.3 3.1	4.2 4.0 3.7 3.5 3.3	4.5 4.3 4.0 3.8 3.6	5.0 4.7 4.4 4.1 3.9	5.3 5.0 4.7 4.4 4.1	5.6 5.3 5.0 4.7 4.4	5.9 5.6 5.2 4.9 4.7

For spacings above single dot the safe loads are too great for standard connections.

as follows:

Intensity of loading from table. Required spacing=

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{380}$  span. Spacings for other intensities of loading may be obtained from those in tables

### SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance between	STANDARD I-BEAM. 15 Inch No. B 53.							
supports	42	45	50	<b>55</b> lbs.	60			
in feet.	lbs.	lbs.	lbs.		lbs.			
10	62.8	64.8	68.8	72.7	76.6			
11	51.9	53.6	56.8	•60.1	•63.3			
12	43.6	45.0	47.7	50.5	53.2			
13	37.2	38.4	40.7	43.0	45.3			
14	32.0	33.1	35.1	37.1	39.1			
15	27.9	28.8	30.6	32.3	34.0			
16	24.5	25.3	26.9	28.4	29.9			
17	21.7	22.4	23.8	25.1	26.5			
18	19.4	20.0	21.2	22.4	23.6			
19	17.4	18.0	19.0	20.1	21.2			
20	15.7	16.2	17.2	18.2	19.1			
21	14.2	14.7	15.6	16.5	17.4			
22	13.0	13.4	14.2	15.0	15.8			
23	11.9	12.3	13.0	13.7	14.5			
24	10.9	11.3	11.9	12.6	13.3			
25	10.1	10.4	11.0	11.6	12.3			
26	9.3	9.6	10.2	10.8	11.3			
27	8.6	8.9	9.4	10.0	10.5			
28	8.0	8.3	8.8	9.3	9.8			
29	7.5	7.7	8.2	8.6	9.1			
30	7.0	7.2	7.6	8.1	8.5			
31	6.5	6.7	7.2	7.6	8.0			
32	6.1	6.3	6.7	7.1	7.5			
33	5.8	6.0	6.3	6.7	7.0			
34	5.4	5.6	5.9	6.3	6.6			
35	5.1	5.3	5.6	5.9	6.3			

For spacings above single dot the safe loads are too great for standard connections.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{340}$  span. Spacings for other intensities of loading may be obtained from those in tables

as follows:

Required spacing =  $\frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$ 

### SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER SOUARE FOOT.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance between			IAL I-I			
supports	60			75	80	
in feet.	lbs.			lbs.	lbs.	
10	86.6	90.5	94.4	98.3	102.2	
11	71.6	74.8	78.0	81.2	84.5	
12	60.1	62.8	65.5	68.3	71.0	
13	•51.3	•53.5	55.9	58.2	60.5	
14	44.2	46.2	•48.2	•50.2	52.2	
15	38.5	40.2	41.9	43.7	•45.4	
16	33.8	35.3	36.9	38.4	39.9	
17	30.0	31.3	32.7	34.0	35.4	
18	26.7	27.9	29.1	30.3	31.6	
19	24.0	25.1	26.1	27.2	28.3	
20	21.7	22.6	23.6	24.6	25.6	
21	19.6	20.5	21.4	22.3	23.2	
22	17.9	18.7	19.5	20.3	21.1	
23	16.4	17.1	17.8	18.6	19.3	
24	15.0	15.7	16.4	17.1	17.7	
25	13.9	14.5	15.1	15.7	16.4	
26	12.8	13.4	14.0	14.5	15.1	
27	11.9	12.4	12.9	13.5	14.0	
28	11.0	11.5	12.0	12.5	13.0	
29	10.3	10.8	11.2	11.7	12.2	
30	9.6	10.1	10.5	10.9	11.4	
31	9.0	9.4	9.8	10.2	10.6	
32	8.5	8.8	9.2	9.6	10.0	
33	8.0	8.3	8.7	9.0	9.4	
34	7.5	7.8	8.2	8.5	8.8	
35	7.1	7.4	7.7	8.0	8.3	

For spacings above single dot the safe loads are too great for standard connections.

as follows:

Required spacing = Intensity of loading from table.

New intensity of loading 

Computed spacing from table.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings  $= \frac{1}{3}\delta_0$  span. Spacings for other intensities of loading may be obtained from those in tables

### SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance between			IAL I-I		
supports	80	85	90	95	100
in feet.	lbs.	lbs.	lbs.	lbs.	lbs.
10	112.2	116.0	120.0	123.9	127.8
11	92.8	95.9	99.1	102.4	105.6
12	77.9	80.6	83.3	86.0	88.7
13	66.4	68.7	71.0	73.3	75.6
14	57.3	59.2	61.2	63.2	65.2
15	49.9	51.6	53.3	55.1	56.8
16	•43.8	45.3	46.9	48.4	49.9
17	38.8	•40.2	•41.5	42.9	44.2
18	34.6	35.8	37.0	• 38.2	39.4
19	31.1	32.1	33.2	34.3	•35.4
20	28.1	29.0	30.0	31.0	31.9
21	25.4	26.3	27.2	28.1	29.0
22	23.2	24.0	24.8	25.6	26.4
23	21.2	21.9	22.7	23.4	24.2
24	19.5	20.1	20.8	21.5	22.2
25	18.0	18.6	19.2	19.8	20.4
26	16.6	17.2	17.7	18.3	18.9
27	15.4	15.9	16.5	17.0	17.5
28	14.3	14.8	15.3	15.8	16.3
29	13.3	13.8	14.3	14.7	15.2
30	12.5	12.9	13.3	13.8	14.2
31	11.7	12.1	12.5	12.9	13.3
32	11.0	11.3	11.7	12.1	12.5
33	10.3	10.7	11.0	11.4	11.7
34	9.7	10.0	10.4	10.7	11.1
35	9.2	9.5	9.8	10.1	10.4

For spacings above single dot the safe loads are too great for standard connections.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{780}$  span. Spacings for other intensities of loading may be obtained from those in tables

as follows:

Required spacing= Intensity of loading from table.

New intensity of loading X Computed spacing from table.

### SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance	STANDARD I-BEAMS.							
between	1	8 Inch	No. B 6	5.	20 Inch No. B 73.			
supports	55	60	65	70	65	70	75	
in feet.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	
14	48.1	50.9	53.3	55.7	63.6	66.4	69.1	
15	41.9	•44.3	•46.4	48.5	55.4	57.8	60.2	
16	36.8	39.0	40.8	•42.6	48.7	50.8	52.9	
17	32.6	34.5	36.2	37.8	43.2	45.0	46.8	
18	29.1	30.8	32.2	33.7	•38.5	40.2	41.8	
19	26.1	27.6	28.9	30.2	34.6	•36.0	37.5	
20	23.6	24.9	26.1	27.3	31.2	32.5	•33.8	
21	21.4	22.6	23.7	24.8	28.3	29.5	30.7	
22	19.5	20.6	21.6	22.6	25.8	26.9	28.0	
23	17.8	18.9	19.7	20.6	23.6	24.6	25.6	
24	16.5	17.3	18.1	19.0	21.7	22.6	23.5	
25	15.1	16.0	16.7	17.5	20.0	20.8	21.7	
26	13.9	14.8	15.5	16.2	18.5	19.2	20.0	
27	12.9	13.7	14.3	15.0	17.1	17.8	18.6	
28	12.0	12.7	13.3	13.9	15.9	16.6	17.3	
29	11.2	11.9	12.4	13.0	14.8	15.5	16.1	
30	10.5	11.1	11.6	12.1	13.9	14.5	15.0	
31 32 33 34 35	9.8 9.2 8.7 8.2 7.7	9.7 9.2 8.6 8.1	10.9 10.2 9.6 9.0 8.5	11.4 10.7 10.0 9.4 8.9	13.0 12.2 11.5 10.8 10.2	13.5 12.7 11.9 11.3 10.6	14.1 13.2 12.4 11.7 11.0	
36	7.3	7.7	8.1	8.4	9.6	10.0	10.4	
37	6.9	7.3	7.6	8.0	9.1	9.5	9.9	
38	6.5	6.9	7.2	7.6	8.6	9.0	9.4	
39	6.2	6.5	6.8	7.2	8.2	8.5	8.9	
40	5.9	6.2	6.5	6.8	7.8	8.1	8.4	

For spacings above single dot the safe loads are too great for standard connections.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings = 1/360 span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

 $\label{eq:Required_spacing} \begin{aligned} & \underline{\text{Intensity of loading from table}}. & \\ & \underline{\text{New intensity of loading}}. & \\ & \underline{\text{Computed spacing from table}}. \end{aligned}$ 

### SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER SOUARE FOOT.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance	SPECIAL I-BEAM.							
between supports	20 Inch No. B 121.							
in feet.	80	85	90	95	100			
	lbs.	lbs.	lbs.	lbs.	lbs.			
16	61.1	62.9	64.9	66.9	69.0			
17	54.1	55.7	57.5	59.3	61.1			
18	48.3	49.7	51.3	52.9	54.5			
19	43.3	44.6	46.0	47.5	48.9			
20	39.1	40.2	41.5	42.8	44.1			
21	35.5	36.5	37.7	38.9	40.0			
22	32.3	33.2	34.3	35.4	36.5			
23	•29.6	30.4	31.4	32.4	33.4			
24	27.2	27.9	•28.8	29.8	30.7			
25	25.0	25.7	26.6	•27.4	28.3			
26	23.1	23.8	24.6	25.4	•26.1			
27	21.5	22.1	22.8	23.5	24.2			
28	19.9	20.5	21.2	21.9	22.5			
29	18.6	19.1	19.8	20.4	21.0			
30	17.4	17.9	18.5	19.0	19.6			
31	16.3	16.7	17.3	17.8	18.4			
32	15.3	15.7	16.2	16.7	17.2			
33	14.4	14.8	15.3	15.7	16.2			
34	13.5	13.9	14.4	14.8	15.3			
35	12.8	13.1	13.6	14.0	14.4			
36	12.1	12.4	12.8	13.2	13.6			
37	11.4	11.8	12.1	12.5	12.9			
38	10.8	11.1	11.5	11.9	12.1			
39	10.3	10.6	10.9	11.2	11.6			
40	9.8	10.0	10.4	10.7	11.0			

For spacings above single dot the safe loads are too great for standard connections.

Required spacing= Intensity of loading from table New intensity of loading Computed spacing from table.

Spacings for other intensities of loading may be obtained from those in tables as follows:

### SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance	STANDARD I-BEAM.								
between supports	24 Inch No. B 89.								
in feet.	80	85	90	95	100				
	lbs.	lbs.	lbs.	lbs.	lbs.				
18	57.3	59.5	61.4	63.3	65.3				
19	51.4	•53.4	•55.1	56.9	58.6				
20	46.4	48.2	49.7	•51.3	•52.9				
21	42.1	43.7	45.1	46.5	48.0				
22	38.3	39.8	41.1	42.4	43.7				
23	35.1	36.4	37.6	38.8	40.0				
24	32.2	33.5	34.5	35.6	36.7				
25	29.7	30.8	31.8	32.8	33.8				
26	27.4	28.5	29.4	30.4	31.3				
27	25.5	26.4	27.3	28.2	29.0				
28	23.7	24.6	25.4	26.2	27.0				
29	22.1	22.9	23.7	24.4	25.2				
30	20.6	21.4	22.1	22.8	23.5				
31	19.3	20.1	20.7	21.4	22.0				
32	18.1	18.8	19.4	20.0	20.7				
33	17.0	17.7	18.3	18.8	19.4				
34	16.0	16.7	17.2	17.8	18.3				
35	15.1	15.7	16.2	16.8	17.3				
36	14.3	14.9	15.4	15.8	16.3				
37	13.5	14.1	14.5	15.0	15.4				
38	12.8	13.3	13.7	14.2	14.6				
39	12.2	12.6	13.1	13.5	13.9				
40	11.6	12.0	12.4	12.8	13.2				
41	11.0	11.5	11.8	12.2	12.6				
42	10.5	10.9	11.3	11.6	12.0				
43	10.0	10.4	10.8	11.1	11.4				
44	9.6	9.9	10.3	10.6	10.9				
45	9.2	9.5	9.8	10.1	10.4				
46	8.7	9.1	9.4	9.7	10.0				
47	8.4	8.7	9.0	9.3	9.6				
48	8.0	8.3	8.6	8.9	9.2				

For spacings above single dot, the safe loads are too great for standard connections.

Spacings for other intensities of loading may be obtained from those in tables as follows:

Required spacing = Intensity of loading from table.

New intensity of loading X Computed spacing from table.

### SPACING OF CAMBRIA I-BEAMS FOR UNI-FORM LOAD OF 100 LBS. PER SQUARE FOOT.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance	SI	SPECIAL I-BEAM.					
between	24	Inch No. B 19	27.				
supports	105	110	115				
in feet.	lbs.	lbs.	lbs.				
18	77.1	79.1	81.1				
19	69.2	71.0	72.8				
20	62.5	64.1	65.7				
21	56.7	58.1	59.6				
22	51.6	53.0	54.3				
23	47.2	48.4	49.6				
24	• 43.4	• 44.5	45.6				
25	40.0	• 41.0	42.0				
26	37.0	37.9	38.8				
27	34.3	35.1	36.0				
28	31.9	32.7	33.5				
29	29.7	30.5	31.2				
30 31	27.8	28.5	29.2				
32	26.0	26.7	27.3				
	24.4	25.0	25.6				
33	22.9	23.5	24.1				
34	21.6	22.2	22.7				
35 36	20.4	20.9	21.4				
37	18.3	18.7	19.2				
38	17.3	17.7	18.2				
39	16.4	16.8	17.2				
40	15.6	16.0	16.4				
41	14.9	15.2	15.6				
42	14.2	14.5	14.9				
43	13.5	13.8	14.2				
44	12.9	13.2	13.6				
45	12.3	12.6	13.0				
46	11.8	12.1	12.4				
47	11.3	11.6	11.9				
48	10.8	ii.i	11.4				

For spacings above single dot the safe loads are too great for standard connections.

Spacings for other intensities of loading may be obtained from those in tables as follows:

Intensity of loading from table

Required spacing = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}

# MAXIMUM BENDING MOMENTS IN FOOT POUNDS FOR CAMBRIA I-BEAMS.

	Depth	Weight		Bending nent.	WIDE	Depth	Weight	Maximun	Bending nent.
Section	of	per	Foot P	ounds.	Section	of	per	Foot P	ounds.
Num- ber:	Beam,	Foot.		Fibre Stress 12 500 lbs.	Num- ber.	Beam.	Foot.		Fibre Stress 12 500 lbs.
	Тисцев.	rounus.	per Sq. In.	per sq. In.		Inches.	Pounds.	per Sq. In.	per Sq. In.
B . 5	3 "	5.5 6.5 7.5	2270 2400 2530	1770 1880	B 53	15	42 45	78530 81070	61350 63330
B 9	4	7.5	4000	1980 3130	"	"	50 55	86000 90800	67190 70940
"	ш	8.5 9.5	4270 4530	3330 3540		66	60	95730	74790
ш	"	10.5	4800	3750	B109	15	60 65	108270 113070	84580 88330
B 13	5	9.75	6400	5000	46	44	70	118000	92190
"	ш	12.25	7200	5630	ш	66	75	122930	96040
"	- 66	14.75	8130	6350	. "	"	80	127730	99790
B 17	6	12.25	9730	7600	B113	15	80 85	140270 145070	109580 113330
II	"	14.75 17.25	10670	8330	26	66	90	150000	117190
		17.20	11600	9060	"	13	95	154800	120940
B 21	7	15 17.5	13870 14930	10830 11670	u	и	100	159730	124790
66	-11	20	16130	12600	B 65	18	55 60	117870 124670	92080 97400
B 25	. 8	18	18930	14790	"	66	65	130530	101980
"	u	20.25 22.75	20000 21330	15630 16670	. "	"	70	136530	106670
"	"	25.25	22670	17710	B 73	20	65 70	156000 162670	121880 127080
B 29	g "	21 25	25200 27200	19690 21250	ш	"	75	169200	132190
"	"	30 35	30130	23540 25830	B121	20	80	195470	152710
		00	99010	20000	66	66	85	201200	157190
B 33	10	25	32530	25420	"	"	90 95	207730 214270	162290 167400
EE	#4 #4	30 35	35730 39070	27920 30520	ш	"	100	220800	172500
"	п	40	42270	33020	B 89	24	80	231870	181150
B 41	12	31.5	48000	37500	66	"	85	240930	188230
"	66	35	50670	39580	66	u	90	248670	194270
66	"	40	54670	42710	"	"	95	256530	200420
B105	12	40	59730	46670	"	"	100	264400	206560
4	4	45	63470	49580	B127	24	105	312380	244050
"	"	50	67470	52710	66	"	110	320380	250300
66	"	55	71330	55730	66	"	115	328380	256550

# MAXIMUM BENDING MOMENTS IN FOOT POUNDS FOR CAMBRIA CHANNELS.

Section	Depth	Weight		Bending lent.	Section Depth W		Weight		Maximum Bending Moment.	
Num- ber.	of Chan- nel.	per Foot.	Foot P	ounds.	Num- ber.	of Chan- nel.	per Foot.	Foot P	ounds.	
	AOL.		Fibre Stress	Fibre Stress 12 500 lbs.				Fibre Stress	Fibre Stress 12 500 lbs.	
-	Inches.	Pounds.		per Sq. In.		Inches.	Pounds.		per Sq. In.	
C 5	3	4	1470	1150	C29	9 "	13.25	14000		
	44	5	1600	1250	"	46	15	15070	11770	
"	-	6	1870	1460	"	46 W	20	18000	14060	
				4000	64	14	25	20930	16350	
C 9	4 "	5.25	2530	1980	CIOO	.40	42	AMOMO	40000	
**		6.25	2800	2190	C33	10	15	17870	13960	
44	"	7.25	3070	2400	"	"	20	20930	16350	
	-				11	4	25	24270	18960	
C13	5	6.5	4000	3130			30	27470	21460	
"	46	9	4670	3650	16	"	35	30800	24060	
ec	"	11.5	5600	4380	~		00 14		00000	
	4	293			C41	12	20.5	28530	22290	
C17	6	8	5730	4480	"	21	25	32000		
"	46	10.5	6670	5210	"	66	30	35870		
ш	46	13	7730	6040	и	66	35	39870	31150	
ш	"	15.5	8670	6770	ш	W.	40	43730	34170	
C21	7	9.75	8000	6250	C53	15	33	55600	43440	
"	"	12.25	9200	7190	u	"	35	56930		
az.	"	14.75	10400	8130	66	11	40	61730		
"	"	17.25	11470	8960	66	"	45	66670		
"	24	19.75	12670	9900	66	III	50	71600		
	1	20110	2010	0000	II.	ш	55	76530	59790	
C25	8	11.25	10800	8440			-	, 0000	55,00	
"	"	13.75	12000	9380	C65	18	45	86530	67600	
"	65	16.25	13330	10420	"	"	50	92310		
"	66	18.75	14670	11460	EE.	"	55	98070		
"	66	21.25	15870	12400	12	66	60	104190		
	1	21.20	10010	INTO		1	00	101100	OLTIO	

Distance between supports

in feet.

234

Б

1ŏ

# SAFE LOADS IN POUNDS UNIFORMLY DISTRIBUTED FOR CAMBRIA ANGLES.

### EQUAL LEGS.

# NEUTRAL AXIS PARALLEL TO EITHER LEG.

Section

2.34

per

4

290

240

200

180

200

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

1.80 lbs.

per ft.

560

280

190 160

140

1.23 lbs.

per ft.

390

190

130

110

01 10	or 16 000 pounds							
No. A	No. A 11.							
1½"								
11	5 // 16	3//						
lbs. ft.	2.86 lbs. per ft.	8.35 lbs. per ft.						
20 80 60	860 1010 580 670 430 500							

400

340

290 250

350

290

240

ð	1 90	120	100	190	1 440					
Distance	Section No. A 40.									
between			13" x 13"							
supports	1//	3 "	1//	16"	3//					
in feet.	1.44 lbs. per ft.	2.12 lbs. per ft.	2.77 lbs. per ft.	3.39 lbs. per ft.	3.99 lbs. per ft.					
2 8 4 5	530 350 260 210	770 510 380 310	990 660 500 400	1200 800 600 480	1400 940 700 560					
6 7 8	170 150 130	260 220 190	330 280 250	400 340 300 270	470 400 350					

150

Distance	1		Section	on No.	A 15.							
between		2" x 2"										
supports	1//8	3 11	1//	16	3"	7/16	1/1					
in feet.	1.65 lbs.	2.44 lbs.	3.19 lbs.	3.92 lbs.	4.7 lbs.	5.3 lbs.	6.0 lbs.					
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.					
2	690	1020	1320	1600	1870	2130	2380					
8	460	680	880	1070	1250	1420	1590					
4	340	510	660	800	940	1070	1190					
5	270	410	530	640	750	850	950					
6	230	340	440	530	620	710	790					
7	190	290	380	460	540	610	680					
8	170	250	330	400	470	530	600					
9	150	230	290	360	420	470	530					
10	130	200	260	320	370	430	480					

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{380}$  span.

### EQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



Distance	Section No. A 41										
between	$2\frac{1}{4}'' \times 2\frac{1}{4}''$										
supports	3//	1//	5//								
in feet.	2.75 lbs. per ft.	3.62 lbs. per ft.	4.5 lbs. per ft.								
2 3 4 5	1300 870 650 520	1690 1120 840 670	2060 1370 1030 820								
6 7 8 9	430 370 320 290 260	560 480 420 380 340	590 510 460 410								
11 12	240 220	310 280	370 340								

Distance		Section No. A 17.										
between		$2\frac{1}{2}'' \times 2\frac{1}{2}''$										
supports	1//	3/1	1//	5/1	3//	7/1	1/1					
in feet.	2.08 lbs.	3.07 lbs.	4.1 lbs.	5.01bs.	5.9 lbs.	6.81bs.	7.71bs.					
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.					
2	1060	1610	2100	2570	3020	3450	3860					
8	710	1080	1400	1710	2010	2300	2580					
4	530	810	1050	1290	1510	1720	1930					
5	420	650	840	1030	1210	1380	1550					
6 7	350	• 540	700	860	1010	1150	1290					
	300	460	600	730	860	990	1100					
8	260	400	530	640	760	860	970					
9	230	360	470	570	670	770	860					
10	210	320	420	510	600	690	770					
11	190	290	380	470	550	630	700					
12	170	270	350	430	500	580	640					

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{100}$  span.

### EQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



Di la latara	S	ection No. A 43	
Distance between supports in		2¾" x 2¾"	
feet.	4.5 lbs.	5.6 lbs.	6.6 lbs.
	per ft.	per ft.	perft.
2	2570	3140	3700
8	1710	2090	2460
4	1280	1570	1850
5	1030	1260	1480
6 7	860	1050	1230
	730	900	1060
8 9 10	570 510	790 700 630	920 820 740
11	470	570	670
12	430	520	620

Distance	Section No. A 19.												
between		3" x 3"											
supports	1//	5//	3//	7/16	1/1	9//							
in feet.	4.9 lbs. per ft.	6.1 lbs. per ft.	7.2 lbs. per ft.	8.3 lbs. per ft.	9.4 lbs. per ft.	10.4 lbs. per ft.							
2	3080	3770	4440	5090	5720	6320							
8	2050	2510	2960	3390	3810	4210							
4	1540	1890	2220	2540	2860	3160							
5	1230	1510	1780	2040	2290	2530							
6	1030	1260	1480	1700	1910	2110							
7	880	1080	1270	1450	1630	1810							
8	770	940	1110	1270	1430	1580							
10	630	840	990	1130	1270	1410							
	620	750	890	1020	1140	1260							
11	560	690	810	930	1040	1150							
12	510	630	740	850	950	1050							

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{380}$  span.

### EQUAL LEGS.

NEUTRAL AXIS PARALLEL TO EITHER LEG.
Safe loads below are figured for fibre stress of 16 000 pounds

1

per square inch and include weight of angle.												
D' 4				S	ectio	n No	. A 2	1.				
Distance		$3\frac{1}{2}'' \times 3\frac{1}{2}''$										
between	\frac{1}{4''}   \frac{2}{3''}   \frac{2}{4''}   \frac{1}{2}''   \frac{1}{4}''   \frac{2}{3''}   \frac{1}{42''}										7''	
supports	5.8	7.2	8.5	9.8	11.1	12.4	13.6	14.8	16.0	17.1	18.3	
in feet.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	
2	4210	5200	6140	7050	7940	8800	9630	10440	11230	12010	12760	
284	2810 2110	3470 2600	4100 3070	4700 3530	5290 3970	5860 4400	6420 4810	6960 5220	7490 5620	8000 6000	8510 6380	
5	1680	2080	2460	2820	3180	3520	3850	4180	4490	4800	5110	
6	1400	1730	2050	2350	2650	2930	3210	3480	3740	4000	4250	
7 8	1200 1050	1490 1300 ·	1760 1540	2020 1760	2270 1980	2510 2200	2750 2410	2980 2610	3210 2810	3430	3650 3190	
ğ	940	1160	1370	1570	1760	1950	2140	2320	2500	2670	2840	
10	840	1040	1230	1410	1590	1760	1930	2090	2250	2400	2550	
11	770	950	1120	1280	1440	1600	1750	1900	2040	2180	2320	
12 13	700 650	870 800	1020 950	1180 1090	1320 1220	1470 1350	1600 1480	1740 1610	1870 1730	2000 1850	2130 1960	
14	600	740	880	1010	1130	1260	1380	1490	1610	1720	1820	
15	560	600	820	940	1060	1170	1280	1390	1500	1600	1700	
16	530	650	770	RRY	900	1100	1200	1310	1400	1500	1600	

				Sec	tion 1	No. A	23.			
Distance					4":	x 4"				
between	16"	3"	7 "	1"	16"	5//	11/1	3"	13"	7"
in feet.	lbs. per ft.	9.8 lbs. per ft.	11.3 lbs. per ft.	12.8 lbs. per ft.	lbs. per ft.	15.7 lbs. per ft.	17.1 lbs. per ft.	18.5 lbs. per ft.	19.9 lbs. per ft.	21.2 lbs. per ft.
2	6870	8120	9340	10530	11690	12810	13910	14980	16030	17060
8	4580	5420	6230	7020 5270	7790	8540	9270	9990	10690	11370
2 2 4 5	3430 2750	4060 3250	4670 3740	4210	5840 4670	6410 5130	6960 5560	7490 5990	8020 6410	8530 6820
	2100				-	196	0000	0000	0220	0000
6	2290	2710	3120	3510	3900	4270	4640	4990	5340	5690
7	1960	2320	2670	3010	3340	3660	3970	4280	4580	4870
ä	1720 1530	2030 1810	2340 2080	2630 2340	2920 2600	3200 2850	3480	3740 3330	4010 3560	4260 3790
6 7 8 9 10	1370	1620	1870	2110	2340	2560	2780	3000	3210	3410
11	1250	1480	1700	1910	2130	2330	2530	2720	2910	3100
12	1140	1350	1560	1760	1950	2140	2320	2500	2670	2840
13	1060	1250	1440	1620	1800	1970	2140	2300	2470	2620
14	980	1160	1340	1500	1670	1830	1990	2140	2290	2440
15	920	1080	1250	1400	1560	1710	1860	2000	2140	2270
16	860	1020	1170	1320	1460	1600	1740	1870	2000	2130

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{380}$  span.

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# SAFE LOADS IN POUNDS UNIFORMLY DIS-TRIBUTED FOR CAMBRIA ANGLES.

### EQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

Distance				2	ectio	n No.	. A 4	1.				
between					E	5" x 5	"					
supports	3/	'	7 "	1 1	"	9//	1	5//	116	"		3//
in feet.	12.3		4.3 lbs			18.1 lt	8. 20	0.0 lbs.	21.8			.6 lbs.
	per f		per ft.	per	ft.	per ft.	1	er ft.	per f		p	er ft.
2 3 4 5 6 7 8 9 10	1291		14900		330	18720		20570	2238			1160
3	861		9930		220	12480		13710	1492			3110
5	646 517		7450 5960		110	9360 7490		10280 8230	1119 895			2080 9660
6	431	ŏ	4960		810	6240		6860	746	30		3050
7	369	00	4260		810	5350		5880	639			3900
8	323		3720		210	4680		5140	560			6040
10	287 258		3310 2980		740	4160 3740		4570 4110	497			5370 4830
11	235		2710		060	3400		3740	407			1390
12	215	50	2480	2	800	3120		3430	373	30		1030
	199	90	2290	2	590	2880		3160	344	_		3720
14 15	185		2130		400	2670		2940	320			3450
15	172		1990 1860		240	2500 2340		2740 2570	298 280			3220 3020
16 17	161 152		1750		080	2200		2420	263			2840
18	144		1660		870	2080		2290	249			2680
	1			9	ectio	n No	AG	7				
Distance												
between						$3'' \times 6'$	_					
sup-	3/1	18"	1"	16"	5"	118"	3"	13"	7"		5"	1"
ports in feet,	14.9	17.2	19.6	21.9	24.2	26.5	28.7		33.1	35		37.4
TIT 100P	lbs. per ft.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lb		lbs. per ft.
- 0	18820	21720	per ft. 24610	27420	per ft.	per ft. 32880	35540		40720	432		45720
2	12550	14480	16400	18280	20120	21920	23690		27150	288		30480
4	9410	10860	12300	13710	15090	16440	17770	19080	20360	216	20	22860
5	7530	8690	9840	10970	12070	13150	14220		16290	173		18290
6	6270 5380	7240 6210	8200 7030	9140 7830	10060 8620	10960 9390	11850 10150		13570 11630	144		15240 13060
á	4700	5430	6150	6850	7540	8220	8890		10180	108		11430
28456789	4180	4830	5470	6090	6710	7310	7900	8480	9050	96	10	10160
10 11	3760	4340	4920	5480	6030	6580	7110		8140	86		9140
11	3420	3950	4470	4990	5490	5980	6460		7400		60	8310 7620
12 13	3140 2900	3620 3340	4100 3790	4570 4220	5030 4640	5480 5060	5920 5470	6360	6790 6260	66	10	7020
14	2800	2100	2500	2000	4910	4700	5000		E000		00	6590

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = 380 span.

# EQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



	Section No. A 35.												
Distance between		8" x 8"											
sup- ports	12"	9"	5"	116"	3"	18"	7"	15"	1"	116"	11/1"		
in feet.	26.4	29.6	32.7	25.8	38.9	42.0	45.0	48.1	51.0	54.0	56.9		
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.		
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.		
. 5	22310	24910	27470	30000	32490	34950	37370	39760	42120	44450	46750		
	17850	19920	21980	24000	25990	27960	29900	31810	33700	35560	37400		
6	14880	16600	18310	20000	21660	23300	24920	26510	28080	29630	31160		
7	.12750	14230	15700	17140	18570	19970	21360	22720	24070	25400	26710		
8	11160	12450	13740	15000	16250	17480	18690	19880	21060	22220	23370		
9	9920	11070	12210	13330	14440	15530	16610	17670	18720	19760	20780		
10	8930	9960	10990	12000	13000	13980	14950	15910	16850	17780	18700		
11	8110	9060	9990	10910	11820	12710	13590	14460	15320	16160	17000		
12	7440	8300	9160	10000	10830	11650	12460	13250	14040	14820	15580		
13	6870	7660	8450	9230	10000	10750	11500	12240	12960	13680	14380		
14	6380	7120	7850	8570	9280	9990	10680	11360	12030	12700	13360		
15	5950	6640	7330	8000	8660	9320	9970	10600	11230	11850	12470		
16	5580	6230	6870	7500	8120	8740	9340	9940	10530	11110	11690		
17	5250	5860	6460	7060	7650	8220	8790	9360	9910	10460	11000		
18	4960	5530	6100	6670	7220	7770	8310	8840	9360	9880	10390		
19	4700	5240	5780	6320	6840	7360	7870	8370	8870	9360	9840		
20	4460	4980	5490	6000	6500	6990	7470	7950	8420	8890	9850		
21	4250	4740	5230	5710	6190	6660	7120	7570	8020	8470	8900		
22	4060	4530	4990	5450	5910	6350	6800	7230	7660	8080	8500		
23	3880	4330	4780	5220	5650	6080	6500	6920	7330	7730	8130		
24	3720	4150	4580	5000	5420	5830	6230	6630	7020	7410	7790		
25	3570	2980	4400	4800	5200	5590	5980	6360	6740	7110	7480		
26 27 28 29 30	3430 3310 3190 3080 2980	3690 3560 3440 3320	4230 4070 3920 3790 3660	4620 4440 4290 4140 4000	5000 4810 4640 4480 4330	5380 5180 4990 4820 4660	5750 5540 5340 5160 4980	5890 5680 5480 5300	6480 6240 6020 5810 5620	6840 6590 6350 6130 5930	7190 6930 6680 6450 6230		

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{340}$  span.

### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

		Sect	ion :	No.	A 91.		1	Secti	on I	To. A	129	
Distance			21/1	x 2"					3":	x 2"		
between	3 //	1//	5/1	3//	7 "	1/1	3 "	1"	5/1	3//	7 11	1/1
supports		3.62	4.5	5.3	6.1	6.8	3.07	4.1	5.0	5.9	6.8	7.7
in feet.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs. per	lbs. per	lbs. per	lbs. per	lbs. per	lbs. per	lbs. per
	foot.	foot.	foot.	foot.	foot.	foot.	foot.	foot.	foot.	foot.	foot.	foot.
23	1050	1360	1650	1930	2200	2460	1070	1390	1690	1980	2260	2530
4	700 520	900 680	1100 830	1290 970	1470 1100	1640 1230	710 530	920 690	1120 840	1320	1510 1130	1690 1260
5	420	540	660	770	880	990	430	550	670	790	900	1010
В	350	450	550	640	730	820	360	460	560	660	750	840
7	300	390	470	550	630 550	700 620	310 270	400 350	480 420	570 500	850 560	720 680
7 8 9	260 230	340 290	410 360	480 420	480	540	240	310	370	440	500	560
10	210	260	330	380	430	490	210	280	340	400	450	510
11 12	190 170	240 220	300 270	340 320	390 360	440 400	190 180	250 230	310 280	360 330	410	400 420

Distance		Section No. A 93.											
between		3" x 2½"											
supports	1//	5//	3" x 2½"  "" 3" 76" ½"  "" 8" 76" ½"  "" 8.5 1bs. per ft. per ft. per ft.  100 3100 3540 3970 100 2060 2360 2650 100 1550 1770 1980 100 1240 1420 1590 100 1030 1180 1320 100 600 790 880 100 600 790 880 100 620 710 790 100 560 560 540 720										
in feet.	4.5 lbs. per ft.	5.6 lbs. per ft.				9.5 lbs. per ft.							
2 3 4 5	2160 1440 1080 860	2640 1760 1320 1050	2060 1550	2360 1770	2650 1980	4380 2920 2190 1750							
6 7 8	720 620 540	880 750 660	880	1010	1130	1460 1250 1100							
8 9 10	480 430	590 530	690	790	880	970 880							
11 12	390 360	480 440				800 730							

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span.

### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



Distance		8	Section N	To. A 95.							
between		$3\frac{1}{2}$ " x $2\frac{1}{2}$ "									
supports	1//	16	3//	7//	1/1	16"					
in feet.	d.9 lbs. per ft.	6.1 lbs. per ft.	7.2 lbs. per ft.	8.3 lbs. per ft.	9.4 lbs. per ft.	lbs. per ft.					
2 3 4 5	2200 1460 1100 880	2690 1790 1340 1080	3160 2110 1580 / 1260	3610 2410 1810 1450	4050 2700 2030 1620	4480 2990 2240 1790					
6 7 8 9	730 630 550 490 440	900 770 670 600 540	1050 900 790 700 630	1200 1030 900 800 720	1350 1160 1010 900 810	1490 1280 1120 1000 900					
11 12	400 370	490 450	570 530	660 600	740 680	810 750					

Section No. A 97.										
	3½" x 3"									
1//	16"	3"	16"	1/1	16"	5//	16"	3//	13"	7''
5.4 lbs	6.6 lbs.	7.9 lbs.	9.1 lbs.	10.2 lbs.	11.4 lbs.	12.5 lbs.	13.6 lbs.	14.7 lbs.	15.8 lbs.	16.8 lbs.
per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.
4160	3850 2570	4540 3030	5200 3470	5840 3900	6460	7070	7660	8230 5490	8790 5880	9350 6230
2080 1660	1930 1540	2270 1820	2600 2080	2920 2340	3230 2590	3530 2830	3830 3060	4120 3290	4400 3520	4670 3740
1390 1190	1280 1100	1510 1300	1730 1490	1950 1670	2150 1850	2360 2020	2550 2190	2740 2350	2930 2510	3120 2670
920 830	860 770	1010 910	1160 1040	1300 1170	1440 1290	1570 1410	1700 1530	1830 1650	1950 1760	2340 2080 1870
750 690 640	700 640 590 550	830 760 700 650	950 870 800	1060 970 900	1180 1080 990	1290 1180 1090	1390 1280 1180	1500 1370 1270	1600 1470 1350	1700 1560 1440 1340
	5.4 lbs per ft. 4160 2770 2080 1660 1390 1190 1040 920 830 750 690	5.4 6.6 lbs. per ft. 160 3850 1540 1540 1540 1540 1540 1540 1540 15	5.4 6.6 7.9 lbs. lbs. per ft.	1	Total   Tota	3½" x  \[ \frac{1}{4}" \] \[ \frac{1}{16}" \] \[ \frac{3}{8}" \] \[ \frac{7}{16}" \] \[ \frac{2}{3}" \] \[ \frac{1}{16}" \] \[ \frac{1}{2}" \] \[ \frac{1}{16}" \] \[ \frac{1}{2}" \] \[ \frac{1}{16}" \] \[ \	3½" x 3"   3½" x 3" x 3"   3½" x 3"	1	3½" x 3"   3"   3"   3"   3"   3"   3"   3	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{380}$  span.

### UNEQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



				Sec	tion l	No. A	99.					
Distance		4" x 3"										
between	5"	3''	7 "	1/1	9 "	5"	11 "	3"	18"	7''		
in feet.	7.2	8.5	9.8	11.1	12.4	13.6	14.8	16.0	17.1	18.3		
	lbs.											
	per ft.											
2 2 2 3 4 5	3920 2610 1960 1570	4620 3080 2310 1850	5290 3530 2650 2120	5950 3960 2970 2380	6580 4390 3290 2630	7200 4800 3600 2880	7810 5200 3900 3120	8400 5000 4200 3360	8980 5980 4490 3590	9550 6360 4770 3820		
6	1310	1540	1760	1980	2190	2400	2600	2800	2990	3180		
7	1120	1320	1510	1700	1880	2060	2230	2400	2560	2730		
8	980	1150	1320	1490	1650	1800	1950	2100	2240	2390		
9	780	1030	1180	1320	1460	1600	1730	1870	1990	2120		
10		920	1060	1190	1320	1440	1560	1680	1800	1910		
11	710	\$40	980	1080	1200	1310	1420	1530	1630	1740		
12	650	770	880	990	1100	1200	1300	1400	1500	1590		
18	600	710	810	910	1010	1110	1200	1290	1380	1470		
14	560	660	760	850	940	1030	1120	1200	1280	1360		

	Section No. A 131.										
Distance between	4" x 3½"										
supports	5 '' 16	3"	7/1	1/2"	16"	5"	11''				
in feet.	7.7 lbs. per ft.	9.1 lbs. per ft.	10.6 lbs. per ft.	11.9 lbs. per ft.	13.3 lbs. per ft.	14.7 lbs. per ft.	16.0 lbs. per ft.				
2345	5300 2530 2650 2120	6260 4170 3130 2500	7190 4790 3590 2870	8090 5390 4040 3240	8970 5980 4480 3590	9760 6510 4880 3900	10650 7100 5320 4260				
6 7 8 9	1770 1510 1320 1180 1060	2090 1790 1560 1390 1250	2400 2050 1800 1600 1440	2700 2310 2020 1800 1620	2990 2560 2240 1990 1790	3250 2790 2440 2170	2550 3040 2660 2370 2130				
11 12 18 14	960 880 820 760	1140 1040 960 890	1310 1200 1110 1030	1470 1350 1240 1160	1630 1490 1380 1280	1770 1630 1500 1390	1940 1770 1640 1520				

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{340}$  span.

### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



	Section No. A 101.										
Distance					5" 3	3"					
between supports	16"	3"	16"	1/1	16"	5"	116"	3"	13"	7''	
in feet.	8.2 lbs. per ft.	9.8 lbs. per ft.	11.3 lbs. per ft.	12.8 lbs. per ft.	14.3 lbs. per ft.	15.7 lbs. per ft.	17.1 lbs. per ft.	18.5 lbs. per ft.	19.9 lbs. per ft.	21.2 lbs. per ft.	
28445	4020 2680 2010 1610	4740 3160 2370 1900	5430 3620 2720 2170	6110 4070 3060 2440	6770 4510 3380 2710	7410 4940 3710 2960	8040 5360 4020 3220	8660 5770 4330 3460	9270 6180 4630 3710	9870 6580 4940 3950	
6 7 8 9	1340 1150 1000 890	1580 1350 1180 1050	1810 1550 1360 1210	2040 1750 1530 1360	2260 1930 1690 1500	2470 2120 1850	2680 2300 2010 1790	2890 2470 2160 1920	3090 2650 2320 2060	3290 2820 2470 2190	
10	800	950	1090	1220	1350	1480	1610	1730	1850	1970	
11 12 13 14	730 670 620 570	880 790 730 689	910 910 840 780	1110 1020 940 870	1230 1130 1040 970	1350 1240 1140 1060	1460 1340 1240 1150	1570 1440 1330 1240	1690 1540 1430 1820	1790 1650 1520 1410	

Distance				Se	ection	No.	A 10	3.			
between		5" x·3½"									
sup-	16"	3"	16"	1/1	16"	8"	116"	3"	18"	₹"	15"
ports in feet,	8.7	10.4	12.0	13.6	15.2			19.8	21.8	22.7	24.2
111 1001.	lbs. per ft.										
0	5450	0.100	7400	pape	0000	10110	10000	11000	10050	13450	14270
2345	3630	6430 4290	7400 4930	8320 5550	9230 6150	10110 6740	10980 7320	11820 7880	12650 8430	8970	9510
4 5	2720 2180	3220 2570	3700 2960	4160 3330	4610 3690	5060 4050	5490 4390	5910 4730	6330 5060	6730 5380	7130 5710
						-					-
7	1820 1560	2140 1840	2470 2110	2770 2380	3080 2640	3370 2890	3660 3140	3940 3380	4220 3610	4490 3850	4760 4080
6789	1360 1210	1610	1850	2080	2310	2530	2740	2960 2630	3160 2810	3370 2990	3570 3170
10	1090	1430 1290	1640 1480	1850 1660	2050 1850	2250	2440	2360	2530	2690	2850
770	1000		1200	1000	1000	210210	2200				
11	990 910	1170 1070	1340 1230	1510 1390	1680 1540	1840 1690	2000 1830	2150 1970	2300 2110	2450 2240	2590 2380
18	840	990	1140	1280	1420	1560	1690	1820	1950	2070	2190
14	780	920	1060	1190	1320	1440	1570	1690	1810	1920	2040

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{3}$  span.

## UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

	Section No. A 135.									
Distance between			5":	x 4"						
supports in feet.	3/1 11.0 lbs. per ft.	12.8 lbs. per ft.	14.5 lbs. per ft.	16.2 lbs. per ft.	5/' 17.8 lbs. per ft.	11/1/ 19.5 lbs. per ft.				
2 3 4 5	8370 5580 4180 3350	9630 6420 4810 3850	10860 7240 5430 4340	12050 8030 6030 4820	13220 8810 6610 5290	14360 9570 7180 5740				
6 7 8 9 10	2790 2390 2090 1860 1670	3210 2750 2410 2140 1930	3620 3100 2710 2410 2170	4020 3440 3010 2680 2410	4410 3780 3300 2040 2610	4790 4100 3590 3190 2870				
11 19 18 14 15	1520 1390 1290 1200 1120	1750 1600 1480 1380 1280	1970 1810 1670 1550 1450	2190 2010 1850 1720 1610	2400 2200 2030 1890 1760	2610 2390 2210 2050 1910				
16	1050	1200	1360	1510	1650	1790				

Distance				S	ection	n No.	A 10	)5.				
between		6" x 3½"										
sup-	3//	16"	1 2"	16"	5"	11/1	3"	13"	7"	15"	1"	
ports in feet.	11.7 lbs. per ft.	13.5 lbs. per ft.	15.3 lbs. per ft.	17.1 lbs. per ft.	18.9 lbs. per ft.	20.6 lbs. per ft.	lbs.	24.0 lbs. per ft.	lbs.	27.3 lbs. per ft.	28.9 lbs. per ft.	
2345	6570 4380 3280 2630	7550 5030 3770 3020	8500 5670 4250 3400	9430 6290 4720 3770	10340 6890 5170 4140	11230 7480 5610 4490	12100 8070 6050 4840	12960 8640 6480 5180	13800 9200 6900 5520	14640 9760 7320 5850	15470 10310 7730 6190	
6 7 8 9	2190 1880 1640 1460 1310	2520 2160 1890 1680 1510	2830 2430 2120 1890 1700	3140 2690 2360 2100 1890	3450 2950 2580 2300 2070	3740 3210 2810 2490 2250	4030 3460 3020 2690 2420	4320 3700 3240 2880 2590	4600 3940 3450 3070 2760	4880 4180 3660 3250 2930	5160 4420 3870 3440 3090	
11 12 18 14	1190 1090 1010 940	1370 1260 1160 1080	1550 1420 1310 1210	1710 1570 1450 1350	1880 1720 1590 1480	2040 1870 1730 1600	2200 2020 1860 1730	2360 2160 1990 1850	2510 2300 2120 1970	2660 2440 2250 2090	2810 2580 2380 2210	

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span.

# SAFE LOADS IN POUNDS UNIFORMLY DIS-TRIBUTED FOR CAMBRIA ANGLES.

## UNEQUAL LEGS.

Section No. A 107.

NEUTRAL AXIS PARALLEL TO LONG LEG. Safe loads below are figured for fibre stress of 16 000 pounds

per square inch and include weight of angle.

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = 300 span.

### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



		Section No. A 112.											
Distance between		8" x 6"											
supports in feet.	1''	9/1	8"	118"	3''	13"	7''	15"	1"				
	23.0	25.7	28.5	31.2	33.8	36.5	39.1	41.7	44.2				
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.				
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.				
4 5	12770	14230	15670	17080	18460	19830	21170	22490	23790				
	10210	11380	12530	13660	14770	15860	16930	17990	19030				
6 7 8 9	8510 7290 6380 5670 5100	9480 8130 7110 6320 5690	10440 8950 7830 6960 6260	11380 9750 8540 7590 6830	12310 10550 9230 8200 7380	13220 11336 9910 8810 7930	14110 12090 10580 9400 8460	14990 12850 11240 9990 8990	15860 13590 11390 10570 9510				
11	4640	5170	5690	6210	6710	7210	7690	8170	5650				
12	4250	4740	5220	5690	6150	6610	7050	7490	7930				
13	3920	4370	4820	5250	5680	6100	6519	8020	7320				
14	3640	4060	4470	4880	5270	5660	6040	6420	6790				
15	3400	3790	4170	4550	4920	5280	5640	5990	6340				
16	3190	3550	3910	4270	4610	4950	5290	5620	5940				
17	3000	3340	3680	4010	4340	4660	4980	5290	5590				
18	2830	3160	3480	3790	4100	4400	4700	4990	5280				
19 20	2680	2990	3290	3590	3880	4170	4450	4730	5000				
	2550	2840	3130	3410	3690	3960	4230	4490	4750				
21	2430	2710	2980	3250	3510	3770	4030	4280	4530				
22	2320	2580	2840	3100	3350	3600	3840	4090	4320				
23	2220	2470	2720	2970	3210	3440	2680	3910	4130				
24	2120	2370	2610	2840	3070	3300	3520	3740	8900				

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{380}$  span.

## UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



		S	ection :	No. A 91					
Distance between	2½" x 2"								
supports in	3/1	1"	5//	3''	7/16	1/1			
feet.	2.75 lbs. per ft.	3.62 lbs. per ft.	4.5 lbs. per ft.	5.3 lbs. per ft.	6.1 lbs. per ft.	6.8 lbs. per ft.			
2 3 4 5	1560 1040 780 620	2030 1360 1020 810	2490 1660 1240 990	2920 1940 1460 1170	3330 2220 1660 1330	3730 2480 1860 1490			
6	520	0.80	830	970	1110	1240			
7	450	580	710	830	950	1070			
10	390 350 310	510 450 410	620 550 500	730 650 580	830 740 670	930 830 750			
11 12	280 260	370 340	450 410	530 490	610 560	680 620			

	Section No. A 129.									
Distance between										
supports in	3/1	1/1	5/1	3"	7 16	1/1				
feet.	3.07 lbs.	4.1 lbs.	5.0 lbs.	5.9 lbs.	6.8 lbs.	7.7 lbs.				
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.				
234455	2210	2890	3540	4170	4770	5350				
	1470	1930	2360	2780	3180	3570				
	1110	1440	1770	2080	2380	2670				
	880	1160	1420	1670	1910	2140				
6 7 8	740	960	1180	1390	1590	1780				
	630	830	1010	1190	1360	1530				
	550	720	890	1040	1190	1340				
10	490	640	790	930	1060	1190				
	440	580	710	830	950	1070				
11 12	400	530	640	760	870	970				
	370	480	590	690	800	890				

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span.

# UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO SHORT LEG.

skiem Me

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

		2	section .	No. A 93						
Distance between			3":	x 2½"						
supports in	1//	5/1	3//	7/16	1''	9//				
feet.	4.5 lbs.	5.6 lbs.	6.6 lbs.	7.6 lbs.	8.5 lbs.	9.5 lbs.				
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.				
2	2990	3670	4320	4950	5560	6140				
3	2000	2450	2880	3300	3700	4000				
4	1500	1840	2160	2470	2780	3070				
5	1200	1470	1730	1980	2220	2460				
6 7	1000	1220	1440	1650	1850	2050				
	860	1050	1230	1410	1590	1760				
8	750	920	1080	1240	1390	1540				
10	670	820	960	1100	1230	1360				
	600	730	860	900	1110	1230				
11	540	670	790	900	1010	1120				
12	500	610	720	820	930	1020				
13	400	560	660	760	850	940				
14	430	520	620	710	790	880				
	Section No. A 95.									
Distance	$3\frac{1}{2}$ " x $2\frac{1}{2}$ "									
between	1//	5//	3//	7/1	1//	9//				
in feet	4.9	6.1	7.2	8.3	9.4	10.4				
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.				
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.				
2	4020	4940	5830	6690	7530	8330				
3	2680	3300	3890	4460	5020	5560				
4	2010	2470	2920	3350	3760	4170				
5	1610	1980	2330	2680	3010	3330				
6789	1340	1650	1940	2230	2510	2780				
	1150	1410	1670	1910	2150	2380				
	1010	1240	1460	1670	1880	2080				
	890	1100	1300	1490	1670	1850				
10	800	990	1170	1340	1510	1670				
11	730	900	1060	1220	1370	1520				
12	670	820	970	1120	1250	1390				

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{180}$  span.

1910 2030

# SAFE LOADS IN POUNDS UNIFORMLY DIS-TRIBUTED FOR CAMBRIA ANGLES.

### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

		Section No. A 97.										
Distance					3	1/1 X 3	3′′					
between	1"	16"	3"	7/1	1/1	16"	5//	116"	3//	13"	7"	
in feet.	5.4 lbs. per ft.	6.6 lbs. per ft.	7.9 lbs. per ft.	9.1 lbs. per ft.	10.2 lbs. per ft.	11.4 lbs. per ft.	12.5 lbs. per ft.	13.6 lbs. per ft.	14.7 lbs. per ft.	15.8 lbs. per ft.	16.8 lbs. per ft.	
2845	3090 2060 1550 1240	5090 3390 2540 2040	6010 4000 3000 2400	0890 4600 3450 2760	7750 5170 3880 3100	8590 5730 4290 3440	9400 6270 4700 3760	10190 6790 5090 4080	10960 7300 5480 4380	11710 7800 5850 4680	12440 8290 6220 4980	
6 7 8 9	1030 880 770 690	1700 1450 1270 1130	2000 1720 1500 1330 1200	2300 1970 1720 1530 1380	2580 2220 1940 1720 1550	2860 2450 2150 1910 1720	3130 2690 2350 2090 1880	3400 2910 2550 2260 2040	3650 3130 2740 2430 2190	3900 3340 2930 2600 2340	4150 3550 3110 2760 2490	
11 12 18 14 15	560 520 480 440 410	930 850 780 730 680	1090 1000 920 860 800	1250 1150 1060 980 920	1410 1290 1190 1110 1030	1560 1430 1320 1230 1150	1710 1570 1450 1340 1250	1850 1700 1570 1460 1360	1900 1830 1690 1570 1400	2130 1950 1800 1670 1560	2260 2070 1910 1780 1660	
16	390	640	750	860	970	1070	1180	1270	1370	1460	1550	
					Sect	tion l	No. A	99.				
Dista			- 1-			-	x 3"					
betw		5"	3''	7 "	1/1	9"	5"	116"	3"	13"	7"	
in fo		7.2 lbs. per ft.	8.5 lbs. per ft.	9.8 lbs. per ft.	11.1 lbs. per ft.	12.4 lbs. per ft.	13.6 lbs. per ft.	14.8 lbs. per ft.	16.0 lbs. per ft.	17.1 lbs. per ft.	18.3 lbs. per ft.	
	8	6580 4390 3290 2630	7780 5180 3890 3110	8940 5960 4470 3580	10070 6710 5040 4030	11170 7450 5590 4470	12240 8160 6120 4900	13280 8860 6640 5310	14300 9530 7150 5720	15290 10190 7650 6120	16260 10840 8130 6500	
1	8	2190 1880 1640 1460 1320	2500 2220 1940 1730 1560	2080 2550 2240 1990 1790	2880 2520 2240 2010	3720 3190 2790 2480 2230	4080 3500 3060 2720 2450	4430 3800 3320 2950 2660	4770 4090 3580 3180 2860	5100 4370 3820 3400 3060	5420 4650 4060 3610 3250	

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings = 380 span.

NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

		,	Section	n No.	A 131.		
Distance between				4" x 3½'	,		
supports in	16"	3"	7/1	1/1	9//	5"	110"
feet.	7.7 lbs. per ft.	9.1 lbs. per ft.	10.6 lbs. per ft.	11.9 lbs. per ft.	13.3 lbs. per ft.	14.7 lbs. per ft.	16.0 lbs. per ft.
2 8 4 5	6740 4490 3370 2690	7970 5310 3980 3190	9160 6110 4580 3660	10320 6880 5160 4130	11450 7640 5730 4580	12550 8370 8280 5020	13630 9080 6810 5450
6 7 8 9	2250 1920 1680 1500 1350	2660 2280 1990 1770 1590	3050 2620 2290 2040 1830	3440 2950 2580 2290 2060	3820 3270 2860 2550 2290	4180 3590 3140 2790 2510	4540 3890 3410 3030 2730
11 12 18 14 15	1220 1120 1040 960 900	1330 1230 1140 1060	1670 1530 1410 1310 1220	1880 1720 1590 1470 1380	2080 1910 1760 1640 1530	2280 2090 1930 1790 1670	2480 2270 2100 1950 1820
16	840	1000	1150	1290	1430	1570	1700

	Section No. A 101.													
Distance		5" x 3"												
between	5 "	3//	7/1	1/1	9 "	5//	11/1	3"	13"	7"				
supports in feet.	lbs. per ft.	9.8 lbs. per ft.	lbs. per ft.	12.8 lbs. per ft.	14.3 lbs. per ft.	15.7 lbs. per ft.	17.1 lbs. per ft.	18.5 lbs. per ft.	19.9 lbs. per ft.	21.2 lbs. per ft.				
2845	10060 6710 5030	11920 7950 5960	13740 9160 6870	15510 10340 7760	17240 11490 8620	18930 12620 9470	20580 13720 10290	22190 14790 11100	23770 15850 11880	25310 16870 12660				
	4020	4770	5500	6210	6900	7570	8230	8880	9510	10120				
6 7 8 9 10	3350 2870 2520 2240 2010	3970 3410 2980 2650 2380	4580 3930 3440 3050 2750	5170 4430 3880 3450 3100	5750 4930 4310 3830 3450	6310 5410 4730 4210 3790	5860 5880 5140 4570 4120	7400 6340 5550 4930 4440	7920 6790 5940 5280 4750	8440 7230 6330 5620 5060				
11 12	1830 1680	2170 1990	2500 2290	2820 2590	3130 2870	3440 3160	3740 3436	4030 3700	4320 3960	4600 4220				
18	1550	1830	2110	2390	2650	2910	3170	3410	3660	3890				
14 15	1440 1340	1700 1590	1960 1830	2220 2070	2460 2300	2700 2520	2940 2740	3170 2960	3400 3170	3620 3370				
16 17 18	1260 1180 1120	1490 1400 1330	1720 1620 1530	1940 1830 1720	2160 2030 1920	2370 2230 2100	2570 2420 2290	2770 2610 2470	2970 2800 2640	3160 2980 2810				

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{3}$  span.

# UNEQUAL LEGS. NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

per squ	uare men and mende weight of angle.													
Distance		Section No. A 103.												
between		5" x 3½"												
sup-	5"	3//	16"	1//	18"	5//	18"	3//	13"	7''	15"			
ports	8.7	10.4	12.0	13.6	15.2	16.8	18.3 lbs.	19.8 lbs.	21.3	22.7 lbs.	24.2 lbs.			
in feet.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	per ft.		lbs. per ft.		per ft.			
2	10320	12240	14100	15930	17710	19450	21150	22810	24440	26030	27590			
2 3	6880	8160	9400	10620	11810	12970	14100	15210	16290	17350	18400			
4 5	5160 4130	6120 4890	7050 5840	7960 6370	8850 7080	9720 7780	10570 8460	11410 9120	12220 9780	13020	13800 11040			
	111111111111111111111111111111111111111													
8	3440	4080	4700	5310	5900	5480	7050	7600	8150	8680	9200			
7	2950 2580	3500	4030 3530	4550 3980	5060 4430	5560 4860	5290	6520 5700	6110	7440 6510	7880			
8	2290	2720	3130	3540	3940	4320	4700	5070	5430	5780	6130			
10	2060	2450	2820	3190	3540	3890	4230	4560	4890	5210	5520			
11	1880	2220	2560	2900	3220	3540	3850	4150	4440	4730	5020			
12	1720	2040	2350	2650	2950	3240	3520	3800	4070	4340	4600			
13	1590	1880	2170	2450	2720	2990	3250	3510	3760	4000	4240			
14	1470	1750	2010	2280	2530	2780	3020	3260	3490	3720	3940			
15	1380	1630	1880	2120	2360	2590	2820	3040	3260	3470	3080			
16	1290	1530	1760	1990	2210	2430	2840	2850	3050	3250	3450			
17	1210	1440	1660	1870	2080	2290	2490	2680	2880	3060	3250			
18	1150	1360	1570	1770	1970	2160	2350	2530	2720	2890	3070			

	1	S	ection N	To. A 13	5.						
Distance between	5" x 4" .										
supports in	3"	7/1	1/2"	16"	5"	118"					
feet.	11.0 lbs.	12.8 lbs.	14.5 lbs.	16.2 lbs.	17.8 lbs.	19.5 lbs.					
	per ft.										
28445	12500	14410	16280	18100	19880	21620					
	8330	9610	10850	12070	13250	14420					
	6250	7200	8140	9050	9940	10810					
	5000	5760	6510	7240	7950	8650					
6 7 8 9	4170 3570 3120 2780 2500	4800 4120 3600 3200 2880	5430 4650 4070 3620 3260	5030 5170 4520 4020 3620	6630 5680 4970 4420 3980	7210 6180 5410 4810 4320					
11	2270	2620	2960	3290	3610	3930					
12	2080	2400	2710	3020	331 <del>0</del>	3600					
18	1920	2220	2500	2780	3060	3330					
14	1790	2060	2330	2590	2840	3090					
15	1670	1920	2170	2410	2650	2880					
16	1560	1800	2030	2260	2490	2700					
17	1470	1700	1910	2130	2340	2540					
18	1390	1600	1810	2010	2210	2400					

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{340}$  span.

### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



				S	ection	n No.	A 10	5.								
Distance		6" x 3½".														
sup-	3"	7 ''	1/2"	9"	<u>8</u> "	110"	3"	13"	7"	15"	1"					
in feet.	11.7 . lbs. per #.	13.5 lbs. per ft.	15.8 lbs. per ft.	17.1 lbs. per ft.	18.9 lbs. per ft.	20.6 lbs. per ft.	22.4 lbs. per ft.	lbs.	25.7 lbs. per ft.	27.8 lbs. per ft.	28.9 lbs. per ft.					
2845	17300	19980	22600	25160	27670	30130	32550	34910	37230	39510	41630					
	11540	13320	15060	16770	18450	20090	21700	23270	24820	26340	27750					
	8650	9990	11300	12580	13840	15070	16270	17460	18620	19760	20810					
	6920	7990	9040	10060	11070	12050	13020	13960	14890	15800	16650					
6	5770	8660	7530	8390	9220	10040	10850	11640	12410	13170	13880					
7	4940	5710	6460	7190	7910	8610	9300	9970	10640	11290	11890					
8	4330	4990	5650	6290	6920	7530	8140	8730	9310	9880	10410					
9	3850	4440	5020	5590	6150	6700	7230	7760	8270	8780	9250					
10	3460	4000	4520	5030	5530	6030	6510	6980	7450	7900	8330					
11	3150	3630	4110	4570	5030	5480	5920	6350	6770	7180	7570					
12	2880	3330	3770	4190	4610	5020	5420	5820	6210	6590	8940					
13	2660	3070	3480	3870	4260	4640	5010	5370	5730	6080	6400					
14	2470	2850	3230	3590	3950	4300	4650	4990	5320	5640	5950					
15	2310	2660	3010	3350	3690	4020	4340	4850	4960	5270	5550					
16	2160	2500	2820	3150	3460	3770	4070	4360	4650	4940	5200					
17	2040	2350	2660	2960	3260	3550	3830	4110	4380	4650	4900					
18	1920	2220	2510	2800	3070	3350	3620	3880	4140	4390	4630					
19	1820	2100	2380	2650	2910	3170	3430	3680	3920	4160	4380					
20	1730	2000	2260	2520	2770	3010	3250	3400	3720	3950	4160					
21	1650	1900	2150	2400	2640	2870	3100	3320	3550	3760	3960					
22	1570	1810	2050	2290	2520	2740	2960	3170	3380	3590	3780					

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings  $= \frac{1}{340}$  span.

## UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of  $16\,000$  pounds per square inch and include weight of angle.



		Section No. A 107.													
Distance between	6" x 4"														
sup- ports	3"	7 "	₹"	9"	8"	116"	<b>3''</b>	13"	7"	15"	1"				
in feet.	12.3	14.8	16.2	18.1	20.0	21.8	23.6	25.4	27.2	28.9	30.6				
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.				
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.				
2034	17700	20430	23120	25750	28320	30850	33330	35760	38140	40480	42780				
	11800	13620	15410	17160	18880	20570	22220	23840	25430	26990	28520				
	8850	10230	11560	12870	14160	15420	16660	17880	19070	20240	21390				
	7080	8170	9250	10300	11330	12340	13330	14300	15260	16190	17110				
6	5900	6810	7710	8580	9440	10280	11110	11920	12710	13490	14260				
77	5060	5840	6600	7360	8090	8810	9520	10220	10900	11570	12220				
8	4420	5110	5780	6440	7080	7710	8330	8940	9540	10120	10700				
9	3930	4540	5140	5720	6290	6860	7410	7950	8480	9000	9510				
10	3540	4090	4620	5150	5660	6170	6670	7150	7630	8100	8560				
11	2220	3720	4200	4680	5150	5610	6060	5960	6930	7360	7780				
12	2950	3410	3850	4290	4720	5140	5550	5960	6360	6750	7130				
18	2720	3140	3560	3960	4360	4750	5130	5500	5870	6230	6580				
14	2530	2920	3300	3680	4050	4410	4760	5110	5450	5780	6110				
15	2360	2720	8080	3430	3780	4110	4440	4770	5090	5400	5700				
16	2210	2550	2890	3220	3540	3500	4170	4470	4770	5060	5350				
17	2080	2400	2720	3030	3330	3630	3920	4210	4490	4760	5030				
18	1970	2270	2570	2860	3150	3430	3700	3970	4240	4500	4750				
19	1860	2150	2430	2710	2980	3250	3510	3760	4020	4260	4500				
20	1770	2040	2310	2570	2830	3080	3330	3580	3810	4050	4280				
21	1690	1950	2200	2450	2700	2940	3170	3400	3630	3860	4070				
22	1610	1860	2100	2340	2570	2800	3030	3250	3470	3680	3890				

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{160}$  span.

## UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



	Section No. A 109.											
Distance					7" ×	31"						
between supports	7 16	1"	9"	5"	11"	3"	13''	7"	15"	1"		
in feet.	15.0	17.0	19.1	21.0	23.0	24.9	26.8	28.7	30.5	32.3		
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.		
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.		
4 B	13360	15140	16900	18570	20260	21910	23530	25110	26670	28210		
	10690	12120	13520	14850	16210	17530	18830	20090	21340	22560		
6	8910	10100	11270	12380	13510	14600	15690	16740	17780	18800		
7	7640	8650	9660	10610	11580	12520	13450	14350	15240	16120		
8	6680	7570	8450	9280	10130	10950	11770	12560	13340	14100		
9	5940	6730	7510	8250	9010	9740	10460	11160	11850	12540		
10	5840	6060	6760	7430	8100	8760	9410	10050	10670	11280		
11	450	5510	6150	6750	7370	7970	9560	9130	9700	10260		
12	4450	5050	5630	6190	6750	7390	7840	8370	8890	9400		
18	4110	4660	5200	5710	6230	6740	7240	7730	8210	8680		
14	3820	4330	4830	5310	5790	6260	6720	7180	7620	8080		
16	3560	4040	4510	4950	5400	5840	6280	6700	7110	7520		
16	3340	3790	4230	4640	5070	5480	5880	5280	6670	7050		
17	3140	3560	3980	4370	4770	5150	5540	5910	6280	8640		
18	2970	3370	3760	4130	4500	4870	5230	5580	5930	6270		
19	2810	3190	3560	3910	4270	4610	4950	5290	5620	5940		
20	2670	3030	3380	3710	4050	4380	4710	5020	5330	5640		
21	2550	2880	3220	3540	3860	4170	4480	4780	5080	5370		
22	2430	2750	3070	3380	3680	3980	4280	4570	4850	5130		
23	2320	2630	2940	3230	3520	3810	4090	4370	4640	4910		
24	2230	2520	2820	3090	3380	3650	3920	4190	4450	4700		

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{340}$  span.

### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



	Section No. A 112.													
Distance		8" x 6"												
supports	1/"	9"	5"	11"	3"	13"	7"	15"	1"					
	23.0 lbs. per ft.	25.7 lbs. per ft.	28.5 lbs. per ft.	81.2 lbs. per ft.	88.8 lbs. per ft.	36.5 lbs. per ft.	39.1 lbs. per ft.	41.7 lbs. per ft.	dd.2 lbs. per ft.					
4 5	21370 17090	23860 19090	26310 21050	28730 22980	31110 24890	33450 26760	35770 28610	38040 30430	40290 32230					
8 9 10	14250 12210 10680 9500 8550	15900 13630 11930 10600 9540	17540 15040 13150 11690 10520	19150 16410 14360 12770 11490	20740 17770 15550 13820 12440	22300 19110 16720 14860 13380	23840 20440 17880 15890 14300	25360 21740 19020 16900 15210	26860 23020 20140 17900 16110					
11 12 13 14 14	7770 7120 6570 6100 5700	8670 7950 7340 6810 6360	9570 8770 8090 7510 7010	10440 9570 8840 8200 7660	11310 10370 9570 8880 8290	12160 11150 10290 9550 8920	13000 11920 11000 10220 9540	13830 12680 11700 10870 10140	14650 13430 12390 11510 10740					
16 17 18 19 20	5340 5020 4750 4500 4270	5960 5610 5300 5020 4770	6570 6190 5840 5540 5260	7180 6760 6380 6040 5740	7770 7320 6910 6550 6220	8360 7870 7430 7040 8690	8940 8410 7950 7530 7150	9510 8950 8450 8010 7600	10070 9480 8950 8460 8050					
21 22	4070 3880	4540 4330	5010 4780	5470 5220	5920 5650	6370	6500	7240 6910	7670					
28 24 25	3710 3560 3420	4150 3970 3810	4570 4380 4210	4990 4780 4590	5410 5180 4970	5910 5570 5350	5960 5720	6610 6340 6080	7000 6710 6440					
26 27 28	3280 3160 3050	3670 3530 3410	3890 3760	4420 4250 4100	4780 4600 4440	5140 4950 4780	5500 5300 5110	5850 5630 5430	6190 5960 5750					

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{30}$  span.

### GENERAL FORMULÆ FOR FLEXURE OF BEAMS. NOTATION.

= Area of Section in square inches. = Depth of Cross Section in inches.

Length of Span in inches.
 Length of Span in feet.

p = Stress in extreme fibre of section in pounds per square inch.

X<sub>1</sub> = Distance of Center of Gravity of Section from extreme fibre in inches.

W = Total Load, in pounds, Uniformly Distributed inch. = Total Load, in pounds, Uniformly Distributed, including the Weight of

W<sub>1</sub> = Total Superimposed or Live Load, in pounds, Uniformly Distributed.
 W<sub>2</sub> = Total Weight of Beam, in pounds, Uniformly Distributed.

W. = Total Safe Load, in pounds, Uniformly Distributed.

Load, in pounds, concentrated at any point.
 Coefficient of Strength of the Tables of Properties = Safe Load, in pounds,

for a fibre stress of 16 000 pounds per square inch for a span of one foot.

= Coefficient of Strength of the Tables of Properties = Safe Load, in pounds, for a fibre stress of 12 500 pounds per square inch for a span of one foot.

D = Total Deflection of Beam, in inches, due to weight W, Dw<sub>1</sub> and D<sub>p</sub> = Deflections of Beams, in inches, due to the weights W<sub>1</sub> and P

respectively. = Coefficient of Deflection of the Tables of Properties = Deflection, in = Coefficient of Deflection of the Tables of Properties = Deflection, in span of one foot.

N' = Coefficient of Deflection of the Tables of Properties = Deflection, in inches, due to a superimposed load of 1 000 pounds, concentrated at the middle of a Beam with a span of one foot.

= Coefficient of Deflection, in inches, for fibre stress of 16 000 pounds per square inch, for any section used as a Beam subjected to its safe load

Uniformly Distributed. (See table, page 98.)

H' = Coefficient of Deflection, in inches, for fibre stress of 12 500 pounds per square inch for any section used as a Beam subjected to its safe load Uniformly Distributed. (See table, page 98.)

M = Total Bending Moment, in inch pounds, due to the Weight of Beam and

Superimposed Load.

Moment of Inertia, in inchest, Axis through Center of Gravity.

Moment of Inertia, in inchest, Axis parallel to above but not through Center of Gravity.

Distance, in inches, between these Axes.

Section Modulus in inchess.

Radius of Gyration in inches.
 Modulus of Elasticity, in pounds, per square inch (Steel = 29 000 000).

GENERAL FORMULE.  $S = \frac{I}{X_1} \qquad I_1 = I + Av^2 \qquad r = \sqrt{\frac{I}{A}}$   $M = \frac{pI}{X_1} = p \cdot S \cdot D = \frac{MX_1}{I} = \frac{M}{S} \cdot \text{ Or for Symmetrical Section } M = \frac{2pI}{d}$ For Beam supported at both ends and Uniformly Loaded:  $M = \frac{WI}{8} = \frac{(W_1 + W_2)I}{8} \cdot W = (W_1 + W_2) = \frac{8M}{I} = \frac{8pI}{IX_1} = \frac{8pS}{I}$ 

$$M = \frac{w_1}{8} = \frac{(w_1 + w_2)^2}{8}$$
  $\therefore W = (W_1 + W_2) = \frac{o_M}{1} = \frac{o_{D1}}{1X_1} = \frac{o_{D2}}{1}$ 

 $F = \frac{8pS}{1}$  where p = 16 000 pounds and 1 = 12" therefore  $F = \frac{2}{3}$  16 000 S  $F' = \frac{8pS}{r}$  where p = 12500 pounds and 1 = 12" therefore  $F' = \frac{2}{3}$  12500 S

To obtain the Safe Load for any span in feet, for fibre stress of 16 000 pounds per square inch:

 $Safe\ Load = W_s = \frac{2}{3} \frac{16\,000\,S}{L} = \frac{F}{L}$  To obtain the Safe Load for any span in feet, for fibre stress of 12 500 pounds per square inch:

Safe Load =  $W_s = \frac{2}{3} \frac{12500 \text{ S}}{I} = \frac{F'}{I}$ 

# GENERAL FORMULÆ FOR FLEXURE OF BEAMS.

(CONTINUED.)

#### DEFLECTIONS.

(1) Beam supported at both ends and Uniformly Loaded:

Deflection for Total Load = D = 
$$\frac{5}{384} \frac{\text{Wl}^3}{\text{EI}} = \frac{5}{384} \frac{(\text{Wi} + \text{W2}) \, \text{I}^8}{\text{EI}}$$

Deflection for Superimposed Load =  $Dw_1 = \frac{5}{384} \frac{W_1 l^3}{EI}$ 

(2) Beam supported at both ends with load concentrated at the middle:

. Deflection for Total Load = D = 
$$\frac{Pl^3}{48EI} + \frac{5}{384} \frac{W_1l^3}{EI}$$
  
Deflection for Superimposed Load =  $D_p = \frac{Pl^3}{48EI}$ 

(3) Beam fixed at one end, unsupported at the other, and Uniformly Loaded:

Deflection for Total Load = D = 
$$\frac{\text{Wl}^3}{8\text{EI}} = \frac{(\text{W}_1 + \text{W}_2) \ l^3}{8\text{EI}}$$

Deflection for Superimposed Load =  $Dw_1 = \frac{W_1 l^3}{8EI}$ 

(4) Beam fixed at one end, and unsupported at the other, with load concentrated at the unsupported end:

Deflection for Total Load = D = 
$$\frac{Pl^s}{3EI} + \frac{W_2l^s}{8EI}$$

Deflection for Superimposed Load =  $D_p = \frac{Pl^3}{3EI}$ 

$$N = \frac{5}{384} \frac{Wl^3}{EI} = \frac{5}{384} \frac{(W_1 + W_2)l^3}{EI}$$
, where  $W = (W_1 + W_2) = 1000$  pounds and  $l = 12^9$ 

 $N' = \frac{Pl^3}{48 El^4}$ , where P = 1000 pounds and  $l = 12^9$ 

Total Deflection, in inches, due to a Beam Uniformly Loaded for any span in feet = D =  $\frac{NWL^3}{1000} = \frac{N(W_1 + W_2)L^3}{1000}$ 

Total Deflection, in inches, due to a Superimposed Load P and the Weight of Beam W<sub>2</sub> for any span in feet = D =  $\frac{N'PL^3}{1\ 000} + \frac{NW_2L^3}{1\ 000}$ 

$$H = \frac{12}{725} L^2$$
  $H' = \frac{3}{232} L^3$ 

#### FOR SYMMETRICAL SECTIONS.

Total Deflection, in inches, for a fibre stress of 16 000 lbs. per square inch =  $D = \frac{H}{\frac{A}{a}}$ 

Total Deflection, in inches, for a fibre stress of 12 500 lbs. per square inch =  $D = \frac{H'}{a}$ 

#### FOR UNSYMMETRICAL SECTIONS.

Total Deflection, in inches, for a fibre stress of 16 000 pounds per square inch =  $D = \frac{H}{2X_1}$ 

Total Deflection, in inches, for a fibre stress of 12 500 pounds per square inch  $\mathbf{E} \mathbf{D} = \frac{\mathbf{H}'}{2N}$ 

# BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION.

W=Total Load, in lbs., uniformly distributed, ncluding the weight of beam.

W<sub>1</sub>=Total Superimposed or Live Load, in lbs., uniformly distributed, W<sub>2</sub> = Total Weight of Beam or Dead Load, in lbs., uniformly dis-

tributed. P, P<sub>1</sub>, P<sub>2</sub>, P<sub>3</sub> = Loads, in lbs., con-

centrated at any points.

 $M = Total \ Bending Moment, in inch-lbs.$   $M_{wl}, M_p = Bending Moments, in inch-lbs.$ , due to Weights  $W_1$  and P respectively.

I = Moment of Inertia, in inchest.

l=Length of Span, in inches. E=Modulus of Elasticity, in lbs. per guare inch=29 000 000 for steel.

square inch = 29 000 000 for steel.

W<sub>i</sub> = Total Safe Load, in lbs., uniformly distributed, including weight of beam = Total Safe Load of Tables.

The ordinates in diagrams give the bending moments for corresponding points on beam. For superimposed load only, make W<sub>2</sub> in formulæ equal to zero.

#### (1) Beam Supported at both ends and Uniformly Loaded.

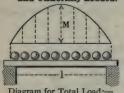


Diagram for Total Load:—
Draw parabola having  $M = \frac{Wl}{2}$ 

# Safe Superimposed Load, in lbs., uniformly distributed, $W^\prime_{\text{s}}\!=\!W_{\text{s}}\!-\!W_{\text{2}}\!.$

Maximum Bending Moment at middle of beam = 
$$M = \frac{Wl}{8} = \frac{(W_1 + W_2)l}{8}$$
.

Maximum Shear at points of support  $=\frac{W}{2}=\frac{W_1+W_2}{2}$ .

 $\begin{array}{ll} \text{Maximum deflection} & = & \frac{5}{384} & \frac{\text{Wl}^3}{\text{EI}} & = \\ & \frac{5}{384} & \frac{(\text{W}_1 + \text{W}_2) \, l^3}{\text{EI}} & = \\ & & & & & & & & & & & & & \\ \end{array}$ 

#### (2) Beam Supported at both ends with Load Concentrated at the Middle.

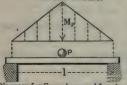


Diagram for Superimposed Load:—
Draw triangle having  $M_p = \frac{Pl}{4}$ Diagram, Dead Load, similar to Case(1)

# Safe Superimposed Load, in lbs., concentrated, $P_s = \frac{W_s - W_2}{2}$ .

Maximum Bending Moment at middle of beam =  $M = \frac{Pl}{4} + \frac{W_2l}{8}$ .

Maximum Shear at points of support =  $\frac{P + W_2}{2}$ .

Max. Deflection =  $\frac{\text{Pl}^3}{48\text{EI}} + \frac{5}{384} \frac{\text{W}_2 \text{l}^3}{\text{EI}}$ .

(3) Beam fixed at one and, Unsupported at the other and Uniformly Loaded.

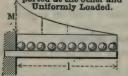


Diagram for Total Load.

Draw Parabola having  $M = \frac{Wl}{2}$ 

Safe Superimposed Load, in lbs., uniformly distributed,  $W_s' = \frac{W_s}{4} - W_2$ .

Maximum Bending Moment at point of support =  $\frac{Wl}{2} = \frac{(W_1 + W_2) l}{2}$ .

Maximum Shear at point of support = W = W 1 + VV 2.

Max. Deflection =  $\frac{Wl^3}{8EI} = \frac{(W_1 + W_2)l^3}{8EI}$ 

#### BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION.

W = Total Load, in lbs., uniformly distributed, including the weight of

W<sub>1</sub> = Total Superimposed or Live Load, in lbs., uniformly distributed. W2 = Total Weight of Beam or Dead Load, in lbs., uniformly distributed.

 $P, P_1, P_2, P_3 = Loads$ , in lbs., con-

centrated at any points.

The ordinates in diagrams give the bending moments for corresponding points on beam. For superimposed load only, make W2 in formulæ equal to zero.

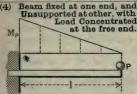


Diagram for Superimposed Load:-Draw triangle having M<sub>p</sub> = Pl. Diagram, Dead Load, similar to Case(3)

(5) Beam Supported at both ends with Load Concentrated at any point.

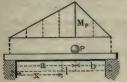


Diagram for Superimposed Load:-

Draw triangle having  $M_p = \frac{Pab}{1}$ .

Diagram, Dead Load, similar to Case(1)

(6) Beam Supported at both ends with two Symmetrical Loads.

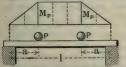


Diagram for Superimposed Load:-Draw trapezoid having  $M_p = Pa$ . Diagram, Dead Load, similar to Case(1)  $\frac{Pa}{24 \text{ EI}} \left(3l^2 - 4a^2\right) + \frac{5}{384} \frac{W_2 l^3}{\text{EI}}$ 

M = Total Bending Moment, in inch-lbs.  $M_{wl}$ ,  $M_p$  = Bending Moments, in inch-lbs., due to Weights  $W_1$  and P respectively.

I = Moment of Inertia, in inches.

I = Length of Span, in inches.

E = Modulus of Elasticity, in Ibs. per square inch = 29 000 000 for steel.

W, = Total Safe Load, in Ibs., uniformly distributed, including weight of beam = Total Safe Load of Tables.

Safe Superimposed Load, in lbs., concentrated,  $P_s = \frac{W_s - 4W_2}{8}$ .

Maximum Bending Moment at point of support =  $Pl + \frac{W_{2}l}{Q}$ .

Maximum Shear at point of support = P + W2.

Maximum Deflection =  $\frac{Pl^3}{3EI} + \frac{W_2l^3}{8EI}$ .

Safe Superimposed Load, in lbs., concentrated,  $P_a = \frac{W_a l^2 - 4a W_2 (l - a)}{Sob}$ .

Maximum Bending Moment under load  $a (2 Pb + W_{2}l - W_{2}a)$ 

Max. Shear at Sup. near  $a = \frac{Pb}{1} + \frac{W_2}{2}$ .

Max. Shear at Sup. near  $b = \frac{Pa}{1} + \frac{W_2}{2}$ . Deflection at distance x from left sup $port = \frac{1}{3EH} \left[ \frac{2al - a^2}{3} \right]^{\frac{3}{2}}$ 

$$\begin{split} & \left[ \text{Pb} + \frac{W_2}{8} \left( \sqrt{\frac{2al - a^3}{3}} + \frac{3l^3}{2al - a^2} - 2l \right) \right] \\ & x = \sqrt{\frac{2al - a^3}{3}} = \text{Distance, from left} \end{split}$$

support, of point of maximum deflection for superimposed load.

Safe Superimposed Load, in lbs., concentrated, each,  $P_s = \frac{W_s l - W_s l}{8a}$ .

Maximum Bending Moment at center of beam =  $Pa + \frac{W_1l}{g}$ .

Maximum Shear at points of support = 2P + W2

Maximum Deflection =

#### BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION.

W = Total Load, in lbs., uniformly distributed, including the weight of

W<sub>1</sub> = Total Superimposed or Live Load, in lbs., uniformly distributed. W2 = Total Weight of Beam or Dead Load, in lbs., uniformly dis-

tributed.  $P, P_1, P_2, P_3 = Loads, in lbs., con-$ 

centrated at any points.

 $M = Total \ Bending \ Moment, in inch-lbs.$   $M_{u_i}, M_p = Bending \ Moments, in inch-lbs.$ , due to Weights  $W_1$  and P respectively.  $I = Moment \ of \ Inertia, in inches^s.$ 

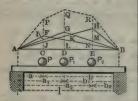
1 = Length of Span, in inches.

E = Modulus of Elasticity, in lbs., per square inch = 29 000 000 for steel.

W<sub>s</sub> = Total Safe Load, in lbs., uniformly distributed, including the weight of beam = Total Safe Load of Tables.

The ordinates in diagrams give the bending moments for corresponding points on beam. For superimposed load only, make W2 in formulæ equal to zero.

(7) Beam Supported at both ends with Loads Concentrated at various Points.



The total bending moment at any point produced by all the weights is equal to the sum of the moments at that point produced by each of the weights separately.

Diagram for Dead Load similar to Case (1).

The Maximum Bending Moment occurs at the point where the vertical shear equals zero and will be at one of the loads P, P1, or P2 depending upon their amounts and spacing if W2 is neglected.

Let R = Reaction at Left Support.

Bending Moment at P =  $M_p = Ra - \frac{W_2 a^2}{}$ 

Bending Moment at P1 =

$$M_{p1} = Ra_1 - \left[ \frac{W_2 a_1^2}{2l} + P(a_1 - a) \right]$$

Bending Moment at P2 = Mp2 = Ra2 - $\frac{W_2 a_2^2}{21} + P_1 (a_2 - a_1) + P (a_2 - a)$ 

Shear or Reaction at Left Support =  $P_2 b_2 + P_1 b_1 + Pb + \frac{W_2}{Q}$ 

Shear or Reaction at Right Support =  $\frac{P_2 a_2 + P_1 a_1 + P_2}{1} + \frac{W_2}{2}$ 

Diagram for Superimposed Load:-Draw as in Case (5) the Ordinates FC, GD and HE representing the bending moments due to loads P, P1 and P2 re. spectively. Produce FC to P, making PC = FC + IC + JC; GD to Q, making QD = GD + KD + LD; and HE to R, making RE = HE + ME + NE. Join the points A, P, Q, R and B, then the ordinates between A B and polygon A P QRB will represent the bending moments for corresponding points on beam.

#### BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION.

W = Total Load, in lbs., uniformly distributed, including the weight of beam.

W<sub>1</sub> = Total Superimposed or Live Load, in lbs., uniformly distributed. W2 = Total Weight of Beam or

tributed.

centrated at any points.

E = Modulus of Elasticity, in lbs., per Dead Load, in lbs., uniformly dissquare inch = 29 000 000 for steel. W<sub>a</sub> = Total Safe Load, in lbs., uni-P, P<sub>1</sub>, P<sub>2</sub> = Loads, in lbs., conformly distributed, including the weight of beam = Total Safe Load of Tables. The ordinates in diagrams give the bending moments for corresponding points

on beam. For superimposed load only, make W2 in formulæ equal to zero.

#### (8) Beam Fixed at both ends and Uniformly Loaded.

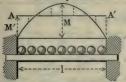


Diagram for Total Load:-Draw parabola having M = parallel to base and at a distance  $M' = \frac{Wl}{12}$ . The Vertical distances between the parabola and line A A' are the moments for corresponding points on beam.

#### (9) Beam Fixed at both ends with Load Concentrated at the Middle.



Draw triangle having M = A A' parallel to base and at a distance  $M' = \frac{Pl}{2}$ . The Vertical distances between the triangle and line A A' are the moments for corresponding points on beam.

Diagram for Dead Load similar to Case (8).

Safe Superimposed Load, in lbs., uniformly distributed,  $W'_{\delta} = \frac{3}{2} W_{\delta} - W_{2}$ .

M = Total Bending Moment in inch-lbs.

Mw1, Mp = Bending Moments, in inch-lbs.. due to Weights W1 and P respectively.

I = Moment of Inertia, in inches.

1 = Length of Span, in inches.

Distance of points of contra-flexure from supports = .21131.

Maximum Bending Moment at points of support =  $\frac{Wl}{12} = \frac{(W_1 + W_2) l}{12}$ .

Bending Moment at middle of beam =  $\frac{W1}{24} = \frac{(W_1 + W_2) 1}{24}$ 

Maximum Shear at points of support =  $W_1 + W_2$ 

W13 Maximum Deflection = 384EI  $(W_1 + W_2) 1^8$ 384EI

Safe Superimposed Load, in lbs., concentrated, Pa = Wa - 4 W2.

Distance of points of contra-flexure from supports  $= \frac{1}{2}$ l.

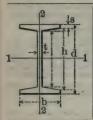
Maximum Bending Moment at points of support =  $\frac{Pl}{8} + \frac{Wil}{12}$ .

Bending Moment at middle of beam =  $\frac{P1}{8} + \frac{W_21}{24}$ .

Maximum Shear at points of support = P+W2

P[8 Maximum Deflection 192EI W213. 384EI

#### VALUES OF MOMENTS OF INERTIA FOR STAND-ARD AND CAMBRIA SECTIONS.

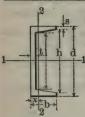


$$A = td + 2s (b-t) + \frac{(b-t)^2}{12}$$

1, Axis 
$$1-1 = \frac{bd^3}{12} - \frac{h^4-1^4}{8}$$
.

I', Axis 
$$2-2 = \frac{b^3s}{6} + \frac{1t^3}{12} + \frac{b^4-t^4}{288}$$

Slope of flange =  $g = \frac{h-1}{h-1} = \frac{1}{6}$  for standard sections. h = d - 2s.



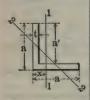
$$A = td + 2s (b-t) + \frac{(b-t)^2}{6}.$$

$$x = \left[b^9s + \frac{ht^3}{2} + \frac{(b-t)^2(b+2t)}{18}\right] \div A.$$

$$I, Axis 1 - 1 = \frac{bd^3}{12} - \frac{h^4 - l^4}{16}.$$

$$I', Axis 2 - 2 = \frac{1}{3}\left[2sb^3 + lt^3 + \frac{b^4 - t^4}{12}\right] - Ax^3.$$

Slope of flange =  $g = \frac{h-1}{2(h-1)} = \frac{1}{6}$  for standard sections. 1 = h - 2g(b - t).

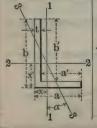


$$A = t (2a - t).$$

$$x = \frac{a^2 + at - t^2}{2(2a - t)}.$$

I, Axis 
$$1 - 1 = \frac{t(a-x)^3 + ax^3 - (a-t)(x-t)^3}{3}$$
.

I", Axis 
$$2-2 = \frac{2x^4 - 2(x-t)^4 + t\left[a - \left(2x - \frac{t}{2}\right)\right]^3}{3}$$



$$A = t (a + b - t),$$

$$x = \frac{t (2a' + b) + a'^2}{2(a' + b)}, \quad x' = \frac{t (2b' + a) + b'^2}{2(b' + a)},$$

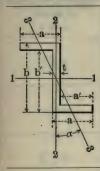
$$Tan. 2a = + \frac{[(2x - t)b(b - 2x') + (2x' - t)(a - t)(a + t - 2x)]t}{2([i' - 1])}$$

I, Axis 
$$1 - 1 = \frac{t(a-x)^{\frac{1}{2}} + bx^{\frac{3}{2}} - (b-t)(x-t)^{\frac{3}{2}}}{3}$$
.

I', Axis 
$$2 - 2 = \frac{t(b-x')^2 + ax'^2 - (a-t)(x'-t)^2}{3}$$
  
I'', Axis  $3 - 3 = \frac{I\cos^2 a - I'\sin^2 a}{\cos^2 a}$ .

I", Axis 
$$3-3=\frac{1000 \text{ at 1 sm}}{\cos 2a}$$

#### VALUES OF MOMENTS OF INERTIA FOR STAND-ARD AND CAMBRIA SECTIONS.



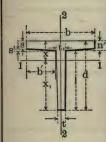
$$A = [b + 2 (a - t)] t$$

Tan. 
$$2a = + \frac{(bt - t^2)(a^2 - at)}{I - I'}$$

I, Axis 
$$1-1=\frac{ab^3-a'(b-2t)^3}{12}$$

I'. Axis 
$$2-2=\frac{b(a+a')^3-2a'^3b'-6a'a^2b'}{12}$$

I" Minimum, Axis 
$$3-3=\frac{I'\cos^2\alpha-I\sin^2\alpha}{\cos 2\alpha}$$



$$A = \frac{1(t+t_1)}{2} + n't_1 + b'(s+n').$$

$$x = \frac{3s^2(b-t_1) + 2b's' \left(s' + 3s\right) + 3t_1d^2 - 1 \left(t_1 - t\right) \left(3d - 1\right)}{6A}.$$

I, Axis 
$$1 - 1 = \frac{l^3(3t + t_1) + 4bn'^3 - 2b's'^3}{12} - A(x - n')^2$$

$$\begin{split} I', Axis \, 2 - 2 &= \frac{sb^3 + s't_1^s + lt^s}{12} + \frac{s'b'[2b'^2 + (2b' + 3t_1)^2]}{36} \\ &\quad + \frac{l \, (t_1 - t) \, [(t_1 - t)^2 + 2 \, (t_1 + 2t)^3]}{144}. \end{split}$$

e = Area of head.  $A = e + t (d - k) + (b - t) \left( a + \frac{8'}{2} \right).$ 

$$\mathbf{x} = \frac{e(2d - \mathbf{k}) + t(d - \mathbf{k})^2 + (b - t)(s^2 + ss' + \frac{s'^2}{3})}{2A}$$

$$\begin{split} \text{I, Axis } 1 - 1 &= \text{e} \left[ \frac{k^2}{16} + \left( \text{d} - \frac{2s + k}{2} \right)^2 \right] + \frac{\text{t} \; (l + s')^3}{3} \\ &+ \frac{b' \, s'^3 + 2bs^3}{6} - \text{A} \; (x - s)^2. \end{split}$$

$$I', Axis 2 - 2 = \frac{ek^2}{16} + \frac{t^3(1+s') + sb^3}{12} + \frac{s'b'[2b'^2 + (2b' + 3t)^2]}{36}$$

Sections.	Area of Section.	Distance from Neutral Axis to Extremities of Section. x and x
å	a <sup>g</sup>	$x_1 = \frac{a}{2}$
	a <sup>3</sup>	*x1 = a
	a² — aı²	$x_1 = \frac{a}{2}$
	ä³	$x_1 = \frac{a}{\sqrt{2}} = .707a$
4b **	bd	$x_1 = \frac{d}{2}$
d ×,	bd	* x1 = d
(d, d) (x) (x) (x) (x) (x) (x) (x) (x) (x) (x	bd — bıdı	$x_1 = \frac{d}{2}$
7. 7	bd	$x_1 = \frac{b d}{\sqrt{b^2 + d^3}}$ *Not the neutral axis.

Moment of Inertia.	Section Modulus.	Radius of Gyration.
I	$S = \frac{I}{x_i}.$	$r = \sqrt{\frac{I}{A}}.$
a4 12	$\frac{\mathbf{a}^8}{6}$	$\frac{a}{\sqrt{12}} = .289a$
a4 3	a <sup>2</sup> 3	$\frac{a}{\sqrt[4]{3}} = .577a$
$\frac{\mathbf{a^4 - a_1^4}}{12}$	a4 — a14 6a	$\sqrt{\frac{a^2+a_1^2}{12}}$
a4 12	$\frac{a^3}{6 \sqrt{2}} = .118a^3$	$\frac{a}{\sqrt{12}} = .289a$
bd³ 12	bd* 6	$\frac{d}{\sqrt{12}} = .289d$
bd <sup>3</sup> 3	$\frac{\mathrm{bd}^2}{3}$	$\frac{\mathrm{d}}{\sqrt[4]{3}} = .577\mathrm{d}$
bd* — bıdı* 12	$\frac{\mathbf{b}\mathbf{d}^3 - \mathbf{b}_1\mathbf{d}_1{}^3}{6\mathbf{d}}$	$\sqrt{\frac{\mathrm{bd^3 - b_1d_1^3}}{12(\mathrm{bd - b_1d_1})}}$
$\frac{b^3\mathrm{d}^3}{6\ (b^2+\mathrm{d}^2)}$	$\frac{b^2d^2}{6\sqrt{b^2+d^2}}$	$\frac{\mathrm{bd}}{\sqrt{6\left(\mathrm{b}^2+\mathrm{d}^2\right)}}$

Sections.	Area of Section.	Distance from Neutral Axis to Extremities of Section. x and x <sub>1</sub>
10 x,	bd	$x_1 = \frac{d\cos\alpha + b\sin\alpha}{2}$
×1 d	bd 2	$\mathbf{x} = \frac{\mathbf{d}}{3}$ $\mathbf{x}_1 = \frac{2\mathbf{d}}{3}$
x, d	<u>bd</u>	* x <sub>i</sub> = d
i d	$\frac{\pi  \mathrm{d}^2}{4} = .785 \mathrm{d}^2$	$x_1 = \frac{d}{2}$
	$\frac{\pi(d^2 - d_1^2)}{4} = .785 (d^3 - d_1^2)$	$x_1 = \frac{d}{2}$
X, X, X	$\frac{\pi d^2}{8} = .393d^2$	$x = \frac{2d}{3\pi} = .212d$ $x_t = \frac{(3\pi - 4) d}{6\pi} = .288d$
e-b;	$\frac{b+b_1}{2}$ · d	$\mathbf{x} = \frac{\mathbf{b} + 2\mathbf{b_1}}{\mathbf{b} + \mathbf{b_1}} \cdot \frac{\mathbf{d}}{3}$ $\mathbf{x_1} = \frac{\mathbf{b_1} + 2\mathbf{b}}{\mathbf{b} + \mathbf{b_1}} \cdot \frac{\mathbf{d}}{3}$ *Not the neutral axis.

1101221		
Moment of Inertia.	Section Modulus. $S = \frac{I}{x_i}$	Radius of Gyration. $r = \sqrt{\frac{I}{A}}$
$\frac{\text{bd}}{12} (d^2 \cos^2 a + b^2 \sin^2 a)$	$\frac{db}{6} \left( \frac{d^2 cos^2 \alpha + b^2 sin^2 \alpha}{d cos \alpha + b sin \alpha} \right)$	$\sqrt{\frac{d^2\cos^2\alpha+b^2\sin^2\alpha}{12}}$
bds 36	bd <sup>2</sup> 24	$\frac{\mathrm{d}}{\nu/\overline{18}} = .236\mathrm{d}$
Axis through base; $\frac{bd^3}{12}$ Axis through apex; $\frac{bd^3}{4}$	bd2 12 bd2 4	$\frac{\frac{d}{\sqrt[4]{6}} = .408d}{\frac{d}{\sqrt{2}} = .707d}$
$\frac{\pi d^4}{64} = .049d^4$	$\frac{\pi d^3}{32} = .098d^3$	<u>ā</u>
$\frac{\pi(d^4-d_1^4)}{64} = .049 (d^4-d_1^4)$	$\frac{\pi}{32} \frac{(d^4 - d_1^4)}{d} = .008 \frac{(d^4 - d_1^4)}{d}$	$\frac{\sqrt{d^2+d_1^2}}{4}$
$\frac{9\pi^3 - 64}{1152\pi} \cdot d^4 = .007d^4$	$\frac{9\pi^3 - 64}{192(3\pi - 4)} \cdot d^3 = .024d^3$	$\frac{\sqrt{9\pi^2 - 64}}{12\pi} \cdot d = .132d$
$\frac{b^3 + 4bb_1 + b_1^2}{36(b + b_1)} \cdot d^8$	$\frac{b^3 + 4bb_1 + b_1^2}{12(b_1 + 2b)} \cdot d^2$	$\frac{d}{6(b+b_1)}\sqrt{\frac{2(b^2+4bb_1+b_1^2)}{}}$

Sections.	Area of Section.	Distance from Neutral Axis to Extremities of Section. x and x <sub>1</sub>			
- ( ) X,	$\frac{3}{2}$ d <sup>2</sup> tan. 30° = .866d <sup>2</sup>	$x_1 = \frac{d}{2}$			
	$\frac{3}{2}$ d <sup>3</sup> tan. 30° = .866d <sup>2</sup>	$x_1 = \frac{d}{2\cos 30^\circ} = .577d$			
- ( ) <del>*</del> <del>*</del> ·	2d² tan. 22½° = .828 d²	$x_i = \frac{d}{2}$			
	$\frac{\pi  \mathrm{bd}}{4} = .785  \mathrm{bd}$	$x_1 = \frac{d}{2}$			
*, *	td + 2b' (s + n')	$x_1 = \frac{d}{2}$			
$\begin{array}{c c} \rightarrow S \leftarrow & D \leftarrow \\ \hline \uparrow & D \leftarrow \\ \hline \downarrow & D$	td + 2b' (s + n')	$x_1 = \frac{b}{2}$			
The state of the s	td + b' (s + n')	$x_1 = \frac{d}{2}$			
**	td + b' (s + n')	$x = [b^{2}s + \frac{ht^{2}}{2} + \frac{g}{3}(b-t)^{3}$ $(b+2t)] + A$ $x_{1} = b - x$			

Moment of Inertia.	Section Modulus.	Radius of Gyration.			
1	$S = \frac{I}{x_1}$	$r = \sqrt{\frac{I}{A}}$			
$\frac{A}{12} \left[ \frac{d^2 (1 + 2 \cos^2 30^\circ)}{4 \cos^2 30^\circ} \right] = .06d^4$	$\frac{A}{6} \left[ \frac{d(1+2\cos^2 30^\circ)}{4\cos^2 30^\circ} \right] = .12d^3$	$\frac{d}{4\cos 30^{\circ}} \sqrt{\frac{1+2\cos^{2}30^{\circ}}{3}}$ = .264d			
$\frac{A}{12} \left[ \frac{d^2 (1 + 2 \cos^2 30^\circ)}{4 \cos^2 30^\circ} \right] = .06d^4$	$\frac{A}{6} \left[ \frac{d (1 + 2 \cos^2 30^\circ)}{4 \cos 30^\circ} \right]$ = .104d <sup>8</sup>	$\frac{d}{4\cos 30^{\circ}} \sqrt{\frac{1+2\cos^{9}30^{\circ}}{3}}$ = .264d			
$\frac{A}{12} \left[ \frac{d^2 (1 + 2 \cos^2 22 \frac{1}{2}^{\circ})}{4 \cos^2 22 \frac{1}{2}^{\circ}} \right]$ = .055d <sup>4</sup>	$\frac{A}{6} \left[ \frac{d (1 + 2 \cos^{5} 22\frac{1}{2}^{\circ})}{4 \cos 22\frac{1}{2}^{\circ}} \right]$ = .109d <sup>3</sup>	$\frac{d}{4\cos 22\frac{1}{2}} \sqrt{\frac{1+2\cos^2 22\frac{1}{2}}{3}}$ = .257d			
$\frac{\pi  \text{bd}^3}{64} = .049 \text{bd}^3$	$\frac{\pi  \text{bd}^2}{32} = .098 \text{bd}^3$	<u>d</u>			
$ \frac{1}{1} \left[ bd^3 - \frac{1}{4g} (h^4 - l^4) \right] $ where $g = \frac{h-l}{b-t}$	2 <u>I</u>	$r = \sqrt{\frac{1}{A}}$			
$ \frac{1}{12} \left[ b^3 \left( d - h \right) + lt^3 + \frac{g}{4} \left( b^4 - t^4 \right) \right] $ where $g = \frac{h-1}{b-t}$	2 <u>I</u> b	$r = \sqrt{\frac{I}{A}}$			
$\frac{1}{1.1} \left[ bd^3 - \frac{1}{8g} (h^4 - l^4) \right]$ where $g = \frac{h-1}{2(b-t)}$	2 <u>1</u>	$r = \sqrt{\frac{I}{A}}$			
$\begin{split} \frac{1}{3} \bigg[ 2sb^3 + lt^3 + \frac{g}{2}(b^4 - t^4) \bigg] \\ &- Ax^2 \\ where \ g = \frac{h-1}{2(b-t)} \end{split}$	$\frac{1}{b-x}$	$r = \sqrt{\frac{I}{A}}$			

Sections.	Area of Section.	Distance from Neutral Axis to Extremities of Section. x and xı
* t	bd - h (b - t)	$x_i = \frac{d}{2}$
*	bd h (b t)	$x_1 = \frac{b}{2}$
1 t b 2	bd - h (b - t)	$x_i = \frac{d}{2}$
*   S   D   D   D   D   D   D   D   D   D	bd - h (b - t)	$x = \frac{2b^2e + ht^3}{2A}$ $x_1 = b - x$
t d	td + s (b - t)	$\mathbf{x}_1 = \frac{\mathbf{d}}{2}$
	bs + ht	$x = \frac{d^3t + s^2 (b - t)}{2A}$ $x_1 = d - x$
X b b b d X b d X s s s s s s s s s s s s s s s s s s	bs + ht + bis	$x = \frac{td^{2}+s^{2}(b-t)+s(b_{1}-t)(2d-s)}{2A}$ $x_{1} = d-x$
t b d h d d d d d d d d d d d d d d d d d	$bs + \frac{h(t+t_1)}{2}$	$x = \frac{3bs^2 + 3th (d+s) + h(t_1-t)(h+3s)}{6A}$ $x_1 = d - x$

Moment of Inertia.	Section Modulus. $S = \frac{I}{x_1}$	Radius of Gyration. $r = \sqrt{\frac{I}{A}}$
$\frac{\mathrm{bd^3 - h^3  (b - t)}}{12}$	$\frac{bd^3 - n^3 (b - t)}{6d}$	$\sqrt{\frac{bd^3 - h^3(b-t)}{12[bd - h(b-t)]}}$
2sb <sup>3</sup> + ht <sup>3</sup> 12	2sb <sup>2</sup> + ht <sup>2</sup> 6b	$\sqrt{\frac{2sb^3+ht^3}{12[bd-h(b-t)]}}$
$\frac{\mathrm{bd^3-h^3(b-t)}}{12}$	$\frac{bd^{8}-\overset{\cdot}{h}^{8}\left( b-t\right) }{6d}$	$\sqrt{\frac{bd^9 - h^9(b-t)}{12[bd - h(b-t)]}}$
$\frac{2\mathrm{sb}^3 + \mathrm{ht}^3}{3} - \mathrm{Ax}^3$	$\frac{I}{b-x}$	$\sqrt{\frac{1}{A}}$
$\frac{\operatorname{td}^{3}+\operatorname{s}^{3}\left(\mathrm{b}-\mathrm{t}\right)}{12}$	$\frac{\operatorname{td}^{3}+\operatorname{s}^{3}\left(\mathrm{b}-\mathrm{t}\right)}{6\mathrm{d}}$	$\sqrt{\frac{td^{3}+s^{3}(b-t)}{12[td+s(b-t)]}}$
$\frac{tx_1^2 + bx^3 - (b-t)(x-s)^2}{3}$	$\frac{1}{d-x}$	$\sqrt{\frac{\tan^3 + \tan^3 - (b-t)(x-s)^3}{3(bs+ht)}}$
$\frac{bx^3 + b_1x_1^3 - (b-t)(x-s)^3}{3} - \frac{(b_1-t)(x_1-s)^3}{3}$	$\frac{\mathbf{I}}{\mathbf{d} - \mathbf{x}}$	$\begin{bmatrix} \frac{bx^3 + b_1x_1^3 - (b-t)(x-s)^3}{3(bs+ht+b_1s)} \\ -\frac{(b_1-t)(x_1-s)^3}{3(bs+ht+b_1s)} \end{bmatrix}^{\frac{1}{2}}$
$\frac{4bs^{3}+h^{3}(3t+t_{1})}{12}-A(x-s)^{3}$	1 d-x	$\sqrt{rac{\mathrm{I}}{\mathrm{A}}}$

EXPLANATIONS OF THE TABLES OF PROPERTIES OF STANDARD AND SPECIAL I-BEAMS, STANDARD AND SPECIAL CHANNELS, AND STANDARD AND SPECIAL ANGLES WITH EQUAL AND UNEQUAL LEGS.

#### PROPERTIES OF I-BEAMS.

PAGES 182 TO 185 INCLUSIVE.

The figures or values in the various columns give the section numbers, dimensions, weights, areas and properties of the sections as noted in the different headings.

The columns which require special explanation are as follows:

#### SECTION MODULUS—Column 8.

This is obtained from the moment of inertia in column 7 by dividing it by the distance from the neutral axis to the most remote fibre, which in this case is one-half the depth of the beam.

#### COEFFICIENTS OF STRENGTH-Columns 13 and 14.

The coefficients of strength F and F' have been computed for fibre stresses of 16 000 and 12 500 pounds per square inch respectively, as stated in the headings of the columns, and are the safe loads in pounds uniformly distributed, including its own weight, for a beam one foot long. Thus the safe load for any span may be obtained by dividing the proper coefficient by the length of the span in feet.

The coefficients of strength were obtained from the following formulæ:

$$F = \frac{2}{3} \times 16000 \times S$$
  
 $F' = \frac{2}{3} \times 12500 \times S$ 

in which S is the section modulus.

#### COEFFICIENTS OF DEFLECTION-Columns 15 and 16.

The Coefficients of Deflection N and N' for uniform and center loads, respectively, were obtained from the following formulæ:

$$N = \frac{Wl^{s}}{76.8EI} \qquad N' = \frac{Pl^{s}}{48EI}$$

in which

P and W = 1000 pounds.

1 = 12 inches.

 $E = 29\,000\,000$ .

I = moment of inertia about axis 1-1.

These coefficients are, therefore, the deflections in inches of a beam one foot long with a load of 1 000 pounds, hence, the deflection of a beam for any load and span may be obtained by multiplying the proper coefficient by the cube of the span in feet, and by the number of 1 000-pound units in the given load.

#### PROPERTIES OF STANDARD AND SPECIAL CHANNELS.

PAGES 186 TO 191 INCLUSIVE.

The various columns in the Tables of Properties of Standard Channels are similar to those in the Tables of Properties of I-Beams, as explained above, with the addition of column 11, which gives the Section Modulus about an axis through the center of gravity parallel to the web, and column 13, which gives the distance of the center of gravity from the outside of the web.

In this case the Section Modulus  $S' = \frac{I'}{b-x}$  the notation being

as given at the heads of the columns.

#### PROPERTIES OF ANGLES.

The values in the Tables of Properties of Standard and Special Angles, with Equal Legs, pages 198 to 203, are those stated in the headings, and those in the Tables of Properties of Standard and Special Angles, with Unequal Legs, on pages 204 to 209, are similar, but with the addition of values for I", S" and r" about the inclined axis 3-3, the position of which, in order to give the minimum values, was determined by the formula on page 166 or the value of the tangent of 2a. After determining the position of the inclined axis, the properties corresponding thereto were obtained by the formula on page 166.

#### MOMENTS OF INERTIA OF RECTANGLES.

Tables of Moments of Inertia of Rectangles, about a transverse axis through the center of gravity, are added on pages 210 to 213 for convenience in calculating the Moments of Inertia, Section Moduli, and Radii of Gyration for compound shapes in which plates are used.

Table I is more convenient when depth of rectangle is expressed without fraction, and is directly applicable to rectangles of various widths,  $\frac{1}{2}$  to 1 inch, varying by  $\frac{1}{16}$ ths. Table II gives values for 1 inch widths of rectangle only, but for all depths from  $\frac{1}{16}$  to  $50\frac{1}{16}$  inches, varying by  $\frac{1}{16}$ ths. Value for any other width may be obtained from Table II by direct multiplication of tabular value by that other width.

## GENERAL FORMULÆ FOR PROPERTIES AND FLEXURE.

Formulæ for obtaining the Properties of Standard Sections are given on pages 166 and 167, and for various usual sections on pages 168 to 175 inclusive.

General formulæ for Flexure of Beams, Bending Moments, and Deflections for various cases of loading are given on pages

160 to 165 inclusive.

## EXAMPLES OF APPLICATION OF THE TABLES OF PROPERTIES.

#### EXAMPLE I.

What is the proper size of I-Beam to carry a load of 35 000 pounds concentrated at the center of a span of 25 feet, the fibre stress not to exceed 16 000 pounds per square inch?

In the Tables of Properties of Standard I-Beams, the column headed F gives the coefficient of strength for a uniform load corresponding to a fibre stress of 16 000 pounds per square inch.

The coefficient of strength for a concentrated load at the center is twice that for the same load uniformly distributed, hence the coefficient necessary to meet the conditions is  $35\,000\times25\times2$  = 1750 000. From the Table of Properties of Standard I-Beams, page 185, column 13, the coefficient F for a 24-inch 80-pound beam is found to be 1855 310. The weight of the beam itself is  $80\times25=2000$  pounds, which corresponds to a coefficient of  $2000\times25=50\,000$ , which deducted from 1855 310 gives a net coefficient of 1805 310. A 24-inch beam weighing 80 pounds per foot is, therefore, the proper size.

#### EXAMPLE II.

What is the deflection of the beam in the preceding example under the given load?

In the Table of Properties of Standard I-Beams, pages 182 to 185 inclusive, the coefficient of deflection for beams with center loads is given in column 16. To obtain the required deflection it is only necessary to multiply the coefficient by the cube of the span and the number of 1 000 pounds units contained in the load.

Thus for the given example the deflection in inches =

$$.0000006 \times 25^3 \times \frac{35\,000}{1\,000} = .328$$
 inch.

#### EXAMPLE III.

What is the safe load uniformly distributed that can be placed on an 8-inch standard channel weighing 11.25 pounds per foot, with a clear span of 15 feet for a maximum fibre stress of 12 500 pounds per square inch, the web to be placed vertically?

From the table of Properties of Standard Channels, page 187, column 16, the coefficient of strength F' for the given channel under the conditions named, is found to be 67 300. Hence, the total load may be  $67\,300 \div 15 = 4487$  pounds, and, as the channel itself weighs 169 pounds, the net superimposed load which is can safely carry under the given conditions is 4318 pounds.

#### EXAMPLE IV.

What is the fibre stress in a 5" x 3" angle weighing 8.2 pounds per foot if loaded at the center with a weight of 1500 pounds, used as a beam with a span of 6 feet, the 5-inch leg to be placed vertically?

The bending moment at the center will be

$$\frac{W_1 l}{4} + \frac{W_2 l}{8} = \frac{1500 \times 72}{4} + \frac{8.2 \times 6 \times 72}{8} = 27443$$
 inch pounds.

Referring to the Table of Properties of Standard Angles, Unequal Legs, on page 207, the Section Modulus for this angle, corresponding to the axis 2—2, is found to be 1.89.

The maximum fibre stress is obtained by dividing the bending moment by the section modulus, thus:  $\frac{27443}{1.89} = 14520$ , which is

the maximum fibre stress in pounds per square inch at the point most remote from the neutral axis, which in this case is the extremity of the longer leg of the angle.

The second term in the above expression for the bending moment is that due to the weight of the angle itself and is inconsiderable, so that in practice it might be neglected for short spans, but should be taken into consideration for the longer ones.

#### PROPERTIES OF COMPOUND SHAPES.

The moments of inertia, section moduli, and radii of gyration of compound sections used as beams or columns, composed of plates and angles, channels, beams, or any combination of these, may be obtained with the aid of the Tables of Properties as follows:

The first step is to find the center of gravity of the proposed section, which in the case of symmetrical sections is at the center of the figure

For unsymmetrical sections the position of the center of gravity may be determined by multiplying the areas of the component parts by the distances of their centers of gravity from any convenient line, taken as an axis, and dividing the sum of these products by the sum of the areas, which will give the distance of the center of gravity of the compound section from the assumed axis.

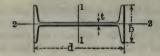
The position of the center of gravity for all sizes of angles and channels, is given in the Tables of Properties for these shapes, and is given for various geometrical sections on pages 168 to 175 inclusive, in connection with their other properties.

After determining the position of the center of gravity of a compound section, as explained above, the moment of inertia about an axis through its center of gravity may be found by taking the sum of the moments of inertia of each component part about an axis through its own center of gravity, parallel to the axis of the compound section, and adding thereto the sum of products obtained by multiplying the area of each component part by the square of the distance of its center of gravity from the axis of the compound section.

Having thus obtained the moment of inertia of the compound section, the section modulus may be obtained by dividing this moment of inertia by the distance from the neutral axis to the most remote extremity of the section.

The square of the radius of gyration for the compound section may be obtained by dividing the moment of inertia by the total area.

The moment of inertia of a compound section about any axis other than that through its center of gravity may be found in a manner similar to that above described.



1	2	8	4	5	6	7	8	9	10	11
Section Number.	Depth of Beam,	Weight per Foot.	Area of Section.	Thick- ness of Web.	Width of Flange.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.	Radius of Gyra- tion Aris 1-1.	Moment of Inertia Axis 2-2,	Radius of Gyration Axis 2-2.
	d	1	A	t	b	1	S	r	I'	r'
	Inches.	Pounds.	Sq. Ins.	Inch.	Inches.	Inches.4	Inches,3	Inches.	Inches.4	Inch.
B.,5	3	5.50 6.50 7.50	1.63 1.91 2.21	.17 .26 .36	2.88 2.42 2.52	2.5 2.7 2.9	1.7 1.8 1.9	1.28 1.19 1.15	.46 .58 .60	.53 .52 .52
B 9	66	7.50 8.50 9.50 10.50	2.21 2.50 2.79 3.09	.19 .26 .34 .41	2.66 2.73 2.81 2.88	6.0 6.4 6.7 7.1	3.0 3.2 3.4 3.6	1.64 1.59 1.54 1.52	.77 .85 .93 1.01	.59 .58 .58
B13	5	9.75 12.25 14.75	2.87 3.60 4.34	.21 .36 .50	3.00 3.15 3.29	12.1 18.6 15.1	4.8 5.4 6.1	2.05 1.94 1.87	1.23 1.45 1.70	.65 .63 .63
B17	6 "	12.25 14.75 17.25	8.61 4.34 5.07	.28 .85 .47	3.33 3.45 3.57	21.8 24.0 26.2	7.8 8.0 8.7	2.46 2.35 2.27	1.85 2.09 2.36	.72 .69 .68
B21	7	15.00 17.50 20.00	4.42 5.15 5.88	.25 .35 .46	8.66 3.76 3.87	36.2 39.2 42.2	10.4 11.2 12.1	2.86 2.76 2.68	2.67 2.94 3.24	.78 .76 .74
B25	8 "	18.00 20.25 22.75 25.25	5.83 5.96 6.69 7.43	.27 .35 .44 .58	4.00 4.08 4.17 4.26	56.9 60.2 64.1 68.0	14.2 15.0 16.0 17.0	3.27 3.18 3.10 3.03	4.36	.82
B29	9 "	21.00 25.00 30.00 35.00	6.31 7.35 8.82 10.29	.29 .41 .57 .78	4.88 4.45 4.61 4.77	84.9 91.9 101.9 111.8	18.9 20.4 22.6 24.8	3.67 3.54 3.40 3.30	5.65 6.42	.88
B36 "	10	25.00 30.00 35.00 40.00	8.82	.31 .45 .60 .75	4.66 4.80 4.95 5.10	122.1 134.2 146.4 158.7	24.4 26.8 29.3 31.7	4.07 3.90 3.77 3.67	7.65 8.52	.98
B41	12-	31.50 35.00 40.00		.35 .44 .56	5.00 5.09 5.21	215.8 228.3 245.9	36.0 38.0 41.0	4.88 4.71 4.57	10.07	.99
B53	15	45.00	12.48 13.24 14.71 16.18 17.65	.41  46  .56  66  .75	5.50 5.55 5.65 5.75 5.84	441.8 455.8 483.4 511.0 538.6	58.9 60.8 64.5 68.1 71.8	5.87	14.62 15.09 16.04 17.06 18.17	1.07



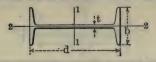
12	13	14	14   15   16				
Increase of	Coefficient	of Strength.	Coefficient o	Coefficient of Deflection.			
Thickness of Web for each Pound Increase in Weight.	For Fibre Stress of 16 000 Pounds per Square Inch for Buildings.	For Fibre Stress of 12500 Pounds per Square Inch for Bridges.	Uniform Load.	Center Load.	Section Number.		
t	, F	F'	N	N'			
.098	17650 19140 20710	18790 14950 16180	.00031253 .00028827 .00026644	.00050006 .00046124 .00042630	B.5		
.074	\$1810 33890 85980 38070	24850 26480 28110 29750	.00013009 .00012209 .00011500 .00010868	.00020815 .00019535 .00018400 .00017389	B.9		
.059	51590 58100 64630	40300 45390 50490	.00006417 .00005698 .00005122	.00010267 .00009117 .00008195	B18		
.049	77460 85270 93110	60520 66610 72740	.00003561 .00003235 .00002963	.00005698 .00005177 .00004741	B17		
.042	110410 119400 128560	\$6260 93290 100430	.00002142 .00001980 .00001839	.00003427 .00003168 .00002943	B21		
.087	151660 160510 170970 181430	118490 125400 133570 141740	.00001364 .00001289 .00001210 .00001140	.00002183 .00002062 .00001936 .00001825	B25		
.088	201800 217930 241460 264990	157260 170260 188640 207020	.00000914 .00000844 .00000762 .00000694	.00001462 .00001350 .00001219 .00001110	B29		
:029	260470 286250 312390 338530	268500 228630 244050 264480	.00000635 .00000578 .00000530 .00000489	.00001017 .00000925 .00000848 .00000782	B38		
.025	383670 405800 437170	299740 317080 341540	.00000360 .00000340 .00000316	.00000575 .00000544 .00000505	B41		
.020	628270 648310 687530 726740 765960	490840 506490 537130 567770 598410	.00000176 .00000170 .00000161 .00000152 .00000144	.00000281 .00000272 .00000257 .00000243 .00000231	B53		



1	2	3	4	5	6	7	8	9	10	11
Section Number.		Weight per Foot.	Area of Section.	Thick- ness of Web.	Width of Flange.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.	Radius of Gyra- tion Axis 1-1.	Moment of Inertia Axis 2-2.	Radius of Gyra- tion Axis 2-2.
	d		A	t	b	1	S	T	I'	T'
	Inches.	Pounds.	Sq. Ins.	Inch.	Inches.	Inches.4	Inches.3	Inches.	Inches.4	Inch.
B 65	18	60.0 65.0	15.93 17.65 19.12 20.59	.46 .56 .64 .72	6.00 6.10 6.18 6.26	795.6 841.8 881.5 921.2	88.4 93.5 97.9 102.4	6.91 6.79	21.19 22.38 23.47 24.62	1.13
B 73	50	70.0	19.08 20.59 22.06	.50 .58 .65	6.25 6.33 6.40	1169.5 1219.8 1268.8	117.0 122.0 126.9	7.70	27.86 29.04 30.25	1.19
B 89	24	85.0 90.0	28.82 25.00 26.47 27.94 29.41	.50 .57 .63 .69 .75	7.00 7.07 7.13 7.19 7.25	2167.8 2238.4	173.9 180.7 186.5 192.4 198.3	9.31 9.20 9.09	42.86 44.35 45.70 47.10 48.55	1.38 1.31 1.30

#### PROPERTIES OF SPECIAL I-BEAMS.

		1	1	1	1	1			
B 105	12	40.0 11.8 45.0 13.2		5.25	268.9	44.8 47.6		13.81 14.89	
"	W W	50.0 14.7 55.0 16.1	1 .70	5.49 5.61	303.4 321.0	50.6	4.54	16.12 17.46	1.05
B 109	15	60.0 17.6 65.0 19.1 70.0 20.5 75.0 22.0 80.0 23.5	2 .69 9 .78 6 .88	6.00 6.10 6.19 6.29 6.39	609.0 636.1 663.7 691.2 718.8	81.2 84.8 88.5 92.2 95.8	5.77 5.68 5.60	25.96 27.42 29.00 30.68 32.46	1.20 1.19 1.18
B113 " "	15	80.0 23.5 85.0 25.0 90.0 26.4 95.0 27.9 100.0 29.4	0 .90 7 .99 4 1.09	6.40 6.50 6.59 6.69 6.79		116.1	5.71 5.64 5.58	41.31 43.46 45.79 48.25 50.84	1.32 1.32 1.31
B 121	20	80.0 23.7 85.0 25.0 90.0 26.4 95.0 27.9 100.0 29.4	0 .66 7 .74 4 .81	7.00 7.06 7.14 7.21 7.28	1508.5 1557.5	146.6 150.9 155.8 160.7 165.6	7.77 7.67 7.58	45.81 47.25 48.98 50.78 52.65	1.37 1.36 1.35
B 127	24	105.0 30.9 110.0 32.4 115.0 33.9	8 .69	7.88 7.94 8.00	2811.5 2883.5 2955.5		9.42	81.04	1.58



12	18	14	15	16	1
Increase of	Coefficient	of Strength.	Coefficient	f Deflection.	
of Web for each Pound Increase in Weight.	For Fibre Stress of 16 000 Pounds per Square Inch for Buildings.	For Fibre Stress of 12500 Pounds per Square Inch for Bridges.	Uniform Load.	Center Load.	Section Number.
1	F	F'	N	N'	
.016	942880 997680 1044740 1091800	736620 779440 816200 852970	.00000098 .00000092 .00000088	.00000156 .00000148 .00000141 .00000135	B 65
.015	1247490 1301110 1353400	974600 1016490 1057340	.00000066 .00000064 .00000061	.00000106 .00000102 .00000098	B 78
.0123	1855310 1926950 1989700 2052440 2115190	1449460 1505430 1554450 1603470 1652490	.00000087 .00000036 .00000035 .00000034 .00000038	.00000060 .00000057 .00000056 .00000054 .00000052	B 89

## PROPERTIES OF SPECIAL I-BEAMS.

.025	478130 507930 539300 570670	373540 396820 421320 445830	.00000288 .00000272 .00000256 .00000242	.00000462 .00000435 .00000409 .00000887	B 105
.020	866130 904660 943870 983090 1022300	676670 706770 737400 768040 798670	.00000127 .00000122 .00000117 .00000112 .00000108	.00000204 .00000195 .00000187 .00000180 .00000173	B 109
.020	1122290 1160340 1199550 1238770 1277980	876790 906520 937150 967790 998420	.00000098 .00000095 .00000092 .00000089 .00000086	.00000157 .00000152 .00000147 .00000143 .00000138	B 118
.015	1564060 1609100 1661390 1713670 1765960	1221920 1257110 1297960 1338810 1379660	.00000053 .00000051 .00000050 .00000048 .00000047	.00000085 .00000082 .00000080 .00000077 .00000075	B 121
.0128	2499090 2563090 2627090	1952420 2002420 2052420	.00000028 .00000027 .00000026	.00000044 .00000043 .00000042	B 127

## PROPERTIES OF STANDARD CHANNELS.



1	2	8	4	5	6	1 7	8	1 9	10	11	12
Section Num-	Depth of Channel,	Weight per Foot.	Area of Section.	Thick- ness of Web.		Moment of Inertia Axis 1-1.	Beetien Mod- ulus Axis 1-1.	Radius of Gyra- tion Axis 1-1.	Moment of Inertia Axis 2-2.	Section Mod- ulus Axis 2-2.	Radius of Gyra- tion Axis 2-2.
ber.	đ		A	t	b	E	S	r	I'	8'	T'
	Inches.	Pounds.	Sq. Ins.	Inch.	Inches.	Inches.4	Ins.3	Inches.	Inches.4	Ins.3	Inch.
C,5	8 "	4.00 5.00 6.00	1.19 1.47 1.76	.17 .26 .36	1.41 1.50 1.60	1.6 1.8 2.1	1.1 1.2 1.4	1.17 1.12 1.08	.20 .25 .31	.21 .24 .27	.41 .41 .42
C.9	4	5.25 6.25 7.25	1.55 1.84 2.13	.18 .25 .33	1.58 1.65 1.73	3.8 4.2 4.6	1.9 2.1 2.3	1.56 1.51 1.46	.82 .88 .44	.32 .35	.45 .45
C18	5	6.50 9.00 11.50	1.95 2.65 8.38	.19 .33 .48	1.75 1.89 2.04	7.4 8.9 10.4	3.0 3.5 4.2	1.95 1.83 1.75	.48 .64 .82	.55 .45 .54	.50 .49
C17	- 6	8.00 10.50 13.00 15.50	2.38 3.09 8.82 4.56	.20 .32 .44 .56	1.92 2.04 2.16 2.28	13.0 15.1 17.3 19.5	4.3 5.0 5.8 6.5	2.34 2.21 2.13 2.07	.70 .88 1.07 1.28	.50 .57 .65	.54 .53 .53
C21	7	9.75 12.25 14.75 17.25 19.75	2.85 3.60 4.34 5.07 5.81	.21 .32 .42 .53	2.09 2.20 2.30 2.41 2.51	21.1 24.2 27.2 30.2 33.2	6.0 6.9 7.8 8.6 9.5	2.72 2.59 2.50 2.44 2.39	.98 1.19 1.40 1.62	.63 .71 .79 .87	.59 .57 .57 .56
C25	66	11.25 13.75 16.25 18.75 21.25	3.35 4.04 4.78 5.51 6.25	.32 .31 .40 .49	2.26 2.35 2.44 2.53 2.62	32.3 36.0 39.9 43.8 47.8	8.1 9.0 10.0 11.0 11.9	3.10 2.98 2.89 2.82 2.76	1.85 1.33 1.55 1.78 2.01 2.25	.96 .79 .87 .95 1.02 1.11	.56 .63 .61 .60
C29	9 "	13.25 15.00 20.00 25.00	3.89 4.41 5.88 7.35	.23 .29 .45	2.43 2.49 2.65 2.81	47.8 50.9 60.8 70.7	10.5 11.8 13.5 15.7	3.49 3.40 3.21 3.10	1.77 1.95 2.45 2.98	.97 1.03 1.19 1.36	.67 .66 .65
C88	10	15.00 20.00 25.00 30.00 35.00	4.46 5.88 7.35 8.82 10.29	.24 .38 .53 .68 .82	2.60 2.74 2.89 3.04 3.18	66.9 78.7 91.0 103.2 115.5	13.4 15.7 18.2 20.6 23.1	3.87 3.66 3.52 3.42 3.35	3.99	1.17 1.34 1.50 1.67 1.87	.72 .70 .68 .67
C41	12	20.50 25.00 30.00 35.00 40.00	6.03 7.35 8.82 10.29 11.76	.28 .39 .51 .64 .76	2.94 3.05 3.17 3.30 3.42	128.1 144.0 161.6 179.3 196.9	21.4 24.0 26.9 29.9 32.8	4.61 4.43 4.28 4.17 4.09	5.90	1.75 1.91 2.09 2.27 2.46	.81 .78 .77 .76
C58	15	33.00 35.00 40.00 45.00 50.00 55.00	9.90 10.29 11.76 13.24 14.71	.40 .43 .52 .62 .72	3.40 3.43 3.52 3.62 3.72	312.6 319.9 347.5 375.1 402.7 430.2	41.7 42.7 46.3 50.0 53.7	5.62 5.57 5.44 5.82 5.28	8.23 8.48 9.89 10.29	3.16 3.22 3.43 3.63 3.85	.91 .91 .89 .88 .87

## PROPERTIES OF STANDARD CHANNELS.



18	14	15	16	17	18	1
Distance	Increase of	Coef. of	Strength.	Coef. of D	eflection.	
of Center of Gravity from	Thickness of Web for each Pound	Fibre Stress 16 000 Pounds	Fibre Stress 12500 Pounds	Uniform	Center	Section
Outside of Web.	Increase in Weight.	per Sq. Inch for Buildings.	per Sq. Inch for Bridges.	Load.	Load.	Number.
Inch.	Inches.	F	F'	N	N'	
Inon.	Inches.					
.44 .44 .46	.098	11630 13140 14710	9090 10270 11490	.0004743 .0004199 .0003751	.0007589 .0006718 .0006001	C'.R
.46	.074	20230	15800	.0002046	.0003273	C 9
.46 .46		22270 24360	17400 19030	.0001858	.0002973	66
.49	.059	31640	24720	.0001046	.0001674	C18
.48	.000	87860	29570	.0000875	.0001399	44
.51	.049	44890 46210	34680 36100	.0000746	.0001193	C17
.50	10-20	53750	42000	.0000513	.0000821	66
.52		61600	48120 54250	.0000448	.0000717	66
.55	.042	64270	50210	.0000368	.0000588	C21
.53	10 2.0	73650	57540	.0000321	,0000514	44
.58		82740 91950	71840	.0000286	.0000457	44
.58		101100	78990	.0000234	.0000374	66
.58	.037	86140	87300 75000	.0000240	.0000384	C25
.56 .56	-	95990 106450	83170	.0000216	.0000311	44
.57		116910	91340 99510	.0000177	.0000283	66
.61	.088	127370	87630	.0000162	.0000260	C29
.59	,000	120540	94170	.0000153	.0000244	**
.58		144070 167590	112550 130930	.0000128	.0000204	66
.64	.029	142680	111470	.0000116	.0000186	C88
.61	10.00	167940	131210	.0000099	.0000158	46
.6 <b>2</b>	0 = 0	194090 220230	151630 172060	.0000085	.0000136	44
.69		246380	192480	.0000067	.0000107	44
.70	.025	227750 256000	177930 200000	.0000061	.0000097	C41
.68		287370	224510	.0000048	.0000077	66
.69	-	318750 350120	249020	.0000043	.0000069	46
.72	.020	444520	347280	.0000025	.0000040	C58
.79	.000	455030	355500	.0000024	.0000039	44
.78		494250 533470	386130 416770	.0000022	.0000036	44
.80	11 32	572680	447410	.0000019	.0000031	66
.82	-	611900	478050	.0000018	.0000029	

## PROPERTIES OF SHIP AND SPECIAL CHANNELS.

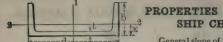


1	2	3	4	5	6	7	8	9	10	11	12	13
Section Number	Depth of Channel.	W'ght per Foot.	Area of Section.	Thick- ness of Web.		Thickness of Flange.	Slope of Flange.	Moment of Inertia Axis 1-1.	mod- ulus Axis	of Gyra- tion Axis	Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.
	d		A	t	b	В	g	I	8	r	I'	S'
	Ins.	Lbs.	Sq. Ins.	Inch.	Ins.	In.	6	Ins.4	Ins.3	Ins.	Ins.4	Ins.3
C 269 C 72	3	7.1	2.07		1.94	.26			1.81		1.12	.52
C _86	6	15.3 17.7	4.47	.34	3.50 3.62	.33		25.3 27.5		2.38 2.30	5.14	2.13
C "88	6 "	19.0 21.6 23.4	5.58 6.36 6.87	.41	3.56 3.69 3.78	.46	.02	31.1 33.4 34.9	$10.4 \\ 11.1$	2.36	6.79 7.85 8.53	2.85 3.10
C _89	7	20.9 23.8	6.15	.45	3.45	.48	.02	44.6 48.0	12.7	2.69	6.74	2.81
C 101	8	21.5 24.7	6.30 7.26	.40	3.50 3.62	.48	.02	60.7 65.8			7.20	2.94
C 103	8	23.8 27.1	7.00	.62	3.50 3.62	.48	.02	63.6 68.7	15.7 17.2	3.01 2.94	7.42 8.41	2.96 3.18
C _90	"	21.9 26.0 27.4 31.5	7.64 8.04	.50	3.38 3.50 3.54 3.66	.41	"	92.0 102.0 105.4 115.4	20.4	3.66	6.29 7.17 7.45 8.30	2.70
66 66 68	12	35.0 40.0 44.3 46.3 48.4	10.30 11.76 13.02 13.62 14.22	.47 .60 .70 .75	3.77 3.90 4.00 4.05 4.10 4.14	.65 ""	.03	215.7 233.3 248.4 255.6 262.8 268.6	36.0 38.9 41.4 42.6 43.8	4.58 4.45 4.37 4.33 4.30	12.98 14.61 15.99 16.64 17.31	4.79 5.13 5.41 5.55 5.68
C 95	44	40.0	10.29	.50	4.00 4.08 4.12 4.19 4.30 4.42 4.53	.34	« « «	237.5 251.5 259.8 272.2 292.9 313.7 334.4	38.7 40.0 41.9 45.1 48.3	4 94 4.89 4.81 4.70 4.62	12.54 $13.10$ $13.94$	4.33 4.59 4.86
C _65	18	45.0 50.0 55.0	13.25 14.71	.47 .55	3.77 3.85 3.93 4.02	.45	.17	584.3 623.1 662.0 703.3	64.9 69.2 73.6	6.64 6.51 6.40	12.89 13.90 14.93	4.40 4.61 4.82

## PROPERTIES OF SHIP AND SPECIAL CHANNELS.



14	15	16	17	18	19	20	1
Radius	Distance	Increase of	Coef. of S	trength.	Coef. of I	eflection.	
Gyration Axis 2–2.	of Center of Gravity from Outside of Web.	Thickness of Web for each Lb. Increase in Weight.	Fibre Stress 16 000 Lbs. per Sq. Inch. for Buildings.	Fibre Stress 12 500 Lbs. per Sq. Inch. for Bridges.	Uniform Load.	Center Load,	Section
r'	x	Ĭ		,			
Inch.	Inch.	Inch.	F	F'	N	N'	
.50	.65	.098	19310		.0002857		
.62	.67	.074	34880	1	.0001186		C 72
1.07	1.08	.049	89160 97680	76310	.0000307	.0000491	C "86
1.10 1.11 1.11	1.18 1.16 1.15	.049	110450 118770 124270	92790	.0000250 .0000232 .0000222	.0000400 .0000372 .0000356	C 88
1.05	1.05	.042	135950 146350	106210	.0000174		C _89
1.07	1.05	.037	161930 174930		.0000128		C 101
1.08 1.08	.99	.037	167470 183470		.0000122	.0000195	C 103
.99 .97 .96 .95	.87 .84 .84 .84	.029	196310 217650 224760 246100	170030 175580	.0000085 .0000077 .0000074 .0000068	.0000135 .0000123 .0000118 .0000108	C _90
1.12 1.11 1.11 1.11	1.07 1.05 1.05 1.05	.0245	383550 414790 441670 454470	324060 345060 355060	.0000036 .0000033 .0000031 .0000030	.0000053 .0000050 .0000049	C 105
1.10	1.05	"	467270	373060	.0000030	.0000047	ш
1.11 1.10 1.10	1.01	.023	389710 412750 426340	322460	.0000033 .0000031 .0000030	.0000049	C _95
1.09	.97	H #	446740	349010	.0000029	.0000046	
1.08 1.07 1.06	.97 .98 1.00	4	480720 514710 548700	402120	.0000027 .0000025 .0000023		æ
.99	.84	.016	692270	540830	.0000014	.0000022	
.96 .95	.83	et et	784600		.0000012	.0000019	



## PROPERTIES OF STANDARD SHIP CHANNELS.

General slope of flange=2° or .035.

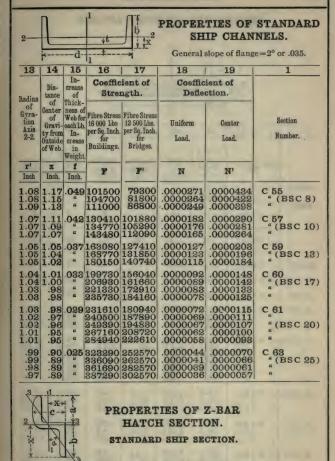
1	2	3	4	5	6	7	8	9	10	11	12
Section	Depth of Channel.	W'ght per Foot.	Area of Section.	Thick-	Width of Flange.	Thick- neem at Mid Flange.	Moment of Inertia Axis 1-1.	Section Mod- ulus Axis 1-1.	Radius of Gyration Axis 1-1.	Moment of Inertia Axis 2-2.	Section Mod- ulus Axis 2-2.
	d		A	E	b		I	8	r	I'	81
	Inn	Lbs.	Sq. Ins.	Inch.	Ins.	Inch.	Ins.4	Ins.3	Ins.	Ins.4	Ins.3
C 55 "(BSC8)	8 4	16.8 17.8 19.8	4.92 5.22 5.82			.475	28.5 29.4 31.2	9.5 9.8 10.4	2.41 2.38 2.32	5.69 6.09 6.86	2.58
C 57 "(BSC10)	7 "	18.9 20.1 22.5		.350 .400 .500		.500	44.2	12.2 12.6 13.5	2.74	6.31 6.78 7.54	2.78
C 59 "(BSC13)	8 "	21.2 22.6 25.3	6.63		3.45 3.50 3.60	.525	63.3	15.3 15.8 16.9	3.09	6.92 7.36 8.21	2.98
C 60 "(BSC17)	9 "	23.7 25.2 28.3 31.3	8.31	.450	3.45 3.50 3.60 3.70	.550	87.3 93.4	18.7 19.4 20.7 22.1	3.43	7.52 7.97 8.85 9.71	3.17
C 61 "(BSC20)	10	26.3 28.0 31.4	7.73	.425 .475	3.40 3.45 3.50 3.60 3.70	u	108.6 112.7 116.9 125.2 133.6	22.5 23.4 25.0	3.82 3.77 3.69	8.10	3.15 3.25 3.37 3.60 3.80
C 63 "(BSC25)	12	32.7			3.50	44	189.0 203.4	31.5	4.44	8.89 9.37 10.31 11.26	3.80



## PROPERTIES OF Z-BAR HATCH SECTION.

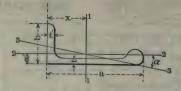
STANDARD SHIP SECTION.

Section	Size	Weight	Area		THICKN	CONTRACT CON	Moment	Section	
Number.	$\mathbf{a} \times \mathbf{b} \times \mathbf{c}$ .	Foot.	of Section.	Web.   Plain   Leg.		Rounded Leg.	of Inertia		
-	Inches.	Lbs.	Sq. Ins.	Ins.	Ins.	Ins.	Ins.4	Ins.3	
Z 101	2 ½ x3 x2 ¾	13.6	3.98	1/2	7	3/4	3.57	2.52	



	13							
Radius	Distance Center of	Moment	Section Modulus	Radius	Distance Center of	Tangent	Least Radius of	Section
Gyration. Axis 1-1.		Inertia Axis 2-2.	Axis 2-2.	Gyration Axis 2-2.	Gravity	of Angle	Gyration. Axis 3-3.	Number.
Ins.	Ins.	Ins.4	Ins.3	Ins.	Ins.	a	Ins.	
.95	1.42	6.98	2.39	1.33	2.93	1.560	.55	Z-101

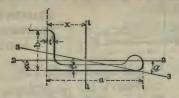
## PROPERTIES OF BULB ANGLES.



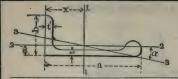
1	2	3	4	5	6	7	8
Section	Size	Weight per Foot.	Area of Section.	Thickness of Bulb Leg.	Thickness of Plain Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
Number.	axb		A	t	t'	I	8
	Inches.	Lbs.	Sq. Ins.	Ins.	Ins.	Ins.4	Ins.3
* A174	4 x 3 ½	11.7	3.42	3/8	3/8	7.7	8.25
* A176	5 x 4 1/2	19.2	5.64	7 16	7 16	20.7	7.89
A 171	5 x 2 ½	10.2	3.00	19 64	9 to 13 32 to 22	10.4	4.05
A 177	6 x 3	11.8 13.5 15.0	3.47 3.95 4.41	5 16 3/8 7 16	.34 .39 .43	16.8 18.5 20.1	5.10 5.56 6.02
A 178	6 x 3½ « « « « «	12.5 14.1 15.7 17.8 18.9 20.5	3.66 4.13 4.60 5.07 5.53 6.02	3/8 1/2 1/2 5/8	.87 .41 .45 .49 .53	18.0 19.6 21.3 22.8 24.4 25.9	5.16 5.62 6.11 6.53 6.97 7.42
A 179	7 x 3½	15.7 17.5 19.1	4.61 5.13 5.60	3/8 7 16 1/2	.43 .46 .48	29.3 31.6 33.7	7.21 7.79 8.36
A 181	8 x 3½	17.4 19.3 21.5	5.09 5.64 6.30	3/8 1/2	.42 .44 .50	42.8 45.3 50.1	9.54 10.15 11.14
A 183	9 x 3½	20.3 22.6 24.8	5.96 6.62 7.27	13 15 15 17	.44 .48 .52	62.6 68.0 72.7	12.78 13.81 14.75
A 185	10 x 8 1/2	23.6 26.1 28.5	6.91 7.64 8.35	16 1/2 16	.47 .51 .55	88.6 95.6 102.2	16.62 17.81 19.00

\*Top Guard Angle.

## PROPERTIES OF BULB ANGLES.



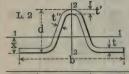
. 9	10	11	12	18	14	15	16	1
Radius of Gyration Axis 1-1.	Distance Center of Gravity from back of Plain Log.	Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.	Radius of Gyration Axis 2-2.	Distance Center of Gravity from back of Bulb Leg.	Tangent of Angle.	Least Radius of Gyration Axis 3-3.	Section
r	I	ľ	8′	r'	x'	α	r".	Number.
Ins.	Ins.	Ins.4	Ins.3	Ins.	Ins.		Ins.	
1.50	1.78	3.07	1.19	.95	.94	.398	.81	A174*
1.92	2.38	7.96	2.41	1.19	1.19	.385	1.01	A176*
1.86	2.43	3.47	1.81	1.08	.59	.198	1.03	A171
2.20 2.16 2.14	2.70 2.67 2.66	1.88 2.11 2.33	.79 .90 1.00	.74 .73 .73	.63 .65 .67	.161 .161 .159	.65 .65	A177
2.22 2.18 2.15 2.12 2.10 2.08	2.51 2.50 2.52 2.50 2.51 2.50	3.27 3.60 3.92 4.21 4.50 4.85	1.21 1.33 1.46 1.57 1.69 1.84	.95 .93 .92 .91 .90	.80 .80 .81 .82 .84	.250 .247 .244 .239 .238 .236	.79 .79 .78 .78 .77	A178
2.52 2.48 2.45	2.94 2.94 2.97	3.70 3.99 4.16	1.85 1.46 1.52	.90 .88 .86	.75 .76 .76	.193 .190 .183	.77 .76 .75	A179
2.90 2.83 2.82	3.52 3.54 3.50	3.73 3.95 4.41	1.33 1.42 1.59	.86 .84 .83	.70 .71 .73	.143 .138 .136	.76 .75 .75	A181
3.24 3.20 3.16	4.10 4.08 4.07	4.00 4.37 4.71	1.42 1.56 1.69	.82 .81 .80	.68 .70 .71	.110 .109 .108	.73 .73 .73	A183
3.58 3.54 3.50	4.67 4.63 4.61	4.34 4.73 5.09	1.53 1.68 1.82	.79 .79 .78	.67 .68 .70	.087 .087 .086	.78 .73 .72	A185



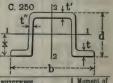
## PROPERTIES OF STANDARD BULB ANGLES.

1	2	8	4	5	6	7	8
Section Number,	Size.	Weight per Foot.	Area of Section.	of	Thickness of Plain Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
1	axb		A	t	ti	1	S.
-	Inches.	Lbs.	Sq. Ins.	Ins.	Ins.	Ins.4	Ins.3
A 187 "(BSBA 4)	6x 3	12.2 12.8 14.1 15.6	3.58 3.76 4.14 4.58	.350 .375 .425 .475	.375	16.6 17.4 18.8 20.2	4.9 5.1 5.5 5.9
A 188 "(BSBA 8)	7x 3 ½	15.3 16.8 18.6 20.0	4.50 4.94 5.46 5.90	.375 .425 .475 .525	.425	28.6 30.9 33.2 35.5	7.2 7.7 8.8 8.8
A 189 "(BSBA 12)	8x 3 ½  " "	18.0 19.6 21.6 23.2	5.29 5.78 6.34 6.83	.400 .450 .500 .550	.450	43.8 47.1 50.4 53.7	9.8 10.6 11.2 11.9
A 190 "(BSBA 16) "	9x 3 ½  " " " "	20.9 22.7 24.8 26.6 28.6	6.14 6.68 7.29 7.82 8.41	.425 .475 .525 .575 .625	.475	63.8 68.4 73.1 77.6 81.8	13.1 13.9 14.8 15.6 16.4
A 191 "(BSBA 18) "	10x 3 ½  " " " " " "		7.32 7.90 8.55 9.14 9.77 10.35	.475 .525 .575 .625 .675 .725	.525	92.1 98.2 104.3 110.4 115.9 122.0	17.2 18.3 19.2 20.3 21.2 22.3

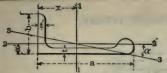
#### PROPERTIES OF CAR SIDE STAKE AND



DOOR
SPREADER
BAR
SECTIONS.



Section	0100	MOTERTE	Alea Ol		1 ILIU AN MICE		Inertia.
Number.	bxd	per Foot.	Section.	Base t	Top t'	Sides t"	Axis 1-1.
	Ins.	Lbs.	Sq. In.	Ins.	Ins.	Ins.	Ins.4
L 2 " C 250	7 x2 3/4 7 x213/16 7 x215/16 71/2 x 4	7.2 8.7 11.7 19.8	2.10 2.54 3.41 5.81	3/4 3/8 1/2	3/8 7/16 9/16 .483	.210 .254 .320	1.99 2.90 4.55 11.78



## PROPERTIES OF STANDARD BULB ANGLES.

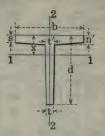
	1 40	11.		10	44	48	10	1
9	10	11	12	18	14	15	16	1
Radius of Gyration Axis 1-1.	Distance Center of Gravity from back of Plain Leg.	2-2.	Section Modulus Axis 2-2.	Radius of Gyration Axis 2-2.	Distance Center of Gravity from back of Bulb Leg.	Tangent of Angle.	Least Radius of Gyra- tion Axis 3-3.	Section Number.
r	X	I'	3'	I'	x'	a	r"	
Ins.	Ins.	Ins.4	Ins.3	Ins.	Ins.		Ins.	
2.16 2.15 2.13 2.10 2.50 2.47 2.45 2.85 2.85 2.82 2.81 3.22 3.27	2.59 2.60 2.55 2.99 3.00 2.94 2.95 3.54 3.48 3.49 4.10 4.03	1.9 2.1 2.3 2.5 3.4 4.5 4.5 4.0 4.4 4.8 3.9 4.7	108.3 .83 .876 1.1 1.2 1.4 1.5 1.6 1.3 1.4 1.5 1.7 1.4 1.5 1.7 1.8 2.0	.74 .75 .74 .87 .88 .87 .88 .84 .83 .84	108. 63. 64. 66. 67. 72. 74. 75. 77. 70. 71. 73. 75. 68. 70. 71.	.173 .174 .176 .178 .177 .178 .180 .182 .136 .138 .139 .106	.65 .65 .65 .75 .76 .77 .74 .75 .75 .78 .74 .74	A 187
3.15 3.12	4.03 3.98	5.1	2.0	.80 .81 .80	.74	.108	.75	4
3.55 3.53 3.49 3.48 3.44 3.43	4.63 4.62 4.56 4.56 4.52 4.53	4.4 4.8 5.1 5.6 5.8 6.8	1.6 1.7 1.9 2.0 2.1 2.3	.78 .78 .77 .78 .77 .78	.68 .69 .70 .72 .74 .76	.085 .085 .086 .087 .089	.72 .72 .73 .74 .74 .75	A 191 a (BSBA 18) a a a

## PROPERTIES OF CAR SIDE STAKE AND



Modulus	Gyration	Center of	Inertia	Modulus	Gyration	Section
Axis 1-1.	Axis 1-1.	Gravity x.	Axis 2-2.	Axis 2-2.	Axis 2-2	Number.
Ing.3	Ins.	Ins.	Ins.4	Ins.3	Ins.	
1.16	.97	1.04	5.45	1.56	1.61	L <sub>u</sub> 2
1.58	1.07	.91	7.23	2.07	1.69	
2.12	1.15	.79	10.81	3.09	1.78	
5.77	1.42	2.04	26.2	7.00	2.12	C 250

## PROPERTIES OF T-BARS.



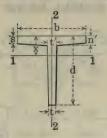
#### EQUAL LEGS.

1	2	3	4	5	6	7	8	9
		Di	mensions				Distance of Center of	Moment
Section Number	Width of Flange	Depth of Bar	Thickness of Flange	Thickness of Stem	Weight per Foot	Area of Section	Gravity from Out- side of Flange	of Inertia
	ъ	a	s to n'	t to t'		A	×	1
	Inches	Inches	Inch	Inch	Pounds	Sq. Ins.	Inch	Inches <sup>4</sup>
T 5	1	1	$\frac{1}{8}$ to $\frac{5}{32}$	$\frac{1}{8}$ to $\frac{5}{32}$	.89	.26	.29	.02
T181	11/8	11/8	3 4 7	$\frac{5}{32}  \text{``}  \frac{7}{32}$	1.37	.40	.33	.04
T183	1 3 16	1 3 16	3 " 1	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.51	.44	.34	.05
T187	11/4	11/4	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{5}{32}$ " $\frac{7}{32}$	1.60	.47	.36	.06
T188	11/4	11/4	3 6 7	$\frac{3}{16}$ " $\frac{9}{32}$	1.70	.50	.40	.07
T191	11/2	11/2	3 " 7 16 32	$\frac{3}{16}$ " $\frac{7}{32}$	1.94	.57	.44	.11
T193	11/2	11/2	1 4 9 32	1 " 9 4 32	2.47	.73	.47	.15
T194	13/4	13/4	1 4 5	1 4 5	3.09	.91	.54	.23
T 37	2	5	1 4 5	1 " 5	3.56	1.05	.59	.37
T 39	2	2	5 4 3	5 4 3	4.3	1.26	.61	.44
T 41	21/4	21/4	1	1	4.1	1.19	.65	.52
T 42	21/4	21/4	5 " 3 16 8	5 " 3	4.9	1.43	.68	.65
T 47	21/2	21/2	1 4 5	1 4 5	4.6	1.33	.71	.74
T 49	21/2	21/2	10   5    5    5    5    5    5    5	10   32   32   32   32   32   32   32   3	5.5	1.60	.74	.88

#### UNEQUAL LEGS.

T	16 18	11/4	1 1/8 11/8	$\begin{array}{c} \frac{3}{16} \text{ to } \frac{1}{4} \\ \frac{3}{16} \text{ "} \frac{7}{32} \\ \frac{1}{8} \text{ "} \frac{5}{32} \end{array}$	5 to 7 32 to 7 3 " 1 16 " 5	1.48	.48	.30	.04
T	20	1/2	1/4	8 32	8 " 37	1.25	.37	.00	.05

## PROPERTIES OF T-BARS.



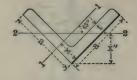
#### EQUAL LEGS.

10	11	12	13	14	15	16	1
		1			Coef. of	Strength	
Modulus Axis 1-1	Radius of Gyration Axis 1-1	Moment of Inertia Axis 2-2	Section Modulus Axis 2-2	Radius of Gyration Axis 2-2 For Fibre Stress I of 16 000 Lbs. per Square Inch.		For Fibre Stress of 12 500 Lbs. per Square Inch	Section
8	r	ľ	S'	r'			Number
Inches <sup>3</sup>	Inch	Inches4	Inches <sup>3</sup>	Inch	Y	F'	
.08	.30	.01	.02	.21	820	250	T 5
.05	.31	.02	.04	.24	280	410	T181
.06	.33	.03	.05	.26	610	480	T183
.06	.35	.03	.05	.27	680	530	T187
.08	.37	.03	.05	.26	820	640	T188
.11	.45	.06	.08	.32	1170	910	T191
.14	.45	.08	.10	.32	1490	1160	T193
.19	.51	.12	.14	.37	2020	1580	T194
.26	.59	.18	.18	.42	2770	2160	T 37
.31	.59	.23	.23	.43	3300	2580	T 39
.32	.66	.25	.22	.46	3410	2660	T 41
.41	.67	.33	.29	.48	4370	8410	T 42
.42	.75	.34	.27	.51	4420	3450	T 47
.50	.74	.44	.35	.52	5330	4160	T 49

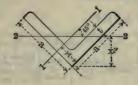
#### UNEQUAL LEGS.

.05	.32	.03	.05		640	500	T 16 T 18
.05	.37	.04	.05	.32	530	410	T 20

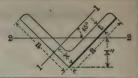
# PROPERTIES OF STANDARD ANGLES. EQUAL LEGS.



Dimensions.   Thickness.   Weight per Foot.   Section   Number.     Example     Example	1	2	3	4	5	в	7	8
RIB   t   Inches.   Sq. Ins.   Inch.   Inches.   Inches.   Sq. Ins.   Inch.   Inches.   Inches.   Inches.   Sq. Ins.   Inch.   Inches.		Dimensions.	Thickness.	per	of	Center of Gravity from Back	of Inertia	Section Modulus Axis 1-1.
A11 1½x 1½ ½ 1.23 .36 .42 .08 .07  " " " 1.80 .53 .44 .11 .10  " 2.34 .69 .47 .14 .18  " " ½ 2.36 .84 .49 .16 .16  " " ½ 3.35 .98 .51 .19 .18  A15 2 x 2 ½ 1.65 .48 .55 .19 .13  " " " 2.44 .72 .57 .27 .19  " " " 3.92 1.15 .61 .42 .30  " " " 3.92 1.15 .61 .42 .30  " " " 5.3 1.56 .64 .48 .35  " " " 5.3 1.56 .64 .48 .35  " " " 5.3 1.56 .64 .54 .40  " " 1 5.3 1.56 .66 .54 .40  " " 1 5.3 1.56 .66 .54 .40  " " 1 5.3 1.56 .66 .54 .40  " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30  " " 3 3.07 .90 .69 .55 .30		BEE	t		A	x	I	S
# # 1.80 .53 .44 .11 .10 .10 # 1.81 # 1.80 .53 .44 .11 .10 .10 # 1.81 # 1.82 .86 .84 .49 .16 .16 .16 .16 .16 .16 .18 .18 # 1.82 .86 .84 .49 .16 .18 .18 # 1.85 .19 .18 .18 # 1.85 .19 .18 .18 # 1.85 .19 .18 # 1.85 .19 .18 # 1.85 .19 .19 .18 # 1.85 .19 .19 .18 # 1.85 .19 .19 .19 .19 .19 .19 .19 .19 .19 .19		Inches.	Inch.	Pounds.	Sq. Ins.	Inch.	Inches.4	Inches,3
1.30 .33 .44 .11 .10 .13 .13 .13 .13 .13 .13 .13 .13 .13 .13		1½x 1½						.072
**								.104
**	- 1	_						.134
A15 2 x 2 ½ 1.65 .48 .55 .19 .18  a a ½ 3.19 .94 .59 .57 .27 .19  a a ½ 3.19 .94 .59 .35 .25  a a a ½ 3.19 .94 .59 .35 .25  a a a ½ 4.7 1.36 .64 .48 .35  a a a ½ 4.7 1.36 .64 .48 .35  a a a a a a a a a a a a a a a a a a a	_							
* * * * * * * * * * * * * * * * * * *			%	8.85	.98	.51	.19	.188
* * * * * * * * * * * * * * * * * * *	A15	2 x 2	1/8	1.65	.48	.55	.19	.13
* * * * * * * * * * * * * * * * * * *	4	46						
* * * * * * * * * * * * * * * * * * *	×	es						
# # # # # # # # # # # # # # # # # # #	æ	æ						
* * * * * * * * * * * * * * * * * * *	æ	46		4.7	1.36	.64	.48	.35
A17 2½x 2½ ½ 2.08 .61 .67 .38 .20 .45 .45 .45 .45 .45 .45 .45 .45 .45 .45	4	44	7 36	5.3	1.56	.66	.54	.40
* * * * * * * * * * * * * * * * * * *	"	æ	1/2	6.0	1.75	.68	.59	.45
*		2½x 2½	1/8	2.08	.61	.67	.38	
4.1 1.19 .772 .770 .39 4 5 5.0 1.47 .74 .85 .48 5 5.9 1.73 .76 .98 .57 6 6.8 2.00 .78 1.11 .65	_	а	16	3.07	.90	.69		
*		a						
*   %   5.9   1.73   .76   .98   .57   .76   .98   .57   .76		a						
16 6.8 2.00 .78 1.11 .00		æ						
* .   *   ½   7.7   2.25   .81   1.28   .72	-							
	* .	-	1/2	7.7	2.25	.81	1.23	.72
A19 3 x 3 1/4   4.9   1.44   .84   1.24   .58	A19	3 x 3	1/4	4.9	1.44	.84	1.24	.58
"   16   6.1   1.78   .87   1.51   .71		и		6.1	1.78	.87	1.51	.71
"	65	44		7.2		.89	1.76	.83
"   18   8.3   2.43   .91   1.99   .95	65	2		8.3	2.43	.91	1.99	.95
"	и			9.4	2.75	.93	2.22	1.07
"   "   10.4   3.06   .95   2.43   1.19	*	4	9 16	10.4	3.06	.95	2.43	1.19



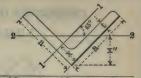
9	10	11	12	13	1
Radius of Gyration	Distance of Center of	Least Moment	Section Modulus	Least Radius of Gyration	
Axis 1-1.	Gravity from External Apex.	Axis 2-2.	Axis 2-2.	Axis 2-2.	Section
r	x"	I"	8″	r"	Number.
Inch.	Inches.	Inches.4	Inches,3	Inch.	
.47	.60	.031	.053	.30	A11
.46	.63	.045	.072	.29	4
.45	.66	.058	.088	.29	4
.44	.69	.070	.101	.29	4
.44	.72	.082	.114	.29	4
.63	.78	.08	.10	.40	A15
.62	.80	.11	.14	.39	66
.61	.84	.14	.17	.39	4
.60	.87	.17	.20	.39	44
.59	.90	.20	.22	.39	46
.59	.93	.23	.25	.38	*
.58	.96	.26	.27	.88	4
.79	.95	.15	.16	.50	A17
.78	.98	.22	.22	.49	65
.77	1.01	.29	.28	.49	4
.76	1.05	.35	.33	.49	
.75	1.08	.41	.38	.48	æ
.75	1.11	.46	.42	.48	æ
.74	1.14	.52	.46	.48	
.93	1.19	.50	.42	.59	A19
.92	1.22	.61	.50	.59	"
.91	1.26	.72	.57	.58	4
.91	1.29	.82	.64	.58	"
.90	1.32	.92	.70	.58	44
.89	1.35	1.02	.76	.58	a a



1	2	8	4	5	6	7	8
Section Number.	Dimensions,	Thickness.	Weight per Foot.	Area of Section.	Distance of Center of Gravity from Back of Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
	axa	t		A	x	I	8
	Inches.	Inch.	Pounds.	Sq. Ins.	Inches.	Inches.4	Inches.3
421	3½ x3½ 	14 5 6 8 7 6 7 6	5.8 7.2 8.5 9.8 11.1 12.4 13.6 14.8 16.0 17.1 18.3	1.69 2.09 2.48 2.87 3.25 3.62 4.69 5.03 5.36	.97 .99 1.01 1.04 1.06 1.08 1.10 1.12 1.15 1.17 1.19	2.01 2.45 2.86 3.64 3.99 4.83 4.65 4.95 5.58	.79 .98 1.15 1.32 1.49 1.65 1.81 1.96 2.11 2.25 2.39
44 44 44 44 44 44 44 44	4 x4	# 6 % - 1	8.2 9.8 11.8 12.8 14.3 15.7 17.1 18.5 19.9 21.2	2.40 2.86 3.31 3.75 4.18 4.61 5.08 5.44 5.84 6.28	1.12 1.14 1.16 1.18 1.21 1.28 1.25 1.27 1.29 1.31	3.71 4.86 4.97 5.56 6.12 6.66 7.17 7.66 8.14 8.59	1.29 1.52 1.75 1.97 2.19 2.40 2.61 2.81 3.01 3.20
A27	6 x6	3/8 - EX 2 - EX	14.9 17.2 19.6 21.9 24.2 26.5 28.7 31.0 33.1 35.3 37.4	4.36 5.06 5.75 6.43 7.11 7.78 8.44 9.09 9.73 10.37 11.00	1.64 1.66 1.68 1.71 1.73 1.75 1.78 1.80 1.82 1.84 1.86	15.89 17.68 19.91 22.07 24.16 26.19 28.15 30.06 31.92 88.72 85.46	3.58 4.07 4.61 5.14 5.66 6.17 6.66 7.15 7.69 8.11 8.57
44 44 44 44 44 44 44 44 44 44 44	8 x8	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	26.4 29.6 32.7 35.8 38.9 42.0 45.0 48.1 51.0 54.0 56.9	7.75 8.68 9.61 10.58 11.44 12.34 13.28 14.12 15.00 15.87 16.78	2.19 2.21 2.25 2.25 2.28 2.30 2.32 2.32 2.34 2.37 2.39 2.41	48.65 54.09 59.43 64.64 69.74 74.72 79.58 84.84 88.98 93.53 97.97	8.37 9.34 10.30 11.25 12.18 13.11 14.02 14.91 15.80 16.67 17.53

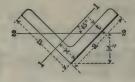
#### PROPERTIES OF STANDARD ANGLES.

EQUAL LEGS.



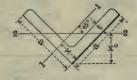
9	10	11	12	13	1
Radius of Gyration Axis 1-1.	Distance of Center of Gravity from External Apex.	Least Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2,	Least Radius of Gyration Axis 2-2.	Section Number.
r	x"	I"	8"	r"	21 100000 0,10
Inches.	Inches.	Inches.4	Inches.3	Inch.	
1.09 1.08 1.07 1.07 1.06 1.05 1.04 1.04 1.03 1.02	1.37 1.40 1.43 1.46 1.50 1.58 1.56 1.59 1.62 1.65	.80 .99 1.16 1.88 1.50 1.66 1.82 1.97 2.18 2.28	.59 .71 .81 .91 1.00 1.09 1.17 1.24 1.81	.69 .68 .68 .68 .88 .88 .68 .67	A21
1.02 1.24 1.23 1.23 1.23 1.21 1.20 1.19 1.19 1.18	1.68 1.58 1.61 1.64 1.67 1.71 1.74 1.75 1.80 1.80	2.48 1.50 1.77 2.02 2.28 2.52 2.76 3.00 8.28 3.46 3.69	1.45 .95 1.10 1.28 1.36 1.48 1.59 1.70 1.80 1.89 1.99	.67 .79 .78 .78 .78 .77 .77 .77 .77	428 44 44 44 44 44 44 44 44 44 44
1.88 1.87 1.86 1.85 1.84 1.83 1.83 1.82 1.81 1.80 1.80	2.82 2.34 2.88 2.41 2.45 2.48 2.51 2.54 2.57 2.60 2.64	6.19 7.13 8.04 8.94 9.81 10.67 11.52 12.35 13.17 13.98 14.78	2.67 3.04 3.37 3.70 4.01 4.81 4.86 5.12 5.37 5.61	1.19 1.18 1.18 1.17 1.17 1.17 1.17 1.16 1.16	427
2.51 2.50 2.49 2.48 2.47 2.46 2.45 2.44 2.44 2.48 2.42	8.09 8.12 8.16 8.19 8.22 8.25 8.38 8.39 8.35 8.36 8.41	19.56 21.79 23.97 26.13 28.24 30.33 32.38 34.40 36.40 88.88 40.33	6.83 6.98 7.60 8.20 8.77 9.83 9.86 10.38 10.88 11.36 11.83	1.59 1.58 1.58 1.57 1.57 1.56 1.56 1.56 1.56	425 44 44 44 44 44 44 44

## PROPERTIES OF SPECIAL ANGLES. EQUALLEGS.

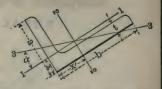


1	2	8	4	5	6	7	8
Section	Dimensions.	Thickness	Weight per Poot.	Area of Section.	Distance of Center of Gravity from Back of Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
	axa	t		Δ	x	I	S
	Inches.	Inch.	Pounds.	Sq. Ins.	Inch.	Inches.4	Inches.8
A36	3/4 x 3/4	1/8 16	.59 .84	.17	.23 .25	.009	.017 .024
A37	1 x 1	1/8 1/6 1/4	.80 1.16 1.49	.23 .34 .44	.30 .32 .34	.022 .030 .037	.031 .044 .056
A28	11/4×11/4	1/8 3 16 1/4	1.01 1.48 1.92	.30 .43 .56	.36 .38 .40	.044 .061 .077	.049 .071 .091
## ## ## ## ## ## ## ## ## ## ## ## ##	1%x1%	1/8 3 16 1/4 5 16 2/8	1.44 2.12 2.77 3.39 3.99	.42 .62 .81 1.00 1.17	.48 .51 .53 .55 .57	.13 .18 .23 .27 .31	.10 .14 .19 .23 .26
A41 "	2½x2½ «	16 1/4 1/4 16	2.75 3.62 4.5	.81 1.06 1.31	.63 .65 .68	.39 .50 .61	.24 .32 .39
A43	2¾x2¾ "	1/4 	4.5 5.6 6.8	1.31 1.62 1.92	.78 .80 .82	.95 1.15 1.33	.48 .59 .69
A47	5 x 5	3/8 1/2 916 1/2 916 5/8 116 3/4	12.3 14.3 16.2 18.1 20.0 21.8 23.6	3.61 4.18 4.75 5.31 5.86 6.40 6.94	1.39 1.41 1.43 1.46 1.48 1.50 1.52	8.74 10.02 11.25 12.44 13.58 14.68 15.74	2.42 2.79 3.16 3.51 3.86 4.20 4.52

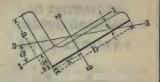
## PROPERTIES OF SPECIAL ANGLES. EQUAL LEGS.



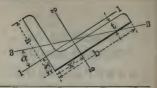
9	10	11	12	13	1
Radius of Gyration Axis 1-1.	Distance of Center of Gravity from External Apex.	Least Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.	Least Radins of Gyration Axis 2-2.	Section Number
r	x"	I"	S"	r"	
Inch.	Inch.	Inches.4	Inches.3	Inch.	
.22 .23	.33	.004	.011 .014	.14	A36
.30 .30 .29	.42 .45 .48	.009 .013 .016	.021 .028 .034	.19 .19 .19	A87
.38 .88 .87	.51 .54 .57	.018 .025 .033	.085 .047 .057	.24 .24 .24	A38
.55 .54 .53 .52 .51	.68 .72 .75 .78 .81	.051 .073 .094 .113 .133	.076 .10 .13 .15	.35 .34 .34 .34 .34	A40
.70 .69 .68	.89 .92 .96	.16 .21 .25	.18 122 .26	.44 .44 .44	A41 "
.85 .84 .83	1.10 1.13 1.17	.38 .47 .55	.35 .41 .47	.54 .54 .58	A43
1.56 1.55 1.54 1.53 1.52 1.51 1.50	1.96 2.00 2.03 2.06 2.09 2.12 2.15	3.53 4.05 4.56 5.06 5.55 6.03 6.53	1.79 2.03 2.25 2.46 2.66 2.84 3.04	.99 .98 .98 .98 .97 .97	A47



1	2	3	4	5	6	7	8
Section Number.	Dimensions.	Thickness	Weight per Foot.	Area of Section.	Distance of Center of Gravity from Back of Longer Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
	Inches.	Inch.	Pounds.	Sq. Ins.	Inch.	Inches.4	Inches.3
A91	2½ x 2	3 16 1/4 7 18 8 8 8 7 16 1/2	2.75 3.62 4.5 5.3 6.1 6.8	.81 1.06 1.31 1.55 1.78 2.00	.51 .54 .56 .58 .60 .68	.29 .37 .45 .51 .58 .64	.20 .25 .31 .36 .41 .46
<b>A93</b> « « « «	3 x 2½	1/4 8 16 8/8 7 16 1/2 9	4.5 5.6 6.6 7.6 8.5 9.5	1.81 1.62 1.92 2.22 2.50 2.78	.66 .68 .71 .73 .75 .77	.74 .90 1.04 1.18 1.30 1.42	.40 .49 .58 .66 .74
A95	3½ x 2½ « « «	1/4 16 8/8 7 16 1/2 2 16	4.9 6.1 7.2 8.3 9.4 10.4	1.44 1.78 2.11 2.43 2.75 3.06	.61 .64 .66 .68 .70	.78 .94 1.09 1.23 1.36 1.49	.41 .50 .59 .68 .76
A97	31/2 x 3	1/4 1/2   1/	5.4 6.6 7.9 9.1 10.2 11.4 12.5 13.6 14.7 15.8 16.8	1.56 1.93 2.30 2.65 3.00 3.34 3.67 4.00 4.31 4.62 4.92	.79 .81 .83 .85 .88 .90 .92 .94 .96 .98	1.30 1.58 1.85 2.09 2.33 2.55 2.76 2.96 3.15 8.83 3.50	.58 .72 .85 .98 1.10 1.21 1.33 1.44 1.54 1.65
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 x3	56 (8) pe (23 de (3 de (4 m)e (8	7.2 8.5 9.8 11.1 12.4 13.6 14.8 16.0 17.1 18.3	2.09 2.48 2.87 3.25 8.62 8.98 4.34 4.69 5.08 5.36	.76 .78 .80 .83 .85 .87 .89 .92 .94	1.65 1.92 2.18 2.42 2.66 2.87 3.08 3.28 3.47 3.66	.73 .87 .99 1.12 1.23 1.35 1.46 1.57 1.68



9	10	11	12	18	14	15	1
Radius of Gyration Axis 1-1.	Distance of Center of Gravity from back of Shorter Leg.	Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2,	Radius of Gyration Axis 2-2.	Tangent of Angle.	Least Radius of Gyration Axis 3-3.	Section Number.
r	x'	I'	S'	r'	α	I''	AT GLANDON.
Inch.	Inch.	Inches.4	Inches.3	Inches.	a	Inch.	
.60 .59 .58 .58 .57 .56	.76 .79 .81 .83 .85	.51 .65 .79 .91 1.08 1.14	.29 .38 .47 .55 .62 .70	.79 .78 .78 .77 .76 .76	.632 .626 .620 .614 .607	.43 .42 .42 .42 .42 .42	491 4 4 4
.75 .74 .74 .78 .72 .72	.91 .98 .96 .98 1.00 1.02	1.17 1.42 1.66 1.88 2.08 2.28	.56 .69 .81 .93 1.04 1.15	.95 .94 .93 .92 .91	.684 .680 .676 .672 .666	.53 .53 .52 .52 .52	# # # # # # # # # # # # # # # # # # #
.74 .78 .72 .71 .70 .70	1.11 1.14 1.16 1.18 1.20 1.23	1.80 2.19 2.56 2.91 3.24 3.55	.75 .93 1.09 1.26 1.41 1.56	1.12 1.11 1.10 1.09 1.09 1.08	.506 .501 .496 .491 .486 .480	.54 .54 .54 .53 .53	<b>A95</b> « « « «
.91 .90 .89 .88 .87 .86 .85 .85	1.04 1.06 1.08 1.10 1.13 1.15 1.17 1.19 1.21 1.23 1.25	1.91 2.33 2.72 3.10 3.45 3.79 4.11 4.41 4.70 4.98 5.24	.78 .95 1.13 1.29 1.45 1.61 1.76 1.91 2.05 2.20 2.33	1.11 1.10 1.09 1.08 1.07 1.07 1.06 1.05 1.04 1.04 1.03	.727 .724 .721 .718 .714 .711 .707 .703 .698 .694 .689	.63 .62 .62 .62 .62 .62 .62 .62 .62	A97
.89 .88 .87 .86 .86 .84 .84 .83	1.26 1.28 1.30 1.33 1.35 1.87 1.89 1.42 1.44 1.46	3.38 3.96 4.52 5.05 6.55 6.03 6.49 6.93 7.35 7.75	1.23 1.46 1.68 1.89 2.09 2.30 2.49 2.68 2.87 8.05	1.27 1.26 1.25 1.25 1.24 1.23 1.22 1.22 1.21	.554 .551 .547 .548 .538 .534 .529 .524 .518	.65 .64 .64 .64 .64 .64 .64	A99

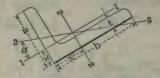


1	2	3	4	5	6	7	8
Section	Dimensions,	Thickness.	Weight per Foot,	Aren of Section.	Distance of Center of Gravity from Back of Longer Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
Kumber.	bxa	t		A	I	I	8
	Inches.	Inch.	Pounds.	Sq. Ins.	Inch.	Inches.4	Inches.3
\$101 *** *** *** *** *** *** ***	5 x8		8.2 9.8 11.3 12.8 14.3 15.7 17.1 18.5 19.9 21.2	2.40 2.86 3.31 3.75 4.18 4.61 5.03 5.44 5.84 6.28	.68 .70 .73 .75 .77 .80 .82 .84 .86	1.75 2.04 2.32 2.58 2.88 3.06 3.29 3.51 8.71 3.91	.75 .89 1.02 1.15 1.27 1.39 1.51 1.62 1.74 1.85
A108	5 x81/2	Party of the Control	8.7 10.4 12.0 13.6 15.2 16.8 18.3 19.8 21.3 22.7 24.2	2.56 3.05 3.53 4.00 4.47 4.92 5.37 5.81 6.25 6.67 7.09	.84 .86 .88 .91 .93 .95 .97 1.00 1.02 1.04 1.06	2.72 3.18 3.63 4.05 4.45 4.88 5.20 5.55 5.89 6.21 6.52	1.02 1.31 1.39 1.56 1.73 1.90 2.06 2.22 2.37 2.52 2.67
A105	6 x81/2	# 10 m 10	11.7 13.5 15.3 17.1 18.9 20.6 22.4 24.0 25.7 27.3 28.9	8.42 8.97 4.50 5.03 5.55 6.06 6.56 7.06 7.55 8.03 8.50	.79 .81 .83 .86 .88 .90 .93 .95 .97 .99	3.34 3.81 4.25 4.67 5.08 5.47 5.84 6.20 6.55 6.88 7.21	1.23 1.41 1.59 1.77 1.94 2.11 2.27 2.43 2.59 2.74 2.90
#107	6 x4	#/0 # 1 / 2 / 4 / 5 / 5 / 5 / 5 / 5 / 5 / 5 / 5 / 5	12.3 14.3 16.2 18.1 20.0 21.8 23.6 25.4 27.2 28.9 30.6	8.61 4.18 4.75 5.31 5.86 6.40 6.94 7.47 7.98 8.50 9.00	.94 .96 .99 1.01 1.08 1.06 1.08 1.10 1.12 1.14 1.17	4.90 5.60 6.27 6.91 7.52 8.11 8.68 9.23 9.75 10.26 10.76	1.60 1.85 2.08 2.31 2.54 2.76 2.97 3.18 3.39 3.59 3.79



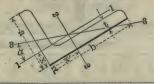
9	10	11	12	18	14	15	1
Radius of Gyration Axis 1-1.	Distance of Center of Gravity from Back of Shorter Leg.		Section Medulus Axis 2-2.	Radius of Gyration Axis 2-2.	Tangent of Angle.	Least Radius of Gyration Axis 3-3.	Section Number.
r	x'	I'	B'	r'	α	T"	number.
Inch.	Inches.	Inches.4	Inches.3	Inch.		Inch.	
.85 .84 .84 .83 .82 .82 .81 .80 .80	1.68 1.70 1.73 1.75 1.77 1.80 1.82 1.84 1.86 1.88	6.26 7.37 8.43 9.45 10.43 11.37 12.28 13.15 13.98 14.78	1.89 2.24 2.54 2.91 3.23 3.55 3.86 4.16 4.46 4.75	1.61 1.61 1.60 1.59 1.58 1.57 1.56 1.55 1.55	.368 .364 .361 .357 .353 .349 .345 .340 .336 .331	.65 .65 .65 .65 .64 .64 .64	A101
1.08 1.02 1.01 1.01 1.00 .99 .98 .98 .97 .96	1.59 1.61 1.68 1.66 1.70 1.72 1.75 1.77 1.77	6.60 7.78 8.90 9.99 11.03 12.03 12.99 13.92 14.81 15.67 16.49	1.94 2.29 2.64 2.99 3.32 3.65 3.97 4.28 4.58 4.58 5.17	1.61 1.59 1.58 1.57 1.56 1.56 1.55 1.54 1.53	489 485 482 479 476 472 468 464 460 455 451	.77 .76 .76 .75 .75 .75 .75 .75 .75	A108
99 98 97 96 96 94 94 93 93	2.04 2.06 2.08 2.11 2.13 2.15 2.18 2.20 2.22 2.24 2.26	12.86 14.76 16.59 18.37 20.08 21.74 23.34 24.89 26.39 27.84 29.15	3.24 3.75 4.24 4.72 5.19 5.65 6.10 6.55 6.98 7.41 7.80	1.94 1.93 1.92 1.91 1.90 1.89 1.88 1.87 1.86 1.85	.850 .947 .844 .841 .838 .984 .831 .827 .828 .820 .817	.77 .76 .76 .75 .75 .75 .75 .75 .75	A105
1.17 1.16 1.15 1.14 1.13 1.13 1.12 1.11 1.11 1.10 1.09	1.94 1.96 1.99 2.01 2.03 2.06 2.08 2.10 2.12 2.12 2.14	13.47 15.46 17.40 19.26 21.07 22.82 24.51 26.15 27.73 29.26 30.75	3.82 3.83 4.83 4.83 5.31 5.78 6.25 6.70 7.15 7.59 8.02	1.93 1.92 1.91 1.90 1.89 1.88 1.87 1.86 1.86	446 448 440 438 431 428 425 421 418 414	88 87 87 86 86 86 86 86 86	A107

## PROPERTIES OF SPECIAL ANGLES. UNEQUAL LEGS.



1	2	8	4	Ď	6	77	8
Section	Dimensions.	Thickness.	Weight per Foot.	Area of Section.	Distance of Center of Gravity from Back of Longer Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
Number.	bra	ŧ		A	X	I	15
	Inches.	Inch.	Pounds.	Sq. Ins.	Inch.	Inches.4	Inches.3
A129	3 x 2	16 1/4 5 16 8/8 16 1/2	3.07 4.1 5.0 5.9 6.8 7.7	.90 1.19 1.47 1.73 2.00 2.25	.47 .49 .51 .54 .56 .58	.31 .39 .47 .54 .61 .67	.20 .26 .32 .37 .42 .47
A131	4 x 8½	5 16 8 8 7 16 1/2 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6	7.7 9.1 10.6 11.9 13.3 14.7 16.0	2.25 2.67 3.09 3.50 3.90 4.30 4.68	.98 .96 .98 1.00 1.02 1.04 1.07	2.55 2.99 3.40 3.79 4.17 4.49 4.86	1.17 1.35 1.52 1.68 1.83 2.00
A135	5 x4	3/8 76 1/2 9 16 5/8 11	11.0 12.8 14.5 16.2 17.8 19.5	3.23 3.75 4.25 4.75 5.23 5.72	1.08 1.05 1.07 1.10 1.12 1.14	4.66 5.32 5.96 6.56 7.14 7.70	1.57 1.81 2.04 9.26 2.48 2.69
A109	7 x 8½	7 6 /2 9 6 /2 1 6 /4 3 6 /2 5	15.0 17.0 19.1 21.0 23.0 24.9 26.8 28.7 30.5 32.3	4.40 5.00 5.59 6.17 6.75 7.31 7.87 8.42 8.97 9.50	.75 .78 .80 .82 .87 .87 .89 .91 .94	3.95 4.41 4.86 5.28 5.69 6.08 6.46 6.83 7.18 7.53	1.44 1.62 1.80 1.97 2.14 2.31 2.48 2.64 2.80 2.96
A112	8 x 6	1/2 -16 /8 116 /4 316 / 2 516 11	23.0 25.7 28.5 31.2 23.8 36.5 39.1 41.7 44.2	6.75 7.56 8.36 9.15 9.94 10.72 11.48 12.25 13.00	1.47 1.50 1.52 1.54 1.56 1.69 1.61 1.63 1.65	21.68 24.04 26.33 28.56 30.72 32.82 34.86 36.85 38.78	4.79 5.34 5.88 6.40 6.99 7.44 7.94 8.43 8.92

## PROPERTIES OF SPECIAL ANGLES. UNEQUAL LEGS.



9	10	11	12	13	14	15	1
Radius of Gyration Axis 1-1.	Distance of Center of Gravity from Back of Shorter Leg.	Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.	Radius of Gyration Axis 2-2.	Tangent of Angle.	Radius of Gyration Axis 3-3.	Section Number.
r	x'	I'	3'	r'	α	I"	Mumber.
Inch.	Inches.	Inches.4	Inches.3	Inches.		Inch.	
.58 .57 .57 .56 .55	.97 .99 1.02 1.04 1.06 1.08	.84 1.09 1.32 1.53 1.78 1.92	.41 .54 .66 .78 .89 1.00	.97 .96 .95 .94 .98	.446 .440 .434 .428 .421 .414	.44 .43 .43 .43 .43 .43 .43	A129
1.07 1.06 1.05 1.04 1.08 1.02 1.02	1.18 1.21 1.23 1.25 1.27 1.29 1.32	3.56 4.18 4.76 5.32 5.86 6.37 6.86	1.26 1.49 1.72 1.94 2.15 2.35 2.56	1.26 1.25 1.24 1.23 1.23 1.22 1.21	.757 .755 .753 .750 .747 .742 .742	.78 .78 .72 .72 .72 .72 .72	A181
1.20 1.19 1.18 1.18 1.17 1.16	1.58 1.55 1.57 1.60 1.62 1.64	8.14 9.32 10.46 11.55 12.61 13.62	2.34 2.70 3.05 8.39 3.73 4.05	1.59 1.58 1.57 1.56 1.55 1.54	.681 .629 .626 .623 .620 .617	.85 .85 .85 .84 .84	A185
.95 .94 .93 .93 .92 .91 .90 .89	2.50 2.53 2.55 2.57 2.60 2.62 2.64 2.66 2.69 2.71	22.56 25.41 28.18 30.86 33.47 85.99 38.45 40.82 43.13 45.87	5.01 5.68 6.34 6.96 7.60 8.22 8.83 9.42 10.00 10.58	2.26 2.25 2.24 2.28 2.22 2.21 2.20 2.19 2.19	.267 .264 .262 .259 .257 .257 .250 .247 .244 .241	.76 .75 .75 .74 .74 .74 .74 .74	A109
1.79 1.78 1.77 1.77 1.76 1.75 1.74 1.73	2.47 2.50 2.52 2.54 2.56 2.61 2.63 2.65	44.31 49.26 54.10 58.82 68.42 67.92 72.32 76.59 80.78	8.02 8.95 9.87 10.77 11.67 12.55 13.41 14.27 15.11	2.56 2.55 2.54 2.54 2.58 2.52 2.51 2.50 2.49	.558 .556 .554 .553 .549 .546 .545 .545	1.30 1.30 1.29 1.29 1.28 1.28 1.28 1.28 1.28	A112

#### MOMENTS OF INERTIA OF RECTANGLES. I

Neutral ...

Axis

Depths 2 to 60 inches; widths 4 to 1 inch, varying by 16 inch.

Depth		Width of Rectangle in Inches.										
in Inches.	1/4	5 16	38	7 16	1/2	9 16	58					
2 3 4	.17 .56 1.33	.21 .70 1.67	.25 .84 2.00	.29 .98 2.33	.33 1.13 2.67	.38 1.27 3.00	1.41 3.33					
5 6 7 8 9	2.60 4.50 7.15 10.67 15.19	3.26 5.63 8.93 13.33 18.98	3.91 6.75 10.72 16.00 22.78	4.56 7.88 12.51 18.67 26.58	5.21 9.00 14.29 21.33 30.38	10.13 16.08 24.00 34.17	6.51 11.25 17.86 26.67 37.97					
10 · 11 12 13 14	20.83	26.04	31.25	36.46	41.67	46.87	52.08					
	27.73	34.66	41.59	48.53	55.46	62.39	69.32					
	36.00	45.00	54.00	63.00	72.00	81.00	90.00					
	45.77	57.21	68.66	80.10	91.54	102.98	114.43					
	57.17	71.46	85.75	100.04	114.33	128.63	142.92					
15	70.31	87.89	105.47	123.05	140.63	158.20	175.78					
16	85.33	106.67	128.00	149.33	170.67	192.00	213.33					
17	102.35	127.94	153.53	179.12	204.71	230.30	255.89					
18	121.50	151.88	182.25	212.63	243.00	273.38	303.75					
19	142.90	178.62	214.34	250.07	285.79	321.52	357.24					
20	166.67	208.33	250.00	291.67	333.33	375.00	416.67					
21	192.94	241.17	289.41	337.64	385.88	434.11	482.34					
22	221.83	277.29	332.75	388.21	443.67	499.13	554.58					
23	253.48	316.85	380.22	443.59	506.96	570.33	633.70					
24	288.00	360.00	432.00	504.00	576.00	648.00	720.00					
25	325.52	406.90	488.28	569.66	651.04	732.42	813.80					
26	366.17	457.71	549.25	640.79	732.33	823.88	915.42					
27	410.06	512.58	615.09	717.61	820.13	922.64	1025.16					
28	457.33	571.67	686.00	800.33	914.67	1029.00	1143.33					
29	508.10	635.13	762.16	889.18	1016.21	1143.23	1270.26					
30	562.50	703.13	843.75	984.38	1125.00	1265.63	1406.25					
32	682.67	853.33	1024.00	1194.67	1365.33	1536.00	1706.67					
34	818.83	1023.54	1228.25	1432.96	1637.67	1842.38	2047.08					
36	972.00	1215.00	1458.00	1701.00	1944.00	2187.00	2430.00					
38	1143.17	1428.96	1714.75	2000.54	2286.33	2572.13	2857.92					
40	1333.33	1666.67	2000.00	2333.33	2666.67	3000.00	3333.33					
42	1543.50	1929.38	2315.25	2701.13	3087.00	3472.88	3858.75					
44	1774.67	2218.33	2662.00	3105.67	3549.33	3993.00	4436.67					
46	2027.83	2534.79	3041.75	3548.71	4055.67	4562.63	5069.58					
48	2304.00	2880.00	<b>34</b> 56.00	4032.00	4608.00	5184.00	5760.00					
50	2604.17	3255.21	3906.25	4557.29	5208.33	5859.38	6510.42					
52	2929.33	3661.67	4394.00	5126.33	5858.67	6591.00	7323.33					
54	3280.50	4100.63	4920.75	5740.88	6561.00	7381.13	8201.25					
56	3658.67	4573.33	5488.00	6402.67	7317.33	8232.00	9146.67					
58	4064.83	5081.04	8097.85	7113.46	8129.67	9145.87	10162.08					
00	4500.00	5625.00	6750.00	7875.00	9000.00	10125.00	11250.00					

#### MOMENTS OF INERTIA OF RECTANGLES. I

Neutral

Axis

Depths 2 to 60 inches; widths 1/4 to 1 inch, varying by 1/8 inch.

	Width	of Rectan	gle in Inc	ches.		Depth
11	3 4	13	7 8	15	1	in Inches.
.46	.50	.54	.58	.63	.67	2 3 4
1.55	1.69	1.83	1.97	2.11	2.25	
3.67	4.00	4.33	4.67	5.00	5.33	
7.16	7.81	8.46	9.11	9.77	10.42	5
12.38	13.50	14.63	15.75	16.88	18.00	6
19.65	21.44	23.22	25.01	26.80	28.58	7
29.33	32.00	34.67	37.33	40.00	42.67	8
41.77	45.56	49.36	53.16	56.95	60.75	9
57.29	62.50	67.71	72.92	78.13	83.33	10
76.26	83.19	90.12	97.05	103.98	110.92	11
99.00	108.00	117.00	126.00	135.00	144.00	12
125.87	137.31	148.75	160.20	171.64	183.08	13
157.21	171.50	185.79	200.08	214.38	228.67	14
193.36	210.94	228.52	246.09	263.67	281.25	15
234.67	256.00	277.33	298.67	320.00	341.33	16
281.47	307.06	332.65	358.24	383.83	409.42	17
334.13	364.50	394.88	425.25	455.63	486.00	18
292.96	428.69	464.41	500.14	535.86	571.58	19
458.33	500.00	541.67	583.33	625.00	666.67	20
530.58	578.81	627.05	675.28	723.52	771.75	21
610.04	665.50	720.96	776.42	831.87	887.33	22
697.07	760.44	823.81	887.18	950.55	1013.92	23
792.00	864.00	936.00	1008.00	1080.00	1152.00	24
895.18	976.56	1057.94	1139.32	1220.70	1302.08	25
1006.96	1098.50	1190.04	1281.58	1373.13	1464.67	26
1127.67	1230.19	1332.70	1435.22	1537.73	1640.25	27
1257.67	1372.00	1486.33	1600.67	1715.00	1829.33	28
1397.29	1524.31	1651.34	1778.36	1905.39	2032.42	29
1546.88	1687.50	1828.13	1968.75	2109.38	2250.00	30
1877.33	2048.00	2218.67	2389.33	2560.00	2730.67	32
2251.79	2456.50	2661.21	2865.92	3070.63	3275.33	34
2673.00	2916.00	3159.00	3402.00	3645.00	3888.00	36
3143.71	3429.50	3715.29	4001.08	4286.88	4572.67	38
3666.67	4000.00	4333.33	4666.67	5000.00	5333.33	40
4244.63	4630.50	5016.38	5402.25	5788.13	6174.00	42
4880.33	5324.00	5767.67	6211.33	6655.00	7098.67	44
5576.54	6983.50	6590.46	7097.42	7604.38	8111.33	46
6336.00	6912.00	7488.00	8064.00	8640.00	9216.00	48
7161.46	7812.50	8463.54	9114.58	9765.63	10416.67	50
8055.67	8788.00	9520.33	10252.67	10985.00	11717.33	52
9021.38	9841.50	10661.63	11481.75	12301.88	13122.00	54
10061.33	10976.00	11899.67	12805.33	13720.00	14634.67	56
11178.29	12194.50	13210.71	14226.92	15243.12	16259.33	58
12375.00	13500.00	14625.00	15750.00	16875.00	18000.00	60

### MOMENTS OF INERTIA OF RECTANGLES. II ONE INCH WIDE.

NEUTRAL AXIS Value for an

Value for any width may be obtained from tabular value by direct multiplication.

Depth		Additional Depth in Fractions of an Inch.										
in Inches.	0	1 16	1 8	3 16	1/4	5 16	8	7 16				
0 1 2 3	.08333 .66667 2.2500 5.3333	.00002 .09995 .73114 2.3936 5.5873	.00016 .11865 .79964 2.5431 5.8491	.00055 .13955 .87229 2.6988 6.1190	.00130 .16276 .94922 2.8607 6.3971	.00254 .18842 1.0305 3.0289 6.6002	.00439 .21663 1.1164 3.2036 6.9783	.00698 .24754 1.2068 3.3849 7.2817				
5 6 7 8	10.417 18.000 28.583 42.667 60.750	10.812 18.568 29.356 43.674 62.024	11.218 19.149 30.142 44.698 63.317	11.633 19.741 30.942 45.737 64.626	12.059 20.345 31.757 46.793 65.954	12.494 20.961 32.585 47.864 67.300	12.941 21.590 33.428 48.952 68.665	13.397 22.232 34.285 50.056 70.047				
10	83.333	84.906	86.498	88.109	89.741	91.392	93.064	94.756				
11	110.92	112.82	114.74	116.69	118.65	120.64	122.65	124.68				
12	144.00	146.26	148.55	150.86	153.19	155.55	157.93	160.33				
13	183.08	185.74	188.42	191.12	193.85	196.61	199.39	202.20				
14	228.67	231.74	234.85	237.98	241.14	244.32	247.54	250.78				
15	281.25	284.78	288.34	291.93	295.55	299.20	302.87	306.58				
16	341.33	345.35	349.40	353.47	357.58	361.73	365.90	370.11				
17	409.42	413.95	418.52	423.11	427.75	432.41	437.11	441.85				
18	486.00	491.41	496.20	501.35	506.53	511.75	517.01	522.31				
19	571.58	577.24	582.94	588.67	594.44	600.25	606.10	611.98				
20	666.67	672.94	679.24	685.59	691.84	698.41	704.87	711.38				
21	771.75	778.66	785.61	792.61	799.65	806.72	813.84	821.00				
22	887.33	894.92	902.54	910.21	917.93	925.68	933.49	941.33				
23	1013.9	1022.2	1030.5	1038.9	1047.3	1055.8	1064.3	1072.9				
24	1152.0	1161.0	1170.1	1178.4	1188.4	1197.6	1206.8	1216.2				
25	1302.1	1311.9	1321.7	1331.6	1341.5	1351.5	1361.6	1371.6				
26	1464.7	1475.3	1485.9	1496.6	1507.3	1518.1	1529.0	1539.9				
27	1640.2	1651.7	1663.1	1674.7	1686.2	1697.9	1709.5	1721.3				
28	1829.3	1841.6	1853.9	1866.3	1878.8	1891.3	1903.8	1916.4				
29	2032.4	2045.6	2058.8	2072.1	2085.4	2098.8	2112.3	2125.8				
30	2250.0	2264.1	2278.2	2292.4	2306.7	2321.0	2335.4	2349.9				
31	2482.6	2497.6	2512.7	2527.9	2543.1	2558.4	2573.8	2589.2				
32	2730.7	2746.7	2762.8	2778.9	2795.2	2811.4	2827.8	2844.2				
33	2994.7	3011.8	3028.9	3046.1	3063.3	3080.4	3098.0	3115.4				
34	3275.3	3293.4	3311.6	3329.8	3348.1	3366.5	3384.9	3403.4				
35	3572.9	3592.0	3611.3	3630.6	3650.0	3669.5	3689.0	3708.6				
36	3888.0	3908.3	3928.6	3949.1	3969.6	3990.1	4010.8	4031.5				
37	4221.1	4242.5	4264.0	4285.6	4307.3	4328.9	4350.7	4372.6				
38	4572.7	4595.3	4617.9	4640.7	4663.5	4686.4	4719.4	4732.4				
39	4943.3	4967.0	4990.9	5014.9	5038.9	5063.0	5087.2	5111.5				
40	5333.3	5358.4	5383.5	5408.7	5433.9	5459.3	5484.7	5510.2				
41	5743.4	5769.7	5796.1	5822.6	5849.1	5875.7	5902.5	5929.2				
42	6174.0	6201.6	6229.3	6257.1	6284.9	6312.8	6340.9	6368.9				
43	6625.6	6654.5	6683.5	6703.5	6741.8	6771.1	6800.4	6829.9				
44	7098.7	7129.0	7159.3	7189.0	7220.3	7251.0	7281.7	7312.5				
45.	7593.8	7625.4	7657.2	7689.1	7721.0	7753.0	7785.2	7817.4				
46	8111.3	8144.7	8177.6	8210.9	8244.3	8277.8	8311.3	8345.0				
47	8651.9	8686.5	8721.1	8755.9	8790.7	8825.6	8860.7	8895.8				
48	9216.0	9252.0	9288.2	9324.4	9360.7	9397.2	9433.7	9470.3				
49	9804.1	9841.6	9879.3	9833.7	9954.9	9992.9	10031	10071				
50	10417	10456	10495	10534	10574	10613	10653	10692				

#### MOMENTS OF INERTIA OF RECTANGLES. II

#### ONE INCH WIDE.

NEUTRAL AXIS

Value for any width may be obtained from tabular value by direct multiplication.

Additional Depth in Fractions of an Inch.											
1 2	9 16	5 8	$\frac{1}{1}\frac{1}{6}$	3 4	13	7/8	$\frac{15}{16}$	in Inches.			
.01041	.01483	.02034	.02708	.03516	.04469	.05583	.06866	0			
.28125	.31789	.35758	.40045	.44661	.49620	.54932	.60610	1			
1.3021	1.4022	1.5073	1.6176	1.7331	1.8539	1.9803	2.1123	2			
3.5729	3.7678	3.9696	4.1784	4.3945	4.6179	4.8488	5.0872	3			
7.5937	7.9146	8.2443	8.5831	8.9310	9.2882	9.6548	10.031	4			
13.865	14.343	14.832	15.331	15.843	16.365	16.898	17.443	5			
22.885	23.552	24.231	24.924	25.629	26.347	27.079	27.825	6			
35.156	36.043	36.944	37.859	38.790	39.736	40.698	41.674	7			
51.177	52.314	53.468	54.639	55.827	57.032	58.254	59.493	8			
71.448	72.867	74.305	75.762	77.238	78.733	80.247	81.780	9			
96.469	98.202	99.955	101.73	103.52	105.34	107.18	109.04	10			
126.74	128.82	130.92	133.04	135.19	137.35	139.55	141.76	11			
162.76	165.21	167.69	170.19	.172.72	175.28	177.85	180.46	12			
205.03	207.89	210.78	213.69	216.63	219.60	222.60	225.62	13			
254.05	257.35	260.68	264.04	267.42	270.83	274.28	277.75	14			
310.32	314.09	317.89	321.72	325.58	329.47	333.40	337.35	15			
374.34	378.61	382.92	387.25	391.62	396.02	400.45	404.92	16			
446.61	451.42	456.25	461.12	466.03	470.97	475.94	480.95	17			
527.63	533.00	538.40	543.84	549.32	554.83	560.38	565.96	18			
617.91	623.87	629.87	635.90	641.98	648.09	654.24	660.44	19			
717.93	724.51	731.14	737.81	744.51	751.26	758.05	764.88	20			
828.20	835.44	842.73	850.05	857.43	864.84	872.29	879.79	21			
949.22	957.15	965.13	973.15	981.21	989.32	997.47	1005.7	22			
1081.5	1090.1	1098.8	1107.6	1116.4	1225.2	1134.1	1143.0	23			
1225.5	1234.9	1244.4	1253.9	1263.4	1273.0	1282.6	1292.3	24			
1381.8	1392.0	1402.2	1412.5	1422.8	1433.2	1443.6	1454.1	25			
1550.8	1561.8	1572.8	1584.0	1595.1	1606.3	1617.6	1628.9	26			
1733.1	1744.9	1756.8	1768.8	1780.8	1792.8	1804.9	1817.1	27			
1929.1	1941.8	1954.6	1967.4	1980.3	1993.2	2006.2	2019.3	28			
2139.4	2153.0	2166.7	2180.4	2194.2	2208.1	2222.0	2236.0	29			
2364.4	2378.9	2393.6	2408.3	2423.0	2437.8	2452.7	2467.6	30			
2604.7	2620.2	2635.8	2651.4	2667.2	2682.9	2698.8	2714.7	31			
2860.7	2877.2	2893.8	2910.5	2927.2	2944.0	2960.8	2977.8	32			
3132.9	3150.5	3168.1	3185.8	3203.6	3221.4	3239.3	3257.3	33			
3422.0	3440.6	3459.3	3478.1	3496.9	3515.8	3534.8	3553.8	34			
3728.2	3748.0	3767.8	3787.6	3807.6	3827.6	3847.6	3867.8	35			
4052.3	4073.1	4094.0	4115.0	4136.1	4157.2	4178.4	4199.7	36			
4394.5	4416.5	4438.6	4460.8	4483.0	4505.3	4527.7	4550.1	37			
4755.5	4778.7	4802.0	4825.4	4848.8	4872.3	4895.9	4919.5	38			
5135.8	5160.2	5184.7	5209.3	5239.6	5285.3	5283.5	5308.4	39			
5535.8	5561.5	5587.3	5613.1	5639.0	5665.0	5691.0	5717.2	40			
5956.1	5983.1	6010.1	6037.0	6064.4	6091.7	6119.0	6146.5	41			
6397.1	6425.4	6453.7	6482.2	6510.7	6539.3	6568.0	6596.7	42			
6867.7	6889.0	6918.7	6948.5	6978.3	7008.3	7038.3	7068.5	43			
7343.4	7374.4	7405.5	7436.6	7467.9	7499.2	7530.6	7562.1	44			
7849.7	7882.1	7914.6	7947.1	7979.8	8012.5	8045.4	8078.3	45			
8378.7	8412.5	8466.5	8480.5	8514.6	8548.8	8583.1	8617.4	46			
8931.0	8966.3	9001.7	9037.2	9072.7	9108.4	9144.2	9180.0	47			
9507.0	9544.1	9580.7	9617.7	9654.8	9692.0	9729.2	9766.6	48			
10107	10146	10184	10223	10261	10300	10339	10378	49			
10732	10772	10812	10852	10892	10933	10973	11014	50			

### PROPERTIES AND PRINCIPAL DIMENSIONS OF STANDARD T-RAILS.



Stand-		Weight						Neutral Axis 1-1.			
(See Foot	Section Number.	per Yard.	Area.	Б	đ	k	t	z	Moment of Inertia.	Section Modulus.	
Note.)		Pounds.	Sq. Ins.	Inches.	Inches.	Inches.	Inch.	Inches,	1	8	
	580 579 578 577 576	12 16 20 25 30	1.17 1.56 1.98 2.40 3.02	23/8 23/8 25/8 23/4 31/8	23/8 23/8 25/8 23/4 23/8	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3 16 32 14 19 64	.96 1.14 1.25 1.33 1.52	.67 1.23 1.93 2.50 4.10	.64 .99 1.41 1.76 2.55	
0000	575 545 549 542 537	35 40 45 50 55	3.42 3.94 4.40 4.87 5.38	3 16 3 1/2 3 11 3 17/8 4 16	3 1/2 3 1/2 3 1/2 3 1/6 3 7/8 4 1/6	1¾ 1⅓ 2 2⅓ 2¼	254 25 35 264 7 16.	1.54 1.69 1.76 1.86 1.98	5.14 6.52 8.09 9.82 12.03	2.90 3.60 4.19 4.86 5.78	
A C B C A	568 533 571 534 567	60 60 65 70	5.86 5.93 5.87 6.33 6.82	4 4 <sup>1</sup> / <sub>4</sub> 3 <sup>11</sup> / <sub>16</sub> 4 <sup>7</sup> / <sub>16</sub> 4 <sup>1</sup> / <sub>4</sub>	4½ 4¼ 4¾ 4¾ 4¾ 4¾ 4¾ 4¾ 4¾	21/4 23/8 21/8 21/8 23/2 23/8	15 31 31 31 1/2	2.13 2.06 1.95 2.15 2.20	15.41 14.56 13.30 16.72 21.05	6.50 6.65 5.94 7.30 8.26	
C B C A C	532 570 529 566 530	70 70 75 80 80	6.81 6.89 7.33 7.86 7.86	45/8 48/4 41/3 45/8 5	45/8 435/4 416/3 51/8 5	27 23/6 23/6 23/2 21/2 21/2	334 64 334 64 7 334 34 354	2.22 2.16 2.29 2.31 2.41	20.06 18.60 23.11 28.80 26.85	8.32 7.78 9.17 10.21 10.17	
B C A C B	569 531 563 535 561	80 85 90 90	7.91 8.33 8.82 8.83 8.87	47 516 518 518 449 464	415 516 558 538 517 517 517	27/16 29/16 25/8 25/8 21/6	35 64 16 16 16 16	2.27 2.47 2.54 2.57 2.45	25.10 30.34 38.70 34.43 32.30	9.40 11.15 12.52 12.25 11.45	
C B M	550 565 586 564 572	95 100 100 100 110	9.28 9.84 9.84 9.85 10.75	5 1/2 5 1/2 5 3/4 5 5/4 5 1/2	5 16 6 5 3/4 5 41 6	211 234 234 234 232 213 213	16 16 16 16 16 16 33	2.67 2.75 2.73 2.63 2.80	38.58 48.94 43.42 41.30 56.00	13.35 15.07 14.38 13.72 17.50	
M	573 574 539	120 130 150	11.76 12.76 14.71	53/4 6 .6	6½ 6½ 6	27/8 215 116 41/4	5/8 21 1	2.89 3.00 3.00	60.04 71.02 69.30	17.87 20.29 23.10	

For detail dimensions of Section No. 539, see page 26.

A; B:—Type A; Type B; American Railway Association Standard. C:—American Society of Civil Engineers Standard. M:—Manufacturers Standard.

## RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK. ANGLES WITH EQUAL LEGS.



Radii of gyration correspond to directions indicated by arrowheads.

Section	Dimensions.	Thickness.	hickness, Two Radii of Gyration.							
Number.			Angles.	ro	r <sub>1</sub>	T <sub>2</sub>	r <sub>2</sub>	T4	T <sub>5</sub>	
	Inches.	Inch.	Sq. Ins.	-0	-1	-2	-3	- 2	-0	
A11	11/2x 11/2	16		0.64	0.64	0.73	0.78	0.88		
a .	a .	*3/8		0.44	0.67	0.77	0.82	0.88		
*A40	13/4 x 13/4	1/8		0.55	0.73	0.82	0.86	0.91	1.02	
и	M	16 3/8	2.34	0.51	0.76	0.86	0.91	0.97	1.07	
A15	2 x 2	*1/8	1.44	0.63	$0.84 \\ 0.84$	$0.92 \\ 0.93$	0.97	1.02	1.12	
44 28		16 8 16 16 16	2.30	0.60	0.86	0.95	1.00	1.05	1.16	
*A41	21/4× 21/4	16 3 16	1.62	-	0.86	1.03	1.08	1.12	1.22	
. "	4	16	2.62	0.68	0.96	1.05	1.10	1.15	1.25	
A17	2½x 2½	*1/8	2.38		1.04	1.12	1.17	1.21 1.24	$\frac{1.31}{1.34}$	
a a	46	*1/8 1/4 8/8 1/2		0.75	1.07	1.16	1.21	1.26	1.36	
*A43	23/x 23/4	1/4	2.62	0.85	1.15	1.24	1.29	1.34	1.43	
at	a	1/4 5 16 3/8		0.84	1.16	1.25 1.26	1.30	1.35 1.35	1.45 1.45	
A19	3 x 3	1/4		0.93	1.26	1.34	1.39	1.43	$\frac{1.53}{1.57}$	
		16 0 16	6.12	0.89	1.30	1.39	1.44	1.49	1.59	
A21	3½x 3½	1/4 5/8 1/8		1.09	1.46	1.54	1.59	1.64	1.73	
ui I	ш	18	10.06	1.02	1.55	1.65	1.70	1.75	1.85	
A23	4 × 4	16 16 16		1.24 $1.21$	1.67	1.76	1.80	1.85	1.94	
"	W	118	11.68		1.75	1.85	1.89	-	2.04	
*A47	5 × 5	3/8 1/2 3/4	9.50	1.54	2.10	2.17 2.19	2.24	2.28	2.38	
A27	6 x 6	3/4	13.88	-	2.14	2.25	2.27	2.32	2.42	
AZ /	6 x 6	16 5/8 7/8	14.22	1.84	2.53	2.62	2.66	2.71	2.80	
A35			19.46		2.57 3.32	3.41	2.70	2.75	2.85	
	8 * 8	1/2 5/4 8/4 7/8	19.22	2.49	3.34	3.43 3.44	3.47	3.51	3.60 3.62	
	н	7/8	26.46	2.45	3.38	3.46	3.51	3.55	3.64	
	44	11/8	30.00		3.40	3.48	3.53 3.55	3.57	3.67	
-			1	1	-	1		1	1	

Angles marked \* are special sections.

## RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK. ANGLES WITH UNEQUAL LEGS.

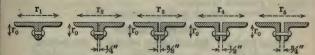


Radii of gyration correspond to directions indicated by arrowheads.

Section	Dimensions.	Thickness	Area of Two	Radii of Gyration.						
Number.	Inches,	Inch.	Angles, Sq. Ins.	r <sub>0</sub>	rı	T2	. <b>r</b> <sub>8</sub>	r4	<b>r</b> <sub>5</sub>	
A91	2½ x 2	16 8 8 1/2	1.62 3.10 4.00	0.79 0.77 0.75	0.79 0.82 0.84	0.88 0.91 0.94	0.92 0.96 0.99	0.97 1.01 1.04	1.07 1.12 1.15	
*A129	8 x2	16 16 16	1.80 2.94 4.00	0.97 0.95 0.93	0.75 0.76 0.79	0.83 0.85 0.88	0.88 0.90 0.93	0.93 0.95 0.98	1.03 1.05 1.09	
A93	3 x 21/2	1/4 8/8 9 10	2.62 3.84 5.56	0.95 0.93 0.91	1.00 1.02 1.05	1.09 1.11 1.15	1.13 1.16 1.20	1.18 1.21 1.25	1.28 1.31 1.35	
A95	8½ x 2½	1/4	2.88 5.50 6.12	1.12 1.09 1.08	0.96 1.00 1.01	1.04 1.09 1.10	1.09 1.14 1.15	1.13 1.19 1.20	1.23 1.29 1.31	
A97	8½ x 3	16 1/4 18 18	3.12 6.68 9.24	1.11 1.07 1.04	1.20 1.25 1.30	1.29 1.84 1.40	1.34 1.39 1.45	1.88 1.44 1.50	1.48 1.54 1.60	
A99	4 x8	5 16 16 16 16 16 16 16 16 16 16 16 16 16	4.18 7.24 10.06	1.27 1.24 1.21	1.17 1.21 1.25	1.25 1.30 1.35	1.30 1.34 1.40	1.34 1.39 1.45	1.44 1.49 1.55	
*A131	4 131/2	5 16 1/2 5/8	4.50 7.00 8.60	1.26 1.23 1.22	1.42 1.44 1.46	1.50 1.53 1.55	1.55 1.58 1.60	1.59 1.63 1.65	1.69 1.72 1.75	
A101	5 x8	16 16 16 16	4.80 8.36 11.68	1.61 1.58 1.55	1.09 1.13 1.17	1.17 1.22 1.27	1.22 1.26 1.32	1.26 1.31 1.37	1.86 1.41 1.47	
A108	5 x 3½	\$/8 5/8 7/8	6.10 9.84 13.34	1.60 1.56 1.53	1.34 1.37 1.42	1.42 1.46 1.51	1.46 1.51 1.56	1.51 1.56 1.61	1.60 1.66 1.71	
*A185	5 x4	3/6 1/2 5/8	6.46 8.50 10.46	1.59 1.57 1.55	1.58 1.60 1.62	1.66 1.68 1.71	1.71 1.78 1.75	1.75 1.78 1.80	1.85 1.87 1.90	
A105	6 x 81/2	3/8 5/8 7/8	6.84 11.10 15.10	1.94 1.90 1.87	1.26 1.30 1.34	1.34 1.39 1.44	1.39 1.43 1.49	1.43 1.48 1.53	1.58 1.58 1.64	
A107	6 x4	3/8 5/8 7/8	7.22 11.72 15.96	1.93 1.90 1.86	1.50 1.53 1.58	1.58 1.62 1.67	1.62 1.67 1.71	1.67 1.71 1.76	1.76 1.81 1.86	
*A109	7 x 8½	1	8.80 10.00 12.34 15.74 19.00	2.26 2.25 2.24 2.21 2.19	1.16 1.22 1.24 1.27 1.31	1.29 1.30 1.32 1.36 1.40	1.33 1.35 1.37 1.41 1.45	1.38 1.39 1.42 1.46 1.50	1.47 1.48 1.51 1.56 1.60	

Angles marked \* are special sections.

## RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK. ANGLES WITH UNEQUAL LEGS.



Radii of gyration correspond to directions indicated by arrowheads.

Section	Dimensions.	Thickness.	Area of Two		1	Radii of	Gyration	1.	
Number.	Inches.	Inch.	Angles.	r <sub>0</sub>	r <sub>1</sub>	T <sub>2</sub>	r <sub>3</sub>	<b>r</b> <sub>4</sub>	<b>T</b> 5
A91	2½×2	16 /8	1.62	0.60	1.10 1.13	1.19 1.23	1.24	1.29	1.89
*A129	8 x2	1/2	4.00 1.80 2.94	0.56 0.58 0.57	1.15 1.37 1.39	1.25 1.46 1.48	1.51	1.56	1.46
66	**	10 10	4.00	0.55	1.41	1.51	1.53 1.56	1.58 1.61	1.68 1.71
A98	8 x21/2	1/4 3/8 1/6	2.62 3.84 5.56	0.75 0.74 0.72	1.31 1.33 1.37	1.40 1.42 1.46	1.45 1.47 1.51	1.50 1.52 1.56	1.60 1.63 1.66
A95	3½ x 2½	1/4 1/2 1/6	2.88 5.50 6.12	0.74 0.70 0.70	1.58 1.62 1.64	1.67 1.72 1.73	1.72 1.77 1.78	1.76 1.81 1.83	1.86 1.92 1.93
A97	8½x8	16	3.12 6.68 9.24	0.91 0.87 0.85	1.52 1.57 1.61	1.61 1.66 1.71	1.66 1.71 1.76	1.70	1.80 1.86
A99	4 x8	18 18	4.18 7.24	0.89	1.79	1.88 1.93	1.93	1.81 1.97 2.02	1.91 2.07 2.12
*A131	4 x 31/2	18 16 1/2 6/8	10.06 - 4.50 7.00	0.83 1.07 1.04	1.88 1.73 1.76	1.97 1.81 1.85	2.02 1.86 1.89	2.08 1.91 1.94	2.18 2.00 2.04
A101	5 ×3	5/8 5/8 1/8 1/8	8.60 4.80 8.86	1.02 0.85 0.82	1.78 2.83 2.87	1.87 2.42 2.47	1.92 2.47 2.52	1.97 2.52 2.57	2.67 2.67
<b>∆</b> 103	5 x 8½	3/8 5/8 7/8	11.68 6.10 9.84	0.80 1.02 0.99	2.42 2.27 2.31	2.52 2.36 2.40	2.57 2.41 2.45	2.62 2.45 2.50	2.72 2.55 2.60
**	66	78	13.34	0.96	2.36	2.45	2.50	2.55	2.65
*A135	5 x4	3/8 1/2 5/8	6.46 8.50 10.46	1.20 1.18 1.17	2.20 2.22 2.24	2.29 2.31 2.33	2.34 2.36 2.38	2.38 2.41 2.43	2.48 2.50 2.53
A105	6 x 3½	3/8 5/8 7/8	6.84 11.10 15.10	0.99 0.96 0.93	2.81 2.86 2.90	2.90 2.95 3.00	2.95 3.00 3.05	3.00 3.05 3.10	3.09 3.15 3.20
A107	6 x4	3/8 5/8 7/8	7.22 11.72 15.96	1.17 1.13 1.11	2.74 2.78 2.82	2.88 2.87 2.92	2.87 2.92 2.97	2.92 2.97 3.02	3.02 3.06 3.12
•▲109	7 x 3½	/8 1/2 5/8 1/8	8.80	0.95	3.37	3.47	8.52 8.58	3.56	3.66 3.67 3.70
"	** **	1 1 1 1 1	12.34 15.74 19.00	0.93 0.91 0.89	3.40 3.45 3.48	3.50 3.54 3.58	3.55 3.59 3.63	3.64 3.68	3.74 3.78

Angles marked \* are special sections.

For various values of  $\frac{L}{r}$  in which L = length in feet and r = radius.of gyration in inches.

P = ultimate strength in lbs. per square inch.

#### FOR SOFT STEEL.

$$P = \frac{45\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}} Pin \ and \ square \ bearing} P = \frac{45\ 000}{1 + \frac{(12\ L)^2}{24\ 000\ r^2}} P = \frac{45\ 000}{1 + \frac{(12\ L)^2}{18\ 000\ r^2}}$$

To obtain safe unit stress:

L		e Strengt Square I	h in lbs. nch.	E r		Strengt Square I	h in lbs. nch.
r	Square.	Pin and Square	Pin.	r	Square.	Pin and Square,	Pin.
3.0	43437	42694	41978	7.6	36554	33419	30779
3.2	43230	42395	41593	7.8	36193	32966	30268
3.4	43011	42081	41190				
3.6	42782	41754	40773	8.0	35828 •	32514	29762
3.8	42543	41412	40340	8.2	35462	32064	29260
				8.4	35095	31615	28763
4.0	42294	41058	39893	8.6	34727	31169	28272
4.2	42035	40693	39435	8.8	34358	30724	27787
4.4	41765	40317	38966				
4.6	41488	39930	38485	9.0	33988	30282	27306
4.8	41203	39534	37998	9.2	33611	29844	26832
	-			9.4	33249	29408	26364
5.0	40910	39130	37500	9.6	32880	28977	25903
5.2	40608	38807	36997	9.8	32511	28549	25448
5.4	40299	38300	36488				
5.6	39984	37874	35975	10.0	32143	28125	25000
5.8	39663	37443	35457	10.2	31776	27706	24559
- 200	1			10.4	31411	27290	24125
6.0	39335	37006	34938	10.6	31054	26879	23698
6.2	39003	36566	34416	10.8	30684	26474	23279
6.4	38665	36122	33894				
6.6	38323	35676	33371	11.0	30324	26072	22866
6.8	37976	35219	32849	11.2	29965	25675	22460
				11.4	29608	25285	22063
7.0	37616	34776	32328	11.6	29247	24899	21671
7.2	37272	34324	31809	11.8	28903	24517	21288
7.4	36914	33872	31292				

For various values of  $\frac{L}{r}$  in which L = length in feet and r = radius of gyration in inches.

P = ultimate strength in lbs. per square inch.

#### FOR SOFT STEEL.

Square bearing Pin and square bearing P = 
$$\frac{45\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$$
 P =  $\frac{45\ 000}{1 + \frac{(12\ L)^2}{24\ 000\ r^2}}$  P =  $\frac{45\ 000}{1 + \frac{(12\ L)^2}{18\ 000\ r^2}}$ 

To obtain safe unit stress:

L r		Strengt Square I	h in lbs. ach.	L r	Ultimate Strength in lbs. per Square Inch.			
r	Square.	Pin and Square.	Pin.	r	Square.	Pin and Square.	Pin.	
12.0 12.2 12.4	28553 28207 27863	24142 23771 23406	20911 20542 20179	16.6 16.8	21406 21137	16960 16708	14043 13812	
12.6 12.8	27522 27185	23046 22693	19823 19474	17.0 17.2 17.4	20872 20611 20353	16459 16216 15977	13584 13366 13150	
13.0 13.2 13.4	26850 26524 26189	22343 22005 21662	19133 18797 18469	17.6 17.8	20098 19847	15742 15512	12938 12731	
13.6 13.8	25864 25543	21329 21002	18148 17833	18.0 18.2 18.4	19599 19351 19114	15286 15063 14845	12528 12329 12135	
14.0 14.2 14.4	25224 24909 24598	20680 20363 20052	17523 17221 16925	18.6 18.8	18878 18644	14630 14420	11944 11757	
14.6 14.8	24290 23985	19746 19445	16634 16350	19.0 19.2 19.4	18418 18185 17961	14218 14010 13811	11579 11394 11219	
15.0 15.2 15.4	23684 23387 23093	19148 18858 18572	16071 15799 15532	19.6 19.8	17740 17519	13616 13422	11048 10877	
15.6 15.8	22803 22516	18288 18015	15270 15105	20.0 20.2 20.4	17308 17096 16888	13235 13050 12868	10715 10553 10434	
16.0 16.2 16.4	22234 21954 21678	17744 17478 17216	14764 14518 14279	20.6 20.8	16682 16480	12690 12515	10249 10087	

For various values of  $\frac{L}{r}$  in which L = length in feet and r = radius of gyration in inches.

P = ultimate strength in lbs. per square inch.

#### FOR MEDIUM STEEL.

$$P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}} Pin \ and \ square \ bearing} P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{24\ 000\ r^2}} P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{18\ 000\ r^2}}$$

To obtain safe unit stress:

L		Strengt Square I		I.	1	Ultimate Strength in lbs. per Square Inch.				
r	Square.	Pin and Square.	Pin.	r	Square.	Pin and Square.	Pin.			
3.0 3.2 3.4	48263 48033 47790	47438 47106 46757	46642 46214 45767	7.6 7.8	40616 40214	37132 36629	34199 33631			
3.6 3.8	47536 47270	46393 46013	45303 44822	8.0 8.2 8.4	39809 39402 38994	36127 35627 35128	33069 32511 31959			
4.0 4.2 4.4	46993 46705 46406	45620 45214 44797	44325 43817 43295	8.6 8.8	38585 38175	34632 34138	31413 30874			
4.6 4.8	46098 45781	44367 43927	42761 42220	9.0 9.2 9.4	37764 37354 36943	33647 33160 32676	30340 29813 29293			
5.0 5.2 5.4	45455 45120 44777	43478 43020 42555	41667 41108 40542	9.6 9.8	36533 36123	32197 31721	28781 28275			
5.6 5.8	44427 44070	42082 41603	39972 39397	10.0 10.2 10.4	35714 35307 34901	31250 30784 30322	27778 27288 26806			
6.0 6.2 6.4	43706 43337 42961	41118 40629 40136	38820 38240 37660	10.6	34496 34093	29866 29415	26331 25865			
6.6 6.8 7.0	42581 42196	39640 39141	37079 36499	11.0 11.2 11.4	33693 33294 32898	28969 28528 28094	25407 24956 24514			
7.0 7.2 7.4	41806 41413 41016	38640 38138 37635	35920 35343 34769	11.6 11.8	32505 32114	27665 27241	24079 23653			

For various values of  $\frac{L}{r}$  in which L = length in feet and r = radius of gyration in inches.

P = ultimate strength in lbs. per square inch.

#### FOR MEDIUM STEEL.

$$P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}} \quad P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{24\ 000\ r^2}} \quad P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{24\ 000\ r^2}} \quad P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{18\ 000\ r^2}}$$

To obtain safe unit stress:

L		Strengt Square I		L		Ultimate Strength in lbs. per Square Inch.				
r	Square.	Pin and Square.	Pin.	r	Square.	Pin and Square.	Pin,			
12.0 12.2 12.4	31726 31341 30959	26824 26412 26007	23234 22824 22421	16.6 16.8	23784 23486	18844 18564	15603 15347			
12.6 12.8	30580 30205	25607 25214	22026 21638	17.0 17.2 17.4	23191 22901 22614	18288 18018 17752	15097 14851 14611			
13.0 13.2 13.4	29833 29464 29099	24826 24445 24069	21259 20886 20521	17.6 17.8	22331 22052	17491 17235	14376 14145			
13.6 13.8	28738 28381	23699 23336	20164 19814	18.0 18.2 18.4	21777 21506 21238	16984 16737 16494	13920 13699 13483			
14.0 14.2 14.4	28027 27677 27331	22978 22626 22280	19470 19134 18805	18.6 18.8	20975 20715	16256 16022	13271 13063 .			
14.6 14.8 15.0	26989 26650 26316	21940 21605 21276	18482 18167 17857	19.0 19.2 19.4 19.6	20458 20206 19957 19711	15793 15567 15346 15129	12661 12466 12275			
15.0 15.2 15.4 15.6	25985 25659	20953 20636	17554 17258 16967	19.8	19466	14913	12086			
15.8 15.8	25337 25018	20320 20017	16683 16404	20.2 20.4	18996 18764 18536	14500 14298 14100	11725 11549 11377			
16.2 16.4	24704 24393 24087	19716 19420 19129	16131 15865	20.6 20.8	18311	13905	11208			

# EXAMPLE OF THE USE OF THE TABLES OF RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK AND THE TABLES OF STRENGTH OF STEEL COLUMNS OR STRUTS.

PAGES 215 TO 221 INCLUSIVE

What is the size of truss member required to safely sustain 50 000 pounds in compression, the safety factor being 4, the unsupported length 8 feet, the gusset plates at each end being 3/3" thick?

Assume for trial two 4" x 3" x  $\frac{5}{46}$ " angles with the long legs together. Referring to page 216, the least Radius of Gyration, comparing values in columns  $r_0$  and  $r_3$  is found to be 1.27. The ratio of the length of the column in feet to the Least Radius of Gyration in inches,  $\frac{L}{}$  is, there-

fore, 
$$\frac{8}{1.27} = 6.3$$
.

Referring to the table of Strength of Steel Columns or Struts for medium steel, page 220, the ultimate strength of a column in which

 $\frac{L}{r}$  = 6.3 is found by interpolation between the values for 6.2 and 6.4

to be 43 149 pounds per square inch, which, divided by the safety factor 4, gives 10 787 pounds as the safe unit stress per square inch. Multiplying the safe unit stress per square inch, 10 787 pounds, by 4.18, the area of the two angles in square inches, gives 45 090 pounds as the total safe load. This is slightly less than the specified load of 50 000 pounds, and, therefore, it will be necessary to increase the assumed section. Assume the angles to be 4" x 3" x 3%", for which the Least Radius of Gyration is found by interpolation to be 1.26, and, by

the same process used above,  $\frac{L}{r}$  is found to be 6.35, which corre-

sponds to an ultimate strength of 43 055 pounds per square inch, or a safe unit stress of 10 764 pounds per square inch, which, if multiplied by the area of the two angles, 4.96 square inches, gives a safe total load of 53 389 pounds, which is ample to meet the conditions stated.

#### EXPLANATION OF TABLES RELATING TO DIMEN-SIONS AND SAFE LOADS OF STEEL COLUMNS OF VARIOUS SECTIONS.

PAGES 224 TO 301 INCLUSIVE

Tables of Dimensions for Plate and Angle Columns are given on pages 224 and 225, the Moments of Inertia and Section Moduli about two rectangular axes are given on pages 226 to 228 and the Safe Loads for various lengths, calculated for the Radius of Gyration about each of the two rectangular axes, are given on pages 248 to 267 inclusive.

Tables of Dimensions for Latticed Channel Columns are given on pages 230, the Moments of Inertia and Section Moduli about two rectangular axes are given on page 231, the Safe Loads for various lengths based upon the Least Radius of Gyration, are given on pages 268 to 271, and data relating to the proper sizes of lattice bars and stay-plates to be used with these columns are given on pages 272 and 273.

On pages 232 and 233 are given the Principal Dimensions of Plate and Channel Columns with comparatively narrow plates called, for convenience of reference, Series A, and on pages 234 and 235 for Series B, which differs from Series A, in having wider plates. Moments of Inertia and Section Moduli about two rectangular axes are given for Series A and B on pages 236 to 242 inclusive, and the Safe Loads for different lengths, based upon the Least Radius of Gyration, are given on pages 274 to 301 inclusive.

Safe Loads for I-Beams used as Columns or Struts are given on pages 244 to 247, and the dimensions of these sections can be obtained from the tables on pages 186 to 189 inclusive.

The Plate and Channel Columns given in Series A are particularly useful in buildings or locations in which it is desired to keep the extreme dimensions of the cross section as small as possible for this style of column, although in this series the Radius of Gyration about the central axis parallel to the channel webs is somewhat smaller than the Radius of Gyration about the axis perpendicular to the channel webs. This makes the narrower columns of Series A somewhat less economical of material than the wider columns of Series B, which, however, is small in amount for columns of ordinary story length of 10 feet to 14 feet, such as are used in skeleton buildings.

In Series B of Plate and Channel Columns with wider plates, the Radii of Gyration about the two axes are practically equal for the intermediate thicknesses and these columns are slightly more economical of material than those of Series A, although they require somewhat more space on account of their wider sections.

The Safe Loads for columns of various kinds, as given on pages 244 to 301 inclusive, are expressed in thousands of pounds, and have been figured by the use of Gordon's formula, as stated at the heads of the various tables, using the safety factor 4, which relates to static or quiescent loads such as occur in ordinary buildings.

On page 229 is given a table showing the Distances Back to Back for Spacing Two Channels of the same size in order to produce equal Moments of Inertia about the two rectangular axes. This table will be found to be useful in designing compression members of trusses, etc.

The Safe Loads of the tables are assumed to be centrally applied, and for convenience in computing the proper sizes required to support eccentric loads the tables of Moments of Inertia and Section Moduli for the different sections of columns are given.

The Safe Loads in the various tables are figured for extreme ratios from 30 to 150 for  $\frac{1}{r}$ , in which l is the length of the column and r the

Least Radius of Gyration, both expressed in inches.

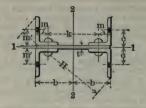
The weights of columns stated in the tables are per lineal foot of shaft, and do not include any allowances for bases, brackets or other connections, as these depend upon the particular details and requirements of each case.

Loads for other safety factors can be figured from the tables by inverse proportion, thus:

New safety factor: 4:: load from tables: new loads.

Drawings of typical details of steel columns are given on page 243.

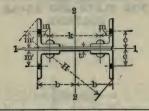
### DIMENSIONS FOR PLATE AND ANGLE COLUMNS.



	of Angles	ı.		Sin	1	Weight of Column.	Area of Column Section.	þ.	С	m	m'	k	H
	Inches		1	ach	108.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
3	x 2½	2 x 1/2	1	6	x 1/4 1/2	23.1 44.2	6.74 13.00	31/8	17/8	13/8	13/4	31/2	811
3	x 21/	2 x 1/2	1	8	x 1/4 1/2	24.8 47.6	7.24 14.00	41/8	11/8	13/8	13/4	51/2	10% 10½
3	x 21	2 x 1/2	1	0	x 1/4 1/2	26.5 51.0	7.74 15.00	51/8	11/8	13/8	13/4	71/2	12 121/8
3	x 21/	2 x 1/2	1	2:	x 1/4 1/2	28.2 54.4	8.24 16.00	61/8	17/8	13/8	12/4	91/2	13¾ 13⅓
31/2	x 2½	2 x ½	1	7:	x 1/4 3/4	25.6 59.5	7.51 17.49	35/8	23/8 25/8	13/8	21/4	41/2	10¼ 105%
81/2	x 23	x l	1	8:	x 1/4 3/4	26.4 62.0	7.76 18.24	41/8	23/8 25/8	13/8	21/4	51/2	11 11*
31/2	123	x 1	1	0:	x 1/4 8/4	28.1 67.1	8.26 19.74	51/8	23/8 25/8	13/8	21/4	71/2	12 <del>1</del> 12 1/8
31/2	x 21	2 x 1/2		2:	x 1/4 3/4	29.8 72.2	8.76 21.24	61/8	23/8 25/8	13/8	21/4	91/2	14¼ 14½
4	x 3	X 1	8	8:	X 18 7/8	37.3 97.0	10.86 28.44	41/8	2 16 2 18	13/4	21/4	43/4	1111 121/8
4	x 8	x f	1	0:	X 5 16 7/8	39.4 103.0	11.49 30.19	51/8	2 to	13/4	21/4	63/4	13 to
4	x 8	X 1	1	2:	X 18 7/8	41.6 108.9	12.11 31.94	61/8	216 218	13/4	21/4	83/4	14 <del>11</del> 15½
4 "	x 8	X &	1	4:	K 5 16 7/8	43.7 114.9	12.74 33.69	71/8	2 16 2 18	13/4	21/4	1034	16½ 16¼

Dimensions m' and c may be varied to suit requirements.

### DIMENSIONS FOR PLATE AND ANGLE COLUMNS.



Size of Angles.	Sine of Plates.	Weight of Column.	Area of Column Section.	b	c	m	m'	k	H
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
5 x 8½ x 4	10 x 10	45.4 128.7	13.87 87.74	51/8	214	21/4	21/4	534	14% 15
5 x 81/2 x #	12 x 10	47.6 135.1	13.99 39.61	61/8	21/4	21/4	21/4	73/4	16 16%
5 x 81/2 x 1	14 × 1	49.7 141.5	14.62 41.49	7.1%	214	21/4	21/4	934	174
5 x 81/2 x #	16 x 16 18	51.8 147.8	15.24 48.86	81/8	21/4	21/4	21/4	113/4	19¼ 19¾
6 x 81/2 x 3/8	12 x 3/8	62.1 156.4	18.18 46.00	61/8	216	21/4	21/4	7%	17元
6 x 31/2 x 3/8	14 x 3/8	64.7 168.2	18.98 48.00	71/8	2½ 2½	21/4	21/4	93/4	18½ 19½
6 x 8 ½ x 1/8	16 x 3/8	67.2 170.0	19.68 50.00	81/8	214	21/4	21/4	1134	201 201
6 x 31/2 x 3/8	18 x 3/1	69.8 176.8	20.43 52.00	91/8	2元	21/4	21/4	1834	22 to
7×8½×4	14 x 1	80.8 176.8	28.78 52.00	71/8	21/2 23/4	21/4	21/4	934	20# 20#
7×8½×4	16 x 1	83.8 183.6	24.60 54.00	81/8	2½ 2¾	21/4	21/4	1134	21¾ 22⅓
7×8½× 1	18 x 1	86.8 190.4	25.48 56.00	91/8	2½ 2¾	21/4	21/4	1834	23¼ 28¾
7, 18 1/2 1 1	20 x 1	89.8 197.2	26.85 58.00	101/8	2½ 2¾	21/4	21/4	15%	24½ 25±

Dimensions m' and c may be varied to suit requirements.

## MOMENTS OF INERTIA AND SECTION MODULI FOR PLATE AND ANGLE COLUMNS.



	-	Axis	1-1.	Axis	2-2.		Axis	1-1.	Axis	2-2.
Size of Angles.	of Plate.	Moment of Inertia.	Section Modulus.	Moment of Inertia.	Section Modulus.	of Plate.	Moment of Inertia.	Section Modulus,	Moment of Inertia.	Section Modulus.
Inches.	Inches.	Ins.4	Ins.3	Ins.4	Ins.3	Inches.	Ins.4	Ins.3	Ins.4	Ins.3
3 x 2½ x ½ x ¼ 4	8 x 1/4 4 5 6 8 8/8 4 7 6 4 1/2 4 16	10.3 13.4 16.7 20.2 24.0 28.1	3.3 4.3 5.2 6.3 7.4 8.6	39.4 47.9 55.9 63.5 70.6 77.3	12.6 15.3 17.9 20.3 22.6 24.8	8 x 1/4 " 5 " 16 " 7 " 16 " 17 " 16 " 17 " 16 " 16	10.3 13.4 16.7 20.3 24.0 28.1	3.3 4.3 5.3 6.3 7.4 8.6	76.7 93.7 110.1 125.6 140.5 154.6	18.6 22.7 26.7 30.5 34.1 37.5
3 x 2½ x ¼ 4 16 4 56 4 56 4 16 4 16 4 16 4 16 4 16	1.0 x 1/4 4 5/6 6 8/8 4 1/6 4 1/2 4 1/2	_	3.3 4.3 5.3 6.3 7.4 8.6	128.4 157.5 185.6 212.5 238.3 263.1	25.1 30.7 36.2 41.5 46.5 51.3	12 x 1/4  " 16  " 3/8  " 10  " 1/2  " 14	10.3 13.4 16.7 20.3 24.1 28.2	3.3 4.3 5.3 6.3 7.4 8.6	195.7 240.5 284.0 325.8 366.1 405.1	32.0 39.3 46.4 53.2 59.8 66.1
3½ x 2½ x ¼ a 16 3,6 16 16 16 16 16 16 16 16 16 1	7 x 1/4  " 5 6  " 8/8  " 1/2  " 1/2	16.0 20.7 25.6 30.8 36.3 42.1	4.4 5.7 6.9 8.3 9.7 11.1	62.4 76.2 89.3 101.7 113.6 124.8	17.2 21.0 24.6 28.1 31.3 34.4	8 x 1/4 = 1/8 = 1/8 = 1/2 = 1/8	16.0 20.7 25.6 30.8 36.3 42.1	4.4 5.7 6.9 8.3 9.7 11.1	84.7 103.6 121.7 138.9 155.5 171.2	20.5 25.1 29.5 33.7 37.7 41.5
8½ x 2½ x ¼ 4 16 6 16 6 16 6 16 6 16 6 16 6 16	10 x 1/4 8 8 8 8 7 8 1/2 4 9 16	16.0 20.7 25.6 30.8 36.3 42.2	4.4 5.7 6.9 8.3 9.7 11.2	140.9 173.0 203.9 233.5 262.1 289.4	27.5 33.8 39.8 45.6 51.1 56.5	12 x 1/4  "	16.0 20.7 25.6 30.8 36.4 42.2	4.4 5.7 7.0 8.3 9.7 11.2	213.7 262.9 310.5 356.2 400.7 443.4	34.9 42.9 50.7 58.2 65.4 72.4

#### MOMENTS OF INERTIA AND SECTION MODULI FOR PLATE AND ANGLE COLUMNS.



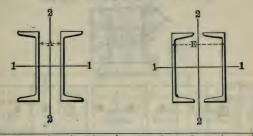
10.0		Axis	1-1.	Axis	2-2.		Axis	1-1.	Axis	2-2.
Size of Angles.	Size of Plate,	Moment of Inertia.	Section Modulus.	Koment of Inertia.	Section Modulus.	Sine of Plate.	Moment of Inertia.	Section Modulus.	Noment of Inertia.	Section Modulus.
Inches,	Inches.	Ins.4	Ins,3	Ins.4	Ins.8	Inches.	Ins.4	Ins,3	Ins.4	Ins,3
Inches. 4 x 3 x 1	81455 + 20456	30.3 37.4 44.8 60.5 78.6 69.5 78.6 69.5 78.6 69.5 69.6 69.6 60.9 69.6 60.9 69.6 78.2 108.7 57.6 78.2 112.2 114.1 160.6 70.6 70.6 70.6 70.6 70.6 70.6 70.6	7.3 8.9 10.6 10.4 14.2 20.1 20.1 20.1 22.3 3.9 9 10.6 10.2 11.2 11.3 11.3 11.3 11.3 11.3 11.3 11	Ins.4  114.6 134.8 154.0 172.4 190.0 206.9 223.8 253.0 267.0 292.3 345.5 396.7 446.6 494.7 541.5 596.5 630.1 672.2 713.1 672.2 713.1 572.5 484.8 856.9 864.2 749.3 832.1 990.8	27.8 27.8 32.7 37.3 34.6.1 50.2 32.7 37.3 44.8 46.1 50.2 54.1 57.8 61.3 64.7 47.7 47.7 47.7 47.7 47.7 47.7 47.7	Inches	30.3 37.4 44.8 52.6 60.9 60.9 60.9 60.0 30.3 37.4 44.0 60.6 60.6 60.6 60.6 60.7 788.3 98.3 52.7 78.1 98.2 128.2 128.2 128.2 119.3 128.2 119.3 128.2 119.3 128.2 119.3 128.2 12	7.3 8.9 10.6 12.4 14.2 16.1 18.1 120.2 2.3 24.5 16.1 120.2 2.3 24.5 16.1 120.2 2.3 24.5 16.1 120.2 2.3 24.5 11.2 12.3 24.5 16.1 18.7 21.4 24.1 22.2 2.3 2.4 16.1 18.7 22.4 22.3 29.9 29.9	192.0 226.4 259.5 322.2 380.5 498.0 434.4 459.8 416.8 493.4 639.7 709.6 677.8 843.7 907.7 969.8 1030.1 341.9 404.6 858.2 689.8 741.8 792.1 841.0 888.2 690.3 841.0 888.2 860.3	37.5 44.2 55.8 56.9 68.7 74.2 68.7 774.2 69.7 69.8 69.7 69.8 69.1 132.4 136.1 136.1 137.3 145.0 94.9 103.9 112.1 123.1 123.1 123.1 125.6 136.3 146.0 147.1 1
" H	** 18	178.0 195.9 214.4	32.9 36.0 39.2	1141.0 1213.2 1283.1	160.1 170.3 180.1	** 7/8 ** 15	178.1 196.0 214.6	32.9 36.0 39.2	1562.6 1663.3 1761.0	192.3 204.7 216.7

#### MOMENTS OF INERTIA AND SECTION MODULI FOR PLATE AND ANGLE COLUMNS.



		Axis	1-1.	Axis	2-2.		Axis	1-1.	Axis	2-2.
Siro of Angles.	Sire of Plate,	Moment of Inertia.	Section Modulus,	Moment of Inertia.	Section Modulus.	Size of Plate.	Moment of Inertia.	Section	Moment of Inertia.	Section Modulus.
Inches.	Inches.	Ins.4	Ins.3	Ins.4	Ins.8	Inches.	Ins.4	lns.3	Ins.4	Ins.3
6 x 81/2 x 3/2 	12x3/8	119.2 141.5 164.5 188.3 212.9 238.3 264.5 291.5 319.5 348.2	19.3 22.8 26.3 30.0 33.7 37.6 41.5 45.5 49.6 53.8	457.5 526.2 593.0 657.9 720.9 781.8 841.2 898.5 954.4 1008.4	74.7 85.9 96.8 107.4 117.7 127.6 137.3 146.7 155.8 164.6	14x3/8	119.2 141.5 164.5 188.3 212.9 238.3 264.6 291.6 319.6 348.4	19.3 22.8 26.3 30.0 33.7 37.6 41.5 45.5 49.6 53.9	649.1 747.7 843.9 937.6 1028.8 1117.3 1203.9 1287.9 1370.0 1449.5	91.1 104.9 118.4 131.6 144.4 156.8 169.0 180.8 192.3 203.4
		377.5 119.2	58.1	1060.8	173.2	18-3/	377.7	58.1 19.3	1526.9	214.3 125.7
6 x 3½ x % 10 x	16x3/8	141.5 164.5 188.4 213.0 238.4 264.6 291.7 319.7 348.5 377.8	19.3 22.8 26.3 30.0 33.7 37.6 41.5 45.5 49.7 53.9 58.1	878.6 1013.2 1144.7 1273.2 1398.6 1520.6 1640.2 1756.4 1870.4 1981.1 2089.1	108.1 124.7 140.9 156.7 172.1 187.2 201.9 216.2 230.2 243.8 257.1	18x3/8 44 14 44 15/8 44 14 44	119.3 141.5 164.6 188.4 213.0 238.4 264.7 291.8 319.8 348.6 378.0	22.8 26.3 30.0 33.7 37.6 41.5 45.5 49.7 53.9 58.2	1147.4 1324.4 1497.5 1667.1 1832.8 1994.3 2152.9 2307.4 2459.2 2606.8 2751.3	145.1 164.1 182.7 200.9 218.6 235.9 252.9 269.5 285.7 301.5
7 x 3½ x 4 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	14x 7 18 12 12 15 16 16 16 18 16 18 16 18 16 18 16 18 16 18 18 16 18 18 18 18 18 18 18 18 18 18 18 18 18	220.8 255.8 292.7 328.5 367.3 406.6 447.2 488.3 530.8 574.3	30.6 35.3 40.2 44.9 50.0 55.1 60.4 65.7 71.1 76.6	831.2 938.4 1043.0 1144.6 1243.9 1340.7 1434.8 1526.7 1615.9 1702.8	116.7 131.7 146.4 160.7 174.6 188.2 201.4 214.3 226.8 239.0	16x76 1/2 1/2 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6	220.8 255.8 292.7 328.5 367.4 406.7 447.3 488.4 530.9 574.5	30.6 35.3 40.2 44.9 50.0 55.1 60.4 65.7 71.1 76.6	1122.6 1268.8 1411.6 1550.9 1687.2 1820.5 1950.3 2077.4 2201.1 2322.0	138.2 156.2 173.7 190.0 207.7 224.0 240.0 255.7 270.9 285.8
7 x 31/2 x 10/20/20/20/20/20/20/20/20/20/20/20/20/20	18x 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	220.8 255.9 292.8 328.6 367.4 406.7 447.4 488.5 531.0 574.7	30.6 35.3 40.2 44.9 50.0 55.2 60.4 65.7 71.1 76.6	1463.2 1655.1 1943.0 2026.6 2206.4 2382.7 2554.7 2723.5 2888.1 3049.1	160.4 181.4 202.0 222.1 241.8 261.1 280.0 298.5 316.5 334.2	20x 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	220.8 255.9 292.8 328.6 367.5 406.8 447.5 488.6 531.2 574.8	30.6 35.3 40.2 44.9 50.0 55.2 60.4 65.7 71.1 76.6	1854.8 2099.4 2339.4 2574.2 2804.4 3030.5 3251.4 3468.5 3680.5 3683.3	183.2 207.4 231.1 254.2 277.0 299.3 321.1 342.6 363.5 384.0

#### SPACING OF CHANNELS FOR EQUAL MOMENTS OF INERTIA ABOUT THE TWO RECT-ANGULAR AXES 1-1 AND 2-2.



Section Num- ber.	Depth of Chan- nel.	Weight per foot of one Chan- nel.	Area of Section of one Chan- nel.	A	E	Section Num- ber.	Depth of Chan- nel.	Weight per foot of one Chan- nel.	Area of Section of one Chan- nel,	A	×
	Inches.	Pounds.	Sq.Ins.	Inches.	Inches.		Inches.	Pounds.	Sq. Ins.	Inches.	Inches.
C5	8 "	4.00 5.00 6.00	1.19 1.47 1.76	1.29 1.17 1.10	3.05 2.93 2.94		10	15.00 20.00 25.00 30.00	5.88 7.35 8.82	6.88 5.96 5.66 5.41	8.89 8.40 8.14 8.01
CĐ "	4	6.25	1.55 1.84 2.13	1.96	3.80	" C41	12	35.00 20.50	6.03	5.18 7.68	7.94
C13	5 "	6.50 9.00 11.50	1.95 2.65 3.38	2.57	4.49		4	25.00 30.00 35.00 40.00	7.35 8.82 10.29 11.76	7.35 7.06 6.83 6.60	10.07 9.78 9.59 9.48
C17	6 "	8.00 10.50 13.00 15.50	3.82	3.29 3.08	5.29	C95	13	32.00 35.00 37.00 40.00	10.29 10.88	7.84 7.66 7.56 7.44	11.62 11.48
C21	7	9.75 12.25 14.75 17.25	4.34	$\frac{4.00}{3.82}$	$6.12 \\ 5.94$	4 4	4	45.00 50.00 55.00	13.24	7.22 7.02 6.84	11.10
" C25	8	19.75	5.81 3.35	3.49 4.92	5.81 7.24	C58	44	33.00 35.00 40.00	10.29 11.76	9.42	12.58 12.28
a	44 44	13.75 16.25 18.75 21.25	4.78 5.51	$\frac{4.53}{4.37}$	6.65	a	es es	45.00 50.00 55.00	13.24 14.71 16.18	8.92 8.72 8.58	12.08 11.92 11.81
C29	9	13.25 15.00 20.00 25.00	4.41 5.88	5.48 $5.14$	7.84	66	18	50.00		11.20 10.98	14.84 14.52 14.30 14.18

### DIMENSIONS FOR LATTICED CHANNEL COLUMNS.



Depth of Channel and Section	Weight per Foot.	t	ь	đ	B	0	8	<b>A</b> ,	m
Number.	Pounds.	Inch.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
6″ C17	8.00 10.50 18.00 15.50	.20 .32 .44 .56	81/4	8,,	9.%	27/8	118 118 148 148 148	2	1 to
7″ C21	9.75 12.25 14.75 17.25 19.75	.21 .32 .42 .53	41/4	81/2	11. "	8%	216 216 116 178 178	21/8	1 % 1 % 1 % 1 % 1 % 8 1 % 8
8″ C25	11.25 18.75 16.25 18.75 21.25	.22 .31 .40 .49 .58	418	4	121/2	81/4	21/2 22/4 22/4 22/4 24/4 24/4	23/4	11/4 11/6 15/8 11/2 11/6
9″. C29	13.25 15.00 20.00 25.00	.23 .29 .45 .61	5,4	41/2	1834	41/8	25/4 211 216 25/8	8, "	13/8 1/6 1/6 1/4
10″ 088	15.00 20.00 25.00 30.00 85.00	.24 .38 .53 .68 .82	53/4	5	151/4	45/8	31/8 31/8 21/8 21/8 21/8	33/8	11/2 15/8 13/4 11/8 21/4
12" C41	20.50 25.00 30.00 35.00 40.00	.28 .39 .51 .64 .76	611	6, "	181/8	55/8	37/8 38/4 35/8 31/2 38/8	41/8	1% 1% 2 2% 2% 2%
15″ C58	33.00 35.00 40.00 45.00 50.00 55.00	.40 .48 .52 .62 .72 .82	81/8	77/2	221/8	65/8	43/4 411 45/8 41/2 41/8 41/8	51/8	1% 1# 2% 2% 2% 2%

#### PROPERTIES OF LATTICED CHANNEL COLUMNS.



	Weight	Axis	1-1.	Axis	2-2.
Depth of Channel and Section Number.	Poot.	Moment of Inertia.	Section Modulus.	Moment of Inertia.	Section Modulus.
	Pounds.	Inches.4	Inches.3	Inches.4	Inches.2
6" C17	8.00 10.50 18.00 15.50	26.0 30.2 34.6 39.0	8.7 10.1 11.5 13.0	27.0 81.1 85.2 88.7	7.8 8.4 9.5 10.4
7″ C21	9.75 12.25 14.75 17.25 19.75	42.2 48.4 54.4 60.4 66.4	12.1 13.8 15.5 17.3 19.0	44.0 50.5 56.4 61.4 66.5	10.8 11.9 13.8 14.4 15.6
8" C25	11.25 13.75 16.25 18.75 21.25	64.6 72.0 79.8 87.7 95.6	16.2 18.0 20.0 21.9 23.9	67.5 75.8 84.5 92.3 99.7	14.0 15.8 17.6 19.8 20.8
9" C29	13.25 15.00 20.00 25.00	94.6 101.8 121.6 141.4	21.0 22.6 27.0 31.4	92.4 100.0 120.1 189.1	17.8 19.2 28.1 26.8
10° 088	15.00 20.00 25.00 30.00 85.00	133.8 157.4 182.0 206.4 281.0	26.8 31.5 86.4 41.8 46.2	181.7 158.5 183.8 205.4 226.0	23.0 27.6 32.0 35.8 39.4
12" C41	20.50 25.00 80.00 85.00 40.00	256.2 288.0 323.2 358.6 393.8	42.7 48.0 53.9 59.8 65.6	256.9 295.6 335.8 370.5 405.7	87.9 43.6 49.5 54.6 59.8
15" C58	83.00 35.00 40.00 45.00 50.00 55.00	625.2 639.8 695.0 750.2 805.4 860.4	88.4 85.3 92.7 100.0 107.4 114.7	618.7 686.1 700.8 763.0 819.5 874.3	76.1 78.8 86.8 98.9 100.9 107.6

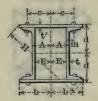
### DIMENSIONS FOR PLATE AND CHANNEL COLUMNS.



SERIES A.

Depth	W. 2.2.4	Size of	Plates.			-				-	
Of Channel and Section	Weight per Foot.	Width.	Thick-	t	b	d	H	c	E	A	m
No.	Pounds.	Inches.	Inch.	Inch.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
6" C17	8.0 10.5 13.0 15.5	8 44 44 44 44 44	1488148148	.20 .32 .44 .56	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	35/8 35/8 35/8 35/8 35/8 35/8 35/8 35/8	10 16 10 16	27/8	1;;; 1;;; 1;;; 1;;;	2	1,76 1,76 1,76 1,76
7″ C21	9,75 12,25 14,75 17,25 19,75	9 46 46 68 68 68 68 68 68	14/8/4/8/4/8/4/8	.21 .32 .42 .53	41/2	334 438 438 438 438 438 438 438 438 438	11¾ 12¼ 11¾ 12¼ 11¾ 12¼ 11¼ 12¼ 11¾ 12¼	81/4	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	21/4	1,36 1,36 1,76 1,76 1,76 1,76
8" C25	11,25 18,75 16,25 18,75 21,25	10	14/8/4/8/4/8/4/8/4/8	.22 .31 .40 .49	5	45% 45% 45% 45% 45% 45% 45% 45% 45% 45%	13½ 13½ 13½ 13½ 13½ 13½ 13½ 13½ 13½ 13½	35/8	2% 2% 2¼ 2¼ 2½ 2%	25/8	11/4 1/4 1/6 11/6 11/6 11/6
9″ C29	18,25 15,00 20,00 25,00	11	58148	.23 .29 .45 .61	51/2	43/4 51/8 43/4 51/8 43/4 51/8 43/4 51/8	14½ 15½ 14½ 15½ 15½ 14½ 15½ 15½	41/8	23/4 211 211 216 23/6	8	13% 13% 13% 13%

## DIMENSIONS FOR PLATE AND CHANNEL COLUMNS.



#### SERIES A.

Depth Weight		Size of	ze of Plates.								
Channel and Section	per Foot.	Width.	Thick- ness t'	t	b	d	H	C	E	A	m
No.	Pounds.	Inches.	Inch.	Inch.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
	15.0	12	1/3	.24	6,,	51/4	15 <del>14</del> 16 <del>14</del> 15 <del>14</del>	41/2	3,	31/4	11/2
811	20.0	44	1/4	.38	44	5 1/4 5 5/8 5 1/4 5 5/8	15 15	48	21/8	44	15/8
10" C83	25.0	66	1/4	.53	66	51/4	16 16 16 16 16 16 16 16 16 16 16 16 16 1	46	23/4	66	13/4
000	30.0	66	1/4	.68	66	514	154	66	2,1	66	1,18
	85.0	44	14/8/4/8/4/8/4/8/4/8/4/8/4/8/4/8/4/8/4/8	-82	46	514 588 514 558 514 558	1616 1518 1616	66	2,7	44	216
	20.5	14	14	128	7,,	6½ 6% 6¼	18¾ 19⅓ 18¾	55/8	37/8	41/8	13/4
	25.0	46	14	.39	46	61/4	18¾ 19¼	66	3%	66	17/8
12" C41	80.0	66	14/8/4/8/4/8/	.51	66	61/4	18¾ 19₺	66	35/8	46	2,,
011	35.0	66	124	.64	66	61/4	18¾ 19¼	66	31/2	66	21/8
	40.0	44	1/4	.76	66	65/8 61/4 65/8	18¾ 19¾	66	8%	66	21/4
	88.0	17	3/8	.40	81/3	77/8 81/4 77/8 81/4	281	63/4	47/8	51/4	17/8
	35.0	66	3/8	.43	88	77/8	23 + 23 + 23 + 3	66	413	66	1,15
15" C58	40.0	66	20/4/0/4/0/4/0	.52	48	71/8	231	46	43/4	- 66	2,,
300	45.0	66	3/8	.62	66	77/8	231	66	45/8	66	21/8
	50.0	66	3/4	.72	66	8¼ 7⅓ 8¼	23 1	66	4,6	66	21/4
10	55.0	"	3/8	.82	46	7% 814	231	66	476	66	2,5

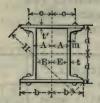
### DIMENSIONS FOR PLATE AND CHANNEL COLUMNS.



SERIES B.

Depth		Size of	Plates.								
Ohannel and Section	Weight per Foot.	Width.	Thick- ness t'	t	b	đ	H	С	E	•	m
No.	Pounds.	Inches.	Inch.	Inch.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
	8.0	9	1/4	.20	41/2	31/4	111/8	83/8	2,4	21/2	1,1
RI	10.5	66	14	182	66	314	111/8	66	2,16	66	1,7
6" 017	13.0	68	1/4	44	66	31/4 35/4	11%	66	210	66	1,4
	15.5	66	14 8 14 8 14 8 14 8 14 8	.56	66	355% 355% 355% 355% 355% 355% 355% 355%	11½ 11½ 11½ 11½ 11½ 11½ 11½	46	1,15	66	1,76
	9.75	1,1	1/4	.21	51/2	834	13 ½ 13 ¾	41/4	3,1	31/4	17
	12.25	66	1/4	132	**	334 41/8 33/4 41/8	13%	46	211	66	1,5
7″ C21	14.75	66	1/4	42	66	33/4 41/8	13 % 13 % 13 % 13 %	44	211	66	1,70
021	17.25	66	1/4	153	44	33/4 41/8	13%	66	23/4	66	11/2
	19,75	66	14.8,4,8,4,8,4,8,4,8,4,8	.63	66	33/4 41/8	13% 13%	66	25/8	66	15/8
	11,25	12	1/4	.22	6,,	41/4	14 <del>11</del> 15½	45/8	3,76	35/8	11/4
8"	18,75	68	14	.31	66	4½ 4½ 45%	14#	86	3,4	66	1,10
C25	16.25	46	1/4	40	66	4½ 4½ 4%	15½ 14¼	46	31/4	66	13/8
	18.75	86	1/4	.49	44	41/4	15½ 14¼ 15½	86	31/8	13	11/2
	21,25	88	14/8/4/8/4/8/4/8/4/8	.58	66	45/8 41/4 45/8	1411	88	84	66	1,76
	18,25	13	1/4	.28	61/2	43/4 51/8 43/4	16½ 16½	51/8	33/4	4,,	13%
9″ C29	15,00	66	8/8/4/8	.29	66	434	16½ 16½	66	8#	66	1,76
200	50,00	86	1/4	45	66	434	16% 16%	66	3/4	46	1,0
	25,00	44	124	.61	46	43% 51%	16½ 16¾	**	83/8	44	13/4

## DIMENSIONS FOR PLATE AND CHANNEL COLUMNS.



### SERIES B.

Depth	307-2-3-4	Size of	Plates.								
of Channel and Section	Weight per Foot.	Width.	Thick- ness. t'	t	b	đ	н	C	E	Δ	m
No.	Pounds.	Inches.	Inch.	Inch.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
	15.0	15	34	24	71/2	51/4 55/8	18 to 18 %	6,,	41/2	43/4	11/2
	20.0	66	1/4	38	44	51/4	18*	44	43/8	16	15/8
10" C88	25.0	66	1/4	.53	44	5 1/4	18¾ 18¾	66	41/4	66	134
Cas	30.0	44	14/8/4/8/4/8/4/8/4/8	.68	66	55/8 51/4 58/8	18¾ 18¼	66	41	**	148
100	35.0	44	1/4	.82	66	5 1/4 5 5/8	18¾ 18¼ 18¾	44	315	**	218
10	20.5	10					MILE		0		404
	20.5	16	5/8	.28	8,,	61/4	20% 20% 20%	65/8	47/8	51/8	13/4
12" C41	25.0	66	5/8	189	68	63/4	20%	66	43/4	66	17/8
C41	80.0	66	8/8	-51	44	6½ 6½	20% 20%	46	45/8	44	2,,
	85.0	66	1/4	.64	66	61/4	20% 20%	66	41/2	44	21/8
	40.0	46	14/8/4/8/4/8/4/8/4/8	.76	44	65/8 61/4 65/8	20% 20%	44	43/8	66	21/4
	88.0	20	3,6	.40	10	776	254	81/4	63/8	63/4	17/8
	85.0	66	3/4		66	71/8 81/4 71/8 81/4 71/8 71/8	25 to	66		"	
15"		66	3/4	.43	46	814	25 H	66	616	66	134
15" C53	40.0	44	3/4	.52	44	814	251	66	61/4	66	2,,
	45.0	66	\$0\4\0\4\0\4\0\4\0\4\0\	.62	66	81/4	25 to 125	66	61/8	66	21/8
	50.0	44	3/8	.72	66	8¼ 7⅓ 8¼	25 H	44	616	44	21/4
	55.0	"	3/3	.82	66	77% 81/4	25 H	66	5 11	46	2,4



				SEI	RIE	S A.				SE	RIE	S B.	
Depth of Chan-	Weight	late.	of Plate.	Axis	1-1.	Axie	2-2.	late.	of Plate.	Axis	1-1.	Axis	2-2.
nel and Section Num- ber.	Foot.	Width of Plate.	Thickness of	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Thickness of	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus,
	Lbs.	In.	In.	Ins.4	Ins.8	Ins.4	Ins.3	In.	In.	Ins.4	Ins.3	Ins.4	Ins.3
6" C 17	8.00 « « « «	10 m m m m	1/4 516/87 16/20 16/8	65.1 75.9 87.0 98.6 110.7 123.1 136.1	20.0 22.9 25.8 28.7 31.6 34.6 37.5	48.4 53.7 59.0 64.4 69.7 75.0 80.4	12.1 13.4 14.8 16.1 17.4 18.8 20.1	0 1 2 2 2 2	1/4 5 16 8/8 7 16 1/2 9 16/8	70.0 82.1 94.7 107.8 121.3 135.3 149.8	21.5 24.8 28.1 31.4 34.6 38.0 41.3	69.6 77.2 84.8 92.4 100.0 107.6 115.2	15.5 17.2 18.9 20.5 22.2 23.9 25.6
6″ C 17	10.50 « « « »	100 m m m m m m	1/4 5 16 3/8 7 16 1/2 9 6 8	69.3 80.1 91.2 102.8 114.9 127.3 140.3	21.3 24.2 27.0 29.9 32.8 35.7 38.7	52.5 57.8 63.1 68.5 73.8 79.1 84.5	13.1 14.5 15.8 17.1 18.5 19.8 21.1	9 « «	1/4 5 18 3/8 7 16 1/2 9 15/8	74.2 86.3 98.9 112.0 125.5 139.5 154.0	22.8 26.1 29.3 32.6 35.8 39.2 42.5	76.5 84.1 91.7 99.3 106.9 114.5 122.1	17.0 18.7 20.4 22.1 23.8 25.4 27.1
6″ C 17	13.00	8 4 4 4 4	1/4 516/8/7/6/19/8/8	73.7 84.5 95.6 107.2 119.3 131.7 144.7	22.7 25.5 28.3 31.2 34.1 37.0 39.9	56.5 61.9 67.2 72.5 77.9 83.2 88.5	14.1 15.5 16.8 18.1 19.5 20.8 22.1	9 " " "	1/4 5 16 3/8 7 16 1/2 16 5/8	78.6 90.7 103.3 116.4 129.9 143.9 158.4	24.2 27.4 30.6 33.9 37.1 40.4 43.7	83.4 91.0 98.6 106.2 113.7 121.3 128.9	18.5 20.2 21.9 23.6 25.3 27.0 28.7
6" C 17	15.50 « « « «	00 m m m m m m	1/4 5 16 8/8 7 6 18/8 18/8	78.1 88.9 100.0 111.6 123.7 136.1 149.1	24.0 26.8 29.6 32.5 35.3 38.2 41.1	60.0 65.4 70.7 76.0 81.4 86.7 92.0	15.0 16.3 17.7 19.0 20.3 21.7 23.0	- A	1/4 5 16 3/8 16 1/2 16 5/8	83.0 95.1 107.7 120.8 134.3 148.3 162.8	25.5 28.7 31.9 35.1 38.4 41.6 44.9	89.5 97.1 104.7 112.3 119.9 127.4 135.0	19.9 21.6 23.3 25.0 26.6 28.3 30.0



Depth		7		SEI	RIE	S A.				SEI	RIE	S B.	
Of Chan-	Weight	ate.	late.	Axis	1-1.	Axis	2-2.	ate.	late.	Axis	1-1.	Axis	2-2
nel and Section Num-	Poot.	Width of Plate.	Thickness Plate.	Mo- meht of Inertia.	Section Mod- ulus,	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	ThicknessPlate.	Mo- ment of Inertia	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.
ber.	Lbs.	In.	In.	Ins.4	Ins.3	Ins.4	Ins.3	In.	In.	Ins.4	Ins.3	Ins.4	Ins.3
7″ C21	9.75	8 8 8 8 8 8 8	1/4 -18/8 -18/2 -18/8 H8/4	101.4 117.4 134.1 151.3 169.0 187.2 206.2 225.6 245.5	27.0 30.8 34.6 38.4 42.2 46.1 50.0 53.9 57.8	70.6 78.1 85.8 93.4 101.0 108.5 116.1 123.8 131.3	15.7 17.4 19.1 20.8 22.4 24.1 25.8 27.5 29.2	11 4 4 4 4 4 4 4 4	1/4 5 16 18/8 7 16 15/8 15/8 11/2 15/8 11/8 11/8 11/8 11/8 11/8 11/8 11/8	114.5 134.2 154.5 175.5 197.1 219.5 242.5 266.3 290.7	30.5 35.2 39.9 44.6 49.3 54.0 58.8 63.6 68.4	130.9 144.7 158.6 172.5 186.3 200.2 214.1 227.9 241.8	23.8 26.3 28.8 31.4 33.9 36.4 38.9 41.4 44.0
7″ C21	12.25	8 8 8 8 8	1/4 4 10/8 - 10/2 - 10/8 10/8	107.6 123.6 140.3 157.5 175.2 193.4 212.4 231.8 251.7	28.7 32.4 36.2 40.0 43.8 47.6 51.5 55.4 59.2	76.3 83.9 91.5 99.1 106.7 114.3 121.9 129.5 137.1	17.0 18.6 20.3 22.0 23.7 25.4 27.1 28.8 30.5	11 a a a a a	1/4 = 16/8 - 16/	120.7 140.4 160.7 181.7 203.3 225.7 248.7 272.5 296.9	32.2 36.8 41.5 46.1 50.8 55.6 60.3 65.1 69.9	144.0 157.9 171.8 185.6 199.5 213.4 227.2 241.1 255.0	26.2 28.7 31.2 33.8 36.3 38.8 41.3 43.8 46.4
7″ C21	14.75	9 " " " " " " " " " " " " " " " " " " "	1/4 15/8 11/2 15/8118/4	113.6 129.6 146.3 163.5 181.2 199.4 218.4 237.8 257.7	30.3 34.0 37.7 41.5 45.3 49.1 53.0 56.8 60.6	81.5 89.1 96.7 104.3 111.9 119.5 127.1 134.7 142.3	18.1 19.8 21.5 23.2 24.9 26.5 28.2 29.9 31.6	11 4 4 4 4 4 4 4 4 4	1/4 56 87 16 15/8116 84	126.7 146.4 166.7 187.7 209.3 231.7 254.7 278.5 302.9	33.8 38.4 43.0 47.7 52.3 57.0 61.8 66.5 71.3	156.3 170.1 184.0 197.8 211.7 225.6 239.4 253.3 267.2	28.4 30.9 33.5 36.0 38.5 41.0 43.5 46.1 48.6
7" C21	17.25	« « « «	1/4 518/8/16/20 16/8/16/3/4	119.6 135.6 152.3 169.5 187.2 205.4 224.4 243.8 263.7	31.9 35.6 39.3 43.1 46.8 50.6 54.4 58.2 62.1	85.9 93.4 101.1 108.7 116.2 123.8 131.4 139.1 146.6	19.1 20.8 22.5 24.2 25.8 27.5 29.2 30.9 32.6	11 4 4 4 4 4 4 4 4 4	1/4 5 8 8 16 8 16 8 16 8 4	132.7 152.4 172.7 193.7 215.3 237.7 260.7 284.5 308.9	35.4 40.0 44.6 49.2 53.8 58.5 63.2 67.9 72.7	167.1 181.0 194.9 208.7 222.6 236.5 250.3 264.2 278.1	30.4 32.9 35.4 38.0 40.5 43.0 45.5 48.0 50.6
7″ C21	19.75	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1/4 5/6 8/8 16/2 0/8 15/8 18/4	125.6 141.6 158.3 175.5 193.2 211.4 230.4 249.8 269.7	33.5 37.1 40.8 44.6 48.3 52.0 55.9 59.7 63.5	90.3 97.9 105.5 113.1 120.7 128.3 135.9 143.5 151.1	20.1 21.8 23.4 25.1 26.8 28.5 30.2 31.9 33.6	11 " " " " " " " " " " " " " " " " " "	1/4 6 16 8 7 16 16 8 16 8 16 8 16 8 16 8 16	138.7 158.4 178.7 199.7 221.3 243.7 266.7 290.5 314.9	37.0 41.5 46.1 50.7 55.3 60.0 64.7 69.4 74.1	178.2 192.0 205.9 219.7 233.6 247.5 261.3 275.2 289.1	32.4 34.9 37.4 40.0 42.5 45.0 47.5 50.0 52.6



Depth	10		10	SEI	RIE	S A.		0	11	SEF	LIE	S B.	
Of Chan-	Weight	ate.	ate.	Axis	1-1.	Axis	2-2.	ste.	ate.	Axis	1-1.	Axis	2-2.
nel and Section Num- ber.	per Foot.	Width of Plate.	ThicknessPlate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Thickness Plate	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.
	Lbs.	In.	In.	Ins.4	Ins.3	Ins.4	Ins.3	In.	In.	Ins.4	Ins.3	Ins.4	Ins.3
8" C 25	11.25	10	14 16 16 16 16 16 16 16 16 16 16 16 16 16	149.7 172.6 196.2 220.5 245.4 271.1 297.5 324.6 352.4	35.2 40.0 44.9 49.7 54.5 59.4 64.3 69.2 74.2	104.0 114.4 124.9 135.3 145.7 156.1 166.5 176.9 187.4	20.8 22.9 25.0 27.1 29.1 31.2 33.3 35.4 37.5	12	14 5 8 8 1 1/2 16/8 16/8	166.7 194.2 222.5 251.7 281.6 312.4 344.1 376.6 410.0	39.2 45.0 50.9 56.7 62.6 68.5 74.4 80.3 86.3	181.1 199.1 217.1 235.1 253.1 271.1 289.1 307.1 325.1	30.2 33.2 36.2 39.2 42.2 45.2 48.2 51.2 54.2
8″ C 25	13.75	10 4 4 6 6 6 6 6 6	1/4 - 1/2 - 1	157.1 180.0 203.6 227.9 252.8 278.5 304.9 332.0 359.8	37.0 41.7 46.5 51.4 56.2 61.0 65.9 70.8 75.8	111.6 122.0 132.4 142.8 153.2 163.6 174.1 184.5 194.9	22.3 24.4 26.5 28.6 30.6 32.7 34.8 36.9 39.0	12 " " " " " " " " " " " " " " " " " " "	1/4 = 16 /8 / 16 /8 16 /	174.1 201.6 229.9 259.1 289.0 319.8 351.5 384.0 417.4	41.0 46.8 52.6 58.4 64.2 70.1 76.0 81.9 87.9	196.4 214.4 232.4 250.4 268.4 286.4 304.4 322.4 340.4	32.7 35.7 38.7 41.7 44.7 47.7 50.7 53.7 56.7
8" C 25	16.25 « « « « « « « « « «	10 « « « « « «	14 51 1/2 1 1	164.9 187.8 211.4 235.7 260.6 286.3 312.7 339.8 367.6	38.8 43.6 48.3 53.1 57.9 62.8 67.6 72.5 77.4	119.4 129.8 140.2 150.6 161.0 171.5 181.9 192.3 202.7	23.9 26.0 28.0 30.1 32.2 34.3 36.4 38.5 40.5	12 " " " " " " " " " " " " " " " " " " "	1/4 -10/8 -10/2 -10/8 +10/4	181.9 209.4 237.7 266.9 296.8 327.6 359.3 391.8 425.2	42.8 48.6 54.3 60.1 66.0 71.8 77.7 83.6 89.5	212.5 230.5 248.5 266.5 284.5 302.5 320.5 338.5 356.5	35.4 38.4 41.4 44.4 47.4 50.4 53.4 56.4 59.4
8" C 25	18.75	10 %	1/4 10/8 10/2 10/8 10/8	172.7 195.6 219.2 243.5 268.4 294.1 320.5 347.6 375.4	40.6 45.4 50.1 54.9 59.7 64.5 69.3 74.2 79.0	126.3 136.7 147.2 157.6 168.0 178.4 188.8 199.2 209.7	25.3 27.4 29.4 31.5 33.6 35.7 37.8 89.9 41.9	12	1/4 16/8 16/2 16/8 16/8	189.7 217.2 245.5 274.7 304.6 335.4 367.1 399.6 433.0	44.6 50.4 56.1 61.9 67.7 73.5 79.4 85.2 91.2	227.3 245.3 263.3 281.3 299.3 317.3 335.3 353.3 371.3	37.9 40.9 43.9 46.9 49.9 52.9 55.9 58.9 61.9
8" C 25	21.25	10 4 4 4 4 4 4 4 4	1/4 16/8/7 16/8/4	180.7 203.6 227.2 251.5 276.4 302.1 328.5 855.6 383.4	42.5 47.2 51.9 56.7 61.4 66.2 71.0 75.9 80.7	133.0 143.4 153.8 164.2 174.6 185.0 195.5 205.9 216.3	26.6 28.7 30.8 32.8 34.9 37.0 39.1 41.2 43.3	12 " " " " " " " " " " " " " " " " " " "	1/4 15/8/11/2 15/8/14/4	197.7 225.2 253.5 282.7 312.6 343.4 375.1 407.6 441.0	46.5 52.2 58.0 63.7 69.5 75.3 81.1 87.0 92.8	241.7 259.7 277.7 295.7 313.7 331.7 349.7 367.7 385.7	40.3 43.3 46.3 49.3 52.8 55.3 58.3 61.3 64.3



1				SEI	RIE	S A.				SEI	RIE	S B.	
Depth of Chan-	Weight	late.	Plate.	Axis	1-1.	Axis	2-2.	late.	of Plate.	Axi	1-1.	Axia	2-2.
nel and Section Num- ber.	Poot.	Width of Plate.	Thickness of Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Intokness of	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.
	Lbs.	In.	In.	Ins.4	Ing.3	Ins,4	Ins.3	In.	In.	Ins.4	Ins.3	Ins.4	Ins.3
9" C 29	13.25	11	1/4 10/8 10/2 10/8 10/4	212.3 243.8 276.0 309.0 343.0 377.9 413.5 449.9 487.5	44.7 50.7 56.6 62.6 68.6 74.7 80.7 86.7 92.9	147.9 161.8 175.6 189.4 203.3 217.3 231.1 244.9 258.8	26.9 29.4 31.9 34.4 37.0 39.5 42.0 44.5 47.1	13	1/4 18/8 18/2 18/8 18/4	233.7 270.8 308.9 348.1 388.2 429.3 471.5 514.7 558.9	49.2 56.3 63.4 70.5 77.6 84.8 92.0 99.2 106.5	244.3 267.2 290.1 313.0 335.9 358.8 381.6 404.5 427.4	37.6 41.1 44.6 48.2 51.7 55.2 58.7 62.2 65.8
9″ C 29	15.00	11 4 4 4 4 4 4 4	14 18/8 11/2 15/8 18/4	219.5 251.0 283.2 316.2 350.2 385.1 420.7 457.1 494.7	46.2 52.2 58.1 64.0 70.0 76.1 82.1 88.1 94.2	155.4 169.3 183.1 197.0 210.9 224.8 238.6 252.4 266.3	28.3 30.8 33.3 35.8 38.3 40.9 43.4 45.9 48.4	13 4 4 4 4 4 4 4 4 4 4	14 18/8 18/2 18/8 18/4	240.9 278.0 316.1 355.3 395.4 436.5 478.7 521.9 566.1	50.7 57.8 64.9 72.0 79.1 86.2 93.4 100.6 107.8	258.5 281.4 304.3 327.2 350.1 373.0 395.8 418.7 441.6	39.8 43.3 46.8 50.3 53.9 57.4 60.9 64.4 67.9
9″ C 29	20.00	11	1/4 10/8/10/2010/8/10/8/10/8/10/8/10/8/10/8/	239.3 270.8 303.0 336.0 370.0 404.9 440.5 476.9 514.5	50.4 56.3 62.2 68.0 74.0 80.0 86.0 91.9 98.0	175.6 189.5 203.3 217.1 231.0 244.9 258.8 272.6 286.5	31.9 34.5 37.0 39.5 42.0 44.5 47.1 49.6 52.1	13	1/4 18/8 16/2 16/8 18/4	260.7 297.8 335.9 375.1 415.2 456.3 498.5 541.7 585.9	54.9 61.9 68.9 76.0 83.0 90.1 97.3 104.4 111.6	297.0 319.9 342.8 365.7 388.6 411.5 434.3 457.2 480.1	45.7 49.2 52.7 56.3 59.8 63.3 66.8 70.3 73.9
9″ C 29	25.00	11 4 4 4 4 4 4 4 4	1/4 16/8 16/8 16/8 16/8	259.1 290.6 322.8 355.8 389.8 424.7 460.3 496.7 534.3	54.5 60.4 66.2 72.1 78.0 83.9 89.8 95.8 101.8	194.6 208.5 222.3 236.1 250.1 264.0 277.8 291.6 305.5	35.4 37.9 40.4 42.9 45.5 48.0 50.5 53.0 55.6	13 4 4 4 4 4 4 4 4	1/4 15/8 15/3 15/8 16/8	280.5 317.6 355.7 394.9 435.0 476.1 518.3 561.5 605.7	59.1 66.0 73.0 80.0 87.0 94.1 101.1 108.2 115.4	333.9 356.8 379.7 402.5 425.4 448.3 471.2 494.1 517.0	51.4 54.9 58.4 61.9 65.5 69.0 72.5 76.0 79.5



Depth				SEI	RIE	S A.				SEI	RIE	S B.	
Chan-	Weight	late.	late.	Axis	1-1.	Axis	2-2.	late.	late.	Axis	1-1.	Axis	2-2.
nel and Section Num- ber.	Poot.	Width of Plate	Thickness Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Thickness Plate.	Mo- mient of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.
001.	Lbs.	In.	In.	Ins.4	Ins.3	Ins.4	Ins.3	In.	In.	Ins.4	Ins.3	Ins.4	Ins.3
10" C 88	15.0 « « « «	12	1/4 5/6/8/7/6/8/8/16/8/4	291.4 333.3 376.1 419.9 464.8 510.7 557.6 605.6	55.5 62.7 70.0 77.2 84.5 91.8 99.1 106.5	195.4 213.4 231.4 249.4 267.4 285.4 303.4 321.4	32.6 35.6 38.6 41.6 44.6 47.6 50.6 53.6	15 " " " " " " " " " " " " " " " " " " "	1/4 5 6 8 7 6 12 9 6 8 1 6 8 4	330.8 383.3 436.7 491.6 547.6 605.1 663.6 723.7	63.0 72.1 81.2 90.4 99.6 108.8 118.0 127.3	381.8 417.0 452.1 487.3 522.4 557.6 592.7 627.9	50.9 55.6 60.3 65.0 69.7 74.3 79.0 83.7
10" C 38	20.0	12 " " " " " " " " " " " " " " " " " " "	1/4 5 16 /8 7 16 /2 9 16 /8 /4 8 /4	654.7 315.0 356.9 399.7 443.5 488.4 534.3 581.2 629.2 678.3	113.9 60.0 67.2 74.4 81.6 88.8 96.1 103.3 110.6 118.0	339.4 220.1 238.1 256.1 274.1 292.1 310.1 328.1 346.1	56.6 36.7 39.7 42.7 45.7 48.7 51.7 54.7 57.7 60.7	15	1/4 516 8/8 716 1/2 116/8 116 8/4	784.9 354.4 406.9 460.3 515.2 571.2 628.7 687.2 747.3 808.5	136.5 67.5 76.6 85.6 94.8 103.9 113.0 122.2 131.4 140.6	663.1 438.0 473.1 508.3 543.4 578.6 613.8 648.9 684.1 719.2	88.4 58.4 63.1 67.8 72.5 77.2 81.8 86.5 91.2 95.9
10″ C 83	25.0	12 " " " " " " " " " " " " " " " " " " "	1/4 = 6/8/7 = 1/2 = 15/8 + 10/4	339.6 381.5 424.3 468.1 513.0 558.9 605.8 653.8 702.9	64.7 71.8 78.9 86.1 93.3 100.5 107.7 115.0 122.2	242.8 260.8 278.8 296.8 314.8° 332.8 350.8 368.8 386.8	40.5 43.5 46.5 49.5	15	1/4 5 6 8 7 6 1/2 0 6 1 5 8 1 6 8 4	379.0 431.5 484.9 539.8 595.8 653.3 711.8 771.9 833.1	72.2 81.2 90.2 99.3 108.3 117.4 126.5 135.7 144.9	491.8 526.9 502.1 507.3 602.4 607.6 702.7 737.9 773.0	65.6 70.3 75.0 79.6 84.3 89.0 93.7 98.4 103.1
10″ C 88	30.0	12	1/4 16 88 16 1/2 16 81 18 14	364.0 405.9 448.7 492.5 537.4 583.3 630.2 678.2 727.3	69.3 76.4 83.5 90.6 97.7 104.9 112.0 119.3 126.5	262.9 280.9 298.9 316.9 334.9 352.9 370.9 388.9 406.9	43.8 46.8 49.8 52.8 55.8 58.8 61.8 64.8 67.8	15 " " " " " " " " " " " " " " " " " " "	1/4 56 88 16 /2 96 /8 16 /8	403.4 455.9 509.3 564.2 620.2 677.7 736.2 796.3 857.5	76.8 85.8 94.8 103.8 112.8 121.8 130.9 140.0 149.1	541.6 576.8 611.9 647.1 682.2 717.4 752.5 787.7 822.9	72.2 76.9 81.6 86.3 91.0 95.7 100.3 105.0 109.7
10″ C 88	35.0 « « « « «	12	1/4 516 3/8 16 1/2 16 5/8 16 8/4	388.6 430.5 473.3 517.1 562.0 607.9 654.8 702.8 751.9	74.0 81.0 88.1 95.1 102.2 109.3 116.4 123.6 130.8	281.7 299.7 317.7 355.7 353.7 371.7 389.7 407.7 425.7	46.9 49.9 52.9 55.9 58.9 61.9 64.9 67.9 70.9	15 4 4 4 4 4 4 4	1/4 5 6 8 8 7 6 8 8 8 1 6	428.0 480.5 533.9 588.8 644.8 702.3 760.8 820.9 882.1	81.5 90.4 99.3 108.3 117.2 126.3 135.3 144.3 153.4	589.2 624.4 659.5 694.7 729.8 765.0 800.2 835.3 870.5	78.6 83.3 87.9 92.6 97.3 102.0 106.7 111.4 116.1

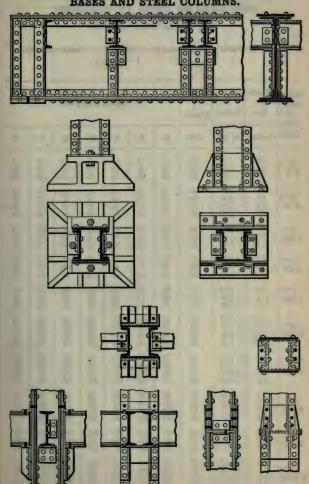


Chan-nell par and section   Montage   Monta	Depth				SEI	RIE	S A.				SEI	RIE	S B.	
Section   Sect	Ohan-	Weight	ate.	ate.	Axis	1-1.	Axis	2-2	876.	late.	Axis	1-1.	Axis	2-2.
Section   Sect			of Pl	A SE		Section		Section	of P	Se P		Section		Section
	Section	FOOL	母	F		Mod-		Mad-	idth	B		Mod-		Mod-
18.   18.					Inertia.		Inertia.			ig.				
12" C41  a	Det.					-	-				-			
12"   14	-	20.5	14	3/4					16	3/4				
12"   14		a		3/8	658.3	103.3	428.4	61.2		3/8	715.8	112.3	634.6	79.3
12"   14	12"	44		16						10				
12"   14	041	*		72						73		147.3		
12"   14		4		5/6						8/8		159.1		
12"   14				17					_	18				
12" C41  " " " " " " " " " " " " " " " " " " "		25.0	14		550.7	88.1	409.9	58.6	18		588.2	94.1	610.8	76.4
12"   14"   103.4   159.0   610.0   87.2   2   4   114.2   175.6   999.4   113.7     30.0   14   14   169.3   638.6   91.2   2   4   114.2   175.6   999.4   113.7     30.0   14   14   158.5   93.7   450.2   64.3   16   14   162.3   168.6   182.4     30.0   14   14   158.5   93.7   1450.2   64.3   16   14   162.3   162.3   119.0     30.0   14   14   158.5   93.7   1450.2   64.3   16   14   162.3   162.3   119.0     30.0   14   14   169.3   163.6   91.2   2   4   114.2   175.6   999.4   113.7     30.0   14   14   158.5   93.7   1450.2   64.3   16   14   1264.5   187.3   182.1     30.0   14   14   169.3   163.6   163.6   163.6   163.6     4			4	10						16				
12"   14"   103.4   159.0   610.0   87.2   2   4   114.2   175.6   999.4   113.7     30.0   14   14   169.3   638.6   91.2   2   4   114.2   175.6   999.4   113.7     30.0   14   14   158.5   93.7   450.2   64.3   16   14   162.3   168.6   182.4     30.0   14   14   158.5   93.7   1450.2   64.3   16   14   162.3   162.3   119.0     30.0   14   14   158.5   93.7   1450.2   64.3   16   14   162.3   162.3   119.0     30.0   14   14   169.3   163.6   91.2   2   4   114.2   175.6   999.4   113.7     30.0   14   14   158.5   93.7   1450.2   64.3   16   14   1264.5   187.3   182.1     30.0   14   14   169.3   163.6   163.6   163.6   163.6     4	10"		4	78					65	78	829.6		738.8	92.4
12"   30.0   4   4   585.9   93.7   480.2   64.3   16   34   623.4   99.7   67.7   84.5     12"   4   4   585.9   93.7   478.5     12"   5   797.1   123.8   505.9   76.6     4   5   797.1   123.8   505.9   76.6     4   5   797.1   123.8   505.9   76.6     5   797.1   123.8   505.9   76.6     6   7   7   7   7   7   7   7     7   8   7   8   7     8   8   8   8   8   8   8     8   8	C41			1/2		128.5	524.3	74.9		1/2		140.5	781.4	
12"   30.0   4   4   585.9   93.7   480.2   64.3   16   34   623.4   99.7   67.7   84.5     12"   4   4   585.9   93.7   478.5     12"   5   797.1   123.8   505.9   76.6     4   5   797.1   123.8   505.9   76.6     4   5   797.1   123.8   505.9   76.6     5   797.1   123.8   505.9   76.6     6   7   7   7   7   7   7   7     7   8   7   8   7     8   8   8   8   8   8   8     8   8		_	-	56						18				
12"   30.0   4   4   585.9   93.7   480.2   64.3   16   34   623.4   99.7   67.7   84.5     12"   4   4   585.9   93.7   478.5     12"   5   797.1   123.8   505.9   76.6     4   5   797.1   123.8   505.9   76.6     4   5   797.1   123.8   505.9   76.6     5   797.1   123.8   505.9   76.6     6   7   7   7   7   7   7   7     7   8   7   8   7     8   8   8   8   8   8   8     8   8		_	_	11	1063.4	159.0	610.0	87.2		報	1174.2	175.6	909.4	113.7
12" C41  a # \$\frac{1}{4}\$ 854.9 103.7 478.8 68.4 a \$\frac{1}{4}\$ 722.3 111.3 718.3 89.8    a # \$\frac{1}{4}\$ 725.3 113.8 507.3 72.5 a \$\frac{1}{4}\$ 578.2 122.8 761.0 95.1    a # \$\frac{1}{4}\$ 797.1 123.8 505.9 76.6 a \$\frac{1}{4}\$ 578.4 133.9 564.5 80.6 a \$\frac{1}{4}\$ \$\frac{1}{4		-			_		_	_	•					
35.0   14   14   22.13   99.4   484.9   69.3   16   14   658.8   105.4   733.6   91.7    12"   4   69.3   10.4   513.4   73.4   4   737.7   116.9   776.3   97.0    14"   5   760.7   119.3   542.0   77.4   4   5   318.2   128.3   818.9   102.4    15   641   7   7   7   7   7   7   7   7   7		30.0	14	1/4					16	1/4		99.7		
35.0   14   14   22.13   99.4   484.9   69.3   16   14   658.8   105.4   733.6   91.7    12"   4   69.3   10.4   513.4   73.4   4   737.7   116.9   776.3   97.0    14"   5   760.7   119.3   542.0   77.4   4   5   318.2   128.3   818.9   102.4    15   641   7   7   7   7   7   7   7   7   7		_	_	3/8	725.3	113.8	507.3	72.5		3/8	782.8	122.8	761.0	95.1
35.0   14   14   22.13   99.4   484.9   69.3   16   14   658.8   105.4   733.6   91.7    12"   4   69.3   10.4   513.4   73.4   4   737.7   116.9   776.3   97.0    14"   5   760.7   119.3   542.0   77.4   4   5   318.2   128.3   818.9   102.4    15   641   7   7   7   7   7   7   7   7   7	12"			18						16	864.8			
35.0   14   14   22.13   99.4   484.9   69.3   16   14   658.8   105.4   733.6   91.7    12"   4   69.3   10.4   513.4   73.4   4   737.7   116.9   776.3   97.0    14"   5   760.7   119.3   542.0   77.4   4   5   318.2   128.3   818.9   102.4    15   641   7   7   7   7   7   7   7   7   7	041	_		72	945.0			84.7		72				
35.0   14   14   22.13   99.4   484.9   69.3   16   14   658.8   105.4   733.6   91.7    12"   4   69.3   10.4   513.4   73.4   4   737.7   116.9   776.3   97.0    14"   5   760.7   119.3   542.0   77.4   4   5   318.2   128.3   818.9   102.4    15   641   7   7   7   7   7   7   7   7   7				18				88.8		5/8				
35.0   14   14   22.13   99.4   484.9   69.3   16   14   658.8   105.4   733.6   91.7    12"   4   69.3   10.4   513.4   73.4   4   737.7   116.9   776.3   97.0    14"   5   760.7   119.3   542.0   77.4   4   5   318.2   128.3   818.9   102.4    15   641   7   7   7   7   7   7   7   7   7		_	_	18					_	18				
12" 14" 14" 15" 16" 16" 16" 16" 16" 16" 16" 16" 16" 16	7	35.0	14		621.3		484.9					105.4	733.6	
40.0   14   34   858.5   108.0   529.1   74.3   16   34   894.0   111.0   792.1   99.0    12"   4   5   725.5   114.9   548.7   78.4   4   5   772.9   122.4   834.8   104.3    12"   5   785.9   124.9   577.2   82.5   4   35   853.4   133.9   877.4   109.7    12"   6   7   887.7   134.8   605.8   86.6   7   7   7   7   7   7   7   7   7    14"   7   8   7   104.8   634.4   90.6   3   2   1019.1   156.8   962.8   120.3    2   7   1015.6   154.8   636.3   94.7   4   7   104.5   168.3   1004.5   126.7    2   8   1091.7   104.8   691.6   98.8   8   9   1191.4   179.8   1048.1   131.0		"	44	16						16			776.3	
40.0   14   34   858.5   108.0   529.1   74.3   16   34   894.0   111.0   792.1   99.0    12"   4   5   725.5   114.9   548.7   78.4   4   5   772.9   122.4   834.8   104.3    12"   5   785.9   124.9   577.2   82.5   4   35   853.4   133.9   877.4   109.7    12"   6   7   887.7   134.8   605.8   86.6   7   7   7   7   7   7   7   7   7    14"   7   8   7   104.8   634.4   90.6   3   2   1019.1   156.8   962.8   120.3    2   7   1015.6   154.8   636.3   94.7   4   7   104.5   168.3   1004.5   126.7    2   8   1091.7   104.8   691.6   98.8   8   9   1191.4   179.8   1048.1   131.0	19"	4	_	78					46	78				
40.0   14   34   858.5   108.0   529.1   74.3   16   34   894.0   111.0   792.1   99.0    12"   4   5   725.5   114.9   548.7   78.4   4   5   772.9   122.4   834.8   104.3    12"   5   785.9   124.9   577.2   82.5   4   35   853.4   133.9   877.4   109.7    12"   6   7   887.7   134.8   605.8   86.6   7   7   7   7   7   7   7   7   7    14"   7   8   7   104.8   634.4   90.6   3   2   1019.1   156.8   962.8   120.3    2   7   1015.6   154.8   636.3   94.7   4   7   104.5   168.3   1004.5   126.7    2   8   1091.7   104.8   691.6   98.8   8   9   1191.4   179.8   1048.1   131.0	C41	45	_	1/2			599.2	85.6		1/2		151.4		113.0
40.0   14   34   858.5   108.0   529.1   74.3   16   34   894.0   111.0   792.1   99.0    12"   4   5   725.5   114.9   548.7   78.4   4   5   772.9   122.4   834.8   104.3    12"   5   785.9   124.9   577.2   82.5   4   35   853.4   133.9   877.4   109.7    12"   6   7   887.7   134.8   605.8   86.6   7   7   7   7   7   7   7   7   7    14"   7   8   7   104.8   634.4   90.6   3   2   1019.1   156.8   962.8   120.3    2   7   1015.6   154.8   636.3   94.7   4   7   104.5   168.3   1004.5   126.7    2   8   1091.7   104.8   691.6   98.8   8   9   1191.4   179.8   1048.1   131.0			-	18						16		174.5		
40.0   14   34   858.5   108.0   529.1   74.3   16   34   894.0   111.0   792.1   99.0    12"   4   5   725.5   114.9   548.7   78.4   4   5   772.9   122.4   834.8   104.3    12"   5   785.9   124.9   577.2   82.5   4   35   853.4   133.9   877.4   109.7    12"   6   7   887.7   134.8   605.8   86.6   7   7   7   7   7   7   7   7   7    14"   7   8   7   104.8   634.4   90.6   3   2   1019.1   156.8   962.8   120.3    2   7   1015.6   154.8   636.3   94.7   4   7   104.5   168.3   1004.5   126.7    2   8   1091.7   104.8   691.6   98.8   8   9   1191.4   179.8   1048.1   131.0			_	118	1134.0	169.6	684.9	97.9		H	1244.8	186.1	1032.3	129.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	7 4	-												
12"	100	30.0	4	4					46	1/4				
12"	-			3/8	795.9	124.9	577.2	82.5		3/8	853.4	133.9	877.4	109.7
* 4 104.5 154.8 663.0 94.7 4 104.5 168.3 1005.4 125.7 104.8 691.6 98.8 5 191.4 179.8 1048.1 131.0 4 1 1169.2 174.8 790.2 102.9 4 1 128.0 191.4 179.8 1048.1 131.0 4 1 131.0 13	12"	_		16						16				
*   \$\begin{array}{c c c c c c c c c c c c c c c c c c c	041			16	1015.6	154.8	663.0	94.7		16	1104.5	168.3	1005.4	125.7
# 8 1109.2 174.8 720.2 102.9 13 1200.0 191.4 1090.8 130.3			_	11						5/8				
1 1/4   1240.4   102.8   140.1   101.0   1/4   1310.3   203.0   1133.4   141.1				3/4	1248.2	184.9	748.7	107.0		11	1370.3			



				SEI	RIE	S A.		8		SEI	RIE	S B.	
Depth			sto.	Axis	1-1.	Axis	2-2.		Plate.	Axis	1-1.	Axis	2-2.
Chan- nel and Section Num- ber.	Weight per Foot.	Width of Plate.	Thickness of Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Thickness of Pla	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus,
	Lbs.	In.	In.	Ins.4	Ins.3	Ins.4	Ins.3	In.	In.	Ins.4	Ins.3	Ins.4	Ins.3
15" C 53	33.0	17 4 4 4 4 4 4	8/8 11/2 15/8 116 13/4	1378.9 1512.0 1646.6 1783.4 1922.9 2064.6 2207.8	175.1 190.5 205.8 221.2 236.7 252.2 267.6	953.4 1004.7 1055.7 1106.8 1158.1 1209.4 1260.4	112.2 118.2 124.2 130.2 136.2 142.3 148.3	20	3/8 16/2 16/8 16/8 116/8	1511.8 1668.1 1826.9 1988.1 2151.9 2318.2 2487.1	192.0 210.2 228.4 246.6 264.9 283.1 301.5	1525.9 1609.2 1692.5 1775.9 1859.2 1942.5 2025.9	152.6 160.9 169.3 177.6 185.9 194.3 202.6
15" C 58	35.0 « « «	17 " " " " " " " " " " " " " " " " " " "	3/8 16/2 16/5/8 16 5/8 16 5/8	1393.5 1526.6 1661.2 1798.0 1937.5 2079.2 2222.4	177.0 192.3 207.7 223.0 238.5 254.0 269.4	971.7 1023.0 1074.1 1125.1 1176.4 1227.7 1278.8	114.3 120.4 126.4 132.4 138.4 144.4 150.4	20 4 4 4 4 4	8/8 TE 1/2 TE 5/8 TE 5/8	1526.4 1682.7 1841.5 2002.7 2166.5 2332.8 2501.7	193.8 212.0 230.2 248.4 266.6 284.9 303.2	1557.3 1640.7 1724.0 1807.3 1890.7 1974.0 2057.3	155.7 164.1 172.4 180.7 189.1 197.4 205.7
15" C 58	40.0 « « «	17 « « « «	8/8 16/23 16 5/816 8/4	1448.7 1581.8 1716.4 1853.2 1992 7 2134.4 2277.6	184.0 199.3 214.6 229.9 245.3 260.7 276.1	1039.9 1091.2 1142.3 1193.3 1244.6 1295.9 1347.0	122.3 128.4 134.4 140.4 146.4 152.5 158.5	20 4 4 4 4 4 4 4	3/8 116 1/2 16 5/8 16 8/4	1581.6 1737.9 1896.7 2057.9 2221.7 2388.0 2556.9	200.8 219.0 237.1 255.3 273.4 291.7 309.9	1674.6 1757.9 1841.2 1924.6 2007.9 2091.2 2174.6	167.5 175.8 184.1 192.5 200.8 209.1 217.5
15" C 58	45.0 « « « «	17	3/8-70-12-06-5%-16	1503.9 1637.0 1771.6 1908.4 2047.9 2189.6 2332.8	191.0 206.2 221.5 236.7 252.0 267.4 282.8	1105.4 1156.8 1207.9 1258.9 1310.2 1361.5 1412.6	130.1 136.1 142.1 148.1 154.2 160.2 166.2	20 " " " " " " " " " " " " " " " " " " "	8/8/16/20 16/8/4	1636.8 1793.1 1951.9 2113.1 2276.9 2443.2 2612.1	207.9 225.9 244.0 262.1 280.2 298.4 316.6	1788.6 1871.9 1955.3 2038.6 2121.9 2205.3 2288.6	178.9 187.2 195.5 203.9 212.2 220.5 228.9
15" C 53	50.0 « « «	17	3/8 TE /20 15/8 118/4	1559.1 1692.2 1826.8 1963.6 2103.1 2244.8 2388.0	198.0 213.2 228.4 243.5 258.8 274.2 289.5	1165.3 1216.6 1267.7 1318.7 1370.0 1421.3 1472.4	137.1 143.1 149.1 155.1 161.2 167.2 173.2	20 4 4 4 4 4	3/8/16/20 16/8/4 16/8/4	1692.0 1848.3 2007.1 2168.3 2332.1 2498.4 2667.3	214.9 232.9 250.9 268.9 287.0 305.2 323.3	1894.9 1978.2 2061.5 2144.9 2228.2 2311.5 2394.9	189.5 197.8 206.2 214.5 222.8 231.2 239.5
15″ 0 53	55.0	17 4 4 4 4 4 4 4 4	3/8 76/2 96/8 116	1614.1 1747.2 1881.8 2018.6 2158.1 2299.8 2443.0	205.0 220.1 235.2 250.4 265.6 280.9	1223.4 1274.7 1325.7 1376.8 1428.1 1479.4 1530.4	143.9 150.0 156.0 162.0 168.0 174.0	20 " " " " " " " " " " " " " " " " " " "	8/8 16/2 16/8 14 5/8 14	1747.0 1903.3 2062.1 2223.3 2387.1 2553.4 2722.3	221.9 239.8 257.8 275.8 293.8 311.9	1998.8 2082.1 2165.5 2248.8 2332.1 2415.5 2498.8	199.9 208.2 216.6 224.9 233.2 241.6 249.9

## TYPICAL DETAILS OF PLATE GIRDERS, COLUMN BASES AND STEEL COLUMNS.



Based on Gordon's Formula, P =  $\frac{50\,000}{1+\frac{(12\,\mathrm{L})^2}{36\,000\,\mathrm{r}^2}}$ . Safety factor 4.

Depth of Beam and Section	Weight per Poot.	Area of Section.	Least Radius of Gyration,			Leng	th in	Feet.		
Number.	Pounds.	Sq. Ins.	Inch.	2	8	4	5	в	7	8
3" B 5	5.5 6.5 7.5	1.63 1.91 2.21	.53 .52 .52	19 23 26	18 21 24	17 19 22	15 17 20	13 16 18	12 14 16	11 12 14
4" B 9	7.5 8.5 9.5 10.5	2.21 2.50 2.79 3.09	.59 .58 .58 .57	26 30 33 37	25 28 31 35	23 26 29 32	21 24 27 29	20 22 24 27	18 20 22 24	16 18 20 22
5" B 18	9.75 12.25 14.75	2.87 3.60 4.34	.65 .63 .63	35 43 52	33 41 50	31 39 47	29 36 43	27 33 40	24 30 36	22 27 33
B 17	12.25 14.75 17.25	3.61 4.34 5.07	.72 169 168	44 52 61	42 51 59	40 48 56	38 45 52	35 42 48	33 39 44	30 35 41
7″ B 21	15.0 17.5 20.0	4.42 5.15 5.88	.78 .76 .74	54 63 71	52 61 -69	50 58 66	47 55 62	45 52 58	42 48 54	39 45 50
8″ B 25	18.00 20.25 22.75 25.25	5.33 5.96 6.69 7.43	.84 .82 .81	65 73 82 91	63 71 79 88	61 68 76 84	58 85 72 80	55 61 09 76	52 58 65 71	49 54 60 66
9″ B 29	21.0 25.0 30.0 35.0	6.31 7.35 8.82 10.29	.90 .88 .85 .84	77 90 108 126	76 88 105 122	73 85 101 118	70 81 97 112	07 78 92 107	63 73 87 101	60 69 81 95
10" B 33	25.0 30.0 35.0 40.0	7.37 8.82 10.29 11.76	.97 .93 .91 .90	01 108 126 144	89 106 123 141	86 103 119 136	83 99 115 131	80 94 110 125	76 90 104 118	73 85 98 112
12" B 41	31.5 35.0 40.0	9.26 10.29 11.76	1.01 .99 .96	114 127 144	112 124 142	109 121 137	105 117 133	102 112 127	97 107 121	93 102 115
12" B 105	40.0 -45.0 50.0 55.0	11.84 13.24 14.71 16.18	1.08 1.06 1.05 1.04	146 163 181 199	144 160 178 196	140 156 174 191	136 152 168 185	132 146 163 178	127 141 156 171	121 135 149 163

Based on Gordon's Formula,  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.

			Leng	th in	Feet.				Weight per Foot.	Depth of Beam and
9	10	11	12	13	14	15	16	17	Pounds.	Section Number.
9 11 13									5.5 0.5 7.5	8″ B 5
14 16 18 19	13 14 16 17								7.5 8.5 9.5 10.5	4" B9
20 25 30	18 22 27	17 20 24							9.75 12.25 14.75	5" B 18
28 32 37	25 29 34	23 27 31	21 25 28						12.25 14.75 17.25	6" B 17
36 41 46	33 38 43	31 35 39	28 32 36	26 30 33					15.0 17.5 20.0	7″ B21
46 50 56 61	43 47 52 57	40 43 48 53	37 40 45 49	34 37 41 45	31 34 38 42				18.00 20.25 22.75 25.25	8" B 25
56 65 76 88	53 60 71 82	49 57 86 76	46 53 61 71	43 49 57 86	40 46 53 61	37 43 49 56			21.0 25.0 30.0 35.0	9" B 29
68 80 92 105	65 75 87 98	61 71 81 92	57 66 76 86	54 62 71 80	50 58 66 74	47 54 62 69	44 50 57 65		25.0 30.0 35.0 40.0	10" B 88
88 97 109	83 91 103	78 86 96	74 81 90	69 76 85	65 72 79	61 67 74	58 63 69	54 59 65	31.5 35.0 40.0	12" B 41
116 128 142 155	110 122 135 148	105 116 128 140	99 110 121 132	94 103 114 124	88 98 108 117	83 92 101 111	79 87 96 104	75 82 90 98	40.0 45.0 50.0 55.0	12" B 105

Based on Gordon's Formula, P =  $\frac{50\,000}{1+\frac{(12\,L)^3}{36\,000\,r^2}}$ . Safety factor 4.

Depth of Beam and Section	Weight per Foot.	Area of Section.	Least Radius of Gyra- tion.			L	ength	in Fe	et.		
Number.	Pounds.	Sq. Ins.	Inches.	2	8	4	5	6	7	8	9
15" B 53	42.0 45.0 50.0 55.0 60.0	12.48 13.24 14.71 16.18 17.65	1.08 1.07 1.04 1.03 1.01	154 163 181 199 217	151 160 178 196 213	148 157 174 191 207	144 152 168 185 201	139 147 162 178 194	133 142 156 171 185	128 135 149 163 177	122 129 141 155 167
15" B 109	80.0 65.0 70.0 75.0 80.0	17.67 19.12 20.59 22.06 23.53	1.21 1.20 1.19 1.18 1.17	218 236 254 273 291	215 233 251 269 286	212 229 246 264 281	207 223 240 258 274	201 217 234 250 266	195 211 226 242 257	188 203 218 233 248	181 195 209 224 238
15" B 113	80.0 85.0 90.0 95.0 100.0	23.57 25.00 26.47 27.94 29.41	1.32 1.32 1.32 1.31 1.31	292 309 328 346 364	289 306 324 342 360	284 302 319 336 354	279 295 313 330 348	273 289 306 322 339	265 281 297 314 330	256 272 288 304 320	249 264 279 293 309
18" B 65	55.0 60.0 65.0 70.0	15.93 17.65 19.12 20.59	1.15 1.13 1.11 1.09	197 218 236 254	194 214 232 250	190 210 227 244	185 205 221 237	180 198 214 230	173 191 206 221	166 184 198 212	160 176 189 202
20" B 78	65.0 70.0 75.0	19.08 20.59 22.06	1.21 1.19 1.17	236 254 273	233 251 268	229 246 264	,223 240 257	217 234 250	210 226 241	203 218 233	196 209 223
20" B 121	80.0 85.0 90.0 95.0 100.0	23.73 25.00 26.47 27.94 29.41	1.39 1.37 1.36 1.35 1.34	294 309 328 346 364	291 307 325 343 361	287 302 320 337 355	282 297 314 331 349	276 290 307 324 340	270 283 300 315 332	261 275 290 307 321	254 266 282 296 312
24" B 89	80.0 85.0 90.0 95.0 100.0	23.32 25.00 26.47 27.94 29.41	1.36 1.33 1.31 1.30 1.28	289 309 328 346 364	286 306 324 342 360	282 302 319 336 354	276 295 313 330 347	271 289 305 322 338	264 281 297 313 328	256 273 288 303 317	248 264 278 293 307
94" B 127	105.0 110.0 115.0	30.98 32.48 33.98	1.60 1.58 1.57	385 403 422	382 400 419	378 396 414	373 390 408	367 384 401	360 376 393	352 368 385	344 359 375

Based on Gordon's Formula, P =  $\frac{50\,000}{1+\frac{(12\,L)^2}{36\,000\,r^2}}$ . Safety factor 4.

	= 10		Weight per Foot.	Depth of Beam and							
10	11	19	Pounds.	Section. Number.							
116 123 134 147 158	110 116 127 139 150	105 110 120 131 141	99 104 113 124 132	93 98 106 116 124	88 93 101 109 117	83 87 94 103 110	79 82 89 97 104	74 78 84 91 97		42.0 45.0 50.0 55.0 60.0	15" B 53
173 187 201 214 228	166 179 192 205 217	159 171 183 195 206	152 163 174 186 197	144 154 165 176 187	137 147 157 168 178	130 140 150 158 168	124 132 142 151 160	117 126 135 142 151	111 120 127 135 143	60.0 65.0 70.0 75.0 80.0	15" B 109
239 254 269 284 299	231 245 259 272 287	221 235 249 261 275	213 226 239 251 264	203 216 228 240 252	194 206 218 228 240	185 197 209 219 230	177 188 199 208 219	169 180 190 199 210	161 171 181 190 200	80.0 85.0 90.0 95.0 100.0	15" B 113
153 168 181 192	145 160 172 183	139 152 163 173	132 144 154 164	125 137 146 155	119 129 138 146	112 122 131 138	106 116 123 130	100 110 117 123	95 104 110 116	55.0 60.0 65.0 70.0	18" B 65
187 201 214	179 192 204	171 183 194	164 174 185	155 165 175	148 157 167	141 150 158	134 142 150	126 135 142	120 127 135	65.0 70.0 75.0	20" B 78
246 258 271 286 300	237 249 262 277 290	229 239 253 265 278	219 230 241 255 267	211 221 232 244 257	202 212 223 234 245	194 202 213 223 235	186 194 204 214 223	177 185 195 205 214	169 176 185 195 203	80.0 85.0 90.0 95.0 100.0	20" B 121
239 255 269 282 296	231 245 258 271 284	223 236 247 261 272	213 226 238 249 260	205 217 227 239 249	196 207 216 228 238	187 198 207 218 226	179 189 197 207 215	172 181 189 198 205	163 172 180 188 196	80.0 85.0 90.0 95.0 100.0	24" B 89
335 350 365	326 340 355	316 330 344	306 319 333	296 309 322	285 298 311	277 288 300	266 278 289	257 267 278	247 257 268	105.0 110.0 115.0	24" B 127

CALCULATED FOR LEAST RADIUS OF GYRA-TION, AXIS 1-1.

Based on Gordon's Formula,  $P = \frac{50000}{1000}$ Safety factor 4.  $1 + \frac{(12 \text{ L})^2}{36000 \text{ r}^2}$ 

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Sixe	Size	Weight	Area	Least	Radius			
. of	of	01	of	Radius of	Gyration.		ength	
Angles.	Plate.	Column.	Section.	Gyration Axis 1-1.	Axis 2-2.	11	Feet	
Inches.	Inches.	Lba.per Ft.	Sq. Ins.	Inches.	Inches.	2	4	6
3 x2½x¼	6 x 1/4	23.1	6.74	1.24	2.41	84	81	77
41 4 5	4 5	28.8	8.36	1.27	2.39	103	100	.06
4 4 3/2	# 18 # 8/8	34.1	9.93	1.30	2.37	123	120	114
# # 1/2 # # 1/2	16	39.3	11.51	1.33	2.35	142	139	133
4 4 1/2	72	44.2	13.00	1.36	2.33	161	157	151
	1.0	49.5	14.50	1.39	2.31	180	175	160
31/2 x 21/2 x 1/4	7 x 1/4	25.6	7.51	1.46	2.88	93	91	88
" 16	4 16	31.8	9.31	1.49	2.86	115	113	100
" %	4 78	37.7	11.07	1.52	2.84 2.82	137 159	135 156	130 151
4 4 10	4 16	43.6	12.78 14.50	1.58	2.80	180	177	171
# # \$\frac{5}{8}\$ # # # \frac{7}{16}\$ # # # \frac{7}{16}\$ # # # \frac{7}{16}\$	# 1/2 # 1/2 # 1/6	55.0	16.18	1.61	2.78	201	197	192
	8 x 16	37.3	10.86	1.67	3.25		133	129
4 x8 x 14 3/8	4 3/8	44.2	12.92	1.70	3.23		158	154
4 4 7	4 7	51.1	14.98	1.73	3.21		183	179
" " 10	4 1/2	58.0	17.00	1.76	3.18		208	203
4 4 9	4 9	84.9	18.98	1.79	3.16		233	227
4 5/8	# 16 # 18	71.4	20.92	1.82	3.14		257	251
4 4 11	1 10	77.9	22.86	1.85	3.12		281	274
4 4 13	74	84.4	24.76	1.89	3.10		304	297
a a 7/8	4 7/8	90.5 97.0	26.62 28.44	1.92	3.08		327 350	320 343
				-				7
5 x 3½ x 5 16 8/8 4 16 1/2	10 x 15	45.4	13.37	2.08	4.10		165	162 193
4 4 7	# 78	54.4 62.9	15.95 18.50	2.10	4.08		196 228	224
4 4 12	4 12	71.4	21.00	2.16	4.04		259	255
4 4 72	" a 32	79.9	23.51	2.19	4.02		290	285
4 4 16 4 5/8 4 4 118	# 1%	88.5	25.93	2.22	4.00		320	315
" " . 11	" 11	96.6	28.36	2.25	3.98		350	345
8 8/4	" 3/4	104.7	30.74	2.29	3.96		380	374
" " 13 16	# 13 # 16	112.8	33.13	2.32	3.93		409	403
« « 13 « « 7/8 « « 16	4 18	120.6	35.43	2.35	3.91		438	432
	18	128.7	37.74	2.38	3.89		466	460
6 x 3 1/2 x 3/8	12 x 1/3	62.1	18.18	2.56	5.01		225	222
# # 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	a 12	71.9	21.13	2.59	4.99		261	258
4 4 1/2	72	81.6	24.00	2.62	4.97 4.95		297	294 329
a a 156 a a 146 a a 146 a a 146	4 18	91.4	26.87 29.70	2.65 2.68	4.95		333 368	364
# #	" 13	110.5	32.49	2.08	4.93		402	398
# 4 8/A	n 34	120.2	35.24	2.74	4.88		437	432
a a 13	. " 13	129.2	37.99	2.77	4.86		471	466
4 4 7/8	4 7/8	138.5	40.70	2.80	4.84		505	499
4 4 7/8	" 15	147.5	43.37	2.83	4.82		538	532
1 1	" 1	156.4	46.00	2.86	4.80		571	565
· · · · ·	4. 1.2						7	

CALCULATED FOR LEAST RADIUS OF GYRA-TION, AXIS 1-1.

Based on Gordon's Formula,  $P = \frac{50\ 000}{1 + \frac{(12\ L)^3}{36\ 000\ r^2}}$ 



8	10	12	14	16	18	20	22	24	26	28	80	32	34
72 90 108 125 143 160	67 84 100 117 134 150	61 77 93 108 124 140	56 70 85 99 114 129	51 64 77 91 105 119									
84 104 125 145 164 184	79 99 118 137 156 175	74 92 111 129 147 166	69 86 103 121 138 155	63 80 96 112 129 145	58 73 89 104 119 135	54 68 82 96 111 125							
124 149 172 196 220 243 266 289 311 333	119 142 165 188 211 234 256 278 300 322	113 135 157 179 201 223 245 266 288 309	106 127 148 170 191 212 233 254 274 295	99 119 139 160 180 200 220 240 260 280	93 112 131 150 169 188 208 227 246 265	86 104 122 140 158 177 195 213 232 250	97 114 131 148 165 183 200 218 236	74 90 106 122 138 155 171 188 205 222					
158 188 219 249 279 308 337 366 395 423 451	153 183 212 242 271 300 329 357 385 413 441	147 176 205 234 262 290 318 346 374 401 428	141 169 197 225 252 280 307 334 361 388 414	135 162 189 215 242 269 295 321 348 374 400	128 154 180 206 231 257 282 308 333 359 384	122 146 171 196 220 245 270 294 319 343 868	115 139 162 186 209 233 257 280 304 328 352	109 131 153 176 198 221 244 267 290 313 336	103 124 145 166 188 210 231 253 275 297 320	97 117 137 157 178 198 219 240 261 283 304			
219 254 289 324 358 392 426 459 493 525 558	214 249 283 318 352 385 418 451 484 516 548	209 243 277 310 344 376 409 442 474 506 537	203 236 269 302 335 367 899 431 462 494 525	197 229 261 293 325 356 388 419 450 481 511	190 221 252 283 314 345 376 405 437 467 497	183 213 243 273 303 333 363 393 423 452 481	176 205 234 263 292 321 350 379 408 437 465	168 196 225 253 281 309 337 365 393 421 449	161 188 215 242 269 297 324 351 378 405 432	154 180 206 232 258 284 311 337 863 390 416	147 172 197 222 247 272 298 323 349 374 400	140 164 188 212 236 261 285 310 334 359 384	133 156 179 202 226 249 273 296 320 344 368

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula,  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^3}}$ 

50 000 (12 L)<sup>2</sup> 36 000 r<sup>2</sup>

Sizo of Angles.	Size of Plate,	Weight of Column.	of Column Section.	Radius of Gyration Axis 1-1,	Radius of Gyration Axis 2-2.		Lengtl n Feet	
Inches.	Inches,	Lbs.per Pt.	Sq. lns.	Inches,	Inches.	2	4	6
8 x 2½ x ½ 4 4 76 6 4 76 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	8 x 1/4 # 1/8 # 1/2 # 1/2	24.8 30.9 36.6 42.3 47.6 53.3	7.24 8.98 10.68 12.38 14.00 15.62	1.19 1.22 1.25 1.28 1.31 1.34	3.25 3.23 3.21 3.19 3.17 3.15	90 111 132 153 173 193	87 108 128 149 169 188	82 102 122 142 161 181
3½ x 2½ x ¼ a a ½ a a ½ a a ¼ a a ¼ a a ¼ a a ¼ a a ¼	8 x 1/4 a 1/6 a 1/8 a 1/2 a 1/2	26.4 32.9 89.0 45.1 51.2 56.9	7.76 9.62 11.44 13.22 15.00 16.74	1.44 1.47 1.50 1.53 1.56 1.59	3.31 3.28 3.26 3.24 3.22 3.20	96 119 142 164 186 208	94 117 130 161 183 204	91 113 134 156 177 198
4 x 8 x 4 x 4 x 4 x 4 x 4 x 4 x 4 x 4 x	10 x 1/4	39.4 46.8 54.1 61.4 68.7 75.7 82.6 89.5 96.0 103.0	11.49 13.67 15.86 18.00 20.11 22.17 24.24 26.26 28.25 30.19	1.62 1.65 1.68 1.71 1.74 1.77 1.80 1.83 1.86 1.90	4.09 4.07 4.04 4.02 4.00 3.98 3.96 3.94 3.92 3.90		140 167 194 220 246 272 297 322 347 371	136 163 189 214 240 265 290 315 339 363
5 x 81/2 x 16 a a 1/2 a a 1/	12 x 18	47.6 56.9 65.9 74.8 83.8 92.7 101.3 109.8 118.4 126.5 135.1	13.99 16.70 19.37 22.00 24.63 27.18 29.73 32.24 34.75 37.18 39.61	2.03 2.06 2.08 2.11 2.14 2.17 2.20 2.23 2.26 2.29 2.33	4.95 4.92 4.90 4.88 4.86 4.84 4.82 4.80 4.78 4.76		172 206 238 271 303 335 367 398 429 459 489	169 202 234 266 298 330 361 392 422 452 482
6 x 3½ x % 1	14 x 3/9 a a 11/2 a a a a a a 11/2 a a a a a a a a a a a a a a a a a a a	64.7 74.8 85.0 95.2 105.3 115.1 125.3 134.7 144.5 153.8 163.2	18.93 22.01 25.00 28.00 30.95 33.87 36.74 30.02 42.45 45.25 48.00	2.51 2.54 2.57 2.59 2.62 2.65 2.68 2.71 2.74 2.77 2.81	5.85 5.83 5.81 5.79 5.77 5.74 5.72 5.70 5.68 5.68		234 272 309 347 383 419 455 491 520 561 595	231 289 306 343 379 415 450 486 521 555 689

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula,  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ 

8 1		12	14	16	18	20	22	24	26	28	80	32	34
	10					20		~=	200	20	-00	-02	0.4
77	71	65	58	53									
96	89	81	74	67									
115	106	98	89	81									
134	124	114	105	95									
152	142	131	120	110									
171	160	148	136	124									
86	81	76	70	65	60	55							
107	101	95	88	81	75	69							
128	121	114	106	98	91	83							
149	141	133	124	115	106	98							
170	161	151	142	132	122	113							
190	180	170	159	149	138	128							
404	40"			100	96	89	00	1997					
131	125	118	111	103 124	116		83	77 93					
156	149	141	133 155	145	136	108 127	100 118	109					
182	174	188	177	167	156	145	135	126					
232	222	211	200	188	176	164	153	143					
256	246	234	222	209	196	184	171	160					
281	270	257	244	230	216	203	190	177					
305	293	280	266	251	237	222	208	195					
329	317	303	288	273	257	242	227	212					
352	340	325	310	294	277	261	245	230					
400	440	400	4.00	140	100	100	110	110	100	200			
165	159	153	147	140	133 160	126 151	119	112 135	105	120			
197	191 222	184 214	176 205	168 196	186	177	167	158	149	141			
260	252	244	234	224	213	202	192	181	171	162			
291	283	273	263	251	240	228	216	205	194	183			
322	313	303	291	279	267	254	241	228	216	204			
353	343	332	320	307	293	279	266	252	239	226			
383	373	361	348	334	320	305	290	276	261	247			
413	403	390	376	362	346	331	315	299	284	269			
443	432	419	405	389	373	357	340	323	307	291			
473	461	447	432	416	399	382	365	347	330	313			
228	223	217	211	204	196	189	181	173	166	158	151	143	136
264	259	252	245	237	229	220	211	202	194	185	176	168	160
301	295	287	279	270	261	251	241	231	221	212	202	193	184
337	330	322	313	304	293	283	272	261	250	239	228	217	207
373	366	357	347	337	325	314	302	290	278	266	254	242	231
408	400	391	381	369	357	345	332	319	306	293	280	268	255
444	435	425	414	402	389	376	362	348	334	320	306	293	280
478	470	459	447	435	421	407	392	377	362	347	333	318	304
513	504	493	480	467	453	438	422	406	390	375	359	344	329
547	538	526	513	499	484	468	452	435	419	402	385	369 395	353
581	571	559	546	531	515	499	482	464	447	428	412	1 1000	. 910

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula, P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}.$ 

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Size of Angles.	Size of Plate.	Weight of Column.	Area of Column Section.	Least Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.	I	engtl	t.
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	2	4	6
3 x 21/2 x 1/4  a a 8  a a 18  a a 18	10 x 1/4 4 8/8 4 1/2 4 1/2 4 1/2	26.5 33.0 39.2 45.3 51.0 57.1	7.74 9.61 11.43 13.26 15.00 16.75	1.16 1.18 1.21 1.24 1.27 1.30	4.07 4.05 4.03 4.01 3.99 3.96	119 141 164 186 207	92 115 137 155 180 202	87 109 130 151 172 193
3½ x 2½ x ¼ 4 4 58 4 4 18 4 4 18 4 4 18 6 7 18	10 x 1/4 5 16 8/8 4 1/2 4 1/2 4 1/8	28.1 35.0 41.6 48.1 54.6 60.7	8.26 10.25 12.19 14.10 16.00 17.87	1.39 1.42 1.45 1.48 1.51 1.54	4.13 4.11 4.09 4.07 4.05 4.03	102 127 151 175 199 222	100 124 148 171 195 217	96 119 143 165 188 210
4 x 8 x 5 x 5 x 5 x 5 x 5 x 5 x 5 x 5 x 5	12 x 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	41.6 49.3 57.1 64.8 72.6 79.9 87.3 94.6 101.6 108.9	12.11 14.42 16.73 19.00 21.23 23.42 25.61 27.76 29.87 31.94	1.58 1.61 1.64 1.66 1.69 1.72 1.75 1.78 1.81	4.91 4.89 4.87 4.85 4.83 4.81 4.79 4.77 4.74		148 176 204 232 260 287 314 340 360 392	143 171 198 226 253 279 306 332 358 383
5 x 31/2 x 5 5 6 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	14 x 8 18 8 7 18 12 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	49.7 59.5 68.8 78.2 87.6 96.9 105.9 114.9 123.9 132.5 141.4	14.62 17.45 20.25 23.00 25.76 28.43 31.11 33.74 36.38 38.93 41.49	1.98 2.01 2.04 2.07 2.09 2.12 2.15 2.18 2.21 2.24 2.27	5.77 5.75 5.73 5.71 5.69 5.67 5.64 5.62 5.60 5.58 5.56		180 215 249 283 317 351 381 416 419 481 512	176 211 245 278 312 345 377 410 442 473 505
8 x 8½ x % 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	16 x 2/16 / 16 / 16 / 16 / 16 / 16 / 16 / 16	67.2 77.8 88.4 99.0 109.6 119.8 130.4 140.2 150.4 160.2 170.0	19.68 22.88 26.00 29.12 32.20 35.24 38.24 41.24 44.20 47.12 50.00	2.46 2.49 2.52 2.54 2.57 2.60 2.63 2.66 2.69 2.72 2.75	6.68 6.66 6.64 6.61 6.59 6.57 6.55 6.53 6.51 6.48 6.46		244 283 322 360 309 436 474 511 548 584 620	240 279 318 356 394 431 408 505 542 578 613

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

50 000 Based on Gordon's Formula, P = -Safety factor 4.

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. . . . . . . . . . . . .

 $1 + \frac{(12 \text{ L})^2}{36\ 000\ r^2}$ 



#### Length in Feet. . . . .

8	10	12	14	16	18	20	22	24	26	28	30	32	34
81 102 122 142 162 182	75 93 112 131 150 169	68 85 103 120 138 156	61 77 93 109 126 143	55 69 84 99 114 130									
91 114 136 158 180 201	86 107 128 149 170 191	80 100 120 140 160 179	73 92 111 130 149 168	88 85 102 120 138 156	78 94 111 127 144	57 71 86 102 117 133							
137 164 191 217 244 270 295 321 346 371	131 156 182 208 233 258 283 308 333 357	123 148 172 197 221 245 270 294 318 341	115 139 162 185 208 232 255 278 301 324	107 129 151 173 196 218 240 262 285 307	100 120 141 162 183 204 225 246 268 289	92 112 131 151 170 190 210 231 251 272	85 103 121 140 158 177 196 216 235 254	79 95 112 130 147 165 183 201 220 238					
171 205 238 271 304 336 369 400 432 463 494	166 198 231 263 295 327 358 389 420 451 481	159 191 222 253 284 315 346 376 407 437	152 183 213 243 273 303 333 362 392 421 450	145 174 203 232 261 290 319 347 376 404 433	137 165 193 221 248 276 304 332 359 387 415	130 156 183 209 236 262 289 316 343 369 396	122 147 173 198 223 249 274 300 326 351 377	115 139 163 187 211 235 260 284 309 334 359	108 131 153 176 199 222 246 269 293 317 340	102 123 144 166 188 210 232 254 277 300 323			
236 274 312 350 387 424 461 407 533 509 805	231 268 306 343 370 416 452 488 523 550 594	225 261 298 334 370 406 441 477 512 546 581	218 254 289 325 360 395 429 464 498 532 566	211 245 280 314 348 382 416 450 484 517 550	203 236 270 303 336 370 403 436 468 501 534	195 227 259 292 324 356 388 420 452 484 516	187 218 249 280 311 342 374 405 436 467 498	178 208 238 268 398 329 359 389 419 449 479	170 199 228 257 286 315 344 373 402 431 460	162 190 217 245 273 301 329 357 385 414 442	154 181 207 234 261 287 314 342 369 396 423	147 172 197 223 249 274 300 326 853 379 405	140 164 188 212 237 262 287 312 337 362 388

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula, P =  $\frac{50\ 000}{1 + \frac{(12\ \mathrm{L})^2}{36\ 000\ \mathrm{r}^2}}.$ 

1-

Sine of Angles.	Sine of Plate,	Weight of Column.	of Column Section.	Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2,		lengtl n Feet	
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	2	4	6
3 x2½x¼ a a 16 a a 78 a a 78 a a 78 a a 78 a a 78	12 x 1/4	28.2 35.2 41.7 48.3 54.4 61.0	8.24 10.23 12.18 14.13 16.00 17.87	1.12 1.15 1.17 1.20 1.23 1.26	4.87 4.85 4.83 4.81 4.78 4.76	102 126 151 174 198 221	98 122 146 169 192 215	92 115 138 160 183 205
3½ x 2½ x ¼ a a 35 a a 4 a a 15 a 15 a a	12 x 1/4  = 1/8  = 1/8  = 1/2  = 1/6	29.8 37.2 44.1 51.1 58.0 64.6	8.76 10.87 12.94 14.97 17.00 18.99	1.35 1.38 1.41 1.43 1.46 1.49	4.94 4.92 4.90 4.88 4.85 4.83	108 135 160 186 211 236	106 131 157 182 206 231	101 126 151 175 199 223
4 x 8 x 1/2 / 2 / 2 / 2 / 2 / 2 / 2 / 2 / 2 / 2	14 x 16 a 1/2 a a	43.7 51.9 60.0 68.2 76.4 84.1 91.9 99.7 107.1 114.9	12.74 15.17 17.61 20.00 22.36 24.67 26.99 29.26 31.50 33.69	1.54 1.57 1.60 1.62 1.65 1.68 1.71 1.74 1.77	5.72 5.70 5.88 5.66 5.63 5.61 5.59 5.57 5.55 6.53		155 185 215 244 273 302 330 358 386 413	150 179 208 237 265 294 322 349 376 403
5 x 3½ x 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	16 x 15/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1 1/2 0 1/	51.8 62.0 71.8 81.6 91.4 101.2 110.6 120.0 129.4 138.4 147.8	15.24 18.20 21.12 24.00 26.88 29.68 32.48 35.24 38.00 40.68 43.36	1.94 1.97 2.00 2.02 2.05 2.08 2.11 2.14 2.17 2.19 2.22	6.59 6.57 6.54 6.52 6.50 6.48 6.44 6.41 6.39 6.37		187 224 260 295 331 366 400 435 468 502 535	183 219 255 290 325 359 393 427 461 404 527
6 x 3½ x 3	18 x 15 15 15 15 15 15 15 15 15 15 15 15 15	69.8 80.8 91.8 102.8 113.9 124.5 135.5 145.7 156.4 166.6 176.8	20.43 23.76 27.00 30.25 33.45 36.62 39.74 42.87 45.95 49.00 52.00	2.42 2.44 2.47 2.50 2.52 2.55 2.58 2.61 2.64 2.67 2.70	7.49 7.47 7.45 7.42 7.40 7.38 7.36 7.34 7.32 7.29 7.27	1	253 294 334 374 414 453 492 531 569 607 644	249 290 330 369 409 448 486 525 563 600 637

CALCULATED FOR LEAST RADIUS OF GYRA-TION, AXIS 1-1.

50 000 Based on Gordon's Formula, P = -

 $1 + \frac{(12 \text{ L})^2}{36\ 000\ r^2}$ Safety factor 4.



8	10	12	14	16	18	20	22	24	26	28	80	32	34
86	78	71	63	57									
107	98	89	80	72									
128	118	107	97	87									
150	138												
171	158	126	114	103 119									
192	178	164	149	135									
192	140	109	149	199									
96	90	83	77	70	64	58							
120	112	104	96	88	81	74							
143	135	125	116	107	98	89							
167	157	146	136	125	115	105							
190	179	167	156	144	132	122							
213	201	188	175	162	150	138							
		-					-						
144	136	128	120	111	103	95	88	81					
172	163	154	144	134	124	115	106	98					
200	190	180	168	157	146	135	125	116					
228	217	205	193	180	168	156	144	133					
255	244	231	217	203	189	176	163	151					
283	270	256	241	226	211	197	183	170					
310	297	282	266	250	234	218	203	188					
337	323	307	290	273	256	239	223	207					
364	349	332	315	296	278	260	243	226					
390	375	357	339	320	301	282	263	246					
178	172	165	158	150	142	134	126	118	111	104	177		
213	206	198	189	180	170	161	152	143	134	126			
248	240	231	220	210	199	188	178	167	157	148			
282	273	263	252	240	228	216	204	192	181	170			
316	307	295	283	270	257	243	230	217	204	192			
350	340	327	314	300	286	271	256	242	228	215			
384	372	359	345	330	314	298	283	267	252	238		_	
417	405	391	376	360	343	326	309	293	277	261			
450	437	423	407	390	372	354	336	318	301	284			
483	470	454	437	419	401	382	363	344	326	308			
515	501	485	468	449	430	410	390	370	350	332			
					-	TAU			-				
245	239	233	225	217	209	201	192	183	175	166	158	150	143
285	278	271	262	253	244	234	224	214	204	194	185	176	167
324	317	308	299	289	278	267	256	245	234	223	212	202	192
363	355	346	336	325	313	301	288	276	264	251	240	228	217
402	393	383	372	360	347	334	321	307	293	280	267	254	242
440	431	420	408	395	382	367	353	338	323	309	295	281	268
478	469	457	445	431	416	401	385	369	353	338	323	308	293
516	506	494	480	466	450	434	417	400	383	367	350	334	319
554	543	530	516	501	484	467	449	431	414	396	378	362	345
591	580	567	552	535	518	o00	481	463	444	425	407	389	371
628	616	602	587	570	552	533	513	494	474	454	435	416	397
					-			-					

CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula,  $F = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ 



Size of Angles.	Size of Plate	Weight of Column.	Area of Column Section.	Least Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.	Leng	th in	Feet.
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	8	8	10
7 x8½x4; " " † " " † " " † " " † " " † " " † " " †	14 x 76 % 1 76 %	80.8 91.8 103.2 113.7 124.7 135.3 145.9 156.5 166.6 176.8	23.73 27.00 30.24 33.43 36.63 39.74 42.86 45.93 49.01 52.00	3.05 3.08 3.11 3.13 3.17 3.20 3.23 3.26 3.29 3.32	5.92 5.90 5.87 5.85 5.83 5.81 5.79 5.76 5.74 5.72	292 332 372 412 451 490 528 567 604 642	289 329 368 407 446 485 523 501 598 635	285 324 363 402 440 478 516 553 591 627
7 x 3½ x 4;	16 x 10 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	83.8 95.2 107.0 118.0 129.4 140.4 151.4 162.4 173.0 183.6	24.60 28.00 31.36 34.68 38.00 41.24 44.48 47.68 50.88 54.00	3.00 3.02 3.06 3.08 3.11 3.14 3.17 3.20 3.23 3.26	6.75 6.73 6.71 6.69 6.67 6.64 6.62 6.00 6.58 6.56	303 345 386 427 468 508 548 588 627 666	299 340 382 422 463 503 542 582 621 659	294 335 376 416 456 496 535 574 612 651
7 x 8½ x 14	18 x 16	86.8 98.6 110.8 122.3 134.1 145.5 156.9 168.4 179.4 190.4	25.48 29.00 32.49 35.93 39.38 42.74 46.11 49.43 52.76 56.00	2.94 2.97 3.00 3.02 3.05 3.08 3.11 3.14 3.17 3.20	7.58 7.55 7.53 7.51 7.49 7.47 7.44 7.42 7.40 7.38	313 357 400 442 485 526 568 609 656 690	309 352 395 437 479 520 562 602 643 683	305 347 389 430 472 513 554 594 634 674
7 x 3½ x L	20 x 11 1/2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	89.8 102.0 114.7 126.5 138.7 150.6 162.5 174.3 185.8 197.2	26.35 30.00 33.61 37.18 40.75 44.24 47.73 51.18 54.63 58.00	2.89 2.92 2.95 2.97 3.00 3.03 3.06 3.09 3.12 3.15	8.39 8.37 8.34 8.32 8.30 8.28 8.25 8.23 8.21 8.19	324 369 413 457 501 545 588 630 673 715	320 364 409 452 495 538 581 623 665 707	314 358 402 445 488 530 572 614 656 697

### CALCULATED FOR LEAST RADIUS OF GYRATION, AXIS 1-1.

Based on Gordon's Formula, P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ 



			_									1		
12	14	16	18	20	22	24	26	28	80	82	84	36	88	40
279	274	267	260	253	246	238	230	222	214	206	198	191	183	176
318	312	305	297	289	280	271	263	254	245	236	227	218	210	201
357	350	342	333	324	315	305	295	288	276	266	256	246	237	228
395	387	379	369	359	349	339	328	317	306	295	284	274	263	253
433	424	415	405	395	384	372	360	349	337	325	313	302	290	279
470	462	452	441	430	418	406	393	880	368	355	342	330	318	306
508	498	488	477	465	452	439	425	412	398 429	385 415	371 400	358 386	345 372	332 358
545 581	535 571	524 559	512 547	499 534	486 520	472 505	490	475	460	444	429	414	399	385
618	807	595	582	568	553	538	522	506	490	474	458	442	427	412
010	001	080	BOM	000	000	DOG	NAME OF TAXABLE PARTY.	uvu	- ADO		100	***	241	****
289	283	276	269	261	253	245	236	228	220	211	203	195	187	180
329	322	315	307	298	289	280	270	261	251	242	232	223	214	206
369	362	353	344	335	325	314	304	293	283	272	262	252	242	233
409	460	391	381	371	360	349	337	326	314	303	291	280	269	259
448	439	429	419	407	396	383	371	359	346	334	321	309	297	286
487	478	467	456	444	431	418	405	391	378	364	351	338	325	313
526	516	505	493	480	466	452	438	424	409	395	381	367	353	340
564	554	542	529	516	501	487	472	456	441	426	411	396	381	367
603	591	579	566	551	536	521	505	489 521	473	457	441	425	409	394 421
640	629	816	602	587	571	555	538	521	504	487	4/1	202	431	921
299	292	285	277	269	260	252	243	234	255	216	208	199	191	
340	333	325	316	307	297	287	277	267	257	248	238	228	219	
382	374	365	355	345	334	323	312	301	290	279	268	258	247	
423	414	404	393	382	371	359	347	335	322	310	298	287	275	
463	454	443	432	420	407	395	382	368	355	342	329	316	304	
504	494	483	470	457	444	430	416	402	388	374	360	346	333	
544	533	521	508	495	481	466	451	436	420	405	390	376	361	
584	573	560	546	532	517	501	485	469	453	437	421	405	390	
624	612	598	584	569	553	536	520	503	486	469	452	435	419	
663	650	636	622	606	589	572	554	536	518	500	483	465	448	
900	201	001	nor	077	000	aro	249	240	230	221	212	204	195	
308 351	301	294 335	285 326	277 316	268 306	258 295	285	274	264	253	243	233	224	
394	385	376	366	355	344	332	321	309	297	286	274	263	253	
436	427	417	405	394	381	369	356	343	330	318	305	293	281	
479	468	457	445	432	419	408	392	378	364	350	337	323	310	
521	510	498	485	471	457	442	427	412	397	383	368	354	340	
562	551	538	524	510	495	479	463	447	431	415	400	384	369	
603	591	578	563	548	532	515	499	482	465	448	431	415	399	
844	632	618	602	586	569	552	534	516	498	480	463	445	428	
685	672	657	641	624	607	588	570	551	532	513	494	476	458	

CALCULATED FOR RADIUS OF GYRATION, AXIS 2-2.

Based on Gordon's Formula,  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ .

TON!	لما	لم	417

Size of Angles.	Size of Plate.	Weight of Column.	of Column Section.	Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.	i	ength a Feet	ì.
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches	Inches.	4	6	8
3 x 21/2 x 1/4 4 4 8 8 6 8 8 6 4 7 6 7 6 4 7 7 7 8 8 8 8 8 8 8 8 8	6 x 1/4 « 1/8 « 1/8 « 1/6 « 1/2 « 1/2	23.1 28.8 34.1 39.3 44.2 49.5	6.74 8.36 9.93 11.51 13.00 14.50	1.24 1.27 1.30 1.33 1.36 1.39	2.41 2.39 2.37 2.35 2.33 2.31	83 103 123 143 161 179	82 102 121 140 158 176	81 100 119 137 155 173
8½ x 2½ x ¼ a a 16 a a 16 a a 16 a a 16 a a 16	7 x 1/4  a	25.6 31.8 37.7 43.6 49.5 55.0	7.51 9.31 11.07 12.78 14.50 16.18	1.46 1.49 1.52 1.55 1.58 1.61	2.88 2.86 2.84 2.82 2.80 2.78	93 115 137 159 180 200	92 114 136 157 178 198	91 113 134 155 176 196
4 x 3 x 1	8 x 1/8 x 1/8 x 1/8 x 4 x 1/8	37.3 44.2 51.1 58.0 64.9 71.4 77.9 84.4 90.5 97.0	10.86 12.92 14.98 17.00 18.98 20.92 22.86 24.76 26.62 28.44	1.67 1.70 1.73 1.76 1.79 1.82 1.85 1.89 1.92	3.25 3.23 3.21 3.18 3.16 3.14 3.12 3.10 3.08 3.06		134 160 185 210 234 258 282 305 328 350	133 158 183 207 231 255 278 301 324 346
5 x 31/2 x ta a a a a a a a a a a a a a a a a a	10 x = 10	45.4 54.4 62.9 71.4 79.9 88.5 96.6 104.7 112.8 120.6 128.7	13.37 15.95 18.50 21.00 23.51 25.93 28.36 30.74 33.13 35.43 37.74	2.08 2.10 2.13 2.16 2.19 2.22 2.25 2.29 2.32 2.35 2.38	4.10 4.08 4.06 4.04 4.02 4.00 3.98 3.96 3.93 3.91 3.89		166 198 229 260 291 321 351 381 410 439 467	165 196 228 258 289 319 349 378 407 436 464
6 x 3½ x % x x x x x x x x x x x x x x x x x	12 x 3/3 a a a a a a a a a a a a a a a a a a	62.1 71.9 81.6 91.4 101.1 110.5 120.2 129.2 138.5 147.5 156.4	18.18 21.13 24.00 26.87 29.70 32.49 35.24 37.99 40.70 43.37 46.00	2.56 2.59 2.62 2.65 2.68 2.71 2.74 2.77 2.80 2.83 2.85	5.01 4.99 4.97 4.95 4.93 4.91 4.88 4.86 4.81 4.82 4.80			225 261 297 333 367 402 436 470 503 536 569

CALCULATED FOR RADIUS OF GYRATION, AXIS 2-2.

Based on Gordon's Formula, P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}.$ 

10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40
							-							-	
79	77	74 92	72 89	69 85	66 82	78	75	58	55 68	52 64					
98 116	95 113	109	105	101	97	92	88	71 84	80	76				::::	
134	130	126	121	116	111	106	101	96	92	87					
151	147	142	137	131	126	120	114	108	103	98					
169	163	158	152	146	139	133	127	120	114	108					
89	88	86	83	81	79	76	73	71	68	65	63	60	58		
111	109	106	103	100	97	94	91	87	84	81	77	74	71 84		
132 152	129	126 146	123 142	119	115	112	108	104	100	110	106	88 101	97		
172	169	165	160	156	151	145	140	135	129	124	119	114	109		
192	188	183	178	173	167	162	156	150	144	138	132	126	121		
131	129	126	124	121	118	115	111	108	105	101	98	94	91	88	85
156	153	150	147	144	140	136	132	128	124	120	116	112	108	104	100
180	177	174	170	166	162	158	153	148	143	139	134	129	124	120	115
204 228	201	197	193 215	188 210	184	178 199	173 193	168	162 181	157 175	151 168	146 162	141 156	135 150	130 145
252	247	243	237	231	225	219	212	206	199	192	185	178	172	165	159
274	270	264	259	252	245	238	231	224	216	209	201	194	187	179	173
297	292	286	280	273	265	258	250	242	233	225	217	209	201	193	186
319 341	314	307 328	300	293 312	285 304	276 295	268 285	259 276	250 266	241 257	232 248	224	215	207 220	199 211
										-			-		
163 195	161	160 190	157 188	155 185	153 182	150 179	147 175	144	141	138 164	134	131 156	128 152	124 148	121 144
226	223	221	218	214	211	207	203	199	194	190	185	181	176	171	166
256	254	250	247	243	239	235	230	225	220	215	210	205	199	194	189
287	284	280	276	272	267	262	257	251	246	240	234	228	222	216	210
316 346	313	309	305	300	295 322	289 316	283	303	271 296	265 289	258 282	251 274	245 267	238 260	232 252
375	371	366	361	355	349	342	335	328	320	312	305	297	289	281	273
403	399	394	388	382	375	368	360	352	344	336	327	319	310	301	293
432	427	421	415	408	401	393	385	377	368	359	350	340	331	322	313
460	454	449	442	435	427	418	410	400	391	381	371	362	352	342	332
224	222	221	218	216	214	211	208	205	202	199	196	192	189	185	181
260 295	258	256 291	253 288	251 285	248	245 278	242 274	238	234 266	231 262	227 257	223 253	218 248	214 243	210 238
330	328	325	322	319	315	311	307	302	298	293	288	282	277	272	266
365	363	360	356	352	348	344	339	334	329	323	318	312	306	300	294
399	397	393	389	385	381	376	371	365	359	353	347	341	334	327	321
433	430	427	422	418 450	413	408	402	396 426	389 419	383 412	376 405	369 397	362 389	355 382	347
500	496	492	487	482	476	470	463	456	449	441	433	425	417	408	400
533	529	524	519	513	507	500	493	486	478	469	461	452	443	434	425
565	561	556	551	544	538	530	523	515	506	497	488	479	469	460	450
								re tank	-						

CALCULATED FOR RADIUS OF GYRATION, AXIS 2-2.

Based on Gordon's Formula,  $P = \frac{50000}{1 + \frac{(12 \text{ L})^3}{36000 \text{ r}^2}}$ 

	Size of Angles	Size of Plate.	Weight Column.	Column Section.	Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.		Lengtl n Feet	
	Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	4	6	8
8	12½1¼ 100 100 100 100 100 100 100 100 100 100	8 x 1/4 4 5 4 5/8 4 1/8 4 1/2 4 1/3	24.8 30.9 36.6 42.3 47.6 53.3	7.24 8.98 10.68 12.38 14.00 15.62	1.19 1.22 1.25 1.28 1.31 1.34	3.25 3.23 3.21 3.19 3.17 3.15	112 133 154 174 194	89 111 132 152 173 192	58 110 130 151 171 190
31,	2 x 2 ½ x ¼ 4	8 x 1/4  a	26.4 32.9 39.0 45.1 51.2 56.9	7.76 9.62 11.44 13.22 15.00 16.74	1.44 1.47 1.50 1.53 1.56 1.59	3.31 3.28 3.26 3.24 3.22 3.20		98 119 141 163 185 206	95 117 140 161 183 204
4 4 4	X	10 x 18 4 16 4 16 4 18 4 18 4 18 4 18 4 18 4	39.4 46.8 54.1 61.4 68.7 75.7 82.6 89.5 96.0 103.0	11.49 13.67 15.86 18.00 20.11 22.17 24.24 26.26 28.25 30.19	1.62 1.65 1.68 1.71 1.74 1.77 1.80 1.83 1.86 1.90	4.09 4.07 4.04 4.02 4.00 3.98 3.96 3.94 3.92 3.90		142 170 197 223 249 275 300 325 350 374	141 169 195 222 247 273 298 323 347 371
<b>8 8 8 8 8 8 8</b>	X X 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	12 x 5 15 8 4 15 8 4 15 8 4 15 8 4 15 8 4 15 8 4 15 8 4 15 8 4 15 8 4 15 8 4 15 8 15 8	47.6 56.9 65.9 74.8 83.8 92.7 101.3 109.8 118.4 126.5 135.1	13.99 16.70 19.37 22.00 24.63 27.18 29.73 32.24 34.75 37.18 39.61	2.03 2.06 2.08 2.11 2.14 2.17 2.20 2.23 2.26 2.29 2.33	4.95 4.92 4.90 4.83 4.86 4.84 4.82 4.80 4.78 4.76			173 206 239 272 304 336 368 369 420 400
8	X X X 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	14 x x x x x x x x x x x x x x x x x x x	64.7 74.8 85.0 95.2 105.3 115.1 125.3 134.7 144.5 153.8 163.2	18.93 22.01 25.00 28.00 30.95 33.87 36.74 39.62 42.45 45.25 48.00	2.51 2.54 2.57 2.59 2.62 2.65 2.68 2.71 2.74 2.77 2.81	5.85 5.83 5.81 5.79 5.77 5.74 5.72 5.70 5.68 5.66 5.64			

CALCULATED FOR RADIUS OF GYRATION, AXIS 2-2.

Based on Gordon's Formula, P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ 

10	12	14	16	18	20	22	24	26	28	80	32	34	36	88	40
87	86	84	83	81	79	77	74	72	70	68	65	63	81	59	56
108	106	104	102	100	97	95	92	89	86	83	81	78	75	72	70
129	127	124	122	119	116	112	109	106	102	99	96	92	89	86	82
149	146	143	140	137	133	130	126 142	122 138	118 133	114	110 124	106 120	102	99	95 107
168	166 184	162 181	159 177	155 173	151 168	147 163	158	153	148	143	138	133	128	123	119
	-						,							-	61
93	92	90	89	87	85 105	100	80	78 95	75 93	73	70	68 84	81	78	75
116 138	114	112	110	108 127	124	102	118	114	110	107	103	100	96	93	89
159	157	154	151	147	144	140	136	132	127	123	119	115	111	107	103
181	178	174	171	167	162	158	153	149	144	139	134	130	125	120	116
201	198	194	190	186	181	176	171	165	160	155	149	144	139	134	129
140	139	137	135	133	131	129	126	124	121	118	115	112	110	107	104
167	165	163	161	159	156	153	150	147	144	141	137	134	130	127	123
194	192	189	187	184	181	177	174	170	166	162	159	155	151	147	143 161
220	217	215	212	208	205	201	197	193	189	184	180	175	170	166 185	180
245 271	243 268	240 264	236 261	233 256	252	224	242	215 237	210 232	205 226	220	195 215	200	203	198
295	292	289	284	280	275	270	264	258	253	246	240	234	228	222	215
320	316	312	308	303	298	292	286	280	273	266	260	253	246	239	232
344	340	336	331	326	320	314	307	300	293	286	279	271	264	257	249
368	364	359	354	348	342	335	328	320	313	305	297	289	282	274	266
172	171	169	168	166	164	162	160	157	155	152	150	147	144	141	139
205	204	202	200	198	196	193	191	188	185	182	178	175	172	168	165 191
238	236	234	232	230 261	227 258	224 254	221 251	218	214 243	210 239	207	203	199 226	195	217
270 303	300	266 298	264	292	288	284	280	276	272	267	262	257	252	247	242
334	332	329	326	322	318	314	309	305	300	295	289	284	278	273	267
365	363	359	356	352	348	343	338	333	327	322	316	310	304	298	291
396	393	390	386	382	377	372	366	361	355	349	342	336	329	322	315
427	423	420	415	411	406	400	394	388	382	375	368	361	354	346	339
457	453 483	449	445	440	434	428 456	422	415	434	401 427	394	386	278 402	394	385
486	1	478	474	1	462	1					1			1	1
234 272	233 270	231	230 267	228 265	226 263	224	222	219 255	217 252	214 249	211 245	209	206	203	199
309	307	305	303	301	298	296	293	289	288	282	279	275	271	267	263
346	344	342	340	337	334	331	327	324	320	316	312	307	303	298	294
382	380	378	375	372	369	365	362	358	353	349	344	340	335	330	324
418	416	413	411	407	404	400	396	391	387	382	377	371	366	360	355
454	451	449	445	442	438	434	429	424	419	414	408	403	397	391	384
489	487	483	480	476	472	467	462	457	452	446	440	433	427	420	414
524 559	521	518	514	510	505	500	495	490 521	484	477 508	501	464		450	443
593	556 589	552 586	548	544	539	566	528 559	553	546						
983	1 009	, 900	1 001	. 011	. 011	. 000	. 000	. 000	. 040	1000	. 002	021	, 010	1000	. 000

CALCULATED FOR RADIUS OF GYRATION, AXIS 2-2.

Based on Gordon's Formula,  $P = \frac{50.000}{1 + \frac{(12 \text{ L})^3}{36.000 \text{ r}^2}}$ 

1

Size of Angles.	Size of Plate.	Weight of Column.	Column Section.	Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.		engtl	
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	6	8	10
3 x 21/2 x 1/4  a a 8  a a 10  a a 12  a a 12  a a 12  a a 12	10 x 1/4 4 5 6 3/8 4 1/3 4 1/2 4 1/3	26.5 33.0 39.2 45.3 51.0 57.1	7.74 9.61 11.43 13.26 15.00 16.75	1.16 1.18 1.21 1.24 1.27 1.30	4.07 4.05 4.03 4.01 3.99 3.96	96 119 142 164 186 207	95 118 141 163 185 206	95 117 140 161 183 204
31/2 x 21/2 x 1/4 a a 35 a a 3/8 a a 17 a a 1/2 a a 1/2	10 x 1/4	28.1 35.0 41.6 48.1 54.6 60.7	8.26 10.25 12.19 14.10 16.00 17.87	1.39 1.42 1.45 1.48 1.51 1.54	4.13 4.11 4.09 4.07 4.05 4.03	102 127 151 175 198 221	102 126 150 174 197 220	101 125 149 172 195 218
4 x 8 x 16	12 x 16 4 16 4 16 4 16 4 16 4 16 4 16 4 16	41.6 49.3 57.1 64.8 72.6 79.9 87.3 94.6 101.6 108.9	12.11 14.42 16.73 19.00 21.23 23.42 25.61 27.76 29.87 31.94	1.58 1.61 1.64 1.66 1.69 1.72 1.75 1.78 1.81	4.91 4.89 4.87 4.85 4.83 4.81 4.79 4.77 4.74		150 179 207 235 262 290 317 343 869 395	149 178 206 234 261 288 315 341 367 392
5 x 8½ x to 10 x 10	14 x 5 16 8 17 18 18 18 18 18 18 18 18 18 18 18 18 18	49.7 59.5 68.8 78.2 87.6 90.9 105.9 114.9 123.9 132.5 141.4	14.62 17.45 20.25 23.00 25.76 28.43 31.11 33.74 36.38 38.93 41.49	1.98 2.01 2.04 2.07 2.09 2.12 2.15 2.18 2.21 2.24 2.27	5.77 5.75 5.73 5.71 5.69 5.67 5.64 5.62 5.60 5.58 5.56			190 215 250 284 318 351 384 417 449 481 512
6 x 8½ x % 1	16 x x x x x x x x x x x x x x x x x x x	67.2 77.8 88.4 99.0 109.6 119.8 130.4 140.2 150.4 160.2	19.68 22.88 26.00 29.12 32.20 35.24 38.24 41.24 44.20 47.12 50.00	2.46 2.49 2.52 2.54 2.57 2.60 2.63 2.66 2.69 2.72 2.75	6.63 6.64 6.61 6.59 6.57 6.55 6.53 6.51 6.48			

CALCULATED FOR RADIUS OF GYRATION, AXIS 2-2.

Based on Gordon's Formula,  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ 

2301

-							_							
12	14	16	18	20	22	24	26	28	30	32	34	36	38	40
94	92	91	90	88	87	- 85	83	81	80	78	76	74	72	70
116	115	113	111	109	107	105	103	101	98	96	94	91	89	86
138	136	135	132	130	128	125	123	120	117	114	111	108	105	103
160	158	156	153	150	148	145	142	138	135	132	128	125	122	118
181	179	176	173	170	167	164	160	157	153	149	145	141	138	134
202	199	196	193	190	186	183	179	174	170	168	162	157	153	149
100	99	97	96	94	93	91	89	87	85	83	81	79	77	78
124	122	121	119	117	115	113	110	108	106	103	101	98	95	93
147	146	144	141	139	137	134	131	128	125	122	119	116		
170	168	166	164	161	158	155	152	148	145	141	138		113	110
			185				172					134	131	127
193	191 213	188 210	207	182 203	179	175 195		168	164	160	156	152	148	144
216	1		-	-	199		191	187	183	178	174	169	165	160
148	147	145	144	142	140	138	136	134	132	129	127	125	122	120
176	175	173	171	169	167	165	162	160	157	154	151	148	145	142
204	202	200	198	196	193	191	188	185	182	178	175	172	168	165
232	230	228	225	222	219	216	213	210	206	202	198	195	191	187
259	257	254	251	248	245	242	238	234	230	226	221	217	213	208
286	283	281	277	274	270	266	262	258	254	249	244	239	234	229
312	310	306	303	299	295	291	286	282	277	272	266	261	256	250
338	335	332	328	324	320	315	310	305	299	294	288	282	277	271
364	361	357	353	348	344	339	333	328	322	316	310	303	297	291
389	386	382	277	373	367	362	356	350	344	337	331	324	317	310
180	178	177	176	174	173	171	169	167	165	163	160	158	156	153
214	213	211	210	208	206	204	202	199	197	194	191	188	186	185
249	247	245	243	241	239	236	234	231	228	225	222	218	215	212
283	281	279	277	274	271	269	265	262	259	255	252	248	244	240
316	314	312	309	307	304	300	297	293	290	286	281	277	273	268
349	347	345	342	339	335	332	328	324	320	315	311	306	301	296
382	380	377	374	370	367	363	358	354	349	345	340	334	329	324
414	412	409	405	402	398	393	389	384	379	373	368	362	357	351
446	443	440	436	432	428	423	418	413	408	402	396	390	384	378
478	475	471	467	463	458	453	448	442	436	430	424	417	411	404
509	506	502	498	493	488	483	477	471	465	458	451	444	437	430
243	242	241	239	238	236	234	232	230	228	225	223	221	218	215
282	281	279	278	276	274	272	269	267	264	262	259	256	253	250
321	319	318	316	314	311	309	306	303	300	297	294	291	287	284
359	357	356	353	351	348	346	343	340	336	333	329	325	321	317
397	395	393	391	388	385	382	379	375	272	368	364	359	355	351
435	433	430	428	425	421	418	414	411	406	402	398	393	388	384
472	470	467	464	461	457	454	450	446	441	436	432	427		
509	506	503	500	497	493	489	485	480	475				421	416
545	542									470	465	459	454	448
		539	536	532	528	524	519	514	509	504	498	492	486	480
581	578	575	571	567	563	558	553	548	542	537	531	524	518	511
617	613	610	606	602	597	592	587	581	575	569	563	556	549	542

CALCULATED FOR RADIUS OF GYRATION, AXIS 2-2.

Based on Gordon's Formula, P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}.$ 

093	1	
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Size of Angles.	Size of Plate.	Weight of Column.	of Column Section,	Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.	i	Length n Feet	i.
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	6	8	10
3 x 2 ½ x ½ a a is a is a a is a i	12 x 1/4  # 1/6  # 1/6  # 1/2  # 1/6	28.2 35.2 41.7 48.3 54.4 61.0	8.24 10.23 12.18 14.13 16.00 17.87	1.12 1.15 1.17 1.20 1.23 1.26	4.87 4.85 4.83 4.81 4.78 4.76	103 127 151 175 199 222	102 126 151 174 198 221	101 126 150 173 197 219
3½ x 2½ x ½ « « ½ « « ½ « « ½ « « ½ « « ½ « « ½	12 x 1/4  a 1/6  a 5/8  a 1/6  a 1/2  a 1/6	29.8 37.2 44.1 51.1 58.0 64.6	8.76 10.87 12.94 14.97 17.00 18.99	1.35 1.38 1.41 1.43 1.46 1.49	4.94 4.92 4.90 4.88 4.85 4.83		108 134 160 185 210 235	108 134 159 184 200 233
4 : 3 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x	14 x x x x x x x x x x x x x x x x x x x	43.7 51.9 60.0 68.2 76.4 84.1 91.9 99.7 107.1 114.9	12.74 15.17 17.61 20.00 22.36 24.67 26.99 29.26 31.50 33.69	1.54 1.57 1.60 1.62 1.65 1.68 1.71 1.74 1.77	5.72 5.70 5.68 5.66 5.63 5.61 5.59 5.57 5.55 5.53		158 188 218 248 277 306 335 363 390 418	157 188 217 247 276 305 333 361 389 416
5 x 81/2 x 1/2 x 1	16 x 16 8 4 16 8 4 16 8 4 16 8 4 16 8 4 16 8 4 16 8 4 16 8 4 16 8 4 16 8 4 16 8 4 16 8 16 8	51.8 62.0 71.8 81.6 91.4 101.2 110.6 120.0 129.4 138.4 147.8	15.24 18.20 21.12 24.00 26.88 29.68 32.48 35.24 38.00 40.68 43.36	1.94 1.97 2.00 2.02 2.05 2.08 2.11 2.14 2.17 2.19 2.22	6.59 6.57 6.54 6.52 6.50 6.48 6.46 6.44 6.41 6.39 6.37			189 225 261 297 333 368 402 436 470 504 537
6 x 3½ x 1/2 x 1/2 x 4 x 4 x 4 x 4 x 4 x 4 x 4 x 4 x 4 x	18 x 3,7 0 1 1 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2	69.8 80.8 91.8 102.8 113.9 124.5 135.5 145.7 156.4 166.6 176.8	20.43 23.76 27.00 30.25 33.45 36.62 39.74 42.87 45.95 49.00 52.00	2.42 2.44 2.47 2.50 2.52 2.55 2.58 2.61 2.64 2.67 2.70	7.49 7.47 7.45 7.42 7.40 7.38 7.36 7.34 7.32 7.29 7.27			

CALCULATED FOR RADIUS OF GYRATION, AXIS 2-2.

Based on Gordon's Formula, P = 
$$\frac{50\,000}{1 + \frac{(12\,\mathrm{L})^2}{36\,000\,\mathrm{r}^2}}.$$



			-		-	-	~	00	-	-		~	00	0.0	140
12	14	1 1	В	18	20	22	24	26	28	80	32	34	36	38	40
10			99	98	97	95	94	93	91	90	88	86	85	83	81
12			23	121	120	118	116	115	113	111	109	107	105	103	101
14			46	144	143	141	139	137	134	132	130	127	125	122	120
17			68	167	165	163	160	158	155	153	150	147	144	141	138
19			91	189	187	184	182	179	176	173	170	166	163	160	156
21	8 21	6   2	14	211	209	206	203	199	196	193	189	185	182	178	174
10	7 10	8 1	05	104	103	101	100	98	97	95	94	92	90	88	87
13			30	129	127	126	124	122	120	118	116	114	112	110	107
15			55	153	152	150	148	145	143	141	138	136	133	130	128
18		1 1	80	178	175	173	171	168	165	163	160	157	154	151	148
20			04	201	199	196	194	191	188	184	181	178	174	171	167
23			27	225	222	219	216	213	209	206	202	198	194	190	186
**	6 15	0 1	54	150	152	150	149	147	145	143	142	140	137	135	133
15 18			84	153 183	181	179	177	175	173	171	169	166	184	161	159
21			13	212	210	208	205	203	201	198	195	193	190	187	184
24			42	240	238	236	233	231	228	225	222	218	215	212	208
27			71	269	266	263	261	258	254	251	248	244	240	236	233
30			99	296	294	291	288	284	281	277	273	269	265	261	257
33			27	324	321	318	314	311	307	303	298	294	289	285	280
35			54	351	348	344	340	336	332	328	323	318	313	308	303
38			81	378	374	370	366	362	357	352	347	342	337	331	326
41			107	404	400	396	392	387	382	377	371	366	360	354	348
18	_	7 1	86	185	184	182	181	179	178	176	174	172	170	168	166
22			222	221	219	218	216	214	212	210	208	205	203	201	198
26			258	256	254	252	250	248	246	243	241	238	235	233	230
29			293	291	289	287	285	282	279	277	274	271	267	264	261
33			328	326	324	321	318	316	313	309	306	303	299	295	292
36			362	360	357	355	352	349	345	342	338	334	330	326	322
40		9 3	396	394	391	388	385	381	378	374	370	365	361	357	352
43	5 43	2 4	130	427	424	421	417	414	410	405	401	396	392	387	382
46			163	460	457	453	450	445	441	437	432	427	422	416	411
50			196	493	489	486	481	477	472	467	462	457	451	446	440
53	4 53	2 5	529	525	521	517	513	508	503	498	492	487	481	475	468
25	3 25	2 2	251	250	248	247	245	244	242	240	238	236	234	232	229
29			291	290	288	287	285	283	281	279	276	274	272	269	266
33			331	330	328	326	324	322	319	317	314	312	309	306	303
37	4 37	3 3	371	369	367	365	363	360	358	355	352	349	346	342	339
41			110	408	408	404	401	398	395	392	389	385	382	378	374
45			149	447	445	442	439	436	433	429	426	422	418	414	410
49			188	485	483	480	477	473	470	466	462	458	453	449	444
53			526	523	520	517	514	510	506	502	498	493	489	484	479
56			563	561	558	554	551	547	542	538	533	529	524	518	513
60			301	598	595	591	587	583	578	574	569	563	558 592	552 586	547 580
64	3   64	EI ! (	638	634	631	627	623	618	614	1 1003	003	989	1 392	986	980

CALCULATED FOR RADIUS OF GYRATION, AXIS 2-2.

Based on Gordon's Formula,  $P = \frac{50\ 000}{1 + \frac{(12\ L)^3}{36\ 000\ r}}$ 

50 000 1+(12 L)<sup>a</sup>/36 000 r<sup>a</sup>

Size of Angles.	Size of Plate.	Weight of Column.	Area of Column Section.	Least Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2–2.	Len in F	
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	10	12
7 x 3½ x 16 1/2 1/2 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4	14 x 10 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	90.8 91.8 103.2 113.7 124.7 135.3 145.9	23.73 27.00 30.24 33.43 36.63 39.74 42.86	3.05 3.08 3.11 3.13 3.17 3.20 3.23	5.92 5.90 5.87 5.85 5.83 5.81 5.79	293 334 374 413 452 491 529	292 332 372 411 450 489 527
" " " "	" 1	156.5 166.6 176.8	45.93 49.01 52.00	3.26 3.29 3.32 3.00	5.76 5.74 5.72 6.75	567 605 642	564 602 639
7 x 33/2 x 15 x 1	16 x 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	95.2 107.0 118.0 129.4 140.4 151.4 162.4 173.0 183.6	24.00 28.00 31.36 34.68 38.00 41.24 44.48 47.68 50.88 54.00	3.00 3.02 3.06 8.08 3.11 3.14 3.17 3.20 3.23 3.26	6.73 6.71 6.69 6.67 6.64 6.62 6.60 6.58 6.56		346 387 428 469 509 549 588 627 666
7 x 31/2 x 1/2 x 1	18 x 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	96.8 98.6 110.8 122.3 134.1 145.5 156.9 168.4 179.4 190.4	25.48 29.00 32.49 35.93 39.38 42.74 46.11 49.43 52.76 56.00	2.94 2.97 3.00 3.02 3.06 3.08 3.11 3.14 3.17 3.20	7.58 7.55 7.53 7.51 7.49 7.47 7.44 7.42 7.40 7.38		315 359 402 445 487 529 570 612 652 693
7 x 8 1/2 x	20 x 10 20 x 1	89.8 102.0 114.7 126.5 138.7 150.6 162.5 174.3 185.8 197.2	26.35 30.00 33.61 37.18 40.75 44.24 47.73 51.18 54.63 58.00	2.89 2.92 2.95 2.97 3.00 3.03 2.06 3.09 3.12 3.15	8.39 8.37 8.34 8.32 8.30 8.28 8.25 8.23 8.21 8.19		

CALCULATED FOR RADIUS OF GYRATION, AXIS 2-2.

Based on Gordon's Formula,  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ 

14	16	18	20	22	24	26	28	80	82	84	36	88	40
290	288	286	284	281	278	275	272	269	266	262	258	255	251
330	328	325	323	320	317	313	310	306	302	298	294	289	285
370 409	367 406	364 403	361	358 396	354 392	351 387	347 383	342 378	338	333	329 363	324 358	319 352
447	444	441	437	433	429	424	419	414	408	403	397	391	385
486	482	478	474	470	465	460	455	449	443	437	431	424	418
523	520	516	511	506	501	496	490	484	477	471	464	457	450
561	557	553	548	543	537	531	525	518	511	504	497	489	482
598	594	589	584	578	572	566	559	552	545	537	529	521	513
635	630	625	620	614	607	600	593	586	578	570	561	553	544
302	301	299	297	295	293	290	288	285	282	279	276	273	270
344	342	340	338	336	333	330	327	324	321	318	314	310	307
385 426	383	381	379	376	373	370	366	363	359	355	352	347	343
426	424	421	419	416	412	409	405	401	397	393	389	384	379
467	464	461	458	455	451	448	443	439	435	430	425	420	415
507 546	504 543	501 540	498 536	494 532	490 528	486 524	481 519	477 514	472 500	467 503	461 497	456 491	450 485
586	582	579	575	571	566	561	556	551	545	539	533	520	520
624	621	617	613	609	604	598	593	587	581	574	568	561	554
663	659	655	651	646	641	635	629	623	616	609	602	595	588
314	313	312	310	308	306	304	302	300	297	295	292	290	287
358	356	354	353	351	348	346	344	341	338	335	332	329	326
401	399	397	395	393	390	388	385	382	379	376	372	369	365
443	441	439	437	434	432	429	426	422	419	415	411	408	403
485 527	483 525	481 522	478 519	476 516	473 513	469 510	466 506	462 502	450 498	455 498	450 489	446 484	442 479
568	566	563	560	557	553	550	546	541	537	532	527	522	517
609	607	604	601	597	593	589	585	580	575	570	565	559	554
650	647	644	641	637	633	628	624	619	613	608	602	596	590
690	687	684	680	676	672	667	662	657	651	645	639	633	626
326	325	324	322	321	319	317	315	313	311	309	307	305	302
371	370	368	367	365	363	361	359	357	354	352	349	346	344
415	414	412	411	409	407	404	402	399	397	394	391	388	385
460 503	458 502	456 500	454 498	452 495	450 493	447 490	445	442 484	439	436	432 473	429 470	426
547	545	543	541	538	535	532	529	526	522	518	514	510	466 506
590	588	585	583	580	577	574	570	567	563	559	554	550	545
633	630	628	625	622	619	615	612	608	603	599	594	590	585
675	672	670	667	664	660	656	652	648	644	639	634	629	623
717	714	711	708	705	701	697	693	688	683	678	673	667	662

### SAFE LOADS IN THOUSANDS OF POUNDS FOR LATTICED CHANNEL COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1+\frac{(12\ L)^2}{36\ 000\ r^2}}.$  Safety factor 4.



Depth of Channel.	Weight of each Channel.	Area of Column Section.	Radius of Gyration.	Length in Feet.						
Inches.	Lbs. per Foot.	Sq. Ins.	Inches.	4	6	8	10	12	14	
6	8.0	4.76	2.34	59	58	57	55	54	52	
66	10.5	6.18 7.64	2.21 2.13	76 94	75 93	73 90	71 88	85	67 81	
66	15.5	9.12	2.06	112	110	107	104	100	96	
7.	9.75	5.70	2.72	71	70	.69	08	66	65	
44	12.25	7.20 8.68	2.59 2.50	89	88	87 104	85 102	83	81 96	
66	17.25	10.14	2.44	107 125	106	121	119	116	112	
66	19.75	11.62	2.39	144	142	139	136	132	128	
8	11.25	6.70	3.11	83	83	82	80	79	77	
66	13.75	8.08 9.56	2.99	100	99	98 116	97	95 112	93 109	
66	18.75	11.02	2.82	137	135	134	131	128	125	
44	21.25	12.50	2.77	155	153	151	149	145	142	
9	13.25	7.78	3.45		96	95	94	93	91	
66	15.00 20.00	8.82 11.76	3.37 3.20		109	108 143	107 142	105 139	103	
, 44	25.00	14.70	3.08		145 181	179	177	173	170	
10	15.0	8.92	3.84	-	110	110	109	107	100	
66	20.0	11.76	3.66		146	144	143	141	139	
23	25.0 30.0	14.70 17.64	3.52 3.41		182 218	180 216	178	176 210	173	
66	35.0	20.58	3.31		254	251	248	245	240	
12	20.5	12.06	4.61			149	148	147	140	
66	25.0	14.70	4.43			181	180	179	177	
66	30.0 35.0	17.64 20.58	4.28			217 254	216 251	214 249	211	
66	40.0	23.52	4.09			289	287	284	281	
15	33.0	19.80	5.59			246	244	243	241	
- 64	35.0 40.0	20.58 23.52	5.56			255 291	254 290	252 288	251 286	
66	45.0	26.48	5.44 5.32			328	326	324	322	
66	50.0	29.42	5.23			364	363	360	357	
66	55.0	32.36	5.16			400	399	396	393	

For detail dimensions see page 230

### SAFE LOADS IN THOUSANDS OF POUNDS FOR LATTICED CHANNEL COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\,000}{1 + \frac{(12\,\mathrm{L})^2}{36\,000\,\mathrm{r}^3}}$ . Safety factor 4.



Depth of Channels.	Weight of each Channel.	Length in Feet.							
Inches.	Lbs. per Foot.	80	28	26	24	22	20	18	16
8	8.0				42	44	46	48	50
66	10.5			,	52	55	58	.61	64
**	13.0				63	67	71	74	78
	15.5				74	78	83	88	92
7.	9.75			52	54	56	58	61	63
	12.25			64	67	70	73	76	78
re-	14.75			76	79	83	86	90	93
44	17.25			87	92	96	100	104	108
	19.75			98	104	108	113	119	123
8	11.25	61	63	65	68	70	72	74	76
	13.75	72	75	78	80	83	86	58	90
44	16.25	83	87	90	94	97	100	104	107
44	18.75	95	99	103	107	111	115	118	122
	21.25	106	111	115	120	124	129	134	138
9	13.25	75	77	80	82	84	86	88	90
66	15.00	84	87	90	92	94	97	99	101
66	20.00	109	113	116	120	124	127	131	134
	25.00	134	139	143	149	153	157	162	166
10	15.0	90	93	95	97	99	101	102	104
66	20.0	116	119	122	125	128	131	134	136
	25.0	143	146	151	155	159	163	166	170
	30.0 35.0	168	174	179	185	189	194	198	203
	30.0	194	201	207	213	219	225	230	236
12	20.5	129	131	134	136	138	140	142	144
. 44	25.0	155	159	161	165	167	170	172	175
66	30.0	184	187	192	198	200	203	206	209
66	35.0 40.0	213 243	218 248	223 253	227 258	231 263	236 268	240 273	243 277
	20.0	240	240	200	200	200	208	210	211
15	33.0	222	225	228	230	233	235	238	240
66	35.0	230	234	236	240	242	245	247	249
	40.0	262	266	269	273	276	279	282	284
66	45.0 50.0	294 325	298 329	302 334	306	310	313 348	316 352	319 354
61	55.0	357	362	368	372	377	381	386	390

For detail dimensions see page 230

### SAFE LOADS IN THOUSANDS OF POUNDS FOR LATTICED CHANNEL COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^4}}$ . Safety factor 4.

Depth of Channels.	Weight of each Channel,	Area of Column Section.	Least Radius of Gyration.	Length in Peet.				
Inches.	Lbs. per Foot.	Sq. Ins.	Inches.	82	34	36	88	40
9	13.25 15.00 20.00 25.00	7.78 8.82 11.76 14.70	3.45 3.37 3.20 3.08	73 81 106 129	71 79 101 124			
10 "	15.0 20.0 25.0 30.0 35.0	8.92 11.76 14.70 17.64 20.58	3.84 3.66 3.52 3.41 3.31	87 113 138 163 188	85 109 134 158 183	83 106 130 153 176		
12 "	20.5 25.0 30.0 35.0 40.0	12.06 14.70 17.64 20.58 23.52	4.61 4.43 4.28 4.17 4.09	127 152 180 208 236	124 149 176 203 231	121 146 172 199 224	119 142 167 193 218	116 139 164 188 212
15	33.0 35.0 40.0 45.0 50.0 55.0	19.80 20.58 23.52 26.48 29.42 32.36	5.59 5.56 5.44 5.32 5.23 5.16	219 228 258 289 320 351	215 224 254 284 315 344	213 220 250 279 309 338	209 217 246 275 303 332	206 213 241 270 299 325

For detail dimensions see page 230.

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR LATTICED CHANNEL COLUMNS. SQUARE ENDS.

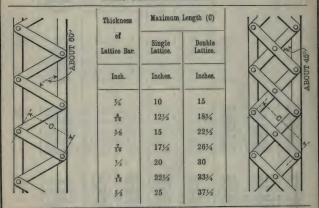
Based on Gordon's Formula P =  $\frac{50~000}{1+\frac{(12~L)^2}{36~000~r^2}}\cdot~~ \text{Safety factor 4.}$ 

42   44   46	48	Length in Feet.											
		50	52	54	Lbs. per Foot.	Inches.							
113 111 10: 135 132 12: 159 155 15: 183 178 17: 206 200 19: 202 199 19: 210 206 20: 238 233 22: 265 260 25: 293 287 28: 319 314 30:	192 199 199 224 250 275	188 194 220 245 269 294	184 191 215 239 264 287	181 187 211 234 258 281	13.25 15.00 20.00 25.00 15.0 20.0 25.0 30.0 35.0 20.5 25.0 30.0 35.0 40.0 45.0 50.0 55.0	9 "" "" "" "" "" "" "" "" "" "" "" "" ""							

# SIZE OF SINGLE LATTICE BARS TO BE USED WITH LATTICED CHANNEL COLUMNS.

Depth of Ohannels.		ns of Lattice ars.	Weight of Lattice Bars	Center of Hole to End of Bar.	Distance Center to Center of Rivets. (d)		
	w	Thickness.	per Foot.	(a)	Maximum.	Minimum.	
Inches.	ches. Inches. Inch.		Pounds.	Inch.	Inches.	Inches.	
6 7 8 9 10 12 15	13/4 2 2 21/4 21/4 21/4 21/4	1/4 1/4 1/6 1/6 1/6 3/8 3/8 1/6	1.49 1.70 2.12 2.39 2.87 2.87 3.72	11/6 11/4 11/4 11/4 11/4 11/4 11/4	10 10 12½ 12½ 15 15	65/8 75/8 81/8 91/2 101/8 13 15/8	

### MAXIMUM LENGTHS OF LATTICE BARS BETWEEN FLANGE RIVET CENTERS FOR DIFFERENT BAR THICKNESSES.



Latticing should be so proportioned to resist a shearing stress, 2% of direct stress.

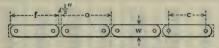
Inclination of lattice bars to axis of member should not be less than 45 degrees. Where distance between lines of flange rivets exceeds 15 inches, if single rivet bars be used, lattice should be double.

Pitch of lattice rivets along flange divided by least radius of gyration of the member between connections should be less than corresponding ratio of the member as a whole.

# SIZE OF STAY PLATES TO BE USED WITH LATTICED CHANNEL COLUMNS.

Mini Plates	imum size of at Ends of Co	Stay lumns.	Weight of Minimum	Diameter	0 0
ъ	Thickness.		Stay Plate.	Rivets.	0 -b0 l
Inches.	Inch.	Inches.	Pounds.	Inch.	0
71/2	1/4	53/4	3.06	5/8	TOK TOK
7½ 8½ 958 1038 11½	1/4	63/4	4.07 5.12	5/8, 3/4 5/8, 3/4	
10% 11½ 135%	1/4	8½ 9¼ 11¼	6.07 7.54 10.86	5/8, 3/4 5/8, 3/4	
161/4	5 16	131/4	19.07	3/4, 7/8	

# DISTANCES TO BE ADDED TO LENGTHS OF LATTICE BARS BETWEEN FLANGE RIVET CENTERS TO GIVE FULL LENGTHS.



	+	Add to Length c										
Width	1	or Finishe	d Length 1	1	For Ordered Length o.							
Bar.		Rivet D	iameter.		Rivet Di	iameter.						
w	1/2	5 8	3 4	7 8	1/2	5 8	3/4	7 8				
Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.	Ins.				
1½ 1¾ 1¾ 1 2¼ 2½ 2½ 2¾ 3	2	2½ 2½ 2½ 2½	2½ 2½ 3 3 3½	3 3 3 1/2	21/2	23/4 3 3	3 3 3½ 3½ 4	3½ 3½ 3½ 4				

Length of end stay plates should be not less than distance between lines of flange rivets.

Length of intermediate stay plates should be not less than one-half same distance.

Thickness of stay plates should be not less than 1/50 same distance.

## SAFE LOADS IN THOUSANDS OF POUNDS FOR 6" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}} \cdot \text{ Safety factor 4.}$ 



## SERIES A.

Weight of each Channel.	Thickness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.	:	Length	in Feet	in Feet.		
Lbs, per Foot.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	4	6	8	10		
8	1/4 # 1/2 #	29.6 33.0	8.76 9.76	2.35 2.35	108 121	107 119	105	102		
66	100	36.4	10.76	2.34	133	131	129	125		
44	70	39.8	11.76	2.34	145	143	141	137		
66	1/2	43.2	12.76	2.34	158	155	152	149		
44	16	46.6	13.76	2.34	170	167	164	160		
••	5/8	50.0	14.76	2.33	182	180	176	172		
10.5	1/4	34.6	10.18	2.27	126	124	121	118		
	1/4 16 2/8 17 2/2 16 1/8	38.0	11.18	2.27	138	136	133	130		
44	8/2	41.4	12.18	2.28	150	148	145	141		
44	7	44.8	13.18	2.28	163	160	157	153		
44	1/2	48.2	14.18	2.28	175	173	169	165		
66	10	51.6	15.18	2.28	187	185	181	176		
••	%	55.0	16.18	2.28	200	197	193	188		
13	1/4	39.6	11.64	2.20	144	141	138	135		
	14 th 1/2	43.0	12.64	2.21	156	154	150	146		
44	8/8	46.4	13.64	2.22	168	166	162	158		
44	16	49.8	14.64	2.23	181	178	174	169		
66	1/2	53.2	15.64	2.23	193	190	186	181		
46	75	56.6	16.64	2.24	205	202	198	192		
	1 %	60.0	17.64	2.24	218	214	210	204		
15.5	1/4	44.6	13.12	2.14	162	159	155	151		
	7	48.0	14.12	2.15	174	171	167	162		
66	3/8	51.4	15.12	2.16	186	183	179	174		
44	16	54.8	16.12	2.17	199	195	191	186		
44	1/2	58.2	17.12	2.18	211	207	203	197		
44	1/4 1/4 1/5 1/5 1/2 1/5 1/8	61.6	18.12	2.19	224	220	215	209		
	1 %	65.0	19.12	2.19	236	232	227	220		

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 6" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES A.

	-	a min		-	- 1	1	Thickness	Weight
		Len	gth in I	Peet,			of	of each
							Plates.	Channel.
12	14	16	18	20	22	24	Inch.	Lbs. per Foot.
99 111 122 133 144 156 166	96 107 118 128 139 150 161	92 103 114 124 135 145 155	89 99 109 119 129 139 149	85 95 104 114 124 133 142	81 90 99 109 118 127 136	77 86 94 103 112 121 130	1/4 1/5 1/5 1/2 1/6 1/6	8 " " " " " " " " " " " " " " " " " " "
114 126 137 148 159 171 182	110 121 133 143 154 165 176	106 117 127 138 148 159 169	102 112 122 132 142 152 162	97 107 116 126 135 144 154	92 102 111 120 130 139 148	88 96 106 114 123 132 140	1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4	10.5
130 141 153 164 175 186 197	125 136 147 158 169 179 190	120 131 141 152 162 173 183	115 125 135 145 155 166 176	109 119 129 138 148 158 167	104 113 122 131 140 150 159	99 107 116 125 133 143 151	1/4 + 1 = 1/2 + 1/2 + 1 = 1/2 + 1/	13
146 157 170 180 191 202 213	140 151 162 172 184 195 205	134 145 155 165 176 187 197	128 138 148 158 168 178 188	122 131 140 150 160 170 180	115 125 133 143 152 162 171	109 118 127 135 144 153 161	1/4 1/5 1/5 1/2 1/5 1/6 1/6	15.5

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



### SERIES A.

Weight of each Channel.	Thickness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.	Length in Fee			•
Lbs. per Foot.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	4	6	8	10
9.75	1/4 50 8 71 6 1/2 1 1/2 1/2 1	34.8 38.6 42.5 46.3 50.1 53.9 57.8	10.20 11.32 12.45 13.58 14.70 15.82 16.95	2.63 2.63 2.62 2.62 2.62 2.62 2.62 2.62	126 140 154 168 182 196 210	125 139 152 166 180 194 207	123 137 150 163 177 190 204	121 134 147 160 174 187 200
12.25	1/4 5e 5/8 7e 1/2 1/2 1/8	39.8 43.6 47.5 51.3 55.1 58.9 62.8	11.70 12.82 13.95 15.08 16.20 17.32 18.45	2.55 2.56 2.56 2.56 2.57 2.57 2.57	145 159 173 187 200 214 228	143 157 171 185 198 212 226	141 154 168 182 195 208 222	138 151 164 178 191 204 217
14.75	1/4 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6	44.8 48.6 52.5 56.3 60.1 63.9 67.8	13.18 14.30 15.43 16.56 17.68 18.80 19.93	2.49 2.50 2.50 2.51 2.52 2.52 2.52 2.53	163 177 191 205 219 233 247	161 175 189 202 216 230 244	158 172 185 199 212 226 239	155 168 181 195 208 221 234
17.25	1/4 10 % 10 % 10 % 10 % 10 % 10 % 10 % 10	49.8 53.6 57.5 61.3 65.1 68.9 72.8	14.64 15.76 16.89 18.02 19.14 20.26 21.39	2.42 2.43 2.45 2.46 2.46 2.47 2.48	181 195 209 223 237 251 265	178 192 206 220 234 248 261	175 189 202 216 229 243 257	171 185 198 211 224 238 251
19.75	1/4 15 % 15 % 15 %	54.8 58.6 62.5 66.3 70.1 73.9 77.8	16.12 17.24 18.37 19.50 20.62 21.74 22.87	2.37 2.38 2.40 2.41 2.42 2.43 2.44	199 213 227 241 255 269 283	197 210 224 238 251 265 279	193 206 220 234 247 260 274	188 201 214 228 242 255 268

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES A.

			Thickness of Plates.	Weight of each Channel.					
12	14	16	18	20	22	24	26	Inch.	Lbs.per Ft.
118 130 143 156 169 182 105	115 127 140 153 165 178 190	111 123 135 148 160 172 184	108 119 131 143 154 166 178	104 115 126 138 149 161 172	99 110 121 132 143 154 165	96 106 116 127 137 148 158	92 102 112 122 132 142 152	1/4	9.75
134 147 160 173 186 199 212	130 143 156 168 181 194 207	126 139 151 163 176 188 200	122 134 146 158 169 181 193	118 129 140 152 163 174 185	113 124 135 145 156 167 178	108 118 129 139 150 161 171	103 113 123 133 144 154 164	14 15 18 15 15 15 15 15 15 15 15 15 15 15 15 15	12.25
151 164 177 190 202 215 229	146 159 171 184 196 209 222	142 154 166 178 191 203 215	136 148 160 171 184 196 207	131 142 154 165 177 188 199	126 136 147 158 170 180 191	120 131 141 151 162 173 183	115 125 135 144 155 165 175	1/4 8/8 1/2 1/2 1/2 8/8	14.75
166 180 193 206 218 231 245	161 174 187 199 212 224 238	156 168 181 193 205 217 229	150 162 174 186 197 209 220	143 155 166 178 190 201 212	137 148 159 171 182 192 203	131 142 153 163 173 184 194	126 135 146 155 165 176 186	1/4 1/8 1/8 1/2 1/2 1/8 1/2 1/8	17.25
183 196 209 222 234 248 261	177 189 202 215 227 240 253	170 183 195 208 220 231 243	164 175 187 199 211 223 235	157 168 180 191 202 214 225	150 161 172 183 194 204 216	143 153 164 174 185 195 207	136 146 157 166 177 186 196	1/4 a 1 8 1 8 1 8 1 8 1 8 1 8 1 8 2 8 8 8 8 8	19.75

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^4}}$ . Safety factor 4.



#### SERIES A.

Weight of each Channel.	Thickness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.	Length in Fee				
Lbs. per Foot.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	4	8	8	10	12
11.25	1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4	39.5 43.7 48.0 52.3 56.5 60.8 65.0	11.70 12.95 14.20 15.45 16.70 17.95 19.20	2.98 2.97 2.97 2.96 2.95 2.95 2.95	145 161 176 192 207 223 238	144 159 175 190 205 221 236	142 157 172 188 203 219 233	140 155 170 185 200 214 229	137 152 167 181 196 210 225
18.75	1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4	44.5 48.7 53.0 57.3 61.5 65.8 70.0	13.08 14.33 15.58 16.83 18.08 19.33 20.58	2.92 2.92 2.92 2.91 2.91 2.91 2.91	162 178 193 209 224 240 255	161 176 191 207 222 237 253	159 174 189 204 220 235 250	156 171 186 201 216 231 246	153 168 182 197 212 226 241
16.95	1/4 1/4 1/4 1/4 1/4 1/4 1/4	49.5 53.7 58.0 62.3 66.5 70.8 75.0	14.56 15.81 17.06 18.31 19.56 20.81 22.06	2.86 2.87 2.87 2.87 2.87 2.87 2.87 2.87	181 196 212 227 243 258 274	179 194 210 225 240 256 271	176 192 207 222 237 252 267	173 188 203 218 233 248 263	170 185 199 214 228 243 258
18.75	1/4 1/4 1/4 1/4 1/4 1/4 1/4	54.5 58.7 63.0 67.3 71.5 75.8 80.0	16.02 17.27 18.52 19.77 21.02 22.27 23.52	2.81 2.81 2.82 2.82 2.83 2.83 2.83	199 214 230 245 261 276 292	197 212 227 243 258 274 280	194 209 224 240 255 270 285	190 205 221 236 250 265 280	186 201 216 230 245 260 275
21.25	1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4	59.5 63.7 68.0 72.3 76.5 80.8 85.0	17.50 18.75 20.00 21.25 22.50 23.75 25.00	2.76 2.77 2.77 2.78 2.79 2.79 2.80	217 233 248 264 279 295 310	215 230 245 261 276 291 307	212 227 242 257 272 287 302	208 223 238 253 267 282 297	204 218 233 247 262 276 291

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES A.

				Thickness of Plates.	Weight of each Channel.					
14	16	18	20	22	24	26	28	80	Inch.	Lbs. per Foot.
134 149 163	131 145 159	128 141 154	124 137 150	120 133 146	116 128 141	112 124 136	108 120 131	104 115 126	3/4	11.25
177 192 206	173 187 201	168 182 195	163 176 189	158 170 183	153 165 178	147 159 171	142 153 165	137 147 158	14 15 15 15 15 15 15 15 15 15 15 15 15 15	44 44
221	215	209	203	196	190	183	177	169		44
150 164 178 193 207 221 236	146 160 174 188 202 216 229	142 155 169 182 196 209 223	138 151 164 177 190 203 216	133 146 159 171 184 106 209	129 141 153 166 178 190 203	124 136 148 160 172 183 195	119 131 142 153 164 176 187	115 126 137 148 159 170 181	14 14 14 14 14 14 14 14 14 14 14 14 14 1	13.75
186 180 195 209 223 237 252	162 176 189 203 217 231 245	157 171 184 198 211 224 238	152 165 178 191 204 217 231	147 180 172 185 198 210 223	142 154 166 178 191 203 215	137 148 160 172 184 195 207	131 143 154 165 177 188 199	126 137 148 159 170 181 191	1/4 1/5 1/5 1/5 1/5 1/5 1/5 1/5 1/5 1/5 1/5	16.25
182 106 210 225 240 254 268	177 191 205 219 233 246 260	172 185 199 212 226 239 253	167 180 193 206 219 232 245	161 174 186 199 211 224 236	155 167 180 192 204 216 228	149 160 173 185 196 208 220	143 154 166 178 189 200 211	137 148 160 171 181 192 203	1/4 1/5 8/8 1/5 1/5 1/5 1/6 1/6 1/8	18.75
198 212 226 241 256 270 284	193 207 220 234 249 263 277	187 200 214 227 241 254 268	181 194 207 220 233 246 260	174 187 200 213 225 238 250	168 180 192 205 217 229 241	162 173 185 196 209 221 232	155 166 178 189 201 212 223	148 159 170 181 192 202 214	1/4 yes 1/8 yes 1/2 yes 1/2 yes 8/8	21.25

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 9" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P = 
$$\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$$
. Safety factor 4.



### SERIES A.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.		NI III	Length in Fe				
Lbs. per Ft.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	в	8	10	12	14	16
18,25	1/4 5 16 8/8 7 16 1/2 18 5/8	45.2 49.9 54.6 59.2 63.9 68.5 73.3	13.28 14.66 16.03 17.40 18.78 20.16 21.53	3.34 3.32 3.31 3.30 3.29 3.28 3.28	164 181 198 215 232 249 266	162 179 196 213 229 246 263	160 177 193 210 227 243 260	158 174 191 207 223 239 255	155 171 187 203 219 235 251	152 168 183 199 214 230 246
15	1/4 5 16 8/8 7 16 1/2 9 16 5/8	48.7 53.4 58.1 62.7 67.4 72.0 76.8	14.32 15.70 17.07 18.44 19.82 21.20 22.57	3.29 3.28 3.28 3.27 3.26 3.26 3.25	177 194 211 228 245 262 279	175 192 209 225 242 259 275	173 189 206 222 239 255 272	170 186 202 219 235 251 267	167 183 199 215 231 247 263	163 179 195 210 226 242 257
80 	1/4 5 16 8/8 7 17 1/2 9 16 5/8	58.7 63.4 68.1 72.7 77.4 82.0 86.8	17.26 18.64 20.01 21.38 22.76 24.14 25.51	3.19 3.19 3.19 3.19 3.19 3.19 3.19	213 230 247 263 280 297 314	210 227 244 261 278 294 311	208 224 241 257 274 291 307	204 220 236 253 269 285 301	200 216 232 248 264 280 296	196 212 227 243 259 274 290
25 26 26 26 46	1/4 5 16 8/8 7 16 1/2 9 16 5/8	68.7 73.4 78.1 82.7 87.4 92.0 96.8	20.20 21.58 22.95 24.32 25.70 27.08 28.45	3.10 3.11 3.11 3.12 3.12 3.12 3.12	249 260 283 300 317 334 351	246 263 279 296 313 330 346	243 259 276 292 309 325 342	238 254 270 287 304 320 336	234 250 265 281 297 313 329	228 244 260 275 291 307 322

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 9" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P = 
$$\frac{50\,000}{1+\frac{(12\,\mathrm{L})^2}{36\,000\,\mathrm{r}^2}}$$
. Safety factor 4.



#### SERIES A.

200	Length in Feet.								Thickness of Plates.	Weight of each Channel.
18	20	22	24	26	28	80	32	34	Inch.	Lbs. per Foot.
149 164 179 194 209 225 240	145 160 175 189 204 219 234	141 156 171 184 199 214 228	137 152 165 179 194 208 222	134 147 160 174 188 202 215	129 143 155 169 182 195 209	125 138 150 163 176 189 202	121 134 146 158 171 182 194	117 129 141 153 165 176 188	1/4 16 8/8 16 1/2 1/2 1/8	13.25
160 175 190 206 221 236 252	156 171 186 201 216 231 245	152 166 181 195 210 225 238	148 162 176 190 203 217 231	143 157 171 184 197 211 225	139 152 166 178 191 204 218	134 147 160 172 185 198 211	130 142 154 167 179 191 204	126 137 149 161 173 185 196	1/4 818 8/8 718 1/2 98 8/8	15 - 65 - 65 - 66 - 66
192 207 222 237 253 268 282	186 201 216 231 246 260 275	181 196 210 224 239 253 268	176 190 204 218 232 246 260	170 184 197 211 224 238 251	165 178 191 204 217 230 243	159 172 185 197 210 223 236	154 166 179 191 203 216 226	148 160 172 183 195 207 219	1/4 #10 3/8 10 10 10 10 10 10 10 10 10 10 10 10 10	20 " " " "
223 238 253 268 283 298 313	216 232 246 261 276 291 306	210 224 239 253 267 282 296	204 218 232 246 260 274 287	197 210 224 238 252 265 279	191 204 217 230 243 256 269	183 197 210 222 235 247 260	177 189 201 213 226 238 250	170 183 194 206 218 229 241	1/4 1/5 1/5 1/5 1/5 1/5 1/5 1/5 1/5 1/5 1/5	25

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES A.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.	adius of Length in Feet.						
Lbs. per Ft.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	6	8	10	12	14	18	
15	1/4	50.4	14.92	3.62	184	183	181	179	178	173	
66	14 to 16 to	55.5 60.6	16.42 17.92	3.61 3.59	203 221	201 220	199 217	197 215	193 211	191 207	
44	78	65.7	19.42	3.58	240	238	235	232	229	225	
46	1/2	70.8	20.92	3.58	259	257	254	250	247	242	
66	र्ड	75.9	22.42	3.57	277	275	272	268 286	264 282	259 277	
	9/8	81.0	23.92	3.56	296	293	290	200	204	211	
30	1/4	60.4	17.76	3.52	219	217	215	212	209	205	
66	1/4 to 1/2 to 1/8	65.5	19.26 20.76	3.52 3.51	238 257	236 254	233 252	230	226 244	223 239	
66	28	70.6 75.7	22.26	3.51	275	272	270	266	262	257	
44	1%	80.8	23.76	3.51	294	291	288	284	270	274	
66	26	85.9	25.26	3.50	312	309	805	302	297	291	
**	9/8	91.0	26.76	3.50	331	328	324	320	314	308	
25	3/4	70.4	20.70	3.42	255	253	250	247	242	238	
66	16	75.5	22.20	3.43	274	272	268	265	260	255	
66	1/8	80.6 85.7	23.70 25.20	3.43 3.43	293 311	290 308	287 305	282 200	278 295	272 289	
66	12	90.8	26.70	3.43	330	327	323	318	313	307	
66	14 16/8	95.9	28.20	3.44	348	345	341	336	330	324	
44	5/8	101.0	29.70	3.44	367	364	359	355	848	341	
80	1/4	80.4	23.64	3.33	292	289	285	281	276	271	
11	16	85.5	25.14	3.34	310	307	303	299	294	288	
66	3/8	90.6 95.7	26.64 28.14	3.35	329 347	325 344	321 340	317 334	311 329	305	
44	1/4 15/8 15/8 15/2 15/8	100.8	29.64	3.36	366	362	358	352	346	339	
44	12	105.9	31.14	3.37	384	380	376	370	364	358	
66	1 5/8	111.0	32.64	3.37	403	399	394	388	381	375	
85	1/4	90.4	26.58	3.26	328	324	320	315	309	303	
	16	95.5	28.08	3.27	347	343	338	333	327	320	
66	1/4 to 1/2 to 1/	100.6	29.58	3.28	365	361	357	351 369	344 362	337 354	
66	12	105.7	31.08 32.58	3.29 3.29	384 402	380 398	375 393	387	362	372	
24	3	115.9	34.08	3.30	421	416	411	405	398	390	
n	1 3/8	121.0	35.58	3.31	439	435	429	423	415	407	

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}.$  Safety factor 4.



#### SERIES A.

				Thick- ness of Plates.	Weight of each Channel						
18	20	22	24	26	28	80	82	34	36	Inch.	Lbs.per Ft.
170 187 204 221 238 255 271	166 183 199 216 232 249 266	162 179 195 211 228 243 259	159 175 190 206 222 238 253	154 170 186 200 216 231 246	151 165 180 195 210 225 239	146 161 175 189 204 219 233	142 156 170 184 199 212 226	138 152 165 178 192 206 218	134 147 160 172 186 199 212	14 th 15 th	15
201 218 235 252 269 286 303	196 213 230 246 263 279 296	192 208 224 240 256 272 289	187 203 219 235 251 265 281	182 197 213 228 244 259 274	177 192 207 222 236 251 268	172 187 201 216 230 244 258	167 181 195 209 223 237 251	161 175 189 202 216 229 243	157 170 182 195 200 222 235	14 th 15 th 16 th	20
233 250 267 284 301 318 335	228 245 261 278 294 311 327	222 238 255 271 287 303 319	216 232 248 263 279 295 310	210 225 241 256 271 286 302	204 219 233 248 263 279 294	198 213 227 242 256 271 285	191 206 220 234 248 262 276	186 199 213 226 240 253 267	180 193 206 219 232 245 258	14	25
265 281 298 315 332 350 357	258 275 291 307 324 342 358	252 268 284 301 317 333 349	245 260 276 293 308 324 339	238 253 268 284 299 315 330	230 245 260 276 290 305 320	223 237 252 267 281 296 310	216 230 243 258 272 286 300	209 222 237 250 263 276 290	201 214 228 241 254 267 280	14 th 14 th 16 16 16 16 16 16 16 16 16 16 16 16 16	80
298 313 330 347 363 380 398	289 306 322 838 854 371 389	282 298 313 329 345 361 379	273 289 305 320 336 351 367	265 279 296 311 326 341 356	256 271 287 301 316 330 345	248 262 278 292 306 320 334	240 254 267 282 296 310 323	232 245 258 273 286 299 312	224 237 249 263 276 289 301	1/4 +te 1/2 +t	35

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1+\frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES A.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration	Radius of Length in Feet.  Gyration							
Lbs.per Ft.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	8	10	12	14	16	18	20	22
20.5	1/4	64.8	19.06	4.41	235	233	232	229	227	223	220	21
66	16	70.8	20.81	4.38	257	255	253	250	247	244	240	234
66	%8	76.7 82.7	22.56	4.36 4.34	278 300	276 298	273 295	271 292	267 288	264 285	260	25
66	16	88.6	24.31 26.06	4.34	321	319	316	313	309	304	280 300	29
44	22	94.6	27.81	4.30	343	340	337	333	330	325	319	31
66	1/4 5 16 8/8 7 16 1/2 9 16 5/8	100.5	29.56	4.28	364	362	358	354	350	345	339	33
25	1/4	73.8	21.70	4.35	268	266	263	261	257	254	250	24
46	16	79.8	23.45	4.32	289	287	284	282	278	274	270	26
46	3/8	85.7	25.20	4.31	311	308	305	303	299	294	290	28
44	16	91.7 97.6	26.95 28.70	4.29	332 354	330 351	327 348	323 344	319	315	310 330	30 32
66	72	103.6	30.45	4.26	375	373	369	365	360	356	350	34
44	1/4 5 18 8/8 7 16 1/2 9 16/8	109.5	32.20	4.25	397	393	390	386	381	376	370	36
ao	1/4	83.8	24.64	4.27	304	302	299	295	292	288	283	27
86	16	89.8	26.39	4.26	325	323	320	316	312	308	303	29
66	8/8	95.7	28.14	4.25	347	344	341	337	333	329	323	31
86	16	101.7 107.6	29.89 31.64	4.23 4.22	368 390	365 387	362 383	358 379	353 374	348 368	343 363	35
66	72	113.6	33.39	4.21	411	408	404	400	395	389	382	37
66	1/4 5 16 3/8 7 16 1/2 9 16/8	119.5	35.14	4.21	433	429	425	421	415	409	402	39
85	1/4	93.8	27.58	4.19	340	337	334	330	326	321	316	31
66	16	99.8	29.33	4.18	361	358	355	351	347	341	336	33
46	3/8	105.7	31.08	4.18	383	380	376	372	367	362	356	36
66	18	111.7 117.6	32.83 34.58	4.17 4.16	405	401	397 418	392 413	409	382 402	376	38
66	2	123.6	36.33	4.16	448	444	439	434	429	423	416	40
66	1/4 5 16 8/8 7 18 1/2 16 5/8	129.5	38.08	4.15	469	465	461	455	449	443	436	42
40	3/4	103.8	30.52	4.13	376	373	369	365	360	354	349	34
44	1/4 5 8 8 1 6 1/22 1 6 5/8	109.8	32.27	4.12	398	394	390	386	380	374	368	36
66	1 1/8	115.7	34.02	4.12	419	416	411	406	401	395	388	38
66	16	121.7 127.6	35.77 37.52	4.12 4.11	441	437 458	433 454	427	421	415	408 428	40
66	72	133.6	39.27	4.11	484	480	475	448	463	456	448	44
66	5/8	139.5	41.02	4.11	505	501	496	490	483	476	468	45

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50~000}{1 + \frac{(12~\mathrm{L})^2}{36~000~\mathrm{r}^2}} \cdot \text{ Safety factor 4.}$ 



## SERIES A.

IV.			1	iengt	th in	Fee	t.				Thick- ness of Plates.	Weight of each Channel.
24	26	28	80	32	34	86	38	40	42	44	Inch.	Lbs. per Ft.
213 232 252 271 289 309 328	209 228 246 266 285 304 322	206 223 242 260 279 297 316	201 220 237 255 274 291 309	196 214 232 249 267 285 502	193 209 227 244 261 278 296	188 205 221 238 255 271 288	184 200 216 232 249 265 281	179 195 211 227 242 258 274	175 190 206 223 237 251 267	170 186 200 216 230 245 259	1/4 10 8/8 116 2/3 16 2/3 16 8/8	20.5
242 260 280 299 319 338 358	237 256 275 293 312 331 350	233 251 269 288 306 324 343	228 246 263 282 300 318 335	223 240 258 275 293 311 329	218 235 252 270 286 303 320	213 230 246 263 280 295 312	208 224 241 256 272 289 306	203 218 234 250 265 281 297	197 213 229 243 259 273 280	193 207 222 237 252 267 281	1/4 1/5 1/5 1/5 1/5 1/5 1/5 1/5 1/5 1/5 1/5	25
274 293 313 331 350 369 389	268 287 306 325 343 362 381	262 281 300 318 337 354 372	257 276 293 311 329 347 365	251 269 287 304 321 339 357	245 263 280 297 313 331 348	240 256 273 290 307 322 339	234 250 267 282 299 315 332	228 244 260 275 291 307 323	223 237 253 268 282 298 314	216 232 246 261 276 290 305	1/4 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6	80 " " "
305 324 344 362 381 400 420	299 318 337 356 375 394 411	292 311 329 348 366 385 404	286 304 322 340 358 376 394	280 296 314 332 349 367 385	273 290 308 323 341 358 375	266 283 300 317 332 349 365	259 275 292 308 325 341 356	253 268 284 300 316 332 348	246 262 277 291 307 323 338	239 254 270 283 298 313 328	1/4 5- 6- 8/8 17- 1/2 2- 16- 5/8	85 " "
336 356 375 394 413 433 452	329 348 367 386 405 424 442	322 340 359 377 396 412 433	314 333 351 369 387 405 423	308 324 342 360 377 395 412	301 316 333 351 368 385 402	293 310 326 343 358 375 391	285 301 318 334 350 367 383	277 293 309 325 341 357 373	269 285 300 316 331 347 362	262 277 292 307 322 337 352	1/4 \$ 15 \$ 8 15 15 16 16 18	40 " " "

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



# SERIES A.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.		Loust Radius of Gyration.			L	engt	h in	Fee	t.	-	
Lbs.per Ft.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	12	14	16	18	20	22	24	26	28
88	3/8	109.4	32.55	5 41	399	396	393	390	386	381	378	373	367
66	16	116.6	34.68	5.38	425	422	418	415	411	406	401	397	391
66	% Te /2 % He /4	123.8 131.0	36.80 38.92	5.36 5.33	451	448	444	440	436	431 456	428 450	420	415
66	8%	138.2	41.05	5.31	502	500	495	490	485	481	475	468	461
66	11	145.4	43.18	5.29	529	526	521	516	510	504	499	492	485
66	3/4	152.7	45.30	5.24	555	550	545	541	535	529	522	515	509
85	3/8	113.4	33.33	5.40	409	406	402	399	395	390	387	381	376
64	16	120.6	35.46	5.37	435	432	428	424	420	415	410	406	400
65	72	127.8 135.0	37.58 39.70	5.35 5.32	461	457	453	449	445 469	440	435	429 453	424
66	8/8 1/2 16/8 16/8 16/4	142.2	41.83	5.30	512	509	505	500	494	488	484	477	470
66	11	149.4	43.96	5.28	538	534	530	525	520	513	508	501	494
66		156.7	46.08	5.27	564	560	556	551	545	538	531	525	518
40	8/8 11/2 15/8 16/4	123.4	36.27	5.35	445	441	438	433	430	425	419	414	409
66	15	130.6 137.8	38.40	5.33 5.31	470	467	463	459	454 479	450	444	438	432
66	72	145.0	40.52 42.64	5.29	498 522	493 519	514	509	504	498	403	462 486	455
44	5/8	152.2	44.77	5.27	548	544	540	535	529	523	516	511	503
66	116	159.4	46.90	5.26	574	570	566	560	554	548	540	535	527
		166.7	49.02	5.24	600	595	590	586	579	572	565	557	551
45	8/8 1-1-2 1-5/8 1-5/8 1-5/8 1-5/8 1-5/8	133.4	39.23	5.31	480	477	473	469	464	459	454	447	441
66	12	140.6 147.8	41.36 43.48	5.29 5.27	508 532	503 528	499 525	494 519	489 514	483 508	478 501	472	485
44	32	155.0	45.60	5.25	558	554	550	545	539	532	525	518	512
66	8/8	162.2	47.73	5.24	584	580	575	570	564	557	550	542	536
66	11	169.4	49.86	5.23	610	606	600	596	589	582	575	567	558
		176.7	51.98	5.21	636	631	626	619	614	607	599	591	582
50	9/8	143.4 150.6	42.17	5.26 5.24	516 542	512 538	509 583	504 529	498 524	492 517	486	481 503	474
44	16	157.8	46.42	5.24	568	564	559	555	549	542	511 535	528	520
66	10	165.0	48.54	5.21	594	590	584	578	574	567	559	552	543
66	8/8	172.2	50.67	5.20	620	615	610	604	599	592	584	576	567
66	3/8 16/2 15/8 15/8 16/8 16/8 16/8 16/8 16/8 16/8 16/8 16	179.4 186.7	52.80 54.92	5.19 5.18	672	641 667	636	654	622 647	616	633	600	591 615
55	3/8	153.4	45.11	5.21	552	548	543	538	533	527	520	513	505
55	10	160.6	47.24	5.19	578	574	560	563	557	552	544	537	520
66	15/22	167.8	49.36	5.18	604	600	594	588	582	576	569	561	553
66	16	175.0	51.48	5.17	630	625	620	613	607	599	593	585	576
66	11	182.2 189.4	53.61 55.74	5.16 5.15	682	651 677	671	639	632 657	624	616	633	800 824
66	3/4	196.7	57.86	5.14	708	703	696	689	682	673	665	655	648

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $\mathbf{P} = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES A.

				Thick- ness of Plates.	Weight of each Channel.								
30	32	34	36	88	40	42	44	46	48	50	52	Inch.	Lbs.per Pt.
363	357	351	345	340	334	327	322	316	309	304	297	3/8	88
385 409	381	374 397	368	361	356 376	349 370	342 362	335 355	329 347	322 342	315	% t 1/2 t 1/	66
432	425	418	411	405	397	389	381	375	367	359	351	22	66
450	449	441	433	425	419	411	402	394	388	379	371	8/8	66
478 501	472	484	456 476	447	488	432	423	414	405	397	390	11	66
370	366	360	353	467 348	342	451 335	442	432	423	416	407		
394	387	383	376	369	364	357	330 349	323 342	316	310	304	% it // 1 // 1 // 1 // 1 // 1 // 1 // 1 /	85
417	411	404	398	391	383	376	370	362	355	349	341	1/2	66
441	434	426	419	413	405	397	389	383	375	367	359	18	66
463	478	472	441	433 455	427 446	418	410	401	393 413	386 404	378 397	28	44
510	501	493	486	477	468	459	452	442	433	423	414	17	66
403	396	390	384	377	370	363	357	350	342	337	329		40
427	420	412	405	399	392	384	376	370	368	355	347	% 15/2 15/2 15/3 14/3 14/3 14/3 14/3 14/3 14/3 14/3 14	
450 472	443	435 458	427 450	420 441	413	405	397 418	389	383	374	366	3/2	- 66
495	487	479	472	464	455	446	439	430	420	411	402	1	44
519	510	502	495	486	476	467	457	450	440	431	421	11	66
542	533	524	515	505	498	488	478	468	458	450	440		- 68
436 458	429 452	421	414	406	400	392	384	376	370	362	354	% to 1/2 to 1/2 to 1/4 1/4	45
481	473	465	459	428 450	420 441	414	405	397 417	388 408	380	390	18	66
504	496	488	479	472	463	454	445	435	428	419	409	72	66
528	519	510	501	492	485	475	465	456	446	438	420	8/8	66
552 573	542 568	533 556	523 546	514 536	506 525	490 515	486 507	476	465	455 475	448	#	46
466	459	451	445	437	428	420	411	405	396	387	379		50
490	482	474	465	456	450	441	432	423	414	407	398	78	80
513	505	496	487	478	471	462	453	443	433	424	417	1/2	- 44
535	528	519	510	500	490	481	473	463	458	443	433	34	- 44
558 582	549 572	542 562	532 554	522 544	512 533	502 523	491 512	484 501	473 493	463 482	452 471	11	44
605	595	585	574	566	555	544	533	521	510	499	490	% 15 1/2 15 % 14 8/4	66
497	491	482	474	465	456	447	440	431	421	412	403		55
520	512	503	496	487	477	468	458	448	441	431	422	% T 1/2 T 1/8 H 1/4	11
544 567	535 558	525 548	516 538	509 528	499 520	489 510	479	469	458	448	441	1/2	- 66
591	581	571	560	550	539	531	520	509	498	487	476	8/8	44
614	604	593	582	572	560	549	541	529	518	506	495	11	66
638	627	616	605	593	582	570	558	549	537	525	514	3/4	64

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 6" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P = 
$$\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^4}}$$
 Safety factor 4.



#### SERIES B.

Weight of each Channel.	Thickness of Plates.	Weight of Column.	of Column Section.	Least Radius of Gyration.		Leng	Feet.		
Lbs. per Poot.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	4	6	8	10	12
8 64 64 64 64 64	1/4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	31.3 35.1 39.0 42.8 46.6 50.4 54.3	9.26 10.39 11.51 12.64 13.76 14.89 16.01	2.74 2.73 2.71 2.70 2.70 2.69 2.68	115 129 142 156 170 184 198	114 127 141 155 169 183 196	112 126 139 153 166 180 193	110 123 136 150 163 176 190	107 121 134 147 160 172 185
10.5	1/4 #16 */8 #16 */2 */6 */8	36.3 40.1 44.0 47.8 51.6 55.4 59.3	10.68 11.81 12.93 14.06 15.18 16.31 17.43	2.68 2.67 2.66 2.66 2.65 2.65 2.65	132 146 160 174 188 202 216	131 145 158 172 186 200 213	129 142 156 170 183 197 210	126 140 153 166 179 193 206	123 137 150 163 176 189 202
18	1/4 5/8 16 2/8 16 2/2 16 5/8	41.3 45.1 49.0 52.8 56.6 60.4 64.3	12.14 13.27 14.39 15.52 16.64 17.77 18.89	2.54 2.62 2.62 2.62 2.61 2.61 2.61	150 164 178 192 206 220 234	148 162 176 190 204 218 231	146 160 173 187 900 214 227	143 157 170 183 197 210 223	139 153 164 179 192 205 218
15.5	1/4 -1e -1e -1e -1e -1e -1e -1e -1e -1e -1e	46.3 50.1 54.0 57.8 61.6 65.4 09.3	13.62 14.75 15.87 17.00 18.12 19.25 20.37	2.47 2.54 2.57 2.57 2.57 2.57 2.57	169 183 196 210 224 238 252	166 180 194 208 222 236 249	164 178 191 205 218 232 245	160 174 187 200 214 227 240	155 169 182 195 208 221 234

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 6" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}} \cdot \quad \text{Safety factor 4.}$ 



#### SERIES B.

			11	Thickness of Plates.	Weight of each Channel.				
14	16	18	20	22	24	26	28	Inch.	Lbs.per Ft.
105 118 130 143 155 168 181	102 114 126 139 151 163 175	99 111 123 134 146 158 170	95 107 118 130 141 153 163	103 114 125 136 147 158	88 109 120 131 141 151	85 95 105 115 126 135 145	82 91 101 110 120 130 140	1/4 110 9/8 11/2 11/2 10/8	8 66 66 66 66
120 133 145 158 171 183 196	116 129 141 154 166 178 190	113 125 136 148 160 172 184	108 121 132 143 155 166 178	105 116 127 138 149 160 171	100 111 122 133 143 153 164	96 107 117 127 137 147 157	92 102 112 122 131 141 151	1/4 1/4 1/6 8/8 1/6 1/2 1/6 5/8	10.5
135 149 162 174 186 199 211	131 144 157 169 181 193 206	126 139 151 163 175 187 198	121 135 146 158 168 180 191	116 129 134 151 162 173 184	112 124 134 145 155 166 176	107 119 129 139 149 159 169	102 114 123 133 143 152 162	1/4 1/6 1/6 1/6 1/2 1/8	18
151 164 178 190 203 215 228	146 159 172 184 196 209 221	140 153 166 178 189 201 213	135 148 160 171 182 194 205	129 142 153 164 175 186 196	124 136 147 158 168 179 189	118 130 141 151 161 171 181	113 124 134 144 154 163 173	1/4 ************************************	15.5

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES B.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.		1	ength	in Fe	et.	
Lbs. per Ft.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	6	8	10	12	14	16
9.75	1/4 16 8/8 7 6 8/8	38.2 42.9 47.6 52.2 56.9 61.5 66.3	11.20 12.58 13.95 15.32 16.70 18.08 19.45	3.20 3.27 3.33 3.35 3.34 3.33 3.32	138 155 172 189 206 223 240	137 154 170 187 204 221 238	135 151 168 185 202 218 235	132 149 166 182 198 215 231	130 146 163 179 195 211 227	127 143 160 175 191 207 223
12.25	1/4 16 18 17 17 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18	43.2 47.9 52.6 57.2 61.9 66.5 71.3	12.70 14.08 15.45 16.82 18.20 19.58 20.95	3.08 3.16 3.22 3.29 3.31 3.30 3.29	156 173 190 208 225 242 259	155 172 188 206 222 239 256	153 169 186 203 220 236 253	150 166 183 200 216 233 249	147 163 180 196 213 229 244	143 159 176 192 208 224 239
14.75	1/4 FE 80/20 FE 80	48.2 52.9 57.6 62.2 66.9 71.5 76.3	14.18 15.56 16.93 18.30 19.68 21.06 22.43	2.99 3.07 3.14 3.20 3.26 3.27 3.27	174 191 200 225 243 260 277	172 189 206 223 240 257 274	170 186 203 220 237 253 270	167 183 200 216 233 250 265	163 179 196 212 229 245 261	159 176 192 208 224 240 256
17.25	1/4 TE 8/8 - TE /2 TE /8	53.2 57.9 62.6 67.2 71.9 76.5 81.3	15.64 17.02 18.39 19.76 21.14 22.52 23.89	2.91 2.99 3.06 3.13 3.19 3.24 3.24	192 209 226 243 260 277 294	190 207 224 240 258 275 291	187 204 220 237 254 271 288	183 200 217 234 250 267 263	179 195 212 228 245 262 278	174 191 207 224 240 257 272
19.75	1/4-18/8-18/9-18/8	58.2 62.9 67.6 72.2 76.9 81.5 86.3	17.12 18.50 19.87 21.24 22.62 24.00 25.37	2.85 2.93 3.00 3.07 3.13 3.19 3.21	210 228 244 261 279 296 313	207 225 241 259 275 293 309	204 221 238 254 272 289 305	200 217 233 250 267 284 301	195 212 228 245 262 278 294	190 206 228 240 256 273 288

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS, SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ 

· Safety factor 4.



#### SERIES B.

			Leng		Thickness of Plates,	Weight of each Channel.				
18	20	22	24	26	28	80	32	34	Inch.	Lbs. per Ft.
124 140 156 171 187 202 218	121 137 152 167 182 198 213	118 133 148 163 178 192 207	114 130 144 159 173 187 201	111 125 140 154 168 182 190	107/ 121 136 149 163 175 190	103 117 132 145 158 171 184	100 114 127 140 153 165 178	97 110 123 136 147 160 172	1/4 -1= -1/2 -1= -1/2 -1= -1/8	9.76
140 156 172 188 204 218 234	136 152 167 183 199 213 228	132 147 163 178 194 207 222	128 143 158 173 188 202 216	124 139 153 168 182 196 210	119 134 148 163 176 190 203	115 129 143 158 171 184 197	111 125 139 153 165 178 190	107 120 133 148 160 172 184	1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4 1/4	12.25
155 171 187 203 219 235 250	150 166 182 198 214 229 244	145 161 177 192 209 223 238	141 156 172 187 202 217 231	136 151 166 181 196 210 223	131 146 161 175 190 203 216	127 141 155 169 184 197 209	122 136 149 163 178 190 203	117 130 144 158 172 184 196	144 10 10 10 10 10 10 10 10 10 10 10 10 10	14.75
169 186 202 218 235 250 265	164 180 197 212 228 244 259	159 175 190 206 222 238 252	154 169 185 200 216 231 245	148 163 178 194 208 224 238	143 157 172 188 202 217 230	137 152 166 180 195 209 222	132 146 160 174 189 202 215	128 140 154 167 181 195 207	144 146 146 146 146 146 146 146 146 146	17.25
185 201 217 233 249 267 282	179 195 211 227 243 259 275	173 189 205 220 236 252 266	167 182 198 214 229 245 259	161 176 191 206 222 236 251	155 169 185 199 215 229 243	149 163 177 192 207 222 236	143 157 170 185 200 214 227	137 150 184 178 192 206 219	1/4 1/5 1/5 1/2 1/8 1/8	19.75

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES B.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.	-	1	leng	th in	Feet	;.	
Lbs.per Ft.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	в	8	10	12	14	16	18
11.25	1/4 #6 *8 176 176 176 178 188	42.9 48.0 53.1 58.2 63.3 68.4 73.5	12.70 14.20 15.70 17.20 18.70 20.20 21.70	3.62 3.70 3.72 3.70 3.68 3.66 3.65	157 176 194 213 231 250 268	156 174 193 211 229 248 266	154 172 191 209 227 245 264	152 171 189 207 224 242 260	150 168 186 203 221 239 256	147 165 183 200 218 234 252	144 162 180 196 213 230 247
18.75	1/4 16 2/8 7-6 1/2 1/2 1/8 8/8	47.9 53.0 58.1 63.2 68.3 73.4 78.5	14.08 15.58 17.08 18.58 20.08 21.58 23.08	3.52 3.60 3.67 3.67 3.66 3.64 3.63	174 193 211 230 248 267 285	172 191 209 228 246 265 283	171 189 207 226 244 262 280	168 187 205 223 241 258 276	165 184 202 220 237 255 272	163 181 198 216 233 250 268	159 177 195 212 229 246 262
16.25	1/4 68 8/8 116 12/2 16/8	52.9 58.0 63.1 68.2 73.3 78.4 83.5	15.56 17.06 18.56 20.06 21.56 23.06 24.56	3.42 3.50 3.58 3.64 3.63 3.62 3.61	192 211 229 248 266 285 303	190 209 228 246 264 283 301	188 206 225 244 261 279 208	185 204 222 240 258 276 294	182 200 219 237 254 272 289	179 197 215 233 250 268 285	175 193 211 229 245 262 279
18.75	1/4 616 8/8 716 11/2 0 16/8	57.9 63.0 68.1 73.2 78.3 83.4 88.5	17.02 18.52 20.02 21.52 23.02 24.52 26.02	3.34 3.42 3.50 3.57 3.61 3.60 3.59	210 229 247 266 284 303 322	208 227 245 264 282 301 319	205 224 242 261 279 297 315	202 221 239 257 276 294 312	199 217 235 254 271 280 307	195 213 231 249 267 284 301	191 208 227 245 262 279 206
21.25	1/4 18 8/8 18 1/2 1/2 18 5/8	62.9 68.0 73.1 78.2 83.3 88.4 93.5	18.50 20.00 21.50 23.00 24.50 26.00 27.50	3.27 3.36 3.43 3.51 3.57 3.57 3.57	228 247 266 284 303 321 340	226 244 263 282 300 319 337	223 241 260 279 297 315 333	219 238 256 275 293 311 329	215 234 252 270 289 306 324	211 229 247 265 283 301 318	206 224 243 260 278 295 313

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}} \cdot \ \mbox{Safety factor 4.}$ 



#### SERIES B.

		- 1	Thick- ness of Plates.	Weight of each Channel.							
20	22	24	26	28	30	82	34	86	38	Inch.	Lbs.per Ft.
142 159 176 193 209 225 242	138 156 172 189 204 221 237	135 152 168 184 200 215 231	131 148 164 180 194 210 226	128 144 160 175 190 204 219	124 141 155 170 184 199 214	121 137 151 166 179 194 207	117 133 147 161 175 188 202	114 129 143 156 169 182 195	110 125 139 151 164 176 189	1/4 5 16 8/8 12 1/2 18 8/8	11.25
156 173 191 208 224 241 257	152 170 187 203 219 236 251	149 165 183 199 214 230 246	144 161 178 193 209 224 239	140 157 173 187 203 218 233	137 153 168 183 198 213 226	132 148 164 178 193 206 220	128 144 159 173 186 200 213	124 139 154 168 181 194 207	120 134 149 162 175 188 200	1/4 1/4 1/4 1/4 1/4 1/8	18.75
171 189 206 224 240 257 274	167 184 202 219 235 251 267	163 179 197 214 230 245 261	158 175 191 209 223 239 254	153 170 187 203 218 233 247	149 165 181 198 211 226 241	144 160 176 191 206 220 233	140 155 170 186 199 213 227	135 150 165 180 194 207 219	130 145 160 175 187 200 213	1/4 1/4 1/4 1/4 1/4 1/4 1/8	16.25
186 204 221 239 257 272 289	181 199 216 233 250 267 283	176 194 210 228 245 260 276	171 188 205 222 238 254 269	166 182 199 216 231 247 262	161 177 193 210 226 240 254	155 171 188 203 219 233 247	150 166 182 198 213 226 239	145 161 176 191 206 219 232	140 155 170 186 200 212 224	1/4 \$15 \$/8 \$15 \$/8 \$15 \$/8 \$15 \$/8	18.75
201 219 237 254 272 289 305	196 214 231 248 265 282 298	191 208 225 243 260 276 291	184 202 218 236 252 268 283	178 196 212 229 246 261 276	173 190 206 223 239 253 268	167 184 200 216 231 245 260	161 178 193 209 225 239 253	156 172 187 202 218 231 244	150 165 180 196 211 224 237	1/4 56 8/8 16 1/2 16 5/8	21.25

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 9" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES B.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.			Len	gth	in F	eet.		
Lbs.per Ft.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	6	8	10	12	14	16	18	20
13.25	1/4 TE 8/8 7 TE 1/2 TE 8/8	48.6 54.1 59.7 65.2 70.7 76.2 81.7	14.28 15.90 17.53 19.16 20.78 22.40 24.03	4.05 4.10 4.07 4.04 4.02 4.00 3.99	177 197 217 237 257 277 297	176 196 216 236 256 276 296	174 194 214 234 253 273 293	172 192 212 231 251 270 290	170 190 209 228 248 267 286	168 187 207 225 244 263 282	166 184 203 222 240 259 278	163 181 200 218 236 255 273
15.0	1/4 5 16 8/8 7/6 1/2 9 16 5/8	52.1 57.6 63.2 68.7 74.2 79.7 85.2	15.32 16.94 18.57 20.20 21.82 23.44 25.07	3.97 4.05 4.05 4.03 4.01 3.99 3.97	190 210 230 250 270 200 310	188 208 228 249 268 288 288 306	187 207 226 246 266 286 306	185 204 224 244 263 283 283 802	183 202 221 241 260 279 299	180 199 218 237 256 275 295	177 197 215 234 252 271 290	174 193 212 230 248 266 285
20.0	1/4 B 16 8 7 16 7 16 7 16 7 16 7 16 7 16 7 16	62.1 67.6 73.2 78.7 84.2 89.7 95.2	18.26 19.88 21.51 23.14 24.76 26.39 28.01	3.78 3.87 3.95 3.98 3.96 3.95 3.94	226 246 266 286 306 327 347	224 244 264 285 305 325 345	222 242 262 282 302 322 342	219 239 260 279 200 318 338	216 236 256 276 295 314 333	213 233 252 272 291 300 328	209 228 248 268 286 304 323	205 224 244 263 280 299 317
25.0	1/4 B 18 8 7 18 1/2 N 1 5/8	72.1 77.6 83.2 88.7 94.2 99.7 105.2	21.20 22.82 24.45 26.08 27.70 29.32 30.95	3.64 3.73 3.81 3.89 3.92 3.91 3.90	262 282 303 323 343 363 383	260 280 300 320 341 361 380	257 277 298 317 337 357 357	254 274 294 314 333 353 373	251 270 290 310 329 348 368	246 266 285 305 324 343 362	242 261 281 301 319 338 357	236 255 276 295 314 332 350

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 9" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50~000}{1+\frac{(12~L)^2}{36~000~r^2}}$ . Safety factor 4.



#### SERIES B.

				Leng	th in	Fee	t.				Thickness of Plates.	Weight of each Channel.
22	24	26	28	80	82	84	86	88	40	42	Inch.	Lbs. per Ft.
160 178 196 214 232 250 268	157 174 192 210 227 245 268	153 172 188 206 222 240 257	150 168 184 201 217 234 251	146 164 180 196 212 229 245	143 160 175 192 207 223 239	139 156 171 187 202 217 233	136 152 167 182 196 211 227	132 148 163 177 191 206 221	128 144 158 172 186 200 215	125 140 154 167 181 194 208	1/4 5 1 5 8 1 5 6 8 1 5 6 6 8 1 5 6 8	13.25
171 190 208 225 243 261 280	167 186 204 221 238 256 274	164 182 199 216 233 251 268	159 178 195 212 228 245 261	156 174 190 207 223 239 255	152 169 186 202 217 233 248	148 165 181 197 212 227 242	144 161 176 192 206 221 235	140 156 172 187 200 215 229	136 152 167 181 195 209 223	132 148 162 176 189 203 216	1/4 58 8/8 76 1/2 96 6/8	15.0
201 220 239 258 275 293 311	197 215 234 253 269 287 305	192 211 229 247 264 281 298	187 206 224 242 258 274 291	183 200 218 236 251 268 284	177 195 213 230 245 261 277	172 190 207 224 239 255 270	168 185 202 218 232 248 263	162 180 196 213 226 241 250	158 174 191 205 220 234 247	153 168 186 200 214 228 240	1/4 56 8/8 76 1/2 6/8	20.0
232 250 269 288 308 326 344	226 245 264 283 301 319 335	221 238 258 276 295 312 328	214 233 252 270 288 304 320	209 227 245 264 280 296 313	202 220 238 257 273 289 309	197 214 232 250 266 281 297	190° 207 226 242 259 274 289	185 201 218 236 252 265 281	179 196 212 229 245 260 273	173 189 206 222 238 251 264	1/4 5/8 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6	25.0

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1 + \frac{(12\ L)^3}{36\ 000\ r^2}} \cdot \text{ Safety factor 4.}$ 



#### SERIES B.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.		Least Radius of Gyration.			L	engt	h in	Fee	t.		
Lbs.per Ft.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	8	10	12	14	16	18	20	22	24
15	1/4 5 18 8/8 7 18 1/2 9 16 5/8	55.5 61.9 68.3 74.6 81.0 87.4 93.8	16.42 18.30 20.17 22.05 23.92 25.80 27.67	4.49 4.58 4.65 4.70 4.67 4.65 4.63	203 226 249 272 296 319 342	201 224 247 271 294 316 339	199 223 245 268 291 314 337	198 220 243 266 289 311 334	195 218 241 263 286 308 330	193 216 238 261 282 304 326	190 212 235 257 278 300 322	187 209 232 253 275 296 317	185 206 228 250 271 291 312
20	1/4 5 8 3/8 7 16 1/2 9 16/8	65.5 71.9 78.3 84.6 91.0 97.4 103.8	19.26 21.14 23.01 24.89 26.76 28.64 30.51	4.29 4.39 4.47 4.55 4.62 4.63 4.61	237 261 284 307 331 354 377	236 259 282 305 328 351 374	233 257 279 303 326 349 371	231 254 277 300 323 346 368	228 251 273 297 319 341 364	225 248 270 292 315 337 359	221 244 206 289 311 333 355	218 240 262 285 306 328 349	214 236 258 280 302 323 344
25	1/4 5 16 8/8 7 16 1/2 9 16 5/8	75.5 81.9 88.3 94.6 101.0 107.4 113.8	22.20 24.08 25.95 27.83 29.70 31.58 33.45	4.13 4.23 4.32 4.40 4.48 4.55 4.58	274 297 320 343 367 390 413	271 294 318 341 364 387 410	268 292 315 333 361 384 407	265 288 312 334 357 380 403	262 285 308 331 353 376 399	258 280 303 326 349 371 394	254 277 299 322 343 366 388	249 272 294 316 339 361 383	245 266 288 310 332 355 377
80 " "	1/4 8 16 3/8 7 16 1/2 9 16 5/8	85.5 91.9 98.3 104.6 111.0 117.4 123.8	25.14 27.02 28.89 30.77 32.64 34.52 36.39	4.01 4.11 4.20 4.28 4.36 4.43 4.50	309 333 356 379 403 426 449	307 330 353 377 400 423 446	303 327 349 373 396 419 442	300 323 346 369 392 415 438	295 318 341 365 387 410 432	291 313 336 359 382 404 428	286 308 331 353 376 399 422	280 302 326 348 371 392 415	275 298 320 342 364 386 409
85 " " "	1/4 56 3/8 7 16 1/2 16 5/8	95.5 101.9 108.3 114.6 121.0 127.4 133.8	28.08 29.96 31.83 33.71 35.58 37.46 39.33	3.90 4.00 4.10 4.18 4.26 4.33 4.40	345 369 392 415 438 462 485	342 365 389 412 436 459 481	338 361 385 408 431 454 478	334 357 380 404 426 450 472	329 352 375 398 420 444 467	324 346 369 392 415 437 461	318 340 363 386 409 432 455	312 334 356 379 401 424 447	304 327 349 373 395 418 439

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



### SERIES B.

			17 (1	Ler	ngth	in Fe	et.					Thick- ness of Plates.	Weight of each Channel.
26	28	30	82	34	36	88	40	42	44	46	48	Inch.	Lbs.per Ft.
181 202 224 246 266 287 307	178 199 220 241 261 282 302	174 195 216 237 257 276 296	171 191 212 233 251 271 291	167 188 208 228 246 266 285	163 183 204 223 242 261 278	159 179 199 218 237 254 273	156 176 195 214 231 249 267	152 171 190 209 226 244 260	148 167 185 204 221 237 254	145 163 181 199 215 232 248	141 159 177 195 210 226 241	1/4 5 16 8/8 7-16 1/2 16 8/8	15
210 232 254 275 297 318 339	208 227 248 270 291 313 332	201 223 244 265 286 306 326	197 218 238 260 281 301 320	193 214 234 254 274 295 313	188 208 228 249 269 288 307	183 203 223 243 264 282 301	179 198 218 238 257 276 293	174 193 213 232 251 269 286	169 189 208 226 246 263 280	165 183 202 221 239 257 272	160 179 197 216 233 250 266	1/4 5 16 8/8 7 11/2 116 5/8	20
239 262 284 305 327 349 370	234 256 277 299 322 342 364	229 250 272 294 315 336 356	224 245 266 287 309 330 350	219 240 260 281 302 322 343	213 234 254 274 296 316 335	207 227 248 268 288 308 328	202 221 241 261 282 301 321	196 216 236 256 274 295 312	190 210 229 248 268 287 305	186 204 223 241 261 280 299	180 199 217 236 255 274 290	1/4 5 16 8/8 17-6 1/2 16 5/8	25
269 291 313 335 357 379 401	263 285 306 329 351 372 394	257 278 300 322 342 364 386	250 272 293 314 336 357 378	244 265 286 308 328 349 370	237 258 279 300 320 342 362	231 252 273 292 313 333 355	224 245 265 286 305 326 345	218 239 258 278 298 317 338	212 232 251 270 290 310 329	205 225 243 264 282 301 321	199 218 238 256 275 294 312	1/4 5 8 7 6 8 7 6 8 7 6 8 8 8 8 8 8 8 8 8 8 8	80 " " "
298 320 343 365 387 409 432	291 313 336 357 379 401 422	284 306 328 349 372 393 415	277 298 320 340 363 384 405	269 291 312 334 354 375 397	262 283 304 325 345 367 387	255 275 296 317 338 358 379	248 267 287 309 329 350 369	239 260 281 301 320 340 361	282 252 273 292 312 331 351	225 245 265 284 303 323 341	219 238 257 276 294 314 333	1/4 5 1/6 8/8 716 1/2 1/6 5/8	35 " " "

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES B.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.		Least Radius of Gyration.			L	engt	h in	Fee	t.		
Lbs.per Ft.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches,	8	10	12	14	16	18	20	22	24
20.5	1/4 5 16 8/8 7 16 1/2 9 16/8	68.2 75.0 81.8 88.6 95.4 102.2 109.0	20.06 22.06 24.06 26.06 28.06 30.06 32.06	5.23 5.18 5.14 5.10 5.07 5.04 5.01	248 273 298 322 347 372 397	247 272 296 321 345 370 394	246 270 295 318 343 367 392	244 268 292 317 340 364 889	241 266 290 314 337 361 385	240 263 287 311 333 357 381	237 260 283 307 331 354 377	234 258 280 303 327 349 372	231 254 276 299 322 344 367
25	1/4 5 8/8 1/2 1/2 1/2 1/8	77.2 84.0 90.8 97.6 104.4 111.2 118.0	22.70 24.70 26.70 28.70 30.70 32.70 34.70	5.09 5.14 5.11 5.07 5.05 5.02 5.00	281 306 330 355 380 405 429	279 304 328 353 378 402 427	277 302 326 351 375 400 424	275 800 324 348 372 396 421	273 297 321 345 369 393 417	270 294 318 341 365 389 412	267 291 315 338 361 384 408	264 287 311 334 356 379 403	261 284 307 330 351 374 397
80	1/4 5 16 8/8 16 1/2 16 5/8	87.2 94.0 100.8 107.6 114.4 121.2 128.0	25.64 27.64 29.64 31.64 33.64 35.64 37.64	4.93 5.04 5.07 5.04 5.02 4.99 4.98	317 342 367 391 416 441 466	315 340 365 389 414 438 463	313 338 362 387 411 435 460	311 335 359 383 408 432 456	308 332 356 380 404 428 452	304 328 352 376 400 424 447	300 326 349 373 895 419 442	296 321 345 367 390 413 437	292 316 340 362 385 408 431
85	1/4 5 18 8/8 18 1/2 18 8/8	97.2 104.0 110.8 117.6 124.4 131.2 138.0	28.58 30.58 32.58 34.58 36.58 38.58 40.58	4.80 4.91 5.01 4.99 4.97 4.95 4.94	353 378 403 428 453 477 502	351 376 401 425 450 475 409	349 374 398 422 447 471 496	346 370 395 419 443 468 492	342 366 391 415 439 463 487	362 387 411 435 458 482	334 358 383 406 430 453 477	329 354 378 401 424 448 469	325 349 373 396 419 442 463
40	1/4 5 16 8/8 16 1/2 16 8/8	107.2 114.0 120.8 127.6 134.4 141.2 148.0	31.52 33.52 35.52 37.52 39.52 41.52 43.52	4.69 4.80 4.90 4.95 4.94 4.92 4.91	369 414 439 464 489 514 538	387 412 437 462 486 511 535	384 409 434 458 483 507 532	380 405 430 455 479 503 526	377 402 425 451 474 497 521	373 396 421 446 470 492 516	367 391 416 441 464 486 510	362 386 411 435 457 480 503	357 381 405 420 451 473 496

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P =  $\frac{50\ 000}{1+\frac{(12\ L)^2}{36\ 000\ r^2}}\cdot \ \mbox{Safety factor 4.}$ 



#### SERIES B.

				Lei	ngth	in F	et.					Thick- ness of Plates.	Weight of each Channel.
26	28	80	82	84	86	88	40	42	44	46	48	Inch.	Lbs.per Ft.
228 251 272 295 318 339 362	225 247 269 291 313 334 356	222 243 265 286 308 328 350	218 239 261 281 303 324 344	215 235 256 276 297 319 338	211 231 251 271 292 313 332	207 227 247 266 286 307 326	204 223 242 262 281 301 319	200 218 237 257 275 275 295 313	196 214 232 251 269 288 306	191 209 228 246 263 282 299	187 205 223 241 258 276 293	1/4 BE 8/8 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	20.5
257 280 302 325 348 369 391	253 276 298 320 342 363 885	249 272 293 315 337 357 357	245 268 288 310 331 351 373	241 263 283 304 325 345 366	236 258 279 299 319 339 359	232 253 274 293 313 332 352	227 248 268 287 307 325 345	222 243 263 281 301 319 338	219 238 258 275 295 312 331	214 234 252 269 288 305 324	210 229 247 264 282 299 317	1/4 10 9/8 10 1/2 10 10 10 10 10 10 10 10 10 10 10 10 10	25
288 312 336 357 379 402 425	284 307 330 351 374 396 418	279 302 325 346 368 389 411	274 298 320 341 361 383 404	269 293 314 335 355 376 397	264 287 308 329 348 369 390	259 282 302 323 342 362 382	254 276 296 316 335 355 375	249 271 290 310 328 347 367	243 265 284 304 321 340 359	238 260 278 297 314 333 351	233 254 272 291 307 326 344	1/4 5 16 8/8 7 10 10 10 10 10 10 10 10 10 10 10 10 10	80
320 344 368 390 413 434 456	315 338 362 384 406 427 449	310 333 356 378 400 420 442	303 327 350 371 393 413 434	297 321 344 365 386 405 426	292 315 337 358 379 398 418	286 309 331 351 371 390 410	280 303 324 344 364 382 402	273 295 318 337 355 374 394	267 289 311 330 347 366 385	261 282 304 323 340 358 377	255 276 298 316 332 350 369	1/4 5 18 8/8 7-8 11/2 118 5/8	85 44 44 44 44 44
351 375 399 422 444 466 489	344 369 393 415 437 459 481	339 363 386 408 430 452 473	333 355 380 401 423 444 465	326 349 373 394 415 436 457	318 342 366 387 407 428 448	312 335 357 379 399 420 440	306 328 350 372 391 411 431	298 320 343 364 383 403 420	291 313 335 356 375 394 411	285 306 328 348 367 886 402	278 299 321 341 359 375 393	1/4 5/8 8/8 1/2 1/2 9 1 8/8	40

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



### SERIES B.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column,	Area of Column Section.	Least Radius of Gyration.			Le	ngt	h in	Fee	t.		
Lbs.per Ft.	Inch.	Lbs.per Ft.	Sq. Ins.	Inches.	12	14	16	18	20	22	24	26	28
38 ** ** ** **	3/8 1/6 1/2 1/6 1/6 1/8 1/8 1/8 1/8	117.0 125.5 134.0 142.5 151.0 159.5 168.0	34.80 37.30 39.80 42.30 44.80 47.30 49.80	6.59 6.57 6.52 6.48 6.44 6.41 6.38	429 460 491 521 552 583 614	427 458 489 519 549 580 611	425 456 485 516 546 577 607	423 453 482 513 543 573 604	420 450 479 509 539 569 509	417 447 476 505 535 565 595	414 442 472 501 531 561 589	410 438 468 497 526 554 583	406 434 463 492 521 549 578
35	3/8 16/2 16/8 16/8 16/8 16/8 16/8 16/8 16/8 16/8	121.0 129.5 138.0 146.5 155.0 163.5 172.0	35.58 38.08 40.58 43.08 45.58 48.08 50.58	6.55 6.56 6.52 6.48 6.44 6.41 6.38	439 470 501 531 562 592 623	437 468 498 528 559 590 620	435 465 495 525 556 586 617	432 463 492 522 552 583 613	428 459 488 519 549 579	425 455 485 515 545 574 604	422 451 481 511 540 570 598	418 447 477 506 535 563 592	414 443 472 501 531 558 587
40	3/8 7 16 1/2 16 5/8 116 8/4	131.0 139.5 148.0 156.5 165.0 173.5 182.0	38.52 41.02 43.52 46.02 48.52 51.02 53.52	6.41 6.51 6.50 6.47 6.43 6.40 6.37	475 506 537 567 598 629 659	472 503 534 564 595 626 656	470 500 531 561 592 622 653	467 497 527 558 588 618 649	464 494 524 554 584 614 644	460 490 520 550 580 610 638	457 486 516 545 575 603 633	451 482 511 541 570 598 627	447 477 507 536 563 592 621
45	3/8 1/2 1/2 16 5/8 116 8/4	141.0 149.5 158.0 166.5 175.0 183.5 192.0	41.48 43.98 46.48 48.98 51.48 53.98 56.48	6.28 6.39 6.48 6.45 6.42 6.39 6.37	511 542 573 604 634 665 696	509 539 570 601 631 662 693	506 536 567 597 628 658 689	502 533 563 594 624 654 685	498 529 559 590 620 650 680	494 525 555 585 615 645 673	490 520 551 580 610 638 667	486 515 546 575 603 632 661	480 510 541 570 597 626 655
50 44 44 44 44	8/8 11/2 16 1/2 16 5/8 11 18 8/4	151.0 159.5 168.0 176.5 185.0 193.5 202.0	44.42 46.92 49.42 51.92 54.42 56.92 59.42	6.17 6.28 6.37 6.43 6.40 6.37 6.35	547 578 109 640 671 701 732	544 575 506 636 667 698 729	541 572 603 633 664 694 725	537 567 599 629 660 690 720	533 563 595 625 655 685 715	528 559 589 620 650 678 708	523 555 584 615 643 673 702	519 550 579 610 637 667 696	514 543 573 602 631 660 689
55 ** ** ** **	3/8 16 1/2 16 5/8 116 8/4	161.0 169.5 178.0 186.5 195.0 203.5 212.0	47.36 49.86 52.36 54.86 57.36 59.86 62.36	6.07 6.18 6.28 6.37 6.38 6.35 6.33	583] 614 645 676 707 738 768	580 610 642 673 703 734 764	576 607 639 669 700 730 760	571 603 633 665 695 726 756	567 599 629 660 690 721 751	563 593 624 654 685 713 743	556 588 619 648 678 707 737	551 582 613 643 672 701 730	546 577 605 636 665 694 724

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



				Lei	ngth	in F	eet.					Thick- ness of Plates.	Weight of each Channel.
80	32	84	36	38	40	42	44	46	48	50	52	Inch.	Lbs.per Ft.
401	397	393	388	383	379	374	369	364	359	353	348	8/8	33
430	425	421	416	411	406	401	395	390	384	379 402	373 396	8/8/16/22   16/8	66
459 487	454 482	449 477	444	439	433 458	427 452	422 446	414	408 434	402	421	72	68
515	509	503	498	492	485	479	473	466	457	450	444	5/8	4.6
543	538	532	525	519	512	504	497	490	483	476	468	118	66
572	566	560	553	544	537	530	523	516	508	501	491		
410	406	401	397 425	392	387 414	382 409	377	372 398	367 392	361 387	356 381	8/8 16/23 16/8 11/8 11/8 11/8 11/8 11/8 11/8 11/8	85
439 468	434	430 358	452	420 447	414	436	430	422	416	410	404	16	66
496	491	486	478	473	467	461	454	448	442	435	429	16	66
523	518	512	506	500	494	487	481	474	465	458	451	5/8	44
552 581	546 575	540 568	534 562	528 553	521 546	512 538	505 531	498 524	491 516	483 509	476 498	18	66
442	438	433	428	423	417	410	404	399	393	387	381		40
473	468	463	457	452	446	439	433	427	421	414	408	7.8	40
502	496	491	485	480	471	465	459	453	446	440	433	1/2	66
530	525	517	511	505	499	492	485	479	472	465	458	10	66
557 586	551 580	545 573	539 567	532 560	526 553	519 543	512 536	502 528	495 521	488 513	480 505	11	66
615	608	601	592	585	577	570	562	554	546	538	527	3/8 16/23 16/81/6 16/8 16/8	66
475	470	464	459	451	445	440	433	427	421	413	407		45
505	500	494	488	483	474	468	462	455	449	442	435	3/8 1-6 1/2 1-6 5/8 1-6 8/4	66
536 563	530 557	524 550	516 544	510 537	504	497 524	490 517	483 509	477 502	470 492	463	1/2	66
591	585	578	572	565	558	550	540	533	525	518	510	5/8	66
620	613	607	600	592	582	575	567	559	551	543	535	16	66
649	642	635	625	617	609	601	593	585	576	568	556		
507	501	495	489 519	481 510	475 504	469	462	453 483	447	440 467	433 460	8/8	50
537 568	562	525 555	547	540	533	526	519	512	504	497	487	1%	66
596	590	583	577	570	563	555	548	538	530	522	514	16	4.4
625	618	612	604	597	590	579	571	563	555	547	539	5/8	66
654 552	647	640	630	622	614	606	598 623	589 615	581 603	572 594	561 585	3/8 11/2 11/6 11/2 11/6 11/8 11/8 11/8	4.6
540	532	526	520	511	504	497	490	481	474	466	457		55
569	562	556	549	542	533	526	519	511	501	494	486	\$\\ \frac{8}{16} \\ \frac{1}{2} \\ \frac{1}{16} \\ \frac{1}{16	8.6
599	593	586	579	570	562	555	547	540	532	521	513	1/2	46
630	623	616	607	599	592	584	576	568	560	552	540 565	16	46
659 687	652	645	637	627	619	611	602	594 620	585 608	577 599	590	11	66
716	706	698	690	681	673	664	652	643	633	624	614	3/4	44

# SAFE LOADS IN THOUSANDS OF POUNDS FOR HOLLOW ROUND CAST IRON COLUMNS. SOUARE ENDS.

Based on Gordon's Formula  $P = \frac{10\ 000}{1 + \frac{P}{800\ d^3}}$ 

P = safe load in pounds per square inch.

l = length of column in inches.

d = outside diameter of column in inches.
Ultimate compressive strength=80 000 pounds per square inch. Safety factor 8.
Safe loads for other safety factors than that of the tables may be obtained as

follows:—New safe load = Safe load from table  $\times \frac{8}{\text{New factor}}$ 

Outside Diam- eter in	Thick- ness in		L	eng	th of	Col	um	n in	Feet	t.		Area of Metal in	Weight per Foot
Inches.	Inches.	6	8	10	12	14	16	18	20	22	24	Sq. Ins.	Pounds.
6	8/4 7/8	105 119	94 107	82 94	72 82	62 71	54 62	47 54	41 47	36 41	32 36	12.4 14.1	38.7 44.0
7	8/4	130	119	108	96	86	76	67	60	53	47	14.7	46.0
	7/8	149	136	123	110	98	87	77	68	61	54	16.8	52.6
8	3/4	155	145	133	122	110	99	89	80	72	85	17.1	53.4
	7/8	178	166	153	139	126	114	104	92	83	75	19.6	61.2
	I	200	186	172	158	142	128	115	103	93	84	22.0	68.7
9	1	207	196	183	169	156	142	130	118	108	98	22.3	69.8
	1	233	220	206	190	175	160	146	133	121	110	25.1	78.5
	1½	258	244	228	211	194	177	162	147	134	122	27.8	87.0
10	7/8	235	225	212	199	185	172	158	146	134	123	25.1	78.4
	1	265	254	240	224	209	194	178	164	151	139	28.3	88.4
	11/8	294	281	266	249	232	215	198	182	168	154	31.4	98.0
	11/4	323	308	291	273	254	235	217	200	184	169	34.4	107.4
11	1 1½ 1¼ 1¾ 13/8	298 330 363 395	287 319 350 380	273 304 333 361	259 287 315 342	243 270 296 322,	227 253 277 301	212 235 258 280	197 219 240 261	183 203 223 242	169 188 206 224	31.4 34.9 38.3 41.6	98.2 109.1 119.7 129.9
12	11/8	108	356	342	326	309	291	274	256	239	223	38.4	120.1
	11/4	404	391	375	358	339	320	300	281	263	245	42.2	131.9
	13/8	439	425	408	389	369	348	327	306	287	267	45.9	143.4
	11/2	473	458	440	419	397	375	352	330	208	288	49.5	154.6
13	11/8	404	393	379	364	347	330	312	294	277	260	42.0	131.2
	11/4	444	432	417	400	382	363	343	323	304	286	46.1	144.2
	13/8	484	470	454	435	415	395	373	352	331	311	50.2	156.9
	11/2	522	507	490	470	448	426	403	380	358	336	54.2	169.4
14	11/4 13/8 11/2 15/8	485 528 570 612	473 515 556 597	459 499 540 579	442 482 520 558	424 462 499 535	405 441 477 511	386 420 454 487	399 431 462	347 378 408 437	327 357 385 413	50.1 54.5 58.9 63,2	156.5 170.4 184.1 197.4
15	13/8	573	560	545	528	509	489	467	446	424	406	58.9	183.9
	11/2	618	605	589	570	550	528	505	482	459	439	63.6	198.8
	15/8	664	650	632	612	590	567	542	517	482	471	68.3	213.4
	13/4	708	694	675	653	630	605	579	552	525	502	72.8	227.6
16	1½ 158 134 178	666 716 764 811	702 750 796	638 686 732 777	620 666 711 756	600 645 689 731	579 622 664 705	557 508 638 678	533 573 611 649	510 548 584 621	486 522 558 502	68.3 73.4 78.3 83.2	213.5 229.3 244.8 260.0

# SAFE LOADS IN THOUSANDS OF POUNDS FOR HOLLOW ROUND CAST IRON COLUMNS. SQUARE ENDS.

10 000 Based on Gordon's Formula P = 1+800 d2

P = safe load in pounds per square inch.
l = length of column in inches.
d = outside diameter of column in inches.

Ultimate compressive strength=80000 pounds per square inch. Safety factor 8. Safe loads for other safety factors than that of the tables may be obtained as

follows:—New safe load = Safe load from table × New factor

Outside Diam- eter in	Thick- ness in Inches.					Col					00	Area of Metal in	Weight per Foot in
Inches.		754	732	708	684	659	633	26 608	596	557	533	Sq. Ins. 83.6	Pounds.
10	15/8 13/4 11/8 2	806 857 907	782 832 880	757 805 852	732 777 823	704 749 792	677 720 762	650 691 731	637 677 717	596 633 670	569 605 641	89.3 95.0 100.5	279.2 296.8 314.2
20	134 138 2 238		900 957 1014 1070	876 932 987 1041	850 905 958 1011	824 877 929 980	797 848 898 948	769 819 867 915	742 789 836 882	714 760 805 <b>849</b>	687 731 774 817	100.3 106.8 113.1 119.3	313.6 333.6 353.4 372.9
22	17/8 2 21/8 21/4	1171 1239	1082 1147 1213 1275	1122 1186	1094 1157	1065 1126	1094	$\frac{1004}{1062}$	1029	888 941 996 1046	859 910 962 1011	132.9	370.5 392.7 415.3 436.3
24	2 2½ 2¼ 2¾ 2¾	1376 1449	1280 1352 1423 1494	1311 1380	1298 1367	1268 1335	1238 1303	$\frac{1206}{1269}$	1173 1235	1140 1200	1106 1165		432.0 456.4 480.4 504.2
26	21/8 21/4 28/4 21/2	1596 1675	1492 1572 1650 1728	1546 1623	1517 1593	1487 1562	1456 1528	1423 1494	1389 1458	$\frac{1354}{1422}$	1319 1385	167.9	498.1 524.6 550.9 576.8
28	21/4 23/4 21/2 28/8	1829 1917	1719 1806 1892 1967	1780 1864	1751 1834	1721 1802	1689 1769	1655 1734	1620 1697	1584 1660	1548 1622	191.2 200.3	568.8 597.5 625.9 653.9
80	23/6 21/2 23/4 23/4	2078 2172	1961 2055 2148 2240	2028 2119	2000	1969 2058	1937 2024	1903 1989	1867 1952	1830 1913	1793 1874	206.1 216.0 225.8 235.4	644.1 675.0 705.5 735.7
82	21/2 25/8 23/4 23/8	2341 2442	2217 2318 2418 2517	2292 2391	2264 2361	2233 2329	2200 2295	2165 2259	2129 2221	2092 2182	$2053 \\ 2141$	242.2	724.0 757.0 789.7 822.1
84	25/8 23/4 27/8 3	2620 2728	2488 2596 2703 2810	2570 2676	2542 2646	2511 2614	2478 2580	2441 2544	2406 2505	2370 2468	2329 2425	281.1	808.6 843.7 878.5 913.0
86	23/4 27/8 3	2913	2774 2889 3003	2863	2834	2803	2770	2735	2698	2659	2619	299.2	897.7 935.0 971.9

#### STRENGTH OF HOLLOW ROUND AND HOLLOW RECTANGULAR CAST IRON COLUMNS.

For various values of L in which:-

L = length of column in feet. d = least outside diameter in inches.

P = ultimate strength in pounds per square inch.

Based on Gordon's Formulæ for Columns with Square Ends. Hollow Round. Hollow Rectangular.

> 80000 (12L)2 800 d2

(12L)2 1067 d2

E d		e Strength er sq. in.	E d		Strength per sq. in.
d	Hollow Round.	Hollow Rectangular.	d	Hollow Round.	Hollow Rectangular.
1.0	67800	70487	2.5	37647	48396
1.1	65692	68770	2.6	36088	41834
1.2	63532	66983	2.7	34599	40326
1.3	61340	65142	2.8	33178	38871
1.4	59137	63265	2.9	31817	37471
1.5	56940	61366	3.0	30534	36123
1.6	54766	59458	3.1	29306	34829
1.7	52625	57553	3.2	28137	33586
1.8	50531	55660	3.3	27025	32393
1.9	48491	53792	3.4	25967	31249
2.0	46512	51954	3.5	24961	30152
2.1	44598	50151	3.6	24004	29101
2.2	42753	48391	3.7	23093	28094
2.3	40979	46676	3.8	22227	27130
2.4	39277	45011	3.9	21403	26206

Safe loads for any given hollow round or hollow rectangular columns, corresponding to any suitable factor of safety, can be found from the above table as follows:-

Find from the table the ultimate strength in pounds per square inch corresponding to the given value of  $\frac{L}{d}$ . Multiply this by the area of the column in square inches and divide the product by the safety factor which will give as a quotient the required safe load in pounds.

EXAMPLE:—Required the safe load for a hollow round cast iron column 16 feet.

long, 10 inches external diameter with metal 1 inch thick with safety factor of 16 eight. The ratio of  $\frac{L}{d}$  in this case is  $\frac{10}{10} = 1.6$  and the corresponding ultimate strength from the tables is 54 766 pounds per square inch.

From the table of areas of circles it is found that the net area of the column is  $54.766 \times 28.3 = 193.735$  pounds 28.3 square inches. The safe load is, therefore. or approximately 97 net tons, which is the required result.

# EXPLANATIONS OF TABLES OF SAFE LOADS FOR BEAM BOX-GIRDERS AND PLATE GIRDERS, PAGES 306 TO 326 INCLUSIVE.

For cases in which the loads to be carried exceed the capacities of single rolled beams or ordinary beam girders composed of two or more beams with the usual

bolts and separators, it is necessary to use built-up sections.

BEAM BOX-GIRDERS.—A useful and economical section of this kind can be composed of two rolled beams with plates riveted to the top and bottom flanges, making a beam box-girder, for which tables of safe uniformly distributed loads are given on pages 306 to 316 inclusive.

The safe loads given in the tables include the weights of the beam box-girders, and are figured from the moment of inertia or the section modulus after making the necessary deductions for rivet holes, the fibre stress used in the calculations being

15 000 pounds per square inch of net section.

Beam box-girders are particularly useful for supporting wide walls and in other locations up to the limits of their capacity, but they should not be placed where exposed to moisture, as the section is such that access cannot be had to their interior for inspection and painting.

PLATE GIRDERS.—In cases where the widths of beam box-girders would prohibit their use, and for loads greater than their capacities, plate girders composed of plates

and angles may be used.

Tables of safe loads uniformly distributed for plate girders from 24" to 48" deep

are given on pages 317 to 326 inclusive.

The loads given in the tables include the weights of the girders and are calculated from the moment of inertia or the section modulus after making a proper deduction for rivet holes, the fibre stress used in the calculation being 15 000 pounds per square

inch of net section.

Although the tables do not show the stiffener angles for plate girders, care should be taken that these are provided in all cases where necessary to prevent buckling of the web due to the shearing action therein. The stiffeners should be made of angles riveted to the web, fitted tightly between the top and bottom fiange angles, and they should be provided, at the end of the girders, of such size and number as to be capable of carrying the total reaction at each end to the supports. Stiffeners should also be provided at intervals along the girder, spaced at suitable distances apart, as determined by the formula and explanations on pages 94 and 95.

Care should also be taken in arranging the rivet spacing for connecting the flange angles to the web, so that sufficient rivets are provided to properly transmit the stresses which act between these two portions of the construction. This will require the rivets to be spaced more closely amphe ends than at the center, and the exact spacing at any point along the girder may be obtained by dividing the product of the distance between the center lines of the rivet holes in the two flanges and the resistance of one rivet by the total vertical shear at the given point, thus:

 $p = \frac{rh}{S}$  in which

S = the total vertical shear, in pounds, at the point under consideration.

r = the resistance of one rivet, i. e., the bearing value or shearing value, whichever is the smaller, expressed in pounds.

h = the depth of the girder between the upper and lower center lines of rivets. expressed in inches.

p = pitch of rivets in the flange angles, expressed in inches.

The formula above will give the theoretical rivet spacing at any point in the flanges due to the total shear, but in practice the pitch for various portions of the length should be stated for the least possible number of spacing panels containing an even number of spaces, the pitch in each of which should preferably be expressed in even inches or even inches and halves or quarters of an inch, and the usual limits of pitch will vary from 21/2" to 6".

The rivet spacing should also conform to the rules given on page 358, and in cases where loads are applied directly to the flanges, sufficient rivets must be provided to carry these in addition to the rivets necessary for securing the web and

flanges together as explained above.

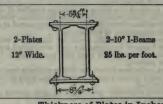
It should also be noted that the safe loads given in the tables are based on the assumption that the girder is supported laterally, otherwise a proper reduction in the allowable safe load must be made, as explained in connection with beams on

pages 82 and 83.

The weights of beam box-girders and plate girders in the tables are expressed in pounds per lineal foot, including the rivets necessary to secure the web and flanges together, but the weights do not include any allowance for brackets, stiffeners, connections or other details, as these will vary, subject to the conditions of each case.

#### SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

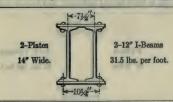
Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with \\\dft\delta^\*\river rivet holes in both flanges deducted, and include weight of girder.



Distance Center to Center of		For	Thickne	sses Gre				lates.	
Bearings in Feet.	1/2	16	5 8	116	3 4	13	7 8	15	1
10 11 12 13 14	90 82 75 09 64	96 87 80 74 69	102 93 85 79 73	109 99 90 84 78	115 104 96 88 82	121 110 101 93 86	127 116 106 98 91	134 121 111 103 95	140 127 117 108 100
15 16 17 18 19	56 53 50 47	64 60 57 53 51	68 64 60 57 54	72 68 64 60 57	77 72 68 64 60	81 76 71 67 64	85 80 75 71 67	80 83 70 74 70	93 87 82 78 74
20 21 22 23 23 24	45 43 41 39	48 46 44 42 40	51 40 47 45 43	54 52 49 47 45	57 55 52 50 48	60 58 55 53 50	64 61 58 55 53	67] 64 61 58 56	70 67 64 61 58
25 26 27 28 29	35 33 32 31	38 37 36 34 33	41 39 38 37 35	43 42 40 39 37	46 44 43 41 40	48 47 45 43 42	51 49 47 45 44	53 51 49 48 46	56 54 52 50 48
80 81 82 88 84	30 29 28 27 26	32 31 30 29 28	34 33 32 31 30	36 35 34 33 32	38 37 36 35 34	40 39 38 37 36	42 41 40 39 37	45 43 42 40 39	47 45 44 42 41
Weight per Foot in Pounds.	94.6	99.8	104.8	110.0	115.0	120.1	125.2	130.3	135.4
Section Modulus.	90.1	96.3	102.4	108.6	114.8	121.0	127.2	133.5	139.8
Coefficient of Deflection.	0	.0000014	15	0	.0000011	8	0	.0000009	8

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{250}$  span.

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with \(\frac{1}{4}\)" rivet holes in both flanges deducted, and include weight of girder.



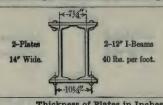
Distance Center to Center of		For '		ness of				ates.	
Bearings in Feet.	1/2	16	58	118	34	13	78	15	1
10 11 12 13 14	132 120 110 102 04	141 128 117 108 101	150 136 125 115 107	159 144 132 122 113	167 152 140 129 120	176 160 147 136 126	185 168 154 143 132	194 177 162 149 139	203 185 169 156 145
15 16 17 18 19	88 83 78 73 70	94 88 83 78 74	100 94 88 83 79	106 99 93 88 88	112 105 98 93 88	118 110 104 98 93	123 116 109 103 98	129 121 114 108 102	135 127 120 113 107
20 21 22 23 24	66 63 60 57 55	70 67 64 61 59	75 71 68 65 62	79 76 72 69 66	84 80 76 73 70	88 84 80 77 73	93 88 84 81 77	97 92 88 84 81	102 97 92 88 <b>85</b>
25 26 27	53 51 49	56 54 52	58 55	63 61 59	67 64 62	71 68 65	74 71 69	78 75 72	81 78 75
28 29	47 46	50 49	53 52	57 55	60 58	63 61	66 64	67	73 70
30 31 32 38 34	44 43 41 40 39	47 45 44 43 41	50 48 47 45 44	53 51 50 48 47	56 54 52 51 49	59 57 55 53 52	62 60 58 56 54	65 63 61 59 57	66 64 62 60
Weight per Foot in Pounds.	114.4	120.4	126.3	132.3	138.3	144.2	150.1	156.1	162.0
Section Modulus.	132.1	140.9	149.7	158.5	167.4	176.3	185.3	194.2	203.2
Coefficient of Deflection.	0	.0000008	42	0.	.0000006	88	0.	0000005	77

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span.

Distance Conte

#### SAFE LOADS IN THOUSANDS OF POUNDS UNIFORMLY DISTRIBUTED FOR BEAM BOX GIRDERS.

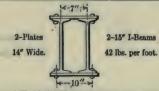
Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with H" rivet holes in both flanges deducted, and include weight of girder.



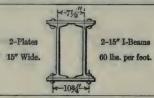
to Center of		For		sses Grea		3/4" Use		ates.	
Bearings in Feet.	1/2	16	5	116	34	13	78	15	1
10 11 12 13 14	147 133 122 113 105	155 141 129 119 111	164 149 137 126 117	173 157 144 133 123	181 165 151 140 130	190 173 158 146 136	199 181 166 153 142	208 189 173 160 148	217 197 181 167 155
15 16 17 18 19	98 92 86 81 77	97 91 86 82	109 102 96 91 86	115 108 102 96 91	121 113 107 101 95	127 119 112 106 100	133 124 117 111 105	139 130 122 115 109	144 135 127 120 114
20 21 22 23 23 24	73 70 87 64 61	78 74 71 68 65	82 78 75 71 68	86 82 78 75 72	91 86 82 79 76	95 91 86 83 79	95 90 87 83	104 99 94 90 87	108 103 99 94 90
25 26 27	59 56 54	62 60 58	66 63 61	69 66 64	73 70 67	76 73 70	80 77 74	83 80 77	87 88 80
28	52	56	59	62	65	68	71	74	77
29	51	54	57	60	63	06	49	72	75
80	49	52	55	58	60	63	06	0.0	72
81 82 88 84	47 46 44 43	50 49 47 46	53 51 50 48	56 54 52 51	59 57 55 53	61 59 58 56	64 62 60 59	67 65 63 61	70 88 66 64
Weight per Foot in Pounds.	131.4	137.4	143.3	149.3	155.3	161.2	167.1	173.1	179.0
Section Modulus.	146.6	155.3	163.9	172.7	181.4	190.2	199.0	207.8	216.7
Coefficient of Deflection.	0.	.0000007	63		8000000		0.	0000005	39

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{380}$  span.

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with \\frac{1}{4}"\) rivet holes in both flanges deducted, and include weight of girder.

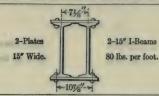


Distance Center to Center of Bearings in		F					es in 1			s.	
Feet.	5 8	118	34	13	7 8	15	1	116	11	$1\frac{3}{16}$	11/4
10 11 12 18 18	212 193 177 163 151	223 203 186 172 159	234 213 195 180 167	245 223 204 188 175	256 233 213 197 183	267 243 223 205 191	278 253 232 214 199	289 263 241 223 207	300 273 250 231 215	312 283 260 240 223	323 293 269 248 231
15 16 17 18 19	141 133 125 118 112	149 139 131 124 117	156 146 138 130 123	163 153 144 136 129	171 160 151 142 135	178 167 157 148 141	185 174 164 155 146	193 181 170 161 152	200 188 177 167 158	208 195 183 173 164	215 202 190 179 170
20 21 22 23 24	106 101 96 92 88	112 106 101 97 93	117 111 106 102 98	122 117 111 107 102	128 122 116 111 107	134 127 121 116 111	139 132 126 121 116	145 138 131 126 121	150 143 137 131 125	156 148 142 135 130	161 154 147 140 135
25 26 27 28 29	85 82 79 76 73	89 86 83 80 77	94 90 87 84 81	98 94 91 88 84	102 98 95 91 88	107 103 99 95 92	111 107 103 99 96	116 111 107 103 100	120 116 111 107 104	125 120 115 111 107	129 124 120 115 111
80 31 82 83 84	71 68 66 64 62	74 72 70 68 66	78 75 73 71 69	82 79 77 74 72	85 83 80 78 75	89 86 83 81 79	93 90 87 84 82	96 93 90 88 85	97 94 91 88	104 101 97 94 92	108 104 101 98 95
Weight per Poot in Pounds.	147.3	153.3	159.3	165.2	171.1	177.1	183.0	189.0	194.9	200.9	206.8
Section Modulus.	212.1	223.0	234.0	245.0	256.0	267.1	278.2	289.3	300.5	311.6	322.8
Coefficient of Deflection.											



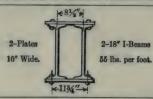
Distance Center to Center of Bearings in	1	F					es in :			s.	77
Feet.	58	11/16	34	13 16	7/8	15	1	116	11	$1\frac{3}{16}$	11
10	259	271	282	294	306	318	329	341	353	365	377
11	236	246	257	267	278	289	299	310	321	332	342
12	216	226	235	245	255	265	274	284	294	304	314
13	199	208	217	226	235	244	253	262	272	281	290
14	185	193	202	210	218	227	235	244	252	261	269
15	173	181	188	196	204	212	220	227	235	243	251
16	162	169	177	184	191	198	206	213	221	228	235
17	152	159	166	173	180	187	194	201	208	215	222
18	144	150	157	163	170	176	183	190	196	203	209
19	136	143	149	155	161	167	173	180	186	192	198
20	130	135	141	147	153	159	165	171	176	182	188
21	123	129	134	140	146	151	157	162	168	174	179
22	118	123	128	134	139	144	150	155	160	166	171
28	113	118	123	128	133	138	143	148	153	159	164
24	108	113	118	123	127	132	137	142	147	152	157
25	104	108	113	118	122	127	132	136	141	146	151
26	100	104	109	113	118	122	127	131	136	140	145
27	96	100	105	109	113	118	122	126	131	135	140
28	93	97	101	105	109	113	118	122	128	130	135
29	89	93	97	101	105	109	114	118	122	126	130
30	86	90	94	98	102	106	110	114	118	122	126
31	84	87	91	95	99	102	106	110	114	118	122
32	81	85	88	92	96	99	103	107	110	114	118
38	79	82	86	89	93	96	100	103	107	111	114
34	76	80	83	87	90	93	97	100	104	107	111
Weight per Foot in Pounds.	187.6	194.0	200.4	206.7	213.1	219.5	225.8	232.2	238.6	245.0	251,4
Section Modulus	259.2	270.8	282.4	294.1	305.8	317.5	329.3	341.1	353.0	364.9	376.8
Coefficient of Deflection.	0.0	000003	50	0.0	000003	03	0.0	000002	66	0.0000	00240

Safe loads below are figured for fibre stress of 15 000 pounds per square inch; with 17" rivet holes in both flanges deducted, and include weight of girder.



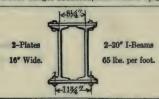
Distance Center to Center of Bearings in		F					es in :		s. o Plate	8.	- 1
Feet.	8	116	34	13 16	7/8	15 16	1	116	11/8	$1\frac{3}{16}$	11/4
10 11 12 18 14	300 272 250 231 214	311 283 259 239 222	322 293 269 248 230	334 303 278 257 238	345 314 288 265 247	357 324 297 274 255	368 335 307 283 263	380 345 316 292 271	391 356 326 301 279	403 366 336 310 288	414 377 345 319 296
15 16 17 18 19	200 187 176 167 158	207 194 183 173 164	215 201 190 179 170	222 209 196 185 176	230 216 203 192 182	238 223 210 198 188	245 230 217 204 194	253 237 223 211 200	261 244 230 217 206	269 252 237 224 212	276 259 244 230 218
20 21 22 23 23 24	150 143 136 130 125	156 148 141 135 130	161 154 147 140 134	167 159 152 145 139	173 164 157 150 144	178 170 162 155 149	184 175 167 160 153	190 181 173 165 158	196 186 178 170 163	201 192 183 173 168	207 197 188 180 173
25 26 27 28 29	120 115 111 107 103	124 120 115 111 107	129 124 119 115 111	133 128 124 119 115	138 133 128 123 119	143 137 132 127 123	147 142 136 131 127	152 146 141 136 131	156 150 145 140 135	161 155 149 144 139	166 159 153 148 143
80 81 82 88 84	100 97 94 91 88	104 100 97 94 91	107 104 101 98 95	111 108 104 101 98	115 111 108 105 102	119 115 111 108 105	123 119 115 112 108	127 122 119 115 112	130 126 122 119 115	134 130 126 122 118	138 134 130 126 122
Weight per Foot in Pounds.	227.6	234.0	240.4	246.7	253.1	259.5	265.8	272.2	278.6	285.0	291.4
Section Modulus.	299.7	311.0	322.4	333.7	345.1	356.6	368.1	379.6	391.2	402.8	414.4
Coefficient of Deflection.	0.0	000003	05	0.0	0000002	69	0.0	000002	39	0.0000	000218

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with  $\frac{15}{16}$ " rivet holes in both flanges deducted, and include weight of girder.



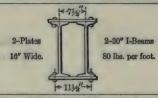
Distance Center to Center of Bearings in	For Thicknesses Greater than 3/4" Use Two Plates.											
Feet.	34	18	7/8	15	1	116	11/8	13/16	14	15	13	
15	227	237	247	258	268	278	289	299	809	320	330	
16	213	222	232	242	251	261	271	280	290	300	310	
17	200	200	218	227	237	246	255	264	273	282	291	
18	189	198	206	215	223	232	241	249	258	267	275	
19	179	187	195	203	212	220	228	236	244	253	261	
20	170	178	186	193	201	209	217	224	232	240	248	
21	162	169	177	184	191	199	206	214	221	228	236	
22	155	162	169	176	183	190	197	204	211	218	225	
23	148	155	161	168	175	182	188	195	202	209	215	
24	142	148	155	161	168	174	180	187	193	200	206	
25	136	142	148	155	161	167	173	179	186	192	198	
26	131	137	143	149	155	161	167	173	179	185	191	
27	126	132	137	143	149	155	160	166	172	178	183	
28	122	127	133	138	144	149	155	160	166	171	177	
29	117	123	128	133	139	144	149	155	160	165	171	
80	113	119	124	129	134	139	144	150	155	160	165	
81	110	115	120	125	130	135	140	145	150	155	160	
82	106	111	116	121	126	130	135	140	145	150	155	
83	103	108	112	117	122	127	131	136	141	145	150	
84	100	105	109	114	118	123	127	132	137	141	148	
35	97	102	106	110	115	119	124	128	133	137	142	
36	95	99	103	107	112	116	120	125	129	133	138	
87	92	96	100	104	109	113	117	121	125	130	134	
88	90	94	98	102	106	110	114	118	122	126	130	
89	87	91	95	99	103	107	111	115	119	123	127	
Weight per Foot in Pounds.	195.5	202.2	209.0	215.8	222.6	229.4	236.2	243.1	249.8	256.7	263.4	
Section Modulus.	340.5	355.8	371.2	386.6	402.1	417.5	433.0	448.6	464.2	479.8	405.4	
Coefficient of Deflection.	0.0	0000002	23	0.0	000001	03	0.0	000001	70	0.0000	00154	

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with 12 rivet holes in both flanges deducted, and include weight of girder.



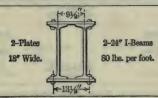
Distance Center to Center of Bearings in	of For Thicknesses Greater than ¾" Use Two Plates.										
Feet.	34	13	7 8	15	1	116	11/8	13	11	15/16	13
15 16 17 18 19	275 257 242 229 217	286 268 252 238 226	297 279 262 248 235	308 289 272 257 244	320 300 282 266 252	331 310 292 276 261	343 321 302 285 270	354 332 312 295 280	365 343 322 305 288	377 350 333 314 298	388 364 343 324 307
20 21 22 28 28 24	206 196 187 179 172	214 204 195 186 179	223 212 203 194 186	231 220 210 201 193	240 228 218 209 200	248 237 226 216 207	257 245 234 223 214	266 253 241 231 221	274 261 249 238 228	283 269 257 246 236	291 277 265 253 243
25 26 27 28 29	165 158 153 147 142	171 165 159 153 148	178 171 165 159 154	185 178 171 165 160	192 184 178 171 165	199 191 184 177 171	206 198 190 184 177	212 204 197 190 183	219 211 203 196 189	226 217 209 202 195	233 224 216 208 201
30 31 32 83 84	137 133 129 125 121	143 138 134 130 126	149 144 139 135 131	154 149 145 140 136	160 155 150 145 141	166 160 155 151 146	171 166 161 156 151	177 171 166 161 156	183 177 171 166 161	188 182 177 171 166	194 188 182 177 171
85 86 87 88 89	118 114 111 108 106	122 119 116 113 110	127 124 120 117 114	132 129 125 122 119	137 133 130 126 123	142 138 134 131 127	147 143 139 135 182	152 148 144 140 136	157 152 148 144 141	162 157 153 149 145	166 162 157 153 149
Weight per Foot in Pounds.	215.5	222.2	229.0	235.8	242.6	249.4	256.2	263.1	269.8	276.7	283.4
Section Modulus.	411.8	428.7	445.7	462.7	479.7	496.7	513.8	531.2	548.1	565.3	582.5
Coefficient of Deflection.	0.000000168 0.000000147 0.000000131 0.000000119										000119

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with \{\frac{1}{4}\]'' rivet holes in both flanges deducted, and include weight of girder.



Distance Center to Center of Bearings in		F					es in :			9.	45
Feet.	34	13	78	15 16	1	$1\frac{1}{16}$	11/8	$1\frac{3}{16}$	11/4	15/16	13
15	309	320	331	343	354	365	376	387	399	410	421
16	290	300	311	321	332	342	353	363	374	384	395
17	273	283	292	302	312	322	332	342	352	362	372
18	258	267	276	285	295	304	313	323	332	342	351
19	244	253	262	270	279	288	297	306	315	324	332
20	232	240	249	257	265	274	282	291	299	307	316
21	221	229	237	245	253	261	209	277	285	293	301
22	211	218	226	234	241	249	256	264	272	279	287
28	202	209	216	223	231	238	245	253	260	267	275
24	193	200	207	214	221	228	235	243	249	256	263
25	186	192	199	206	212	219	226	232	239	246	253
26	178	185	191	198	204	211	247	224	230	236	243
27	172	178	184	190	196	203	209	215	221	228	284
28	166	172	178	184	189	195	201	208	214	220	226
29	160	166	171	177	183	189	195	200	206	212	218
30	155	160	166	171	177	182	188	194	100	205	211
31	150	155	160	166	171	177	182	187	193	198	204
32	145	150	155	161	166	171	176	182	187	192	197
33	141	146	151	156	161	166	171	176	181	186	191
34	136	141	146	151	156	161	166	171	176	181	186
35	133	137	142	147	152	156	161	166	171	176	180
36	129	133	138	143	147	152	157	161	168	171	175
37	125	130	134	139	143	148	152	157	162	166	171
38	122	126	131	135	140	144	148	153	157	162	166
39	119	123	127	132	136	140	145	149	153	158	162
Weight per Foot in Pounds.	245.5	252.2	259.0	265.8	272.6	279.4	286.2	293.1	299.8	306.7	313.4
Section Modulus.	463.8	480.4	497.1	513.8	530.6	547.3	564.1	581.2	597.8	614.7	631.7
Coefficient of Deflection.	0.0	000001	49	0.0	000001	33	0.00	000001	19	0.0000	00110

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with \(\frac{1}{2}\)" rivet holes in both flanges deducted, and include weight of girder.



Distance Center to Center of Bearings in	For Thicknesses Greater than ¾" Use Two Plates.										
Feet.	34	13	7 8	15	1	$1\frac{1}{16}$	11/8	$1_{\frac{3}{16}}$	11/4	$1_{\frac{5}{16}}$	138
15 16 17 18 19	396 371 349 330 312	411 386 363 343 325	427 400 377 356 337	442 415 390 369 349	458 429 404 381 361	473 444 418 394 374	489 458 431 407 386	505 473 445 421 398	520 488 459 433 411	536 502 473 446 423	551 517 487 460 435
20 21 22 23 23 24	297 283 270 258 247	308 294 280 268 257	320 305 291 278 267	332 316 302 288 276	343 327 312 299 286	355 338 323 309 296	367 349 333 319 306	379 361 344 329 315	390 372 355 339 325	402 383 365 349 335	414 394 376 360 345
25 26 27 28 29	237 228 220 212 205	247 237 228 220 213	256 246 237 229 221	265 255 246 237 229	275 264 254 245 237	284 273 263 254 245	293 282 272 262 253	303 291 280 270 261	312 300 289 279 269	321 309 298 287 277	331 318 306 295 285
80 81 82 83 84	198 192 186 180 175	206 199 193 187 181	213 206 200 194 188	221 214 207 201 195	229 222 215 208 202	237 229 222 215 209	244 237 229 222 216	252 244 237 229 223	260 252 244 236 229	268 259 251 244 236	276 267 258 251 243
35 36 37 38 39	170 165 160 156 152	176 171 167 162 158	183 178 173 168 164	190 184 179 175 170	196 191 186 181 176	203 197 192 187 182	210 204 198 193 188	216 210 205 199 194	223 217 211 205 200	230 223 217 211 206	236 230 224 218 212
Weight per Foot in Pounds.	255.7	263.3	271.0	278.6	286.2	293.9	301.5	309.2	316.8	324.5	332.1
Section Modulus.	593.7	616.9	640.1	663.4	686.7	710.0	733.3	757.1	780.2	803.6	827.1
Coefficient of Deflection.	0.0000000983										

Safe loads below are figured for fibre stress of 15000 pounds per square inch, with \prec{1}{k}" rivet holes in both flanges deducted, and include weight of girder.

2 Plates

18" Wide.



2-24" I-Beams

105 lbs. per foot.

Distance Center to Center of Bearings in		F						Inche se Two		3.	
Feet.	3 4	13	7/8	15 16	1	$1\frac{1}{16}$	11/8	$1\frac{3}{16}$	11	$1_{\frac{5}{16}}$	13
15 16 17 18 19	466 437 411 388 368	481 451 424 401 379	496 465 437 413 391	511 479 451 426 403	526 493 464 438 415	541 507 478 451 427	557 522 491 464 439	572 536 505 477 451	587 550 518 489	502 555 532 502 476	618 579 545 515 488
20 21 22 23 24	349 333 317 304 291	361 343 328 314 300	372 354 338 323 310	383 365 348 333 319	395 376 359 352 329	406 387 869 353 338	417 398 379 363 348	429 408 390 373 357	440 419 400 383 367	452 430 411 393 376	463 441 421 403 386
25 26 27 28 29	279 269 259 249 241	288 277 267 258 249	297 286 275 265 256	307 295 284 274 264	316 303 292 282 272	325 312 301 290 280	334 321 309 298 288	343 830 318 306 296	352 339 326 314 304	361 347 335 323 312	371 356 343 231 319
80 81 82 88 84	233 225 218 211 205	240 232 225 218 212	248 240 232 225 219	255 247 239 232 232 225	263 254 246 239 232	271 262 254 246 239	278 269 261 253 245	286 277 268 260 252	293 284 275 267 259	301 291 282 274 266	309 299 289 281 272
35 36 37 38 39	199 194 189 184 179	206 200 195 190 185	212 206 201 196 191	219 213 207 202 196	225 219 213 208 202	232 225 219 214 208	238 232 226 220 214	245 238 232 226 220	251 245 238 237 226	258 251 244 238 232	265 257 250 244 237
Weight per Foot in Pounds	305.6	313.3	320.9	328.6	336.2	343.9	351.5	359.2	366.8	374.5	382.1
Section Modulus.	698.6	721.3	744.0	766.8	789.6	812.4	835.3	858.2	881.1	904.1	927.1
Coefficient of Deflection = 0.000000001 ×	87	84	81	78	76	73	71	69	66	64	63

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at  $\frac{1}{2}$  of an inch in diameter (for  $\frac{3}{4}$ " rivets) from both flanges.

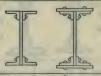
Web 24" >			Flange An		Web P			ge Angles
Distance		nickness				nickness		0 -
Center to Center of Bearings		Angles in	1	1		Angles in		
in Feet.	38	3	5 8	34	3 8	1/2	58	34
25 26 27 28 29	59 57 55 53 51	74 71 68 66 63	87 84 81 78 75	92 89 86	69 67 64 62 60	85 82 79 76 74	101 97 93 90 87	103 99
80 81 82 83 84	50 48 46 45 44	61 59 57 56 54	73 70 68 66 64	83 80 78 75 73	58 56 54 53 51	71 69 67 65 63	84 81 79 76 74	96 93 90 87 85
35 36 37 38 39	42 41 40 29 38	53 51 50 48 47	62 60 59 57 56	71 69 67 66 64	50 48 47 46 44	61 59 58 56 55	72 70 68 66 65	82 80 78 76 74
40 41 42 48 44	37 36 35 35 34	46 45 44 43 42	54 53 52 51 49	62 61 59 58 57	43 42 41 40 39	53 52 51 50 49	63 61 60 59 57	72 70 69 67 65
45 46 47 48 49	33 82 32 31 30	41 40 39 38 38	48 47 46 45 44	55 54 53 52 51	39 38 37 36 35	47 46 45 44 44	55 54 53 51	64 63 61 60 59
50 51 52 53 54	30 29 29 28 28	37 36 35 35 34	44 43 42 41 40	50 49 48 47 46	35 34 33 33 32	43 42 41 40 40	50 49 48 48 47	58 57 55 54 53
Weight per Foot in Pounds.	74.1	86.9	99.7	111.7	78	90.8	103.6	115.6

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at  $\frac{1}{8}$  of an inch in diameter (for  $\frac{1}{8}$ " rivets) from both flanges.

	Plate	ا کاک	Flange Ang		Web Pl			ge Angles
Distance Center to Center of		nickness Angles in					of Flan	
Bearings in Feet.	3 8	1/2	5 8	34	3 8	1/2	5 8	34
80 81 82 83 84	74 71 69 67 65	91 88 86 83 81	108 105 101 98 95	116 113 109	83 81 78 76 74	103 100 97 94 91	122 118 114 111 107	131 127 123
35 36 37 38 39	63 61 60 58 57	78 76 74 72 70	93 90 88 85 83	106 103 101 98 95	72 70 68 66 64	88 86 84 81 79	104 101 99 96 94	119 116 113 110 107
40 41 42 48 44	55 54 53 51 50	69 67 65 64 62	81 79 77 75 74	93 91 89 86 85	63 61 60 58 57	77 75 74 72 70	91 89 87 85 88	104 102 99 97 95
45 46 47 48 49	49 48 47 46 45	51 50 58 57 56	72 71 89 68 60	83 81 79 77 76	56 54 53 52 51	69 67 66 64 63	81 79 78 76 75	93 91 89 87 85
50 51 52 53 54	44 43 43 42 41	55 54 53 52 51	65 64 62 61 60	74 73 72 70 60	50 49 48 47 46	62 61 59 58 57	73 72 70 69 68	84 82 80 79 77
55 56 57 58 59	40 39 39 38 37	50 49 48 47 46	59 58 57 56 55	66 65 64 63	46 45 44 43 42	56 55 54 53 52	66 65 64 63 62	76 75 73 72 71
Weight per Foot in Pounds.	87.0	101.4	115.8	129.8	90.8	105.2	119.6	133.6

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for 7/6" rivets) from both flanges.

Web Plate  $36'' \times \frac{3}{8}''$ Flange Angles  $6'' \times 4''$ 



Web Plate  $36'' \times \frac{3}{8}''$ Flange Angles  $6'' \times 4'' \times \frac{3}{4}''$ Flange Plate 14''

Distance Center to Center of Bearings in		ickne ingles				Th	ickne	ss of in In		ge Pl	ate
Feet.	3/8	1/2	5/8	34	7/8	3 8	1/2	5/8	3 4	78	1
30	95	117	138	158	177	191	209	226	243	260	277
31	92	113	133	152	171	185	202	218	235	252	268
32	89	109	129	148	166	179	196	212	227	244	260
33	86	106	125	143	161	174	190	205	221	236	252
34	84	103	121	139	156	169	184	199	214	229	244
35	81	100	118	135	151	164	179	193	208	223	237
36	79	97	115	131	147	159	174	188	202	217	231
37	77	94	112	128	143	155	169	183	197	211	225
38	75	92	109	124	140	151	165	178	192	205	219
39	73	90	106	121	136	147	160	174	187	200	213
40	71	87	103	118	132	143	156	169	182	195	208
41	69	85	101	115	129	140	153	165	178	190	203
42	68	83	08	113	126	137	149	161	173	186	198
48	66	81	06	110	123	133	146	157	169	181	193
44	65	79	94	107	120	130	142	154	165	177	189
45	63	78	92	105	118	127	139	150	162	173	185
46	62	76	90	103	115	125	136	147	158	169	181
47	61	74	88	101	113	122	133	144	155	166	177
48	59	73	86	98	110	120	130	141	152	162	173
49	58	71	84	96	108	117	128	138	149	158	170
50	57	70	83	95	106	115	125	135	146	156	166
51	56	69	81	93	104	112	123	133	143	153	163
52	55	67	79	91	102	110	120	130	140	150	160
53	54	66	78	89	100	108	118	128	137	147	157
54	53	65	76	88	98	106	116	125	135	144	154
55	52	64	75	86	96	104	114	123	132	142	151
56	51	62	74	84	95	102	112	121	130	139	148
57	50	61	72	83	93	101	110	119	128	137	146
58	49	60	71	82	91	99	108	117	125	134	143
59	48	59	70	80	90	97	106	115	123	132	141
Weight per Foot in Pounds.	98.0	113.6	128.8	143.2	157.6	184.8	196.7	208.6	220.5	232.4	244.3

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15.000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at  $\frac{1}{2}$  of an inch in diameter (for  $\frac{1}{2}$  rivets) from both flanges.

Web Plate 36"×3%"
Flange Angles 6"×6"

Web Plate  $36'' \times \frac{3}{4}''$ Flange Angles  $6'' \times 6'' \times \frac{3}{4}''$ Flange Plates 14''

Distance Center to Center of Bearings in	Thic	kness gles ir	of Fla	nge es.			ness of e in In		Θ
Feet.	38	1/2	58	3	1/2	58	3	78	1
80 81 82 83 84	108 104 101 98 95	134 130 125 122 118	150 154 149 144 140	183 177 171 166 161	238 230 223 216 210	255 247 239 232 225	264 256 248 241	264 256	
85	92	115	136	157	204	219	234	249	264
86	90	112	132	152	198	213	227	242	257
37	87	109	129	148	193	207	221	235	250
38	85	106	125	144	188	201	215	229	243
89	83	103	122	141	183	106	210	223	237
40	81	100	119	137	178	191	205	218	231
41	79	98	116	134	174	187	200	213	225
42	77	96	113	131	170	182	195	207	220
48	75	93	111	128	166	178	190	203	215
44	74	91	108	125	162	174	186	198	210
45	72	89	106	122	158	170	182	194	205
46	70	87	104	119	155	166	178	189	201
47	69	85	101	117	152	163	174	185	197
48	67	84	99	114	149	160	171	182	193
49	66	82	97	112	146	156	167	178	189
50	65	80	95	110	143	153	164	174	185
51	63	79	93	108	140	150	160	171	181
52	62	77	92	106	137	147	157	168	178
58	61	76	90	104	- 135	144	154	164	174
54	60	74	88	102	132	142	152	161	171
55	59	73	87	100	130	139	149	158	168
56	58	72	85	98	127	137	146	156	165
57	57	70	84	96	125	134	144	153	162
58	56	89	82	95	123	132	141	150	159
59	55	68	81	95	121	130	139	148	157
Weight per Foot in Pounds.	107.5	126.3	144.7	162.7	214.1	226	237.9	249.8	261.7

Note.—When Flange plates are thicker than 3/4", use two plates.

The safe loads below include the weight of the girder and are calculated for a fibre stress of  $15\,000$  pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for % rivets) from both flanges.

Web Plate 42" × 3%"
Flange Angles 6" × 4"

Web Plate  $42'' \times \frac{3}{8}''$ Flange Angles  $6'' \times 4'' \times \frac{3}{4}''$ 

Flange Plates 14"

Distance Center to Center of Bearings in				Flan nches		Th	ickne	ss of in In	Flan	ge Pl	ate
Feet.	3 8	1/2	5 8	34	7/8	38	1/2	5 8	34	78	1
35	100	122	143	164	183	198	215	232	249	267	284
36	97	119	139	159	178	192	209	226	242	259	276
37	95	116	136	155	173	187	203	220	236	252	269
38	92	113	132	151	169	182	198	214	230	246	261
39	90	110	129	147	165	178	193	208	224	239	255
40	87	107	125	143	160	173	188	203	218	233	248
41	86	104	122	140	157	169	184	198	213	228	242
42	83	102	119	137	153	165	179	193	208	222	237
43	81	99	117	133	149	161	175	189	203	217	231
44	79	97	114	130	146	157	171	185	198	212	226
45	78	95	111	127	143	154	167	181	194	207	221
46	76	93	109	125	140	151	164	177	190	203	216
47	74	91	107	122	137	147	160	173	186	199	211
48	73	89	105	120	134	144	157	169	182	194	207
49	71	87	102	117	131	141	154	166	178	191	203
50	70	86	100	115	128	139	151	163	175	187	199
51	69	84	98	112	126	136	148	159	171	183	195
52	67	82	96	110	123	133	145	156	168	180	191
58	66	81	95	108	121	131	142	153	165	176	187
54	65	79	93	106	119	128	139	150	162	173	184
55	64	78	91	104	117	126	137	148	159	170	181
56	62	76	90	102	115	124	134	145	156	167	177
57	61	75	85	101	113	121	132	143	153	164	174
58	60	74	86	99	111	119	130	140	150	161	171
59	59	73	85	97	109	117	128	138	148	158	168
60	58	71	84	96	107	115	125	135	145	156	166
61	57	70	82	94	105	114	123	133	143	153	163
62	56	69	81	92	103	112	121	131	141	151	160
63	55	68	80	91	102	110	119	129	138	148	158
64	55	67	78	90	100	108	118	127	136	146	155
Weight per Foot in Pounds.	105.7	121.3	136.5	150.9	165.3	192.5	204.4	216.3	228.2	240.1	252.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for 7/6" rivets) from both flanges.



Web Plate  $42'' \times \frac{3}{6}''$ Flange Angles  $6'' \times 6'' \times \frac{3}{4}''$ Flange Plates 14''

Distance Center to Center of Bearings in	Flar	ckness ige An inche	gles		Thick		Flangaches.	e Plate	
Feet.	1/2	5 8	34	1/2	5	34	78	1	11
35	139	164	189	240	257	275	292	309	309
36	135	160	184	234	250	267	284	301	
37	131	155	179	227	244	260	276	293	
38	128	151	174	221	237	253	269	285	
39	125	148	169	216	231	247	260	278	
40	122	144	165	210	225	240	256	271	301
41	119	140	161	205	220	235	249	264	294
42	116	137	157	200	215	229	243	258	287
48	113	134	154	195	210	224	238	252	280
44	111	131	150	191	205	219	232	246	274
45 46 47 48 49	108 106 103 101	128 125 122 120 117	147 144 141 138 135	187 183 179 175 172	200 196 192 188 184	214 209 205 200 196	227 222 217 213 209	241 235 230 226 221	268 262 256 251 246
50	97	115	132	168	150	192	204	217	241
51	95	113	130	165	177	180	200	212	236
52	94	111	127	162	173	185	197	208	232
58	92	100	125	159	170	181	193	204	227
54	90	107	122	156	167	178	189	201	223
55	88	105	120	153	164	175	186	197	219
56	87	103	118	150	161	172	183	193	215
57	85	101	116	147	158	169	179	190	211
58	84	99	114	145	155	166	176	187	208
59	82	98	112	142	153	163	173	184	204
60	81	96	110	140	150	160	170	180	201
61	80	94	108	138	148	158	168	178	197
62	78	93	137	136	145	155	165	175	194
68	77	91	105	133	143	153	162	172	191
64	76	90	103	131	141	160	160	169	188
Weight per Foot in Pounds.	134.9	153.3	171.3	224.7	236.6	248.5	260.4	272.3	296.1

NOTE.—When Flange plates are thicker than 3/4", use two plates.

#### SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for 1/8" rivets) from both flanges.

Web Plate 4 Flange Angle			م ح	5	7	مع الم	F.	Veb Pla lange A	ingles (	"×4"	× 8/4"
Distance Center to Center of Bearings in		ickne				Th	ickne	ss of in In	Flan	ge Pl	ate
Feet.	3/8	1/2	5 8	34	7/8	38	1/2	5 8	34	7 8	1
35 36 37 38 39	120 117 113 110 108	146 142 138 134 131	170 165 161 157 153	194 189 183 179 174	217 211 205 199 194	233 227 220 215 209	253 246 239 233 227	273 265 258 251 245	293 284 276 269 262	312 303 295 287 280	332 322 314 305 298
40 41 42 43 44	105 102 100 98 95	127 124 121 119 116	149 145 142 139 135	170 166 162 158 154	189 185 180 176 172	204 199 194 190 185	221 216 211 206 201	238 233 227 222 217	256 249 243 238 232	273 266 260 254 248	290 283 276 270 264
45 46 47 48	93 91 89 87	113 111 108 106	132 130 127 124 122	151 148 144 141	168 165 161 158 156	181 177 174 170	197 192 188 184	212 207 203 199	227 222 218 213	243 237 232 227	258 252 247 242 237

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Weight per Foot in 113.3 128.9 144.1 158.5 172.9 200.1 212.0 223.9 235.8 247.7 259.6 Pounds.

The safe loads below include the weight of the girder and are calculated for a fibre stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for 7% rivets) from both flanges.



Web Plate 48" × 34"

Flange Angles 6" × 6" × 34"

Flange Plates 14"

Distance Center to Center of Bearings in	Flan	icknes nge An i Inch	gles	15	Thick	ness of in In	Flang ches.	e Plate	
Feet.	1/2	56	34	1/2	5 8	34	7 8	1	11
35	166	195	224	283	303	322	342	362	361
36	161	190	218	275	294	313	333	352	
37	157	185	212	267	286	305	324	342	
38	153	180	206	260	279	297	315	333	
39	149	175	201	254	272	289	307	325	
40	145	171	196	247	265	282	209	317	352
41	141	167	191	241	258	275	292	309	343
42	138	163	187	236	252	269	285	302	335
43	135	159	182	230	246	263	279	295	327
44	132	155	178	225	241	256	272	288	320
45	129	152	174	220	235	251	266	282	312
46	126	149	170	215	230	245	260	275	306
47	123	145	167	211	225	240	255	270	299
48	121	142	163	206	221	235	249	264	293
49	118	140	160	202	216	230	244	259	287
50	116	137	157	198	212	226	240	253	281
51	114	134	154	194	208	221	235	248	276
52	112	131	151	190	204	217	230	244	270
53	109	129	148	187	200	213	226	239	265
54	107	127	145	183	196	209	222	235	260
55	105	124	142	180	193	205	218	230	256
56	104	122	140	177	189	201	214	226	251
57	102	120	137	174	186	198	210	222	247
58	100	118	135	171	183	195	206	218	242
59	98	116	133	168	179	191	203	215	238
60	97	114	131	165	176	188	200	211	234
61	95	112	128	162	174	185	196	208	231
62	94	110	126	160	171	182	193	204	227
63	92	109	124	157	168	179	190	201	223
64	91	107	122	155	165	176	187	198	220
Weight per Foot in Pounds.	142.5	160.9	178.9	232.3	244.2	256.2	268	279.9	303.7

The safe loads below include the weight of the girder and are calculated for a fibre stress of  $15\,000$  pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for % rivets) from both flanges.

Web Plate 60" × 3%"

Flange Angles 6" × 4"



Web Plate  $60'' \times \frac{3}{8}''$ Flange Angles  $6'' \times 4'' \times \frac{3}{4}''$ Flange Plates 14''

Distance Center to Center of Bearings in	Th	ickne	ss of in I	Flan	ge i.	Th		ss of in In		ge Pl	ate
Feet.	38	1/2	5/8	3	7 8	3/8	1/2	5/8	13	7 8	1
40	143	172	199	226	251	269	291	312	334	356	377
41	140	168	195	220	245	262	284	305	326	347	368
42	137	164	190	215	239	256	277	297	318	339	359
48	133	161	186	210	234	250	270	290	311	331	351
44	130	156	181	205	228	244	264	284	304	323	343
45	127	153	177	201	223	239	258	277	297	316	335
46	125	149	173	196	218	234	253	271	290	309	328
47	122	146	170	192	214	229	247	266	284	303	321
48	120	143	166	188	209	224	242	260	278	296	314
49	117	140	163	184	205	220	237	255	273	290	308
50	115	138	160	181	201	215	233	250	267	285	302
51	112	135	156	177	197	211	228	245	262	279	296
52	110	132	153	174	193	207	224	240	257	274	290
58	108	130	150	171	190	203	219	236	252	268	285
54	108	127	148	167	186	200	215	231	247	263	280
55	104	125	145	164	183	196	211	227	243	259	274
56	102	123	142	161	179	192	208	223	238	254	270
57	101	121	140	159	176	189	204	219	234	250	265
58	99	119	138	156	173	185	200	215	230	245	260
59	97	117	135	153	170	182	197	212	226	241	256
60	96	115	133	151	167	179	194	208	223	237	252
61	94	113	131	148	165	176	191	205	219	233	247
62	92	111	129	146	162	173	187	201	215	229	243
63	91	109	127	143	159	171	185	198	212	226	240
64	90	107	125	141	157	168	182	195	209	222	236
65	88	106	123	139	155	165	179	191	205	220	232
66	87	104	121	137	152	163	176	189	202	216	229
67	86	103	119	135	150	160	173	186	199	213	225
68	84	101	117	133	148	158	171	184	196	210	222
69	83	100	116	131	146	156	168	181	194	207	219
70	82	98	114	129	143	154	166	178	191	204	216
Weight per Foot in Pounds.	128.6	144.2	159.4	173.8	188.2	215.4	227.3	239.2	251.1	263.0	274.9

The safe loads below include the weight of the girder and are calculated for a fibre stress of  $15\,000$  pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for  $\frac{1}{2}$ 6" rivets) from both flanges.

Web Plate 60" × 3/8"

Flange Angles  $6'' \times 6''$ 



Web Plate  $60'' \times \frac{3}{8}'''$ Flange Angles  $6'' \times 6'' \times \frac{3}{8}'''$ Flange Plates 14''

Distance Center to Center of Bearings in	Th	ickne ngles	ss of in I	Flan	ge i.	Thickness of Flange Plate in Inches.					
Feet.	38	1/2	5 8	3/4	7/8	1/2	58	34	7/8	1	14
40	160	194	227	259	290	323	345	366	388	410	453
41	157	190	222	253	283	316	336	357	379	400	442
42	153	185	217	247	276	308	328	340	370	390	431
43	149	181	212	241	270	301	321	341	361	381	421
44	146	177	207	236	264	294	314	333	353	372	412
45	143	173	202	230	258	287	307	326	345	364	403
46	140	169	198	225	252	281	300	319	338	356	394
47	137	165	194	221	247	275	294	312	330	349	385
48	134	162	190	216	242	269	287	305	323	341	377
49	131	159	186	212	237	264	282	299	317	334	370
50	128	156	182	207	232	259	276	293	311	328	362
51	126	152	178	203	227	254	270	287	304	321	355
52	123	150	175	199	223	249	265	282	298	315	348
53	121	147	172	196	219	244	260	277	293	300	342
54	119	144	168	192	215	240	255	271	287	303	335
55	117	141	165	188	211	235	251	268	282	298	329
56	115	139	162	185	207	231	246	262	277	293	323
57	113	136	160	182	203	227	242	257	272	287	318
58	111	134	157	179	200	223	238	253	268	282	312
59	109	132	154	176	197	219	234	248	263	278	307
60	107	130	152	173	193	216	230	244	259	273	302
61	105	127	149	170	190	212	226	240	254	269	297
62	103	125	147	167	187	209	222	236	250	264	292
68	102	123	144	165	184	205	219	232	246	260	288
64	100	121	142	162	181	202	216	229	243	256	283
65	99	120	140	159	178	199	212	225	239	252	279
66	97	118	138	157	176	196	209	222	235	248	274
67	96	116	136	155	173	193	206	219	232	245	270
68	94	114	134	152	171	190	203	215	228	241	267
69	93	113	132	150	168	187	200	212	225	237	263
70	92	111	130	148	166	185	197	209	222	234	259
Weight per Foot in Pounds.	139.0	157.8	176.2	194.2	211.8	247.7	259.6	271.5	283.4	295.3	319.1

#### GRILLAGE BEAMS FOR FOUNDATIONS.

In designing foundations for walls or columns carrying heavy loads resting upon the soil, it is necessary to distribute the weight over a suitable area, and this is readily accomplished, in a small depth, by using a grillage composed of steel beams imbedded in concrete, thus obviating the necessity of large masses of masonry and deep excavations. For heavy loads on soil of small bearing power three tiers of beams may be necessary, while for lighter loads and soil of greater bearing power two tiers of beams will ordinarily suffice.

The grillage beams which are to be surrounded by concrete should be spaced not less than 3" apart in the clear between the flanges, so that the concrete may be thoroughly rammed between them, and gas-pipe, or standard cast-iron separators should

be used to maintain the beams in proper position.

Knowing the total weight to be carried and the allowable intensity of loading per square foot of the supporting soil, the area of the footing required can be readily found, which, taken into consideration with any other conditions limiting the form or proportions of the footing, will determine the external dimensions of the foundation. The beams may be considered as subjected to a uniform load extending over a portion of their upper surfaces, the center of which is at the center of length of the beams, and as being uniformly supported from below throughout their length.

Under these circumstances, the maximum bending moment will occur at the center of the beam and, using the notation given for the upper tier in the sketch below, this bending moment for one beam will be as follows:

Bending moment in inch pounds =  $\frac{1}{2}$  (c - b)

in which c and b are expressed in inches and W is the total weight in pounds on one beam, obtained by dividing the total load by the number of beams composing

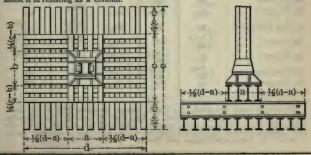
the tier in question.

This formula for the bending moment is the same as that for a beam of the length (c — b) supported at the ends and uniformly loaded with the total weight W, so that the proper sizes of beams, bending considered, may be obtained directly from the tables of safe loads uniformly distributed for Cambria I-Beams, on pages 106to 117 inclusive, or for cases in which the lengths are shorter than those given in these tables, the sizes may be calculated from the coefficients of strength or the section moduli given in the tables of properties of L-Beams, pages 182 to 185 inclusive, taking care, however, to use as the length, the distance (c — b), for the upper tier, and the corresponding figures for the other tiers.

· After determining the size of beam required based upon bending, as stated above, an examination should also be made of the capacity of the beam web to resist buckling. This may be done by considering the web as a column of height equal to the clear distance between the fillets and calculating the safe load therefor by the use of the tables of strength for steel columns or struts, on pages 218 to 221, using the

proper safety factor.

If the beam web is found insufficient as a column when calculated in this manner, a beam with a web of greater thickness should be tried until one is found that will meet this requirement and the conditions for bending; or it might be more economical, in some cases, to use the beam with the thinner web and provide it with sufficient separators, fitting between the beam flanges, or stiffeners secured to the web to assist it in resisting as a column.



#### EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES. Live Loads for Floors in Different Classes of Buildings, Exclusive of the Weight of the Materials of Construction.

(Revised to 1917.) Pounds per Square Foot.

		Dwell's, Apart- ments, Hotels,	Office Bu	ildings.	Schools or	Buildings for
No.	City.	Tenements or Lodgings.	First Floor.	Upper Floors.	Places of Instruction.	Public Assembly.
1 2	Atlanta	60	150	75	75	90
3	Baltimore	60 100(b)	150	75	75 ∫125(c)	75(a), 125
9	Boston	50	100	100	60	125
4	Buffalo	40(d) 70	70	70	100	100
5	Chicago	50(e)	50	50	75	100
6	Cincinnati	40	100	50	80	100
7	Cleveland	{ 60(u) 80	125	180	80(a) 125	{125(c) 100
8	Denver	40 50(h)	70	70	50(a)	80(a) 120(f)
9	Detroit	80(f) 50	125	75	{100(c) 75	80(a)
	Hartford	50	100	100	1	120
11	Jersey City	(105(4)	150	75	75	90
12	Los Angeles	{125(t) 60	75	75		125
13	Louisville	60	150	75	75	100
14	Milwaukee	30	80	40	{ 40 60	80 50(a)
15	Minneapolis	50	100	75	100	125
16	Newark, N. J	60	150	75	75	90
17	New Haven	{100(g) 60			75	110
18	New Orleans	70(b)	70	70	{125(c) 60	125
19	New York	40	60	80	75	100
20	Philadelphia	70	100	100		120
21	Pittsburgh	{ 50 70(h)	70	70	70	125
22	Portland, Ore	80(f) 50	100	60	80(c) 60	80(a)
28	Providence	100(b) 50	150	75	{125(c) 60	25
24	Rochester	60(h)	70	70	, 70	70
25	St. Louis	60	150	70	100	100
26	St. Paul	50	125	60	{125(c) 60	125
27	San Francisco	60	60	60	{125(c) 75(a)	75(a) 125(c)
28	Seattle	{ 75(b) 40	125	50	100(c) 75	75(a)
59	Syracuse	60	{100(g) 75	{100(g) 75	90(c) 75	80(a)
30	Washington	∫ 75(g)	110(g)	110(g)	75	110
31	Worcester, Mass	50 60	125	75	75	125
01	Wordester, Wass	DO	120	10	10	140

<sup>(</sup>a) Where seats are fixed; (b) Public rooms exceeding 500 sq. ft. area; (c) Assembly rooms; (d) Occupied by less than 25 persons; (e) Sleeping accommodations for 20 or more persons; (f) First floor—Hotels, Tenements and Lodging Houses; (g) Rooms and spaces for public use or common use of tenants; (h) Tenement Houses and Hotels.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.
Live Loads for Floors in Different Classes of Buildings, Exclusive of
the Weight of the Materials of Construction.

(Revised to 1917.) Pounds per Square Foot.

Stables		Ord. Stores,	Stores (Heavy	Ro	ofs,		1
Carriage Houses.	Garages.	Light Manu- facturing, Light Storage.	Materials,) Warehouses, Factories.	Slope <20°.	Slope >20°.	Side- walks.	No.
75 100		120 125	150 250(k), 175	40(i) 40(i)	30(j) 20(j)(l)	200 200	1 2
		125	250	40(m)	20()(1)	200	8
'40 (n)		120	150	40(j)	40(j)		4
f 40 (o)	\$ 40(o)	100	100	25(j)	25(j)		5
100	100	100	150	25(j)	25(j) 25(j)	300	6
80	{ 100 150(q)	125(q)	200	35(m)		200	7
	( 190(d)	150	150	40	20		В
(a)(b)	∫ 60(p)		∫ 200(s)				
{ 60(p) 80	80	(130(r), 100	175	40	40	250	9
75		125 120	125 150	50(i) 50(i)	50(i) 30(j)	300	10
*******		150	150	{ 20(v)(u) 30	{ 20(v)(u) 30		12
100	100		150	40	30(j)	300	13
80	80	100	• • • • • • • • • • • • • • • • • • • •	30	30	150	14
85 75	100	100 120	150	30(i) 50(i)	30(i) 30(j)	300(j) 300	15 16
***************************************		120	150	40(i)	40(i)	300	17
		125	200		20(1)	300	18
120	120	120	120	30(m) 40	30(j)	300	19
		120	150	30	30		20
• • • • • • • • • • • •		125	200	{ 50(j) 40(m)	50(j)		21
80		{ 125(q) 100	200	49	. 40	300	22
		125	250	40(m)			23
{ 50(n) 100	{ 50 (n) 100	100	200	40(j)	40(j)		24
	( 100	150	150	40(m)			25
85		100	200	30(j)	30(j)	300	26
75		125	250	30(i)	20(j)	150	27
75	125	125		40(j)	40(j)		28
80	125	125	200	40	40	250	29
		110	150	25(i)	25(i)		30
125	125-175	125	200	50(i)	30(i)	300	31
							-

<sup>(</sup>i) Per square foot of surface; (j) Per square foot, measured horizontally; (k) Heavy storage; (l) Where used for public assembly or special purpose use same load as floors; (m) Flat; (n) Private; (o) Ground area less than 500 sq. ft.; (p) Small; (q) 1st floor; (r) Light storage and manufacturing; (s) Heavy Merchandise storage; (t) Hotel corridors; (u) Dwellings; (v) Sheds and outbuildings.

#### ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.

(Revised to 1917.)

	1 100	1000	Tens	ion.	
No.	Oity.	Rolled Steel.	Cast Steel.	Wrought Iron.	Cast Iron.
1234	Atlanta	16 000 16 000 16 000 16 000	16 000 16 000 16 000 16 000	12 000 12 000 12 000 12 000 12 000	3 000 5 000 3 000
5678	Chicago Cincinnati Cleveland Denver	16 000 16 000 16 000 16 000	16 000 16 000	12 000 12 000 12 000 12 000	3 000
9 10 11 12	Detroit Hartford(f) Jersey City Los Angeles(e)	16 000(d) 16 000	16 000(d) 16 000	12 000 12 000	3 000
13 14 15 16	Louisville. Milwaukee Minneapolis. Newark, N. J	16 000 16 000 16 000 16 000	16 000 16 000 16 000 16 000	12 000 12 000 12 000 12 000	3 000 3 000
17 18 19	New Haven. New Orleans. New York. Philadelphia	16 000 16 000 16 000 14 500(c)	16 000 16 000	12 000 12 000	3 000 3 000
21 22 28 28	Pittsburgh Portland, Ore. Providence(e) Rochester	16 000 16 000 16 000	16 000 16 000	12 000 12 000 12 000	3 000
25 26 27 28	St. Louis(f) St. Paul San Francisco Seattle	16 000 16 000 16 000	16 000 16 000 16 000	12 000 12 000 12 000	3 000
29 30 31	Syracuse Washington Worcester, Mass	16 000 16 000 16 000	{ 10 000(b) 16 000(a) 16 000 16 000	12 000 12 000	3 000 3 000 3 000

<sup>(</sup>a) Annealed; (b) Not annealed; (c) Mild Steel; (d) Medium Steel; (e)

#### ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.

(Revised to 1917.) Pounds per Square Inch.

	Steel.	CBL	Head	Wrought In	on.	Cast	Iron.	No.
Relled Beams.	Rolled Pins, Rivets and Bolts.	Riveted Beams Net Flange Section.	Rolled Beams.	Rolled Pins, Rivets and Bolts.	Riveted Beams Net Flange Section.	Compress- ion Side.	Tension Side.	No.
16 000 16 000 16 000 16 000	20 000 20 000 22 500	14 000 15 000	12 000 12 000 12 000	15 000 15 000 18 000	12 000 12 000	16 000 16 000 16 000 13 000	3 000 5 000 3 00 · 3 000	1234
16 000 16 000 16 000	25 000 24 000 24 000	16 000 16 000 16 000	12 000 12 000 12 000		12 000 12 000	10 000 16 000		5078
16 000	20 000	16 000 14 000	12 000	15 000	12 000 12 000	16 000	3 000	10 11 12
16 000 16 000 16 000 16 000	20 000 25 000 20 000	15 000 16 000 14 000	12 000 12 000 12 000	15 000 15 000	12 000 12 000	16 000 10 000 16 000	3 000 3 000 3 000	18 14 18 16
16 000 16 000 16 000	20 000 22 000 20 000	16 000 16 000	12 000 12 000	15 000 18 000	12 000	16 000 16 000	3 000 3 000 3 750	15
16 000 16 000	24 000 20 000 20 000	16 000 15 000 14 000	12 000 12 000	15 000 15 000	12 000 12 000	16 000 16 000	3 000	2122
16 000 16 000 16 000	20 000	14 000 15 000 16 000	12 000	15 000	12 000 12 000	16 000	3 000 3 000 3 000	200
16 000 16 000	20 000 20 000 20 000	16 000 14 000 16 000	12 000 12 000	15 000 15 000	12 000 12 000	16 000 16 000 16 000	2 500 3 000 3 000	30

Determined by the best modern practice; (f) Building Laws being revised, 1917.

#### ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.

(Revised to 1917.)

	1			Comp	ression.		
No.	City.	Rolled Steel.	Cast Steel.	Wrought Iron.	Cast Iron (in short blocks).	Pins and Rivets Bearing.	Wrought Iron Pins and Rivets Bearing.
1 2 3 4	AtlantaBaltimoreBostonBuffalo	16 000 16 000 16 000	16 000 16 000 16 000	12 000 12 000 12 000	16 000 16 000 16 000 15 000	20 000 20 000 18 000 15 000	15 000 15 000 15 000 15 000
5 678	Chicago Cincinnati Cleveland Denver	14 000(a) 16 000	14 000(a) 16 000 16 000	10 000(a) 12 000 12 000	10 000(a) 16 000	(20 000(f) (25 000(s) 20 000 20 000 18 000	12 000(t) 15 000
9 10 11 12	Detroit  Hartford(l) Jersey City Los Angeles(j)	(b) 16 000	(b)	75%Steel	(b)	\$15 000(f) \$20 000(s) \$20 000	12 000(t)
13 14 15 16	Louisville Milwaukee Minneapolis Newark, N. J.	16 000 12 000(a) 16 000 16 000	16 000 12 000(a) 16 000 16 000	12 000 10 000(a) 12 000 12 000	16 000 8 000(a) 16 000 16 000	20 000 20 000(k) 18 000 20 000	15 000 15 000 15 000
17 18 19 20	New Haven New Orleans New York Philadelphia	16 000 16 000 16 000 (14 500(c) (16 250(d)	16 000	12 000 12 000 12 500	16 000 11 670	20 000 18 000 24 000 \$17 600(f) 122 000(s)	15 000 15 000 15 000 (14 400(f) (18 000(s)
21	Pittsburgh Portland, Ore. Providence (j)	16 000 16 000	16 000 16 000	12 000 12 000	12 000 16 000	20 000(f) 24 000(s) 20 000	20 000(t) 15 000
24 25 26 27	St. Louis(1) St. Paul San Francisco	16 000 16 000 16 000	16 000 16 000 16 000	12 000 12 000 12 000	16 000 16 000 16 000	20 000 20 000 20 000 (20 000/f)	15 000
28 29 30 31	Syracuse Washington Worcester	16 000 16 000 16 000 16 000	16 000 {10 000(g) 16 000(e) 16 000 -16 000	12 000 12 000 12 000	10 000(a) 10 000(g) 16 000 16 000 16 000	\$20 000(f) \( 24 000(s) \) \$16 000(h) \( 20 000 \) \( 20 000 \) \( 20 000 \)	15 000 15 000

<sup>(</sup>a) Based on gross section; (b) Based on values given by standard steel manufacturer's handbook; (c) Mild steel; (d) Medium steel; (e) Annealed; (f) Field rivets; (g) Not annealed; (h) Field rivets driven by hand;

ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.

(Revised to 1917.)

			SI	hear.					
	Stee	ıl.			Wrough	it Iron.			No.
Web Plates,	Shop Rivets and Pins.	Field Rivets.	Field Bolts.	Web Plates.	Shop Rivets and Pins.	Field Rivets.	Field Bolts.	Cast Iron.	
9 000 9 000 10 000 7 000	10 000 10 000 10 000 9 000	8 000 8 000 10 000 8 000	7 000 7 000 8 000	6 000 6 000 9 000 6 000	7 500 7 500 9 000 7 500	6 000 6 000 9 000 6 000	5 500 5 500 7 200	3 000 3 000	1234
10 000(a) 10 000 10 000 9 000	12 000 10 000 10 000 10 000	10 000 9 000 7 000	7 500 6 000	6 000	6 000 7 500	6 000	6 000	2 000(i) 3 000	5 678
10 000	10 000	7 500 10 000	6 000 7 000	6 000	7 500	6 000	5 500	3 000	9 10 11 12
9 000 10 000 10 000 9 000	10 000 10 000 9 000 10 000	8 000 8 000 6 750 8 000	8 000 7 000 7 000	6 000 6 000	7 500 7 500 7 500	6 000 6 000	5 000	2 500 2 000(i) 3 000	13 14 15 16
10 000 10 000 10 000 { 8 750(c) { 10 000(d)		8 000 10 000 8 000 8 800	8 000 7 000	6 000 9 000 7 500	7 500 9 000 9 000	6 000 9 000 7 200	7 200	3 000	17 18 19 20
10 000 9 000 9 000	12 000 10 000 10 000	10 000 8 000 8 000	10 000 7 000 7 000	6 000	7 500 7 500	6 000	5 500 5 500	3 000	21 22 23 24
9 000 9 000 10 000(a)	10 000 10 000 12 000	8 000 8 000 10 000	7 000	6 000 7 000	7 500	6 000	5 500	3 000 2 000(i)	25 26 27 28
10 000 9 000 10 000	10 000 10 000 10 000	8 000(h) 10 000(k) 8 000 8 000	7 000 7 000 7 000	6 000 6 000	7 500 7 500	6 000 6 000	5 500 5 500	2 000 3 000 3 000	29 30 31

<sup>(</sup>i) Brackets; (j) Based on best modern practice; (k) Power driven; (l) Building Laws being revised, 1917; (s) Shop rivets; (t) Bearing on steel bolts.

ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.
(Revised to 1917.) Pounds per Square Inch.

				Columns.		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
37.	(C.A	Steel. ·		Cast Iron.		Wrought Ir	on.
No.	City.	Formula.	MAI. Length L=	Formula.	Max. Length L=	Formula,	Max. Length L=
1	Atlanta	(A)	120 R	(B)	70 R	(C)	120 R
2	Baltimore	Soft Steel (E) Medium " (F)	120 R	<50 R—10 000 > " (G)	60 R		
8	Boston	(H)	120 R	(B)	70 R	(I)	-
4	Buffalo	{<90 R-12 000 > " (J)	40 D	Round (M) Rectangular (N)	30 D	{<90 R-8 000 > " (K)	40 D
5	Chicago	(O) 14 000 max.	120 R	(Q)	70 R	(P) 10 000 max.	=,
6	Cincinnati	{<70 R-13 000 > " (J)	180 R	Round (T) Rectangular (S) Others (U)	180 R		
8	Cleveland(f). Denver	(f) (J)	120 R	(f) (EE)	30 D 30 D	(f) (K)	
9	Detroit	\$\left\{ \left\{ \text{R} \cdot \text{R} \cdot \text{R} \cdot \text{R} \cdot \text{2} \text{ 000} \\ \right\{ \text{CO}(\text{b})} \end{array}}\$	44 D	Round (T)	30 D	75% Steel	
10 11 12	Hartford(e) Jersey City LosAngeles(d)	(A)	120 R		70 R	(C)	120 R
13	Louisville	{ \$70 R-13 000 (CC)	120 R	Round (T) Rectangular(S) Others (U)	120 R		
14	Milwaukee	(J)	120 R	(Q)	25 D	(P)	120 R
15	Minneapolis	(J)	40 D	Round (V)	30 D	(K)	40 D
16	Newark, N.J.	(A)	120 R	(B)	70 R	(C)	120 R

L = Length in inches; R = Radius of Gyration in inches; D = Diameter or Least Dimension in inches,

FORMULÆ:—

(A) 
$$15\ 200-58\frac{L}{R}$$

(B)  $11\ 300-30\frac{L}{R}$ 

(C)  $14\ 000-80\frac{L}{R}$ 

(B)  $11\ 300-80\frac{L}{R}$ 

(C)  $14\ 000-80\frac{L}{R}$ 

(D)  $11\ 000-80\frac{L}{R}$ 

(E)  $11\ 000-80\frac{L}{R}$ 

(I)  $11\ 000-80\frac{L}{R}$ 

(II)  $11\ 000-80\frac{L}{R}$ 

#### ALLOWABLE UNIT STRESSES FOR STEEL AND IRON.

(Revised to 1917.)

Pounds per Square Inch.

				Columns			
	624	Steel		Cast Iron		Wrought Iron	
No.	City	Formula	Max. Length L=	Formula	Max. Length L=	Formula	Max. Length
17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	New Haven New Orleans New York Philadelphia Pittsburgh Portland, Ore Providence Rochester St. Louis St. Paul San Francisco Seattle Syracuse Washington Worcester	(H) (O) (Mild Steel (X) (Med'm" (Y) (GG)Max.13000 (A) (A)	120 R	(B) (BB) (Z) (HH) Max. 9000 (B) (II) (T) (Round (EE) (Rectangular(FF) (Q) (BB)	20 D 70 R 70 R 20 D 70 R 70 R 70 R 25 D 20 D 70 R 70 R	10 000(c) (I) (AA) (C) (C) (P)	140 D 120 R 120 R 120 R 140 R 120 R 120 R 120 R

L = Length in inches; R = Least Radius of Gyration in inches; D = Diameter or Least Dimension in inches.

FORMULÆ (continued):-

FORMULÆ (continued):—
(S) 
$$\frac{10\ 000}{1+\frac{L^2}{1067\ D^2}}$$
 (X)  $\frac{14\ 500}{1+\frac{L^3}{13\ 500\ R^2}}$  (CC)  $17\ 000-57\ \frac{L}{R}$  (DD)  $15\ 000-50\ \frac{L}{R}$  (DD)  $15\ 000-50\ \frac{L}{R}$  (DD)  $15\ 000-50\ \frac{L}{R}$  (DD)  $15\ 000-50\ \frac{L}{R}$  (EE)  $\frac{8\ 000}{1+\frac{L^2}{800\ D^2}}$  (U)  $\frac{10\ 000}{1+\frac{L^2}{6\ 400\ R^2}}$  (Z)  $\frac{11\ 670}{1+\frac{L^2}{400\ D^2}}$  FF)  $\frac{8\ 000}{1+\frac{L^2}{1\ 067\ D^2}}$  (V)  $\frac{13\ 330}{1+\frac{L^2}{400\ D^2}}$  (AA)  $\frac{12\ 500}{1+\frac{L^2}{15\ 000\ R^2}}$  (GG)  $19\ 000-100\ \frac{L}{R}$  (W)  $\frac{13\ 330}{1+\frac{L^2}{500\ D^2}}$  (BB)  $9\ 000-40\ \frac{L}{R}$  (II)  $11\ 100-220\ \frac{L}{R}$ 

(c) Coefficients for use with Gordon's Formula. (d) Based on best modern practice. (e) Building Laws being revised, 1917. (f) See Building Laws.

Allowable Unit Stresses for Masonry and Building Materials.
(Revised to 1917.) Pounds per Square Inch.

					Com	pression	1.		
			Concre	te.				tonework.	
No.	City.	Portland Cement 1:2:4	Portland Cement 1:2:5.	Rosendale Cement 1:2:4.	Rosendale Cement 1:2:5,	Portland Cement Mortar	Rosendale Cement Mortar.	Lime and Coment Mortar.	Lime Nortar.
1	Atlanta	230	208	125	111	140	111	97	70
2	Baltimore	400	350	125	111	125	100	70	50
3	Boston	417							
4	Buffalo	56 (a)	56 (a)			70			
5	Chicago	(400 (d) (350 (e)	$\begin{cases} 350(d,f) \\ 300(e,f) \end{cases}$		150	{200 (b) 100 (c)			{120 (b) 60 (c)
6	Cincinnati	208	208			167	125		83
7 8	Cleveland Denver	400 56	350(h) 139				167		56-111
9	Detroit	417	417	111	111	139	111	{ 83 97(g)	70
10	Hartford	153	153						
11	Jersey City	230	208	125	111	140	111	97	70
	Los Angeles	278(a)	278(a)				167		
14	Milwaukee	400	{ 250(k) 300(f)	111	83	175	125	97	90
15	Minneapolis.	{ 500(i) 300	208(h)			167	125	111	83
16	Newark, N. J.	230	208	125	111	140	111	97	70
17	New Haven	208(a)	208(a)						
18	New Orleans.								
19	New York	500	400(f)	210	150(f)	140	110	100	
	Philadelphia.	208	208			139		111	70
22	Pittsburgh(j). Portland, Ore.	347	278(k)			∫ 208(b)		{ 167(b)	{ 139(b)
	Providence	222	195	111	83	167(c) 139(c) 153(b)	{ 125(b) 97(c)	139(c) 97(b) 70(c)	83(c) 83(b) 56(c)
24	Rochester	230	208	125	111	140	111	97	70
25	St. Louis	250(h)							
26	St. Paul	500	400	125	111	200	100	125(g)	80
27	San Francisco	277	277			( 200(b)			(120(b)
28	Seattle	400	350(f)			(100(c)			60(c)
_	Syracuse	400	900	100	80	110			
	Washington Worcester	400 278	320 208(k)	125 111	111	140 139	111	97 97	70 70

<sup>(</sup>a) Foundations; (b) Coursed; (c) Ordinary; (d) Machine-mixed; (e) Handmixed; (f) 1:2½:5; (g) Portland Cement Mortar; (h) 1:3:5; (i) 300 where height is 12 diameters; 500 for 5 diameters or under; intermediate heights, intermediate values; (j) Based on best modern practice; (k) 1:3:6.

EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES.

Allowable Unit Stresses on Masonry and Building Materials.

(Revised to 1917.)

Pounds per Square Inch.

-				C	omp	ress	ion						_
Portland Cem. Mor-	Rosendale Cem. Mor- tar 1:3	Lime and Den. Mor- tar 1:1:6	Lime Mortar 1:4	Granites (per Test)	Greenwich	Gnoise	Limestone (per Test)	Marble (per Test)	Sandstone (per Test)	Rluestone	Hard-burned  Brick,flatwise	Slate	No.
250	208	160	111	\$1000- 2400 1000-		1200	{ 700- 2300	600- 1200 1000-	{ 400- 1600	2000	_	1000	
250 {278 q 250 r	208 r	1139 r		(2400 833			1000 556	2000 556	400 n	1500 m			3
167 q {350 v {175 u	{125 t 70 u 150	125	83 t 42 u 100	600					400				5
250 200 125	167 175 125	150	111 100 40	1000- 2400 1000 560			600		\$\begin{cases} 400-\ 1600 \ 400 \ 167 \end{cases}\$				6 7 8
208 208 t	208 t	-	97 111 t	(1000-			1 700-	1 600-	400-				9
250 208 250 \$180	208 208 167 (139	160	111 111 111 5 83	2400		1200		1200	1600	2000	300	1000	11 12 13 14
208 250	(160 t  208	160 160	111 111	{1000- 2400		1200	} 700− {2300	{ 600- 1200	∫ 400- 1600	2000	300	1000	15
208 {250 q {167 u		160	111 {125 q 83 u	830			550	550	415				17 18
250 208 (167 u	210	160 167 / 139 u	110	1000	1200	1000	700	600	400	2000		1000	19 20 21
1222 v 1181 u	139 u 167 v	167 v	139 v										22
250 300 250	208 210 208	160  225 g	111 120 111	{1000- 2400 /1000-	1200			{ 600- 1200 ( 600-	{ 400- 1600		300	1000	25
208 175 v	208	139 125 v	97	12000 389y 800y			400	1200	1600 235- 350		300		26 27 28
250 250	175	160 g	111	{1000- 2400 "		1300	{ 700- {2300 "	{ 600− 1200 "	{ 400- 1600	2000 2000		1000 1000	30
208	167	139	111	-		1200	66	45	4	2000	300	1000	31

<sup>(</sup>l) Mortar 1:3; (m) Falls Road Stone; (n) Cement Stone; (o) Mortar 1:2; (p) Mortar 1:6; (q) Hard-burned Brick—first-class work; (r) Same—Ordinary work; (t) Hard-burned Brick; (u) Common Brick; (v) Higher values for special Brick; (w) Local; (x)Medina—2000; (y) Granite Masonry.

### EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES. FROM THE BUILDING IN MASONRY, Etc. Allowable Unit Stresses for Masonry, Etc. Pounds per Square Inch

(Revised to 1917.) Extreme Fibre Stress (Bending). No. City. Greenwich Granite. Gneiss. Limestone. Marble. Slate. Stone. 1,16 Atlanta, Newark
11 Jersey City....
Worcester....
Baltimore.... 180 150 150 400 120 180 150 150 50 180 150(b) 400 120 180 150 400 120 29 Syracuse .....

### Safe Bearing Capacity of Soils, Etc.

150

400

		1	ons per	Square	Foot.			
			Ordinary Clay and	Loam,	Very Firm		tone, Brick in Caisson	18.
No.	City.	Soft Clay.	Sand, in Layers, Wet and Springy.	Firm and Dry.	Coarse Sand, Stiff Gravel or Hard Clay	down to Rock.	down to Firm Gravel or Hard Clay.	to Rock.
1	Atlanta	I	2	2-3	3-4	15	8-10	8
23	Baltimore	Î	2	3	6(a), 4	20-24	12-18(d)	
	Boston							
4	Buffalo				31/2			
Б	Chicago		11/2	13/4-21/2				
6	Cincinnati	1	1-2	4				
7	Cleveland		11/2	2-4	3-8	10(h)		
8	Denver	$\frac{1}{2}(g), 1$	1-2	3	4,8(d)			
11	Detroit Jersey City		2 2	3	4	15	10	
12	Los Angeles	1 2	1 e	2-4	1 1			0
13	Louisville	1-3		21/2	4			
10		_		4/2	(4-5(c)			
14	Milwaukee	{ ½(g)	2	3	6(d)			
			1		20(h)			
15	Minneapolis Newark, N. J New Haven	1	2	3	4			
16	Newark, N. J	1	2	3	4	15	10	8
17	New Haven				4(f)			
18	New Orleans	0.7						
19	New York	1	2		4-6	8-40		
20	Philadelphia							
21	Pittsburgh							
22	Pittsburgh Portland, Ore	1/2(8)	3	78	8(c)			
		1/2(0)						
28	Providence	1 2 (8)	2-3	2-5	4-10(c)	25-50(h)		10-15(d)
24	Rochester	1	2	3	10(c), 6	15	10	8
26	St. Paul	1	2 2	3	6(a), 4			
27	San Francisco	1	2	3	6(a). 4	20(h)		10(d)
28	Seattle	1	2	21/2	8(c) 3½-5			
29	Syracuse	1	2		1 3/2-3			
30	Washington		2	3	1			
00	1	-	- 4					

<sup>(</sup>a) Coarse Gravel; (b) Local; (c) Well cemented; (d) Bearing—Hardpan or Hard Shale rock unexposed to air, frost and water; (e) Sandy loam; (f) Good, solid, natural earth: (g) Quicksand or alluvial soil; (h) Bearing—Very hard, native bed rock.

#### EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES. Allowable Unit Stresses for Masonry, Etc. (Revised to 1917.) Pounds per Square Inch.

Extreme Fibre Stress (Bending). Resendale Concrete. | Brick-No. Portland Concrete. Brickwork Sand-Blue-1:2:4. 1:2:5. 1:2:4. | 1:2:5. Hardburned in Cement. stone. stone. 1,16 11 31 100 300 30 20 16 10 50 30 100 26 50 35 25(k)30(l) 100(j) 50(i) 300 30 20 16 10 100 30 20 16 10 50(i) 30 100 300 

#### Allowable Safe Loads and Sizes for Wooden Piles.

Spa	eing	Min	imum Dian	ieter.	Safe Loa	d-Tons.	Concrete	Capping.	
Maxi- mum C. to C. in inches.	Mini- mum C. to C. in inches.	Of Small End. Inches.	Of Butt. Lengths = <20ft. Inches.	Of Butt. Lengths >20 ft. Inches.	Formula for Single Pile.	Not to exceed per Pile	Thickness Rammed Between Heads. Inches.	Width Outside of Piles. Inches.	No.
36	20	5	10	12	(D)	20	12	12	1
36	24	8(m),6		10			12(n), 6 16(n)		3
36	24	6	12	12		25	12	12	123456789
		6			(D)&(S)	25			8
		6					12	12	7
36	24	5	12 10	12	(D)	25 25	12 10	12 12	8
					(D)	7-20	12	12	11
36	20	5	10	12	(D)	20			12 13
30	20	9	10						
		0			(D)&(S)	500(p)			14
36 36 36	20 20	5 5 6	10 10	12 12	(D) (D)	20 7-20 20	12 12 12	12 12 12	15 16 17
30		5	10	12			6(n), 12	0	18
36	20	6	10(q)	12(q)	(D)&(S)	20	12		19
30		5 6			(D)&(S)	20 20	12	12	20
		6	12	12	(D)	25	6	12	22
					(-)				1
36	24					12	12	12	23
36	20	5	10	12 12	(D) (D)	20 25	12 9(n), 9	12 12	24
	12(o)	7				25	12(n)		27
	24	8	12	12	(D)&(S)	25	{ 6(n)	12	28
		6	10	10	(D)	10-15	9	12	29
									30

<sup>(</sup>i) Common; (j) Medina; (k) 1:3:6 mixture; (l) 1:21/2:5 mixture; (m) Length (0) Common; (1) Medina; (1) 1:5-0 mixture; (1) 1-22-2 mixture; (11) Por -201f.; (n) Capping, on top of heads; (o) In clear between piles; (D) For Drop Hammer, 2WH ...; (S) For Steam Hammer, 2WH where W=Weight of Drop Hammer,  $\frac{2WH}{P+1}$ ; (S) For Steam Hammer,  $\frac{2WH}{P+\frac{1}{1}}$ ; (S) For Steam Hammer,  $\frac{2WH}{P+\frac{1}{1}}$ ;

hammer in Tons; H=Height of drop in Feet; P=Penetration of last blow (or average of last several blows) in Ins.; (p) Pounds per sq.in.; (q) Lengths < or > 25 ft.

#### ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

				Comp	ression.		
No.	Oity.	Oa	ık.	Yello	w Pine.	White	Pine.
		With Grain.	Across Grain.	With Grain.	Across Grain.	With Grain.	Across Grain.
1234	Atlanta	900 1000 810(e) 800(c) 900	800 600 600(e)	1000 1000 900 1000(g) {1100(g,d) 800(f)	600 600 500	800 800 630 700 700(c)	400 400 250 200(c)
6 7 8 9 10	Cincinnati Cleveland Denver Detroit Hartford(q)	900 800(c) 1000	800 300	1000 1000 1250	600 350	800 700 875	400 300
11 12 13 14 15	Jersey City Los Angeles(a) Louisville Milwaukee	900 1000 1500(e) 800(e)	800 600 500(e)	1000 1000 1500(g) 1200(f) 1000(h)	600 (350(g) 300(f)	800 800 1100(d) 700	400 400 200(d)
16	Newark, N. J	1100	800	1500	800	800	400
18 19 20	New Haven(a) New Orleans New York Philadelphia	1400	1000	1600(g) 750	{ 400(f) 500(g) 1000(g) 550	1000(b,f)	800(b,f)
21 22 23 24 25	Pittsburgh(a) Portland, Ore Providence(a) Rochester St. Louis(q)	900	800		600	900(1) 800	200(1)
26	St. Paul San Francisco	1000	700	1100(h)	600(h)	900 800(1)	400 200(1)
28 29 30	Seattle Syracuse Washington	900	800 800	800(f,b) 1000(g) 1000	{ 400(f,b) 600(g) 600	800 800	400 400
31	Worcester(a)						

<sup>(</sup>a) Based on best modern practice; (b) Applies also to North Carollna Pine; (c) Also for Norway Pine; (d) Also for Douglas Fir; (e) White Oak; (f) Shortleaf; (g) Longleaf; (h) Also for Washington or Oregon Fir; (i) Douglas or Yellow Fir only.

#### ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

	-		Compre	ssion.			1	
Spr	uce	Locu	ıst.	Heml	ock.	Chestnut.		
With Grain	Across Grain	With Grain.	Acress Grain.	With Grain.	Across Grain.	With Grain.	Across Grain.	
800 800(b,k) 630	400 400(b,k) 250	1200 1200	1000 1000	<b>500</b> 600	500 500			1934
				700 500	150			5
800	400	1200	1000	500	500	500	1000	67
700 950(n)		850(m)		700 750	200	600(r)		10
800	400	1800	1000	500	500	500	1000	11
1100(o) 1000 800	(300(o) 200	1000(n) 760(n)	250(n)	600 900 600	500 200	600 1100(m)	1000 240(m)	13
800	400	1200	1000	600	500	500	1000	16
1200(d) 500	200(m) 800(d) 300	1200	1000	800 350	<b>600</b> 250	• • • • • • • • •		17 18 19 20
1500(i)	400(i)	1200(j)	250(j)					21
800	400	1200	1000	500	500	500	1000	25
800 800 800	400 200 300	1200 1600(i) 1600(i)	1000 300(i) 400(i)	500 900(j) 1400(p)	300 250(j) 350(p)	800	400	20
800(k)	400 400(k)	1200	1000	600	300	500	1000	28

<sup>(</sup>j) Red Fir only; (k) Also for Virginia Pine; (l) Also for Redwood; (m) Cypress only; (n) Norway Pine only: (o) Cedar; (p) Western Hemlock; (q) Building Laws being revised, 1917; (r) Colorado, Texas or Mexican Hemlock.

#### ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

		1	Extre	ne Fibr	e Stress	(Bendi	ng).	
No.	City.	Yellow Pine.	White Pine.	Spruce.	0ak.	Locust.	Hem- lock.	Chest- nut.
1234	Atlanta	1200 1800(1) 1500(1) 1800(1) {1000(s) 1300(1,m)	800 1000 1000 1080(b) 800(b)	800 1350(f) 1000	1000 1500 1000(d) 1350 1200	1200	1000 1000 1080 500	800
6 7 8 9 10	Cincinnati Cleveland Denver Detroit Hartford(u)	1200 1600 1260(a) 1250	800 1250 750	800 750	1000 1250 1170(w) 1000(d)	1200 950(e)	1000 1000 720(v)	800
11 12 13 14 15	Jersey City Los Angeles Louisville Milwaukee Minneapolis	1200 1620(c) 1200 (1500(s) (1800(l) 1620(a)	800 1260 (1200(e) 1000 1080(b)	800 1260 1000	1000 2160 1000 1500(d) 1350	1200 1300(h)	800 700 1080	800 1100(p)
16 17 18 19 20	Newark, N. J New Haven New Orleans New York Philadelphia	1500 1800 (1200(s) (1500(1) 1600(1) 1600(1)	800 1080 1200	800 1260  1200(m) 1100	1100 1350  1200	900(o)	800 900 900	800 1000(s,
21 22 23 24 25	Pittsburgh(k) Portland, Ore Providence(k) Rochester St. Louis(u)	1600(h) 1200	900	1000(i) 800	800(j) 1000	1200	600	800
26 27 28 29	St. Paul	1200(a) 1200(h) 1600(h) { 800(s)(g)	800 700	800 700 1000 800	1000 800(i) 1200	1200 750(j)	1400(t) 600	800
30 31	Washington Worcester(k)	(1200(I)) 1200	800(f)	800	1000	1200		800

<sup>(</sup>a) Also for Washington and Oregon Fir; (b) Also for Norway Pine; (c) Oregon Pine only; (d) White Oak; (e) Norway Pine only; (f) Also for Virginia Pine; (g) Also for North Carolina Pine; (h) Douglas Oregon Yellow Fir only; (i) Washington or Red Fir only; (j) Redwood only; (k) Based on best modern practice;

#### ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

			Tension.		
N	Hemlock.	Oak.	Spruce.	White Pine.	Yellow Pine.
	600 800	1000 1500	800 1200(f)	800 1000	1200 1800(l)
1	600	1200		800(b)	{1000(s) 1300(l)(m)
	600 (n)	1000	800	800	1200
. 1					
1	600	1000	800	800	1200
. 1		1000			1200
1	600(r)	1200(d)	800(m)(b)	700(q)	{1000(s) 1200(l)
. 1		1000	800	800	1200(a)
1	600	1000	800	800	1200
. 1					
1	600	1200	800(m)	700	{ 900(s) 1200(l)
2	1000		1250		1800(1)
. 2	700(j)		1000(i)	800	1300(h)
. 222	600	1000	800	800	1200
2	600	1000	800	800	1200(a)
2	700(j) 1400(t)	1000(i)	700	700	1200(h) 1600(h)
2	600	1000	800	800	f 800(s)
. 3		1000	800(f)	800	(1200(l) 1200
. 3					

<sup>(</sup>l) Longleaf; (m) Also for Douglas Fir; (n) Also for Chestnut; (o) Cypress only; (p) Cypress and Cedar only; (q) Also for Cedar; (r) Also Cypress;

<sup>(</sup>s) Shortleaf; (t) Western Hemlock; (u) Building Laws being revised, 1917; (v) Colorado or Mexican; (w) Also for Texas Pine, Spruce or Hemlock.

#### ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

				She	ar.		
No.	City.	Yellow	Pine.	White	Pine.	Spri	ace.
		With Fibre.	Across Fibre.	With Fibre.	Across Fibre.	With Fibre.	Across Fibre.
1 2 3 4	Atlanta	70 100(l) 100(l)	500 500(1)	40 85 80	250 350	50 90 80	320 350
5	Chicago	{120(s) 130(l)(c) 70	200	80(d)	250	40	250
7 8 9 10	Cleveland Denver(q) Detroit	150 100(l)	500	80	400	80	
11 12	Jersey City Los Angeles(e) Louisville	70	<b>500</b>	40	250	50	320
13 14 15	Milwaukee Minneapolis(r)	{150(s)(c) 175(l)	(1000(s) (1250(l)	{120(n) 100	500	125	750
16 17	Newark, N. J New Haven(e)	70 65(s)	500	40	250	50	320
18 19 20	New Orleans New York Philadelphia	70(l) 150(l) 100(l)	1000(1) 1125	50(f) 100	500	100 75	500 750
21 22 23 24 25	Pittsburgh(e) Portland, Ore Providence(e) Rochester St. Louis(q)	150(g) 70	500(g) 500	100	500 250	100(h) 50	600(h) 320
26 27 28 29 29	St. Paul. San Francisco Seattle Syracuse Washington	70(j) 150(g) 200(g) 50(s) 70(1)	500(j) 750(g) (300(s) (500(l)	50 100 50 40	250 500 300 250	50 100 130 50 50(k)	320 500 300 320(k)
31	Worcester(e)						

<sup>(</sup>a) Virginia Pine only; (b) White Oak; (c) Also for Douglas Fir; (d) Also for Norway Pine; (e) Based upon best modern practice; (f) Cypress only; (g) Douglas or Yellow Fir only; (h) Red Fir only;

#### ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

				Shear.			
1	Chestnut.	lock.	Hem	ust	Loc	k,	0a.
	Across Fibre.	Across Fibre.	With Fibre.	Across Fibre.	With Fibre.	Across Fibre.	With Fibre.
	150 150	275 350	40 75	720 400(a)	100 90(a)	600 720	100 100 150(b)
			60				200
	150	270 300	40 80	720	100	600 400	100 100
1					90(n)		150(b)
1	150	275	40	720	100	600	100
1		600	100(o)	400(m)	100(m)		240(b)
1	150	275	40	720	100	600	100
E							
100	••••••	600 625	100 63			1000(c)(s)	200
SSC						400(i)	80(i)
80.8585	150	275	40	720	100	600	100
2000	150	275	40	720 400(i)	100 100(i)	600(h)	100 125(h)
2		250	180(p) 35			600	100
200		200	00	720	100	600	100
3							

 <sup>(</sup>i) Redwood only;
 (j) Also for Washington Fir;
 (k) Also for Virginia Pine;
 (l) Longleaf;
 (s) Shortleaf;
 (m) Cedar only;
 (n) Norway Pine only;
 (o) Also for Cypress;
 (p) Western Hemlock;
 (q) Building Laws being revised,
 1917.
 (r) Do not specify.

#### ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

Pounds per Square Inch.

				Column	s.		
No.	City.	Longleaf Yellow Pins.	White Pine, Norway Pine and Spruce.	0ak.	Chestnut and Hemlock.	Locust.	Maxi- mum Length L =
1	Atlanta	(A)	(B)	(I)	5/8 (B)	1½ (B)	30 D
2	Baltimore	{<12D (C) > " (E)	{<12D (C) > " (E)	{<12D (C) > " (E)	{<12D (C) > " (E)	{<12D (C) > " (E)	
3	Boston	(F)	(G)	(H)			30 D
4	Buffalo	{<12D-1000 > " (F)	{<12D-700 > "(J)(b)	{<12D-800 > "(K)(a)	{<12D-700 > " (J)(c)		
5	Chicago	(M)	(M)	(M)	(M) (c)		30 D
6	Cincinnati	{<12D-1000 > " (F)	{<12D-700 > " (J)	{<12D-800 > " (K)			180 R
7	Cleveland(m)	(u)	(u)	(u)	(u)		150 R
8	Denver	{<12D-1000 (O)	.<12D-700 (O)	<12D-800 (O)	<12D-700(c) (O)	<12D-600(v) (O)	
9	Detroit	{<12D-1250 > " (F)	{<10D-875 > " (J)(d)	{<10D-1000 > " (K)(a)			24 D
10	Hartford(m)						
11	Jersey City	(A)	(B)	(I)	5/8 (B)	1½ (B)	30 D
12	Los Angeles (1)						
13	Louisville	{<12D-1000 > " (F)		{<12D-1000 > " (F)			120 R
14	Milwaukee	<15D-1125 > " (T)(k)	{<15D-825 i > " (T)(b)	<15D-1125 > " (T)	{<15D-675 > "(T)(e)		30 D
15	Minneapolis	<12D-1000 > " (F)(e)	<12D-700 > " (J)(b)	<12D-800 > " (K)(a)	<12D-600 > " (J)(c)		
16	Newark, N. J.	(A)	(B)	(I)	5/8 (B)	1½ (B)	30 D

L = Length of column in inches; D = Diameter or least dimension of column in inches; R = Least radius of gyration in inches; C = Allowable compressive unit stress (with grain) for that wood.

(a) Also for Norway Pine; (b) White Pine only; (c) Hemlock only; (d) White Pine and Spruce only; (e) Also for Washington and Oregon Fir; (f) Spruce only; (g) Oregon Pine only; (h) White Pine and Virginia Pine only; (i) Also Douglas

FORMULÆ:--

(E) 
$$C - 125\frac{L}{12D}$$

(H) 
$$900 - 9\frac{L}{D}$$

(A) 
$$1\ 000 - 18\frac{L}{D}$$

(F) 
$$1\ 000 - 10\frac{L}{D}$$

(I) 
$$900 - 17 \frac{L}{D}$$

(B) 
$$800 - 15\frac{L}{D}$$

(G) 
$$700 - 7\frac{L}{D}$$

(J) 
$$625 - 6\frac{L}{D}$$

#### ALLOWABLE UNIT STRESSES FOR TIMBER.

(Revised to 1917.)

Pounds per Square Inch.

				Column	s.		
No.	City.	Longleaf Yellow Pine.	White Pine, Norway Pine and Spruce.	0ak.	Chestnut and Hemlock.	Locust.	Maximum Length L=
17	New Haven	1000 (N)	{ 700(b) (N) 800 (f) (N)	900(N)			
18	New Orleans	(F)			(V) (k)	(U) (t)	30 D
19	New York	(W)	(I)	(W)			30 D
20	Philadelphia	(O)	(O)	(O)	(O)	(O)	
21	Pittsburgh(l)	• • • • • • • • • • • • • • • • • • • •					
22	Portland, Ore	(P)	(P)	(P)	(P)	(P)	20 D
23	Providence(l)						20 D
24	Rochester	(A)	(B)	(I)	5/8 (B)	1½ (B)	30 D
25	St. Louis						
26	St. Paul	(M)	(M)	(M)	(M)	(M)	
27	San Francisco	>15D(Q)(g)					
28	Seattle	(P)	(P)	(P)	(P)	(P)	24 D
29	Syracuse	{ 3/4 (A) (s) (A)	(B)	(I)	(S) (c)		30 D
80	Washington	(A)	(B) (h)	(I)		(A)	30 D
81	Worcester(l)						

L = Length of column in inches; D = Diameter or least dimension of column in inches; R = Least radius of gyration in inches; C = Allowable compressive unit stress (with grain) for that wood.

Fir, Cypress and Cedar; (j) For Norway Pine, Spruce and Eastern Fir only; (k) Shortleaf; (< 15D = 900); (l) Based on best modern practice; (s) Shortleaf; (t) Cypress only; (u) See Building Laws; (v) Colorado, Texas or Mexican Hemlock.

(P) C 
$$(1 - \frac{L}{70D})$$
 (U) 450 — 5  $\frac{L}{D}$ 

U) 
$$450 - 5 \frac{L}{D}$$

(M) C 
$$(1 - \frac{L}{80D})$$
 (Q)  $1300 - 20 \frac{L}{D}$  (V)  $815 - 8 \frac{L}{D}$ 

(N) Coefficients to apply to Gordon's Formula. (S) 
$$500 - 9 \frac{L}{D}$$
 (W)  $1200 - 20 \frac{L}{D}$ 

(S) 
$$500 - 9 \frac{L}{D}$$

(O) C 
$$(1 - \frac{L}{100D})$$

(T) C 
$$(1 - \frac{L}{60D})$$

## EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES. Allowable Unit Stresses for Reinforced Concrete.

(Revised to 1917.)

			Ratio	Conc	rete-	Allowal	ole Uni	t Stres	ses.
	-		Moduli	C	ompression	n.			
No.	City.	Concrete Mixture.	Elastic- ity Steel to Con- crete.	Direct.	Extreme Fibre Bending	In Hooped Columns	Shear.	Tension.	Bond.
2	Baltimore	1:2:4	15	{500(b) 500	500	1200(ff)	50		60
34	BostonBuffalo	1:5(h) 1:2:5	15 12	350	500 500		60 50		60 50
5	Chicago	1:2:4	15	400	700	{500 (l)  500(d)	40	40(w)	$\begin{cases} 50(\mathbf{x}) \\ 70(\mathbf{y}) \end{cases}$
6	Cincinnati	1:2:4	15	600	700	(z)	65		
7	Cleveland	1:2:4	15	500	700	650 (j)	40	40(w)	{ 70 m
8	Denver	1:2:3	15	450	500		50		75
9	Detroit	1:11/2:3t		450	650	(z)	40		5 80
11	Jersey City	1:2:4	18	350	500	(z)	50		100(q) 50
12	Los Angeles	1:21/2:31/2	15		650	800	{ 40		§ 80(y)
13	Louisville	1:2:4	15	{450(b) 650	650	{650 d,1 540	120(n) 50		(120(q)
14	Milwaukee	1:2:4	15	500(b)	700	800(d) 600 600 (1)	120(n) 60 cc 40 bb		{ 40aa 80
15	Minneapolis	1:2:4	{10 15	600 dd	650	800ee 1830 ff			{100(q) 75(u)
16	Newark, N. J	1:2:4	15	450(b)	650	650(d)	40		40
18	New Orleans		15	500 (r)	650 (r)	(340	50 (r)		50
19	New York	1:6(h)	15	500	650	725	{40 150(n)		100(q) 80
20	Philadelphia	1:2:4	15	500	650	750	{120(n) 40		{100(q) 80
21	Pittsburgh	1:6(h)	∫ 8gg \15	500	650	{540(ff) 450	120	90(w)	80
24	Rochester	1:6 (h)	15	1650(b)	650	\$540 (1) 650	60		150(p) 80
25	St. Louis	1:6(h)	20(ii) 15		{400(ii)  800		{100(ii) 175		65
26	St. Paul	1:2:4	15	500(b)	650	750(d)	50		80(q
27	San Francisco	1:6(h)	15	500	500	700	75		60
28	Seattle	1:2:4	15	450	667	500 (j)	{120(n) 60cc		50(x)
30	Washington	1:2:4	15	{120 (c) 450	(150 (c) (650		60	50	( ,0/2

<sup>(</sup>b) Columns not hooped; (c) Cinder-Concrete; (d) Vertical bars with hoops; (e) Actual compression in concrete surrounding steel; (f) Floor slabs; (g) Girders and beams; (h) Cement; aggregate; (i) Pure shear; (i) Spiral reinforcement; (k) Minimum area, gross section; (l) Structural steel units encasing concrete: (m) High carbon steel; (n) Where thoroughly reinforced for shear; (o) Without sign or crack; (p) Where adequate mechanical bond is provided (q) Deformed bars; (r) Rock or gravel concrete; (s) Slag concrete;

## EXTRACTS FROM THE BUILDING LAWS OF VARIOUS CITIES. Allowable Unit Stresses for Reinforced Concrete.

(Revised to 1917.) Pounds per Square Inch.

Steel-Al	lowable	Unit St	resses.	C	olumn	s.	T	ests.	
Tension.	Com- pression.	Compression  Vertical Reinforcement in Columns	Shear.	Maxi- mum Length L D	Mini- mum Allow- able Dimen- sion Inches.	Actual less Effective Diam. Inches.	Ratio Test to Calcu- lated Load.	Ratio Span to Maximum Deflection.	No.
{12000 (v) 15000 16000	{ 8000v 7500		8000v 10000	16	-	3			2 3
16000			10000	16			3		4
18000	10500	7500	12000	12	64(k)	3	2	800	5
16000	16000	9750(j)	10000	32(z)		2	4		6
18000(m)	16000(1)	7500	10000w	15		4			7
1/3 (hh)		( (-)	10000	15		2	2	700	8
{18000m,q 16000	15×(e)	$\begin{cases} (z) \\ 12000 (1) \end{cases}$		15	10	4	2	400	9
16000	16000	6000		12		2			11
16000	15×(e)	(ff)		30	7	3	2		12
16000	16000	,		15		3	4		13
16000	10500	{12000(d) 7500(b)		15	64(k)	3	2(o)		14
{20000(m) 16000	{ 8000- 12000	8000 dd 10000 ee	10000	15	12	3	2	{1000 g 300(f)	15
16000 (m)		8100(d) 6750(b)		15		4			16
16000			10000			4			18
{20000(aa) 16000	16000	7500		15	12	4	13/4		19
1,6000	16000	6000 9000(d) 16000 (l)		15	12	4	2(o)		20
16000	7500	6750	4500	15	9	3	2		21
(20000(m)	9750	8100(ff) 9750(d)		. 15		3		11	24
(16000)	9750 f20000m	6750(b)		10					24
{20000(m) 14000	14000			15		2			25
\$20000(m)	\$ 8000- 12000	7500(b) 10000(d)	10000	. 15	12	4	2	100 gg 300(f)	26
20000	7500	(ff)	10000	15	10	4	2	700	27
18000		7500 (j) 6750	12000	15	8	3	2	700	28
16000	14000	( 0100	10000	15	50(k)	4			30

<sup>(</sup>t) For columns; (u) Bars ¾ inch or less; larger bars, proportionately less; (v) Soft steel; (w) Diagonal tension; (x) Flat bars with size ratio less than 2, and high carbon rounds and squares; (y) Structural steel rounds and squares; (z) For hooped columns, see Building Laws; (aa) Cold drawn material as wire; (bb) Horizontal bars; (cc) Bent up bars; (dd) Square columns; (ee) Round core columns; (ff) Special cases, see Building Laws; (gg) For calculating deflections; (hh) Elastic limit; (ii) Burnt clay concrete.

### EXPLANATION OF TABLES OF RIVETS AND PINS.

#### RIVETS.

In the design of riveted joints the total stress transmitted is assumed to be taken up by the rivets, no allowance being made for the friction between the plates riveted together, and the manner of failure of the joint will be by shearing of the rivet or crushing of the plate. This assumes that the rules given on page 358 are followed and failure by tearing off the plate caused by the rivets being too near the edge is thus prevented.

In the table of "Shearing Value of Rivets and Bearing Value of Riveted Plates," pages 352 and 353, these values are given for all customary sizes and thicknesses corresponding to various usual allowable unit stresses.

For any given size of rivet or thickness of plate to be used, an inspection of the table will show at once if the bearing value of the plate or the shearing value of the rivet is to govern the design and the amount of stress that can be transmitted by each rivet.

#### PINS.

In designing pin-connected joints the points which govern the design are the bending moments produced in the pin by the bars or plates connected, and the bearing value of the plates themselves. The bearing value in the case of eye-bars of proper proportions is sufficiently ample and need not be computed. Shear in pins need not ordinarily be considered, as the bending and bearing stresses usually determine the size.

In the table of "Maximum Bending Moments on Pins," pages 360 and 361, is given the allowable bending moments on pins of various diameters for the usual allowable fibre stresses.

In the table of "Bearing Values of Pin Plates for One-Inch Thickness of Plate," on page 359, is given the allowable bearing values of plates against pins of various usual diameters, corresponding to the customary unit stresses of this character.

If the bearing value exceeds the allowable limit in any given case pin-plates must be added, thus increasing the bearing value until it is reduced to a safe limit as shown by the tables.

### CONVENTIONAL SIGNS FOR RIVETING.

FIELD SHOP Two Full Heads. Countersunk Inside (Farside) and Chipped. Countersunk Outside (Nearside) and Chipped Countersunk both Sides and Chipped. INSIDE. OUTSIDE. BOTH SIDES. Flattened to 1/8" high or Countersunk and not Chipped. Flattened to 1/4" high. Flattened to 3/" high.

This system, designed by F. C. Osborn, C. E., has for foundation the diagonal cross to represent a countersink, the blackened circle for a field rivet and the diagonal stroke to indicate a flattened head. The position of the cross, with respect to the circle (inside, outside or both sides), indicates the location of the countersink and, similarly, the number and position of the diagonal strokes indicate the height and position of the flattened heads.

Any combination of field, countersunk and flattened head rivets liable to occur may be readily indicated by the proper combination of above signs.

## SHEARING VALUE OF RIVETS AND BEARING VALUE OF RIVETED PLATES.

All Dimensions in Inches.

Shearing Value = Area of Rivet × Allowable Shearing Stress per Square Inch.

Diameter	Area	Unit Stress	=6 000 lbs.	Bearin	ng Valu	e for Di	ferent	
of Rivet.	Square Inches.	Single Shear.	Double Shear.	1/4	5 16	8	7 1 8	
3/8	.1105	668	1325	1125	1406	1688		
1/2	.1964	1178	2356	1500	1875	2250	2625	
5/8	.3068	1841	3682	1875	2344	2813	3281	
3/4	.4418	2651	5301	2250	2813	3375	8938	
7/8	.6013	3608	7216	2625	3281	3938	4594	
1	.7854	4712	9425	3000	3750	4500	5250	
Diameter	Area	Unit Stress	=8 000 lbs.	Bearing	ng Valu	e for Di	fferent	
of	in	Single	Double	1	5	8	7	
Rivet.	Square Inches.	Shear.	Shear.	$\frac{1}{4}$	5 16	8	16	
3/8	.1105	884	1767	1500	1875	2250		
1/2	.1964	1571	3142	2000	2500	8000	3500	
5/8	.8068	2454	4909	2500	3125	3750	4375	
3/4	.4418	3534	7069	3000	3750	4500	5250	
7/8	.6013	4811	9621	3500	4375	5250	6125	
1	.7854	6283	12566	4000	5000	6000	7000	
Diameter	Area	Unit Stress	= 10 000 lbs.	Bearing Value for Different				
of	in	Single	Double	1	5	3	7	
Rivet.	Square Inches	Shear.	Shear.	4	16	3 8	16	
3/8	.1105	1105	2209	1875	2344	2813		
1/2	.1964	1964	3927	2500	3125	3750	4375	
5/8	.3068	3068	6136	3125	3906	4688	5469	
8/4	.4418	4418	8836	3750	4688	5625	6563	
7/8	.6013	6013	12026	4375	5469	6563	7656	
1	.7854	7854	15708	5000	6250	7500	8750	
Diameter	Area	Unit Stress	=12 000 lbs.	Bearin	ng Valu	e for Di	fferent	
of					-		7	
	in	Single	Double		5			
Rivet.	Square Inches.	Single Shear.	Double Shear.	1/4	<u>5</u> 16	8	16	
				2250	2813	3375		
Rivet.	Square Inches.	Shear.	Shear.	4	16	8		
Rivet.  3/8 1/2 5/8	Square Inches.	Shear. 1325	Shear. 2651	2250	2813	8 3375 4500 5625	5220 6562	
Rivet. 3/8 1/2	.1105 .1964	Shear. 1325 2356	Shear. 2651 4712	2250 3000	2813 3750	8 3375 4500	T 6 5220	
Rivet.  3/8 1/2 5/8	.1105 .1964 .3068	Shear. 1325 2356 2682	Shear.  2651 4712 7363	2250 3000 3750	2813 3750 4688	8 3375 4500 5625	5220 6562	

In the above tables the bearing values between the lower and upper zigzag black lines are greater than single and less than double shear for the corresponding dimensions, so that in case of single shear, the single shearing value governs, and in case of double shear, the bearing value governs the design.

## SHEARING VALUE OF RIVETS AND BEARING VALUE OF RIVETED PLATES.

#### All Dimensions in Inches.

Bearing Value = Diameter of Rivet X Thickness of Plate X Allowable Bearing

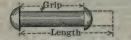
Stress per Square Inch.											
Thickne	esses of	Plate i	n Inche	s at 12	000 Pot	inds pe	r Squai	e Inch.			
$\frac{1}{2}$	9 16	58	$\begin{array}{c c} 11 \\ \hline 16 \end{array}$	3/4	13	7	15	1			
	16	8	10	4	16	8	16				
2222	19.0					-	1 23				
3750	4219	4688				-1-					
4500	5068		6188	6750							
5250	5906			7875	8531	9188	9844				
6000	6750	7500	8250			10500		12000			
Thicknesses of Plate in Inches at 16 000 Pounds per Square Inch.											
$\frac{1}{2}$	$\frac{9}{16}$	58	$\frac{11}{16}$	34	$\frac{13}{16}$	7 8	$\frac{15}{16}$	1			
			10	,			10				
4000											
1 5000	5625	6250	1								
6000	6750		8250	9000	100						
7000	7875	8750			11375	12250	13125				
8000					13000			16000			
							1				
Thicknesses of Plate in Inches at 20 000 Pounds per Square Inch.											
-		1 1400				иниз ре	er aqua	e men.			
1	9					7	-	1			
$\frac{1}{2}$		5 8	11/16	3/4	13 16	$\frac{7}{8}$	15 16				
$\frac{1}{2}$	9					7	-				
1/2 5000	9 16	<u>5</u> 8				7	-				
5000 6250	9 16 7031	5 8 7813	11/16	3/4		7	-				
5000 6250 7500	9 16 7031 8438	7813 9375	10313	11250	13 16	78	15 16				
5000 6250 7500 8750	9 16 7031 8438 9844	7813 9875 10938	10313 12031	$\frac{\frac{3}{4}}{4}$ 11250 13125	14219	15313	16406	1			
5000 6250 7500 8750 10000	9 16 7081 8438 9844 11250	7813 9375 10938 12500	10318 12031 18750	11250 13125 15000	14219 16250	15813 17500	15 16 16406 18750	20000			
5000 6250 7500 8750 10000	9 16 7081 8438 9844 11250	7813 9375 10938 12500	10318 12031 18750	11250 13125 15000	14219 16250	15813 17500	15 16 16406 18750	1			
5000 6250 7500 8750 10000	9 16 7081 8438 9844 11250 esses of	7813 9875 10938 12500 Plate	10313 12031 13750 in Inch	11250 13125 15000	14219 16250	78 15813 17500 unds po	16406 18750 ar Squa	20000			
5000 6250 7500 8750 10000	9 16 7031 8438 9844 11250	7813 9375 10938 12500	10318 12031 18750	11250 13125 15000	14219 16250	15813 17500	15 16 16406 18750	20000 re Inch.			
5000   6250   7500   8750   10000   Thickne	9 16 7081 8438 9844 11250 esses of	7813 9875 10938 12500 Plate	10313 12031 13750 in Inch	11250 13125 15000	14219 16250	78 15813 17500 unds po	16406 18750 ar Squa	20000 re Inch.			
5000 6250 7500 8750 10000 Thickne	7031 8438 9844 11250 esses of	7813 9875 10938 12500 Plate	10313 12031 13750 in Inch	11250 13125 15000	14219 16250	78 15813 17500 unds po	16406 18750 ar Squa	20000 re Inch.			
5000 6250 7500 8750 10000 Thickne 1/2 6000 7500	7031 8438 9844 11250 98888 of	7813 9875 10938 12500  Plate 5 8	10313 12031 13750 in Inch	11250 13125 15000 nes at 2	14219 16250	78 15813 17500 unds po	16406 18750 ar Squa	20000 re Inch.			
12 5000 6250 7500 8750 10000 Thicknot 12 6000 7500 9000	7031 8438 9844 11250 esses of 9 16	7813 9875 10938 12500 Plate 5 8 9875 11250	10313 12031 13750 in Inch 116 12875	11250 13125 15000 les at 2	14219 16250 4 000 Po	15813 17500 unds pe	16406 18750 ar Squa 15 16	20000 re Inch.			
12 5000 6250 7500 8750 10000 Thickne 12 6000 7500 9000 10500	7031 8438 9844 11250 916 8437 10125 11812	7813 9875 10938 12500 Plate 5 8 9975 11250 13125	10313 12031 13750 in Inch 116 12875 14437	11250 13125 15000 18 at 2 3 4	14219 16250 4 000 Po 13 16	15313 17500 unds pe	16406 18750 er Squa 15 1687.	20000 re Inch.			
12 5000 6250 7500 8750 10000 Thickm 12 6000 7500 10500 12000	7031 8438 9844 11250 98568 of 16 8437 10125 11812 13500	7813 9875 10938 12500 Plate 5 8 9875 11250 13125 15000	10313 12031 13750 in Inct 11 1 6 12875 14437 16500	11250 13125 15000 tes at 2 3 4 13500 15750 18000	14219 16250 4 000 Po 1 1 8 1 6 17062 19500	15313 17500 unds p	16406 18750 ar Squa 15 1687. 22500	20000 re Inch.			

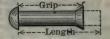
greater than double shear for the corresponding dimensions, so that in these

cases the shearing values govern the design.

The bearing values below and to the left of the lower zigzag black lines are less than single shear, so that in these cases the bearing values govern the design.

#### LENGTH OF RIVETS REQUIRED FOR VARIOUS GRIPS INCLUDING AMOUNT NECESSARY TO FORM ONE HEAD.





Grip of Rivet in Inches.	Diameter of Rivet in Inches.										
in Inches.	1"	3"	1"	5"	311	7"	1"	11/8"			
1/2 5/8 8/4 5/8	1 1½ 1½ 1¼ 1¾	1½ 1½ 1½ 1½ 15%	1½ 15/8 18/4 17/8	184 17/8 2 21/8	17/8 2 21/8 21/4	2 2½ 2½ 2¼ 28/8	2½ 2½ 2½ 28/8 2½	2½ 2¾ 2¾ 2½ 2½ 28%			
1 1½ 1¼ 1¼ 1¾	11/2 15/8 18/4 17/6	13/4 17/8 2 21/8	2 2½ 2¼ 2¼ 284	21/4 28/8 21/2 25/8	28/8 21/2 25/8 27/8	21/2 25/8 28/4 3	25/8 23/4 21/8	23/4 27/8 3 31/6			
11/2 15/8 13/4 17/8	2 21/8 21/4 23/8	214 28/8 21/2 25/8	21/2 25/8 23/4 27/8	284 278 3 314	3 31/8 31/4 38/8	31/8 31/4 38/8 31/2	3½ 3¼ 3½ 3½ 35/8	31/4 31/2 35/8 38/4			
2 2½ 2½ 2¼ 2¾ 23/8	2½ 25/8 28/4 27/8	28/4 21/8 3 31/8	31/8 31/4 33/8 31/2	33/8 31/2 35/8 33/4	31/2 35/8 33/4 37/8	35/8 33/4 37/8 4	384 378 4 418	37/8 4 41/8 41/4			
2½ 25/8 28/4 27/8	31/8 31/4 38/8	3½ 3½ 3½ 35/8 38/4	35/8 33/4 37/8 4	378 4 41/8 41/4	4 4½ 4½ 4¾ 4³/8	41/8 41/4 43/8 41/2	41/4 48/8 41/2 45/8	43/8 41/2 45/8 43/4			
3 1/8 3 1/4 3 1/4 3 1/2 3 1/2 3 1/2 3 1/2 3 1/2 3 1/2 3 1/2	31/2 35/8 38/4 37/8 4 41/8 41/8	37/8 4 41/8 41/4 43/8 41/2 45/8 43/8	41/8 41/4 48/8 41/2 48/8 43/4 47/8	48/8 41/2 48/4 47/8 5 51/8 51/4 58/8	41/2 43/4 47/8 5 51/8 51/4 51/4	45/8 43/4 5 51/8 51/4 53/8 51/2 55/8	434 5 51/8 51/4 53/8 51/2 53/8	47/8 5 51/4 53/8 51/2 55/8 58/4			
41/8 41/4 48/8 41/4 48/8 41/2 45/8 43/4	41/2 45/8 43/4 47/8 5 51/8	4 7/8 5 51/8 51/4 53/8 51/2 58/8	51/8 51/4 51/2 55/8 53/4 57/8	51/2 55/8 53/4 57/8 6 61/8 61/4	55/8 53/4 57/8 6 61/8 61/4 61/2	534 578 6 618 614 638 658	57/8 6 6 1/8 61/4 63/8 61/2 63/4	61/8 61/4 63/4 63/6 61/2 65/6 63/4			
47/8 5 1/8 5 1/4 5 5/8 5 5/8 5/8 5 5/8 5 5 5/8 5/8 5 5/8 5 5 5/8 5 5/8 5/8 5 5/8 5/8 5/8 5/8 5 5/8 5/8	53/8 51/2 55/8 53/4 57/8 6 61/8 61/4 63/8 61/4	53/4 57/8 6 61/8 61/4 68/8 61/2 63/4 67/8	61/8 61/4 68/8 61/2 65/8 63/4 61/8 7	61-2 65-8 63-4 67-8 7 71-8 71-4 73-8 71-2	65/8 63/4 67/8 7 71/8 71/4 78/8 75/8	684 678 7 718 714 738 714 758 758	67/8 7 71/8 71/4 78/8 71/2 75/8 78/4 71/8	67/8 7 71/6 71/4 73/8 71/4 75/8 73/4 71/6			

Amount in Inches to be subtracted from above lengths for Countersunk Heads.

1/8 1/4 1/2 1/2 1/6 1/6 1/6 1/6 1/6

# WEIGHT OF 100 STEEL RIVETS. INCLUDING 100 HEADS.

Length		Diamete	or of Rivet is	n Inches.	
Under Head.	1/2	<u>5</u>	34	7 8	1
Inches.		Average	Weight in	Pounds.	W.L.
134	9.2 10.5	17.0			8 =
11/6 11/4 13/6 11/2	11.15 11.80 12.45 13.10	18.0 19.0 20.0 21.0	28.0 29.5 81.0	41.8 43.4 45.5	68.5
15/8 18/4 17/8 2	18.75 14.40 15.00 15.70	22.0 23.0 24.0 25.0	82.5 84.0 85.5 87.0	47.6 49.7 51.8 53.9	66.2 68.9 71.7 74.4
21/8 21/4 23/8 21/2	16.85 17.00 17.65 18.80	26.0 27.0 28.0 29.0	88.5 40.0 41.5 43.0	56.0 58.0 60.1 62.2	77.1 79.8 82.6 85.3
25/8 23/4 27/8 3	18.95 19.60 20.25 20.90	30.0 31.0 32.0 38.0	44.5 46.0 47.5 49.0	64.8 66.4 68.5 70.6	88.0 90.7 93.5 96.2
3½ 3¼ 3½ 3½ 3½	Line	34.0 35.0 36.0 37.0	50.5 52.0 53.5 55.0	72.7 74.7 76.8 78.9	99.0 101.6 103.8 107.1
35/8 35/4 37/8 4		38.0 39.0 40.0 41.0	56.5 58.0 59.5 61.0	81.0 83.1 85.2 87.8	109.8 112.6 115.2 118.0
41/4 41/2 43/4 5	88		64.0 67.0 70.0 73.0	91.4 95.6 99.8 104.0	123.5 128.9 134.4 139.8
514 514 514 6	8/17		76.0 79.0 82.0 85.0	108.2 112.8 116.5 120.7	145.3 150.7 156.2 161.6
Weight of	5.8	9.0	18.0	20.5	30.8

## AREAS TO BE DEDUCTED TO OBTAIN NET AREA OF RIVETED PLATE.

Square Inches.

Thick- ness Plates in	SIZE OF HOLE. Inches.													
Inches.	1/4	16	3/8	78	1/2	16	8/8	18	3/4	18	3/8	18	1	116
1/4 8 16 8/8 7 16	.06 .08 .09 .11	.08 .10 .12 .14	.09 .12 .14 .16	.11 .14 .16 .19	.13 .16 .19 .22	.14 .18 .21 .25	.16 .20 .23 .27	.17 .21 .26 .30	.19 .23 .28 .33	120 125 .30 .36	.22 .27 .33	.23 .29 .35 .41	.25 .31 .38 .44	.27 .33 .40 .46
1/2 16 5/8 118	.13 .14 .16 .17	.16 .18 .20 .21	.19 .21 .23 .26	.22 .25 .27 .30	.25 .28 .31 .34	.28 .32 .35 .39	.31 .35 .39 .43	.34 .39 .43 .47	.38 .42 .47 .52	.41 .46 .51 .56	.44 .49 155 160	.47 .53 .59 .64	.50 156 163 169	.53 .60 .06 .73
3/4/3/6/8/16/8/16	.19 .20 .22 .23	.23 .25 .27 .29	.28 .30 .33 .35	.33 .36 .38 .41	.38 .41 .44 .47	.42 .46 .49	.47 .51 .55 .59	.52 .56 .60 .64	.56 .61 .66 .70	.61 .66 .71 .76	.66 .71 .77 .82	.70 .76 .82	.75 .81 .88 .94	180 186 198 1.00
1 11/8 11/8 1/8	.25 .27 .28 .30	.31 .33 .35 .37	.38 .40 .42 .45	.44 .46 .49 .52	.50 .53 .56 .59	.56 .60 .63 .67	.63 .66 .70 .74	.69 .73 .77 .82	.75 .80 .84 .89	.81 .86 .91	.93 .98 1.04	1.00 1.05 1.11	1.00 1.06 1.13 1.19	1.06 1.13 1.20 1.26
11/4 11/8 13/8 11/16	.31 .33 .34 .36	.39 .41 .43 .45	.47 .49 .52 .54	.55 .57 .60 .63	.63 .66 .69 .72	.70 .74 .77 .81	.78 .82 .86 .90	.86 .90 .95 .99	.94 .98 1.03 1.08	1.02 1.07 1.12 1.17	1.09 1.15 1.20 1.26	1.17 1.23 1.29 1.35	1.25 1.31 1.38 1.44	1.33 1.39 1.46 1.53
1½ 1½ 1½ 1½ 1½	.38 .39 .41 .42	.47 .49 .51 .53	.56 .50 .61 .63	.66 168 .71 .74	.75 .78 .81 .84	.84 .88 .91 .95	.94 .08 1.02 1.05	1.03 1.07 1.12 1.16	1.13 1.17 1.22 1.27	1.22 1.27 1.32 1.37	1.31 1.37 1.42 1.47	1.41 1.46 1.52 1.58	1.50 1.56 1.63 1.69	1.50 1.66 1.73 1.79
184 118 178 118 118	.44 .45 .47 .48 .50	.55 .57 .59 .61 .63	.68 .70 .73 .75	.77 .79 .82 .85 .88	.88 .91 .94 .97 1.00	1.02 1.05 1.09 1.13	1.09 1.13 1.17 1.21 1.25	1.20 1.25 1.29 1.33 1.38	1.31 1.36 1.41 1.45 1.50	1.42 1.47 1.52 1.57 1.63	1.53 1.59 1.64 1.70 1.75	1.64 1.70 1.76 1.82 1.88	1.75 1.81 1.88 1.94 2.00	1.86 1.93 1.99 2.06 2.13

## MAXIMUM SIZE OF RIVETS IN ANGLES AND IN FLANGES OF BEAMS AND CHANNELS.

		I-BE/	MS.			CH	ANNE	LS.		ANGLES.			
Depth of Beam. Ins. 3 4 5 6 7 8 9 10 12 12	Weight per Foot. Pounds.  5.5 7.5 9.75 12.25 15.0 18.00 21.0 25.0 31.5 40.0	Size of Rivet. Inch.	Depth of Beam. Ins. 15 15 15 18 20 20 24 24	Weight per Foot. Pounds.  42.0 60.0 80.0 55.0 65.0 80.0 80.0 105.0	of	Depth of Channel Inches.	Weight per Foot. Pounds.  4.0 5.25 6.50 8.0 9.75 11.25 13.25 15.0 20.50 33.0	Size of Rivet. Inch.	Length of Leg. Inches. 11413811421342214422344	Size of Rivet. Inch.	Length of Leg. Inches.	Size of Rivet Inch.	

## AREAS TO BE DEDUCTED TO OBTAIN NET AREA OF RIVETED PLATE.

Square Inches.

1	SIZE OF HOLE. Inches.											Thick- ness Plates			
11/8	13	11/4	1 5	13/8	1 7 16	11/2	1%	15/8	111	13/4	113	1 1/8	1 15	2	in Inches.
.28 .35 .42 .49	.30 .37 .45 .52	.31 .39 .47 .55	.33 .41 .49 .57	.34 .43 .52 .60	.36 .45 .54 .63	.38 .47 .56 .66	.39 .49 .59 .68	.41 .51 .61 .71	.42 .53 .63 .74	.44 .55 .66 .77	.45 .57 .68 .79	.47 .59 .70 .82	.48 .61 .73 .85	.50 .63 .75 .88	1/4 8 16 8/8 7 16
.56 .63 .70 .77	.59 .67 .74 .82	.63 .70 .78 .86	.66 .74 .82 .90	.69 .77 .86 .95	.72 .81 .90 .99	.75 .84 .94 1.03	.78 .88 .98 1.07	.81 .91 1.02 1.12	1.16	.88 .98 1.09 1.20	.91 1.02 1.13 1.25	.94 1.05 1.17 1.29	.97 1.09 1.21 1.33	1.00 1.13 1.25 1.38	1/2 16 5/8 11
.84 .91 .98 1.05	.89 .96 1.04 1.11	.94 1.02 1.09 1.17	1.23	1.03 1.12 1.20 1.29		1.22	1.27	1.22 1.32 1.42 1.52	1.27 1.37 1.48 1.58	1.31 1.42 1.53 1.64	1.36 1.47 1.59 1.70	1.41 1.52 1.64 1.76	1.45 1.57 1.70 1.82	1.50 1.63 1.75 1.88	3/4 10 7/8 15
1.13 1.20 1.27 1.34	1.26	1.41		1.46 1.55	1.53 1.62			1.73	1.69 1.79 1.90 2.00	1.75 1.86 1.97 2.08	1.81 1.93 2.04 2.15	1.88 1.99 2.11 2.23	1.94 2.06 2.18 2.30	2.00 2.13 2.25 2.38	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1.41 1.48 1.55 1.62	1.56 1.63	1.64	1.64 1.72 1.80 1.89	1.80	1.89		$\frac{2.05}{2.15}$	2.13	2.11 2.21 2.32 2.43	2.19 2.30 2.41 2.52	2.27 2.38 2.49 2.61	2.34 2.46 2.58 2.70	2.42 2.54 2.66 2.79	2.50 2.63 2.75 2.88	11/4 1 5/6 13/8 1 7/16
1.69 1.76 1.83 1.90		1.88 1.95 2.03 2.11	1.97 2.05 2.13 2.21	2.06 2.15 2.23 2.32	2.16 2.25 2.34 2.43	2.25 2.34 2.44 2.53	2.34 2.44 2.54 2.64	2.44 2.54 2.64 2.74	2.53 2.64 2.74 2.85	2.63 2.73 2.84 2.95	2.72 2.83 2.95 3.06	2.81 2.93 3.05 3.16	2.91 3.03 3.15 3.27	3.00 3.13 3.25 3.38	1½ 1½ 1½ 1½ 1½ 1¼
1.97 2.04 2.11 2.18 2.25	2.23	2.19 2.27 2.34 2.42 2.50	2.30 2.38 2.46 2.54 2.63	2.58 2.66		2.63 2.72 2.81 2.91 3.00	2.73 2.83 2.93 3.03 3.13	3.15	3.16 3.27	3.06 3.17 3.28 3.39 3.50	3.17 3.29 3.40 3.51 3.63	3.28 3.40 3.52 3.63 3.75	3.39 3.51 3.63 3.75 3.88	3.50 3.63 3.75 3.88 4.00	184 111 178 111 2

### RIVET SPACING.

### All Dimensions in Inches.

Size of Rivet.	Minimu	ım Pitch.	Maximum Pitch at Ends of Compression	Minimum Dista of Piece to Rivet	Maximum Pitch in Line of Stress for Plate and Shape	
161 400.	Allowable.	Preferable.	Members.	Sheared Edge.	Rolled Edge.	Members.
1/4 8/8 1/2 6/8 8/4 1/8 1 11/8	34 11/8 11/4 17/8 21/4 25/8 3 33/8	13/4 2 21/2 3	21/2 3 31/2 4 41/2	1 1½ 1½ 1½ 1½	1/8 11/2 11/4	41/2 6 8

For General Rules for Rivet Spacing see next page.

### GENERAL RULES FOR RIVET SPACING FOR BRIDGE AND STRUCTURAL WORK.

The pitch or distance from center to center of rivets should not be less than 3 diameters of the rivet, preferably not less than 3 inches for ½ inch rivets, 2½ inches for ¾ inch rivets, 2 inches for ½ inch rivets and 1¾ inches for ½ inch rivets.

At the ends of compression members the pitch should not exceed 4 diameters of the rivet for a length equal to 1½ times the maximum width of the member.

Where two or more plates are in contact, rivets spaced not more than 12 inches in either direction shall be used to hold them together.

For members composed of plates and shapes the pitch in the direction of the line of stress should not exceed 6 inches for % and ¾ inch rivets, 4½ inches for 5% inch rivets and 4 inches for ½ inch rivets. For angles with two gauge lines in built-up members, rivets staggered, the maximum pitch in each line may be twice these distances.

The distance between the sheared edge of any piece and the center of the rivet hole should not be less than  $1\frac{1}{2}$  inches for  $\frac{1}{2}$  inch rivets,  $1\frac{1}{2}$  inches for  $\frac{3}{2}$  inch rivets,  $1\frac{1}{2}$  inches for  $\frac{5}{2}$  inch rivets and 1 inch for  $\frac{1}{2}$  inch rivets; for a rolled edge, these distances may be  $1\frac{1}{2}$ ,  $1\frac{1}{2}$ , 1 and  $\frac{1}{2}$  inches, respectively; when practicable it should, for all sizes, be at least 2 diameters of the rivet and should not exceed 8 times the thickness of the plate.

Minimum spacing is generally used in pin plates, at ends of columns, girders, etc., etc.

In figuring clearance of rivets for special cases, allow 5% inch in addition to diameter of head.

### BEARING VALUES OF PIN PLATES.

#### For One Inch Thickness of Plate.

Bearing value = Diameter of Pin × 1" × Stress per Square Inch.

Diam- eter of Pin.	Area of Pin.	Bearing Value at 12 000 Pounds per Square Inch.	Bearing Value at 13 500 Pounds per Square Inch.	Bearing Value at 15 000 Pounds per Square Inch.	Diam- eter of Pin.	Area of Pin.	Bearing Value at 12 000 Peunds per Square Inch.	Bearing Value at 13 500 Pounds per Square Inch.	Bearing Value at 15 000 Pounds per Square Inch.
Inches.	Sq. Ins.	Pounds.	Pounds.	Pounds.	Inches.	Sq. Ins.	Pounds.	Pounds.	Pounds.
1 1½ 1¼ 1¼ 1¾	.785 .994 1.227 1.485	12000 13500 15000 16500	13500 15190 16880 18560	15000 16880 18750 20630	41/2 45/8 48/4 47/8	15.90 16.80 17.72 18.67	54000 55500 57000 58500	60750 62440 64130 65810	67500 69380 71250 73130
1½ 15/8 13/4 17/8	1.767 2.074 2.405 2.761	18000 19500 21000 22500	20250 21940 23630 25310	22500, 24380 26250 28130	5 5½ 5½ 5½ 5¾ 53%	19.64 20.63 21.65 22.69	60000 61500 63000 64500	67500 69190 70880 72560	75000 76880 78750 80630
2 2½ 2½ 2¼ 28/8	3.142 3.547 3.976 4.430	24000 25500 27000 28500	27000 28690 30380 32060	30000 31880 33750 35630	5½ 55/8 58/4 57/8	23.76 24.85 25.97 27.11	66000 67500 69000 70500	74250 75940 77630 79310	82500 84380 86250 88130
2½ 2 <sup>8</sup> / <sub>8</sub> 2 <sup>3</sup> / <sub>4</sub> 2½	4.909 5.412 5.940 6.492	30000 31500 33000 34500	33750 35440 37130 38810	37500 39380 41250 43130	61/8 61/4 63/8	28.27 29.46 30.68 31.92	72000 73500 75000 76500	81000 82690 84380 86060	90000 91880 93750 95680
8 3½ 3¼ 3¾ 33/8	7.069 7.670 8.296 8.946	36000 37500 39000 40500	40500 42190 43880 45560	45000 46880 48750 50630	6½ 65/8 63/4 67/8	33.18 34.47 35.79 37.12	78000 79500 81000 82500	87750 89440 91130 92810	97500 99380 101250 103130
3½ 35/8 33/4 37/8	9.621 10.32 11.05 11.79	42000 43500 45000 46500	47250 48940 50630 52310	52500 54380 56250 58130	7 7½ 8 8½	38.48 44.18 50.27 56.75	84000 90000 96000 102000	94500 101250 108000 114750	105000 112500 120000 127500
4 4½ 4½ 4¾ 4¾	12.57 13.36 14.19 15.03	48000 49500 51000 52500	54000 55690 57380 59060	60000 61880 63750 65630	10 11 12	63.62 78.54 95.03 113.10	108000 120000 132000 144000	121500 135000 149500 162000	135000 150000 165000 180000

Example.—The stress in the end post of a bridge is 250 000 pounds and the diameter of the pin is 5%. Required the total thickness of steel pin plates for a bearing value of 15 000 pounds per square inch.

From the table the bearing value of a 5\%" pin in a 1" plate for 15 000 pounds unit stress is 84 380 pounds. Therefore the total thickness of metal required is 250 000

 $\frac{250\ 000}{84\ 380} = 2.96$ ".

The nearest commercial size would therefore be 1½" on each side, including web and necessary reinforcing plates.

### MAXIMUM BENDING MOMENTS ON PINS.

With Extreme Fibre Stresses Varying from 15 000 to 25 000 Pounds per Square Inch.

Diameter of	Area of Pin	Mome	nts in Inch	-Pounds for	Fibre Stre	esses of
Pin in	in Square	15 000 Lbs.	18 000 Lbs.	20 000 Lbs.	22 500 Lbs.	25 000 Lbs
1 411 411	11 pdffw10	per	per	per	per	per
Inches.	Inches.					
334024001	2404001	Square Inch.	Square Inch	Square Inch.	Square Inch.	Square Inch
1	,785	1470	1770	1960	2210	2450
11/8	.994	2100	2520	2800	3150	3490
1 1½ 1½ 1¼	1.227	2900	3450	3830	4310	4790
1%	1.485	3830	4590	5100	5740	6380
1½ 15/8 13/4 17/8	1.767	4970	5960	6630	7460	8280
13/8	2.074 2.405	6320 7890	7580 9470	8430 10520	9480 11840	10530
17/4	2.761	9710	11650	12940	14560	13150 16180
2	3.142	11780	14140	15710	17670	19630
21/8	3.547	14130	16960	18840	21200	23550
21/4	3.976	16770	20130	22370	25160	27960
23/8	4.430	19730	23670	26300	29590	32880
21/2	4.909	23010	27610	30680	34510	38350
25/8	5.412	26640	31960	35520	39960	44400
23/4 27/8	5.940	30630	36750	40830	45940	51040
21/8	6.492	34990	41990	46660	52490	58320
3	7.069	39730	47680	52970	59600	66220
3½ 3½	7.670	44940	53930	59920	67410	74900
31/4	8.296	50550	60660	67400	75830	84250
33/8	8.946	56610	67940	75480	84920	94350
3½ 35/8	9.621	63140	75770	84180	94710	105230
35/8	10.321	70150	84180	93530	105220	116910
33/4	11.045	77660	93190 102820	103540 114250	116490	129430
6/8	11.793	85690	102820	114250	128530	142810
M.	12.566	94250	113100	125660	141370	157080
41/8 41/4	13.364	103360	124040	137820	155040	172270
43/8	14.186 15.033	113050 123320	135660 147980	150730 164420	169570 184980	188410 205530
	-			-		
41/2	15.904	134190	161030	178920	201290	223650
45/8	16.800	145690 157820	174830 189390	194250 210430	218510 236740	242810 263040
43/4 47/8	17.721 18.665	170580	204740	227490	255920	284360
8	19.635	184080	220890	245440	276120	306800
51/8	20.629	198230	237880	264310	297350	330390
51/4	21.648	213090	255710	284120	319640	355160
53/8	22.691	228680	274420	304910	343020	381130
51/2	23.758	245010	294010	326680	367510	408350
53/8	24.850	262100	314510	349460	393140	436830
53/4 57/8	25.967 27.109	279960 298620	335950 358340	373280 398160	419940 447930	497700

### MAXIMUM BENDING MOMENTS ON PINS.

With Extreme Fibre Stresses Varying from 15 000 to 25 000 Pounds per Square Inch.

Diameter	Area of	Mome	nts in Inch	-Pounds fo	r Fibre Stre	esses of
Pin in	in Square	15 000 Lbs.	18 000 Lbs.	20 000 Lbs.	22 500 Lbs.	25 000 Lbs
* TIT TIT	TI Differ 6	per	per	per	per	per
Inches.	Inches.	Square Inch.	Square Inch.	Square Inch.	Square Inch.	Square Inch
6	28.274	318090	381700	424120	477130	530140
61/8	29.465	338380	406060	451180	507580	563970
63/8	30.680 31.919	359530 381530	431430 457840	479370 508710	539290 572300	599210 635890
616	33.183	404420	485400	539230	606630	674030
61/2	34.472	428200	513840	570940	642300	713670
634	35.785 37.122	452900 478530	543480 574240	603870 638040	679350 717800	754830 797550
7	38.485	505110	606130	673480	757660	841850
71/8	39.871	532650	639190	710210	798980	887760
71/8 71/4 73/8	41.282 42.718	561180 590710	673420 708860	748250 787620	841780 886070	935310 984520
	44.179	621260	745510	828350	931890	1035440
75/8	45.664	652850	783410	870460 913980	979270	1088080
71/2 75/8 73/4 73/8	47.173 48.707	685480 719190	822580 863030	958920	1028220 1078780	1142470 1198650
8	50.265	753980	904780	1005310	1130970	1256640
81/8	51.849	789880	947860	1053170 1102530	1184820	1316470
81/8 81/4 83/8	53.456 55.088	826900 865060	992280 1038070	1153410	1240350 1297590	1378170 1441760
81/2 88/8	56.745	904370	1085250	1205830	1356560	1507290
85/8	58.426 60.132	944860 986540	1133830 1183850	1259820 1315390	1417290 1479810	1574770 1644240
83/4	61.862	1029430	1235310	1372570	1544140	1715710
9	63.617	1073540	1288250	1431390	1610310	1789240
918	65.397 67.201	1118900 1165510	1342680 1398610	1491860 1554010	1678340 1748270	1864830 1942520
93/8	69.029	1213400	1456080	1617870	1820100	2022340
91/2 95/8	70.882	1262590	1515110	1683450	1893880	2104310
08/8	72.760 74.662	1313090 1364910	1575700 1637900	1750780 1819880	1969630 2047370	2188480 2274850
934 978	76.590	1418090	1701700	1890780	2127130	2363480
10	78.540	1472620	1787150	1963500	2208930	2454370
1016	82.516 86.590	1585850 1704740	1903020 2045690	2114470 2272990	2378780 2557120	2643090 2841240
101/4 101/2 103/4	90.763	1829430	2195320	2439250	2744150	3049060
11	95.033	1960060	2352070	2613410	2940090	3266770
111/4	99.402	2096760 2239670	2516110 2687610	2795680 2986230	3145140 3359510	3494600 3732790
12	113.098	2544690	3053630	3392920	3817040	4241150

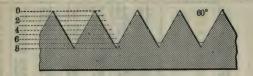
### DIMENSIONS OF BOLTS AND NUTS.

Franklin Institute Standard.

		Bolts a	nd Thre	ads.	* *** ** **	Re	ugh Nu	its and	Head	is.
Diameter of Bolt.	Threads per Inch.	Diameter at Root of Thread.	Width of Flat.	Area of Bolt Body.	Area of Bolt at Root of Thread.	Short Diameter of Square and Hexagon.	Long Diameter of Square.	Long Diameter of Heragon.	Thickness of Muts.	Thickness of Heads.
Ins.	No.	Ins.	Ins.	8q. Ins.	Sq. Ins.	Ins.	Ins.	Ins.	Ins.	Ins.
4-5-1-00-7-1-00-	20 18 16 14 13 11 10 9 8 7 7 6 6 5 5 5 5 4 4 4 4 4 15 15 14 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	.185 .240 .294 .344 .400 .454 .507 .620 .731 .837 .940 1.065 1.160 1.284 1.389 1.490 1.615 2.175 2.425 2.175 2.425 2.879 3.100 3.317 3.567 3.798 4.028 4.255 4.480 4.780 4.953 5.903	.0062 .0070 .0078 .0089 .0096 .0104 .0113 .0125 .0140 .0180 .0210 .0227 .0250 .0280 .0280 .0280 .0380 .0310 .0357 .0357 .0357 .0357 .0367 .0400 .0410 .0400 .0400 .0500 .0500	.049 .077 .110 .150 .196 .249 .307 .442 .601 .785 .994 1.227 1.485 1.767 2.074 2.405 2.761 3.142 3.976 4.909 5.940 7.069 9.621 11.045 12.566 14.186 15.904 17.721 19.635 21.648 23.758	.027 .045 .068 .093 .126 .162 .202 .302 .420 .550 .694 .893 1.057 1.295 1.515 1.744 2.302 3.023 3.715 4.619 5.428 8.641 9.993 11.329 12.743 14.220 14.230 14.240 14	#10110011 110110 100100 100100 100100 100100	.707 .840 .972 1.105 1.238 1.370 1.503 1.768 2.038 2.298 2.568 2.829 3.094 3.359 3.624 4.420 4.950 5.480 6.011 6.541 7.071 7.602 8.132 8.662 9.193 9.723 10.253 10.784 11.314 11.314 11.314	7.073 7.506 7.939 8.372 8.805 9.238 9.671	111111111120 14 20 0 0 0 0 0 4 4 4 5 5 5 5 5 5 5 5 5 5 5	44-40-64-6-14-13 03:00-60-60-60-60-60-60-60-60-60-60-60-60-6
53 53 6	238 238 214	4.953 5.203 5.423	.0526 .0526 .0555	23.758 25.967 28.274	19.267 21.262 23.098	838 834 918	11.844 12.375 12.905	10.104	534	4 1 6 4 8 4 9 4 1 6

# RULES FOR PROPORTIONS OF BOLTS AND NUTS.

#### Franklin Institute Standard.



The dimensions of nuts and bolts are determined by the following rules, which apply to both square and hexagon.

Short diameter of rough nut =  $1\frac{1}{2} \times$  diameter of bolt +  $\frac{1}{8}$  in. Short diameter of finished nut =  $1\frac{1}{2} \times$  diameter of bolt +  $\frac{1}{10}$  in.

Thickness of rough nut = diameter of bolt.

Thickness of finished nut = diameter of bolt  $-\frac{1}{16}$  in.

Short diameter of rough head =  $1\frac{1}{2} \times \text{diameter of bolt} + \frac{1}{8} \text{ in.}$ 

Short diameter of finished head =  $1\frac{1}{2} \times$  diameter of bolt +  $\frac{1}{16}$  in.

Thickness of rough head  $= \frac{1}{2}$  of short diameter of head.

Thickness of finished head = diameter of bolt  $-\frac{1}{16}$  in.

In 1864, a committee of the Franklin Institute recommended the above system of screw threads and bolts which was devised by Mr. William Sellers, of Philadelphia. This system as far as it relates to screw threads is generally used in the United States, but the proportions of bolt heads and nuts are not adhered to because the sizes of bar required to make the nuts are special and extra work is necessary to make the bolt heads. Sizes of nuts and bolt heads in accordance with the Manufacturers' Standard are given on pages 369, 370 and 371.

## WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND HEXAGON NUTS.

Franklin Institute Standard Sizes.

Basis—1 cubic foot Iron = 480 pounds

Basis—1 cubi	c foot	Iron =	480 p	ounds.			
Length under Head to Point.		Diam	eter o	f Bolt	s in I	aches.	
Inches.	1	<u>5</u>	38	7	1/2	9	8
1½ 1¾	4.9	8.2	12.2	17.5	24.0	31.8	41.1
13/4	5.3	8.7	13.0	18.5	25.3	33.5	43.2
2 214 214 224 234	5.6	9.2	13.8	19.6	26.7 28.1	35.2 37.0	45.8 47.8
21/2	6.3	10.3	15.3	21.6	29.4	38.7	49.6
	0.0	10.8	16.1	22.7	30.8	40.4	51.7
3 3 1/4	7.0	11.4	16.8	23.7	32.1 33.5	42.1	53.9
312	7.7	12.4	18.4	25.8	34.9	45.6	58.
33%	8.0	13.0	19.1	26.9	36.2	47.3	60.2
4	8.3	13.5	19.9	27.9	37.6	49.0	62.
41/2	9.0	14.6 15.6	21.4	30.0	40.3	52.5 55.9	70.5
51/2	10.4	16.7	24.5	34.2	45.8	50.4	75.
8	11.1	17.8	26.0	36.2	48.5	62.8	79.
61/2	11.7	18.8	27.6	38.3	51.2	66.3	83.
71/2	12.4 13.1	19.9 21.0	29.1 30.6	40.4	53.9 56.7	69.7	87.5
8	13.8	22.0	32.2	44.6	59.4	76.6	96.
81/2	14.5	23.1	33.7	46.7	62.1	80.1	100.
9	15.1	24.2	35.3	48.8	64.8	83.5	105.
9½ 10	15.8	25.2 26.3	36.8	50.8 52.9	67.6	87.0 90.4	109:
101/2	17.2	27.4	39.9	55.0	73.0	93.9	117.
11	17.9	28.4	41.4	57.1	75.7	97.3	122.
111/2	18.5	29.5	42.9	59.2	78.5	100.8	126.
12 12½		30.5 31.6	44.5	61.3	81.2 83.9	104.2 107.7	130.
13		32.7	47.5	65.4	80.6	111.1	139.
131/2		33.7	49.1	67.5	89.4	114.6	143.
14			50.6	69.6	92.1	118.0	147.
14½ 15			52.1 53.7	71.7	94.8	121.5 124.9	151. 156.
151/2			55.2	75.9	100.3	128.4	160.
16				77.9	103.0	131.8	164.
161/2				80.0	105.7	135.3	168.
17 171/2				82.1 84.2	108.4	138.7 142.2	173. 177.
18				01.4	113.9	145.6	181.
181/2					116.6	149.1	185.
10					119.3	152.5	190.
19½ 20					122.1 124.8	156.0 159.4	194. 198.
One inch in length of 100 Bolts.	1.36	2.13	3.07	4.18	5.45	5.90	8.5
To obtain Weights with Square \\ Nuts per 100: Add	.23	.41	.66	.99	1.42	1.96	2.62
Weight of one Hexagon Nut	.0116	.020	.031	.046	.065	.088	.11
Weight of one Hexagon Head	.0150	.025	.039	.057	.081	.109	.144
Weight of one Square Nut	.0139	.024	.038	.056	.079		

All weights are approximate.

# WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND HEXAGON NUTS.

Franklin Institute Standard Sizes. Basis-1 cubic foot Iron = 480 pounds.

Length under Head to Point.		Diam	eter o	Bolt	in In	ches.	
Inches,	34	7 8	1	11/8	11	13	11/2
11/2	64.5	95.2	134	182	240	309	390
13/4	67.6	99.4	140	189	248	319	402
2	70.6	103.5	145	196	257	329	414
	73.7	107.7	150	203	265	340	426
214 213 234	76.8 79.8	111.9 116.1	156 161	210 216	274 282	350 360	439
31/4	82.9	120.2	167	223	291	371	463
31/4	86.0	124.4	172	230	300	381	475
31/4	89.1	128.6	178	237	308	391	488
33/4	92.1	132.8	183	244	317	402	500
4	95.2	136.9	189	251	325	412	512
4)4	101.3	145.3	199	265	342	432	537
5	107.4	153.6	210	279	359	453	561
5)2	113.6	162.0	221	292	376	474	586
6	119.7	170.3	232	306	393	494	610
6½	125.9	178.7	243	320	410	515	635
7	132.0	187.0	254	334	427	536	659
7½	138.1	195.4	265	348	444	556	684
8	144.3	203.7	276	361	461	577	709
8½	150.4	212.1	287	375	478	597	733
9	156.5	220.4	298	389	495	618	758
9½	162.7	228.8	308	402	513	639	782
10	168.8	237.1	319	417	530	659	807
10½	174.9	245.5	330	430	547	680	831
11	181.1	253.8	341	444	564	701	856
11½	187.2	262.2	352	458	581	721	880
12	193.3	270.5	363	472	598	742	905
12½	199.5	278.9	374	486	615	762	929
13	205.6	287.2	385	499	632	783	954
13½	211.7	295.6	396	513	649	804	978
14	217.9	303.9	407	527	666	824	1003
14½	224.0	312.3	417	541	683	845	1027
15	230.1	320.6	428	555	700	866	1052
15½	236.3	329.0	439	568	717	886	1077
16	242.4	337.3	450	582	734	907	1101
16½	248.5	345.7	461	596	751	927	1126
17	254.7	354.0	472	610	768	948	1150
17½	260.8	362.4	483	624	785	969	1175
18 18½ 19 19½ 20	266.9 273.1 279.2 285.3	370.7 379.1 387.4 395.8	494 505 516 526	637 651 665 679	802 819 836 853	989 1010 1031 1051	1199 1224 1248 1273
One inch in length of 100 Bolts	291.5	16.70	21.82	693 27.61	870 34.09	1072	1297
To obtain Weights with Square \\ Nuts per 100: Add	4.35	6.72	9.81	13.73	18.57	24.42	31.42
Weight of one Hexagon Nut	.190	.289	.417	.579	.777	1.016	1.299
Weight of one Hexagon Head	.235	.357	.516	.616	.962	1.259	1.611
Weight of one Square Nut	.234	.356	.515	.716	.963	1.260	1.614
Weight of one Square Head	.271	.412	.596	.827	1.111	1.453	1.860

## WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND NUTS.

### WROUGHT IRON.

Manufacturers' Standard Sizes.

Basis-Hoopes & Townsend's List.

Length under Head to Point.		Di	amete	or of B	olt in	Inche	s.	
Inches.	1	5 16	38	7 16	1/2	16	5000	3 4
134	3.4	6.0	9.2	13.6	19.1	26.0	33.8	55.
2	4.1	7.1	10.8	15.7	21.8	29.5	38.1	61.
2½		8.2	12.3	17.8	24.6	33.0	42.4	67.
3 31/2	5.5 6.2	9.2	13.8 15.3	19.9 21.8	27.4 29.8	36.5 40.0	46.7 51.0	73. 80.
41/2	6.9	11.4	16.9	24.0	32.6	43.5	55.4	86.
	7.5	12.4	18.4	26.1	35.4	46.7	59.3	92.
5	8.2	13.5	19.9	28.2	38.1	50.2	63.6	98.
5½		14.6	21.5	30.3	40.9	53.7	67.9	104.
6	9.6	15.6	23.0	32.4	43.7	57.2	72.3	110.
6½	10.3	16.7	24.6	34.5	46.4	.60.7	76.6	116.
7 71/2	11.0	17.8	26.1	36.6	49.2	64.2	80.9	123
	11.7	18.9	27.7	38.8	51.9	67.6	85.2	129
8 9	12.4	20.0	29.2	40.9	54.7	71.1	89.5	135
	13.7	22.1	32.4	44.9	60.0	77.8	97.8	147
10	15.1	24.3	35.5	49.1	65.5	84.8	106.4	160.
11	16.5	26.4	38.6	53.4	71.0	91.8	115.1	172.
12	17.9	28.6	41.7	57.6	76.5	98.8	123.7	184
13	19.3	30.7		61.8	82.0	105.5	132.0	197
14	20.6	32.9	47.9	66.0	87.6	112.5	140.6	209
15	22.0	35.1	51.0	70.3	93.1	119.5	149.2	222
18	23.4	37.2	54.1	74.5	98.6	126.4	157.9	234
17	24.8	39.4	57.2	78.7	104.1	133.4	166.5	246
18	26.2	41.5	60.3	82.9	109.7	"140.4	175.1	259.
19	27.5	43.7	63.4	87.2	115.2	.147.4	183.7	271.
20	28.9	45.8	66.5	91.4	120.7	154.4	192.4	284.
21	30.3	48.0	69.6	95.6	126.2	161.4	201.0	296.
22	31.7	50.2	72.7	99.9	131.7	168.4	209.6	309.
23	33.1	52.3	75.8	104.1	137.3	175.4	218.3	321.
24	34.4	54.5	78.9	108.3	142.8	182.4	226.9	333.
25	35.8	56.6		112.5	148.3	189.3	235.5	346.

## WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND NUTS.

#### WROUGHT IRON.

Manufacturers' Standard Sizes. Basis—Hoopes & Townsend's List.

Length under Head		Di	amete	r of B	olt in	Inche	s.	
to Point. Inches.	7 8	1	11	11	138	11/2	13	2
11/2	83.4							
2 2½	91.8 99.7	129.0 140.1	184.5 198.4	264.8				
3 3½	108.1 116.6	151.1 182.2	212.4 226.4	282.0 299.3	350 370	470 495		
4	125.0	173.2	240.4	316.6	390	520	720	
4½	132.9	182.7	253.3	332.6	410	525	753	
5	141.3	193.7	267.3	349.9	430	570	786	1180
5½	149.8	204.8	281.2	367.1	450	595	820	1225
6	158.2	215.8	295.2	384.4	470	620	854	1270
6½	166.7	226.9	309.2	401.6	490	645	888	1315
7716	175.1	237.9	323.2	418.9	510	670	922	1316
	183.6	248.9	337.2	436.2	530	695	956	1405
8 9	192.0	260.0	351.1	453.4	550	725	990	1450
	208.3	281.3	377.0	486.7	590	775	1058	1540
10	225.2	303.3	404.9	521.2	630	825	1126	1630
11	242.2	325.5	432.9	555.8	670	875	1194	1720
12	259.1	347.6	460.8	590.3	710	925	1262	1810
13	276.0	369.6	488.8	624.8	751	975	1330	1900
14	292.9	391.7	516.7	659.3	793	1025	1398	1990
15	309.8	413.8	544.7	693.8	835	1075	1468	2080
16	326.7	435.9	572.7	728.3	877	1125	1536	2170
17	343.6	458.0	600.6	762.8	919	1175	1604	2260
18	360.5	480.1	628.6	797.4	961	1225	1672	2350
19	377.5	502.2	656.5	831.9	1003	1275	1740	2440
20	394.4	524.3	684.5	866.4	1045	1325	1808	2530
21	411.3	546.4	712.4	900.9	1087	1375	1876	2620
22	428.2	568.4	740.4	935.4	1129	1425	1944	2710
23	445.1	590.5	768.3	969.9	1171	1475	2012	2800
<u>54</u>	462.0	612.6	796.3	1004.5	1213	1525	2080	2890
25	478.9	634.7	824.3	1039.0	1255	1575	2148	2980

Bolts from  $1\frac{1}{6}$  inch to 2 inches, inclusive, are fitted with nuts made to U.S. Standard.

# WEIGHTS OF 100 ROUND-HEADED RIVETS OR ROUND-HEADED BOLTS WITHOUT NUTS.

#### WROUGHT IRON.

Basis-1 cubic foot Iron = 480 pounds.

	Diam	eter of	Rive	t in Ir	ches.	
38	1/2	<u>15</u>	34	78	1	11/8
4.7	9.5	16.0	25.2	37.2	52.6	71.3
5.5	10.7	18.1	28.3	41.3	58.0	78.2
6.2	12.1	20.2	31.3	45.5	63.5	85.1
7.0	13.4	22.4	34.4	49.7	68.0	92.0
7.8	14.8	24.5	37.5	53.9	74.4	98.9
8.5	16.2	26.6	40.5	58.0	79.8	105.8
9.3	17.5	28.8	43.6	62.2	85.3	112.7
10.1	18.9	30.9	46.7	66.4	90.7	119.6
10.8	20.3	33.0	49.8	70.6	96.2	126.8
11.6	21.6	35.1	52.8	74.7	101.6	133.4
12.4	23.0	37.3	55.9	78.9	107.1	140.3
13.1	24.3	39.4	59.0	83.1	112.6	147.2
13.9	25.7	41.5	62.0	87.3	118.0	154.1
14.7	27.1	43.7	65.1	91.4	123.5	161.0
15.4	28.4	45.8	68.2	95.6	128.9	167.9
16.2	29.8	47.9	71.2	99.8	134.4	174.8
17.0	31.2	50.1	74.3	104.0	139.8	181.3
17.7	32.5	52.2	77.4	108.2	145.3	188.6
18.5	33.9	54.3	80.4	112.3	150.7	195.6
19.3	35.3	56.4	83.5	116.5	156.2	202.8
20.0	36.6	58.6	86.6	120.7	161.6	209.4
20.8	38.0	60.7	80.6	124.8	167.1	216.3
21.6	39.3	62.8	92.7	129.0	172.5	223.1
22.3	40.7	65.0	95.8	133.2	178.0	230.1
23.1	42 1	67.1	98.8	137.4	183.5	237.0
23.9	43.4	69.2	101.9	141.6	188.9	243.9
24.8	44.8	71.4	105.0	145.7	194.4	250.8
25.4	46.2	73.5	108.0	149.9	199.8	257.7
26.2	47.5	75.6	111.1	154.1	205.3	264.0
27.7	50.2	79.9	117.2	162.4	216.2	278.4
29.2	53.0	84.1	123.4	170.8	227.1	292.1
30.8	55.7	88.4	129.5	179.1	238.0	306.0
32.3	58.4	92.7	135.6	187.5	248.8	319.8
33.8	61.2	96.9	141.8	195.8	259.8	333.6
35.4	63.9	101.2	147.9	204.2	270.7	347.4
36.9	66.6	105.4	154.1	212.5	281.6	361.2
38.4	69.3	109.7	160.2	220.9	292.5	375.6
3.07	5.45	8.52	12.27	16.70	21.82	27.61
	4.7 5.5 6.2 7.0 7.8 8.5 9.3 10.1 11.8 11.1 13.1 11.3 11.7 16.4 16.2 20.0 20.0 21.6 22.3 22.3 22.3 22.3 23.3 23.3 23.3 23	4.7 0.3 5.5 10.7 6.2 12.1 7.0 13.4 7.8 14.8 8.5 16.2 9.3 17.5 10.1 18.9 10.8 20.3 11.6 21.6 12.4 23.0 11.6 21.6 12.4 23.0 13.9 25.7 14.7 27.1 15.4 28.4 16.2 29.8 17.0 31.2 17.7 32.5 18.5 33.9 19.3 35.3 20.0 36.6 20.8 38.0 21.6 39.3 22.3 40.7 23.1 42 1 24.3 24.3 25.7 40.2 26.2 47.5 27.7 50.2 29.2 53.0 30.8 55.7 32.3 58.4 33.8 61.2 33.8 61.2 33.8 61.2 33.9 66.3 38.4 60.3 30.7 5.45	3         1         8           4.7         9.3         16.0           5.5         10.7         18.1           6.2         12.1         20.2           7.0         13.4         22.4           7.8         14.8         24.5           8.5         16.2         26.6           9.3         17.5         28.8           10.1         18.9         30.9           10.8         20.3         36.1           12.4         23.0         37.3           13.1         24.3         39.4           13.9         25.7         41.5           14.7         27.1         43.7           15.4         29.4         45.8           10.2         29.8         47.9           17.0         31.2         50.1           17.7         32.5         52.2           18.5         33.9         54.3           19.3         35.3         56.4           20.0         36.6         58.6           20.8         38.0         60.7           21.6         39.3         62.3           22.3         40.7         65.1	3         1         8         3         4           4.7         9.3         16.0         25.2         5.5         10.7         18.1         28.3         3.6.2         12.1         20.2         31.3         7.0         13.4         22.4         34.4         7.8         14.8         22.4         34.4         4.8         4.8         6.0.1         18.9         26.6         40.5         9.3         17.5         28.8         43.6         10.1         18.9         30.9         46.7         46.7         10.8         20.3         35.1         52.8         12.4         23.0         37.3         55.9         12.4         23.0         37.3         55.9         12.4         23.0         37.3         55.9         12.4         23.0         37.3         55.9         12.4         23.0         37.3         55.9         12.4         23.0         37.3         55.9         12.4         24.0         49.8         11.5         24.8         45.8         68.2         12.4         14.7         27.1         43.7         65.0         14.7         27.1         43.7         65.0         14.7         27.1         14.7         27.1         43.7         65.2         27.7         14.5         6	\$\frac{1}{8}\$         \$\frac{1}{2}\$         \$\frac{1}{8}\$         \$\frac{1}{4}\$         \$\frac{7}{8}\$           4.7         9.3         16.0         25.2         37.2         5.5         10.7         18.1         22.3         41.3         6.5         16.2         12.1         20.2         31.3         45.5         7.0         13.4         22.4         34.4         49.7         7.8         14.8         22.4         34.4         49.7         7.8         1.8         20.3         33.0         49.8         7.5         53.9         8.5         16.2         26.6         40.5         58.0         9.3         17.5         28.8         43.6         62.2         10.1         18.9         30.9         46.7         66.4           10.8         20.3         33.0         49.8         70.6         14.1         12.4         23.0         37.3         55.9         78.9         13.1         12.4         23.0         37.3         55.9         78.9         13.1         12.4         33.0         49.8         70.6         87.3         14.7         26.1         74.3         19.4         16.4         28.4         43.8         68.2         95.6         86.8         29.6         86.6         29.6	4.7

## WEIGHTS AND DIMENSIONS OF BOLT HEADS.

### MANUFACTURERS' STANDARD SIZES.

Basis—Hoopes & Townsend's List.

Diameter		Squ	lare.			Inches.   Inches.   Inches.   Pounds.				
of Bolt.	Short Diameter.	Long Diameter.	Thickness.	Weight per 100.	Short Diameter.		Thickness.			
Inches.	Inches	Inches.	Inch.	Pounds.	Inches.	Inches.	Inches.	Pounds,		
1	. 3 8	.530	3 16	.7	1	.433	3 16	.6		
5 16	15 32	.664	15	1.4	15	.541	15	1.2		
3 8	9 16	795	9 32	2.5	9 16	.670	32	2.2		
75	31	,928	21 64	4.0	313	.758	81	3.4		
3	3	1.061	3 8	5.9	3 4	.866	38	5.1		
9	27 32	1.193	37	8.4	37 32	.974	27 64	7.3		
5 8	15	1.326	15 32	11.5	15	1.083	15 32	10.0		
3 4	11	1.591	9 16	19.9	11/8	1.299	9 16	17.3		
7 8	15	1.856	31	31.1	1 5 16	1.516	31	27.4		
1	11/2	2.122	3 4	47.3	11/2	1.733	3 4	42.0		
11	111	2.386	27 32	67.3	111	1.944	27 32	58.3		
11	17/8	2.652	15	92.3	17	2.166	15 16	80.0		
13	21/16	2.917	1 1 3 2	122.8	21/16	2.383	11/32	106.5		
13	21	3.182	11/8	159.5	21	2.599	11/8	138.2		
15	27	3.447	1 7 3 2	202.7	27/16	2.818	1 7 32	175.7		
13	25	3.712	15	253.2	25	3.032	15	219.5		
178	213	3.977	113	311.5	213	3.349	113	269.8		
2	3	4.243	11/2	378.0	3	3.464	11/2	327.6		

# WEIGHTS AND DIMENSIONS OF HEXAGON NUTS.

### MANUFACTURERS' STANDARD SIZES.

Basis—Hoopes & Townsend's List.

Diameter				Diameter	Pla	in.	Cuj	pped.
of Belt.	Short Diameter.	Long Diameter.	Thickness.	Rough Hole.	Weight per 100.	Number in 100	Weight per 100.	Number in 100
Inches.	Inches.	Inches.	Inches.	Inch.	Pounds.	Pounds.	Pounds.	Pounds,
Terresta de la 11111 de la companya de la 111111 de la companya de	Andreader for for	.578 .722 .568 .668 .668 .668 .6011 .011 .1.155 .1.155 .1.155 .1.299 .1.299 .1.299 .1.299 .1.444 .1.444 .1.588 .1.733 .1.	Para Proper Property Control of C	7일 등 함께 하는 것이 되는 것이 되었다.	1.3. 2.3 4.3 7.0 7.5 9.9 10.8 13.7 15.9 17.9 19.5 23.0 22.2 26.6 30.3 34.5 40.0 37.7 45.9 50.8 57.5 63.7 100.0 138.9 185.2 243.9	7800 4440 2330 1430 1330 1010 930 730 630 560 514 435 450 376 330 290 250 265 218 221 197 174 157 100 72 54	1.2 2.1 4.0 6.3 6.9 9.2 10.2 12.5 15.2 17.0 18.5 21.7 20.6 25.4 28.8 32.3 37.6 35.3 43.5 42.6 47.6 53.8 90.9 126.6 169.5 169.6	8500 4790 2510 1580 1440 1090 980 800 660 588 541 460 485 394 347 310 266 283 230 235 210 186 168 110 79 59 45

# WEIGHTS AND DIMENSIONS OF SQUARE NUTS.

### MANUFACTURERS' STANDARD SIZES.

Basis—Hoopes & Townsend's List.

Diameter				Diameter	Pla	in.	Cu	pped.
of Bolt.	Short Diameter,	Long Diameter.	Thickness.	Rough Hole.	Weight per 100.	Number in 100	Weight per 100.	Number in 100
Inches.	Inches.	Inches.	Inches.	Inch	Pounds.	Pounds.	Pounds.	Pounds.
1	1/2	.707	1	7 32	1.5	6750	1.4	7200
16	5 8	.884	16	33	2.8	3540	2.5	4000
3 8	3	1.061	3 8	/ 11/32	4.8	2100	4.2	2380
7	7 8	1.237	7 16	13 32	7.5	1330	6.8	1460
1/2	7 8	1.237	1 2	7 16	8.9	1120	8.1	1230
1 2	1	1.414	1/2	7 16	11.9	840	10.8	930
16	11/8	1.591	9 16	1/2	15.4	650	14.3	700
-	118	1.591	8	9 16	17.3	575	16.1	620
5 6	114	1.768	5 8	9 16	23.0	435	21.1	475
3	114	1.768	34	21 32	27.8	360	25.0	400
34	138	1.945	34	21 32	31.7	315	29.0	345
3	11/2	2.122	3 4	31 32	41.0	244	37.0	270
78	11/2	2.122	7 8	25 32	46.5	215	41.7	240
현생 이상 이상 가는 가는 가	158	2.298	7 8	25 32	55.6	180	48.8	205
78	13	2.475	7 8	25 82	61.3	163	54.6	183
1	134	2.475	1	7 8	70.9	141	64.1	156
1	2	2.828	1	7 8	95.2	105	87.0	115
11/8	2	2.828	11/8	15 16	102.0	98	94.3	106
118	21	3.182	11/8	18	135.1	74	123.5	81
11	21	3.182	11/4	11/16	156.3	64	142.9	70
11	$2\frac{1}{2}$	3.536	114	116	192.3	52	175.4	57
13	23	3.889	138	1316	250.0	40	227.3	44
11/2	3	4.243	11/2	15/16	307.7	321	285.7	35
15	31/4	4.597	15	17/16	454.5	22	400.0	25
13	31/2	4.950	13	1 9 16	555.6	18	500.0	20
17/8	334	5.303	178	111	666.7	15	625.0	16
2	4	5.657	2	113	816.3	121	784.3	121

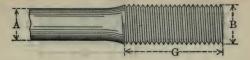
#### UPSET SCREW ENDS FOR ROUND BARS.



Diameter of Bar.	Area inf Body of	Diameter of Screw.	Length of Upset.	Area at Root of	Number of Threads	Weight per Foot of Bar.	Add for Upset.	Area at Root of Thread Over that of
A	Bar.	B	Œ	Thread.	per Inch.			Body of Bar.
Inch.	Sq. Ins.	Inches.	Inches.	Sq. Ins.		Pounds.	Inches.	Per Cent.
16 5 8 11 16	.196 .249 .307 .371	1 1	41 41 41 41 41	.302 .302 .420 .550	10 10 9 8	.668 .845 1.043 1.262	6½ 4¼ 5½ 6¼	54 21 37 48
ale sie ole	.442 .519 .601 .690	1 11 11 11 11	4½ 4¾ 4¾ 4¾ 4¾	.550 .694 .893 .898	8 7 7	1.502 1.763 2.044 2.347	4½ 5½ 6¼ 4½	25 34 49 29
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.785 .887 .994 1.108	1300 121 121	5 5 5	1.057 1.057 1.295 1.295	6 6 6	2.670 3.014 3.379 3.766	51 41 43 31	35 19 30 17
1½ 1½ 1½ 1½ 1½ 1½	1.227 1.353 1.485 1.623	150 134 170 170	51 51 51 51 51	1.515 1.744 1.744 2.048	5 5 5 5	4.173 4.600 5.049 5.518	4½ 5 4 4¾	23 29 18 26
1½ 1½ 1½ 1½ 1½ 1½	1.767 1.918 2.074 2.237	2 2 2 2 2 2 2	51212234 5534 554	2.302 2.302 2.650 2.650	4½ 4½ 4½ 4½ 4½	6.008 6.520 7.051 7.604	5½ 4½ 5 4½	30 20 28 18
13 113 116 116 115	2.405 2.580 2.761 2.948	21 21 21 21 21 21	534 534 6	3.023 3.023 3.419 3.715	4½ 4½ 4½ 4½	8.178 8.773 9.388 10.020	434 4 412 5	26 17 24 26

Lengths of Upset Ends above are best adapted for use with Turnbuckles of standard length, six inches between heads, as shown on page 378, and with Clevises shown on page 380. Lengths of Upset Ends for use with ordinary Right and Left Nuts, shown on page 379 may be one inch shorter than above.

#### UPSET SCREW ENDS FOR ROUND BARS.



Diameter of Bar.	Area of Body of Bar.	Diameter of Screw.	Length of Upset.	Area at Root of Thread.	Number of Threads per Inch.	Weight per foot of Bar.	Add for Upset.	Excess of Area at Root of Thread Over that of Body of Bar.
Inches.	Sq. Ins.	Inches.	Inches.	Sq. Ins.		Pounds.	Inches.	Per Cent.
$\begin{array}{c} 2 \\ 2\frac{1}{16} \\ 2\frac{1}{8} \\ 2\frac{3}{16} \end{array}$	3.142 3.341 3.547 3.758	21/25/20/20/20/20/20/20/20/20/20/20/20/20/20/	6 61 61 61	3.715 4.155 4.155 4.619	4 4 4	10.68 11.36 12.06 12.78	41 41 4 4 4	18 24 17 23
$2\frac{1}{4}$ $2\frac{5}{16}$ $2\frac{3}{8}$ $2\frac{7}{16}$	3.976 4.200 4.430 4.666	278 278 3 3 3	6½ 6½ 6½ 6¾	5.108 5.108 5.428 5.957	4 4 3½ 3½ 3½	13.52 14.28 15.07 15.86	51 41 43 43 51	28 22 23 28
2½ 2½ 2½ 2½ 2½ 2½	4.909 5.157 5.412 5.678	20 14 14 14 15 20 20 20 20 20 20 20 20 20 20 20 20 20	62 62 63 64 7	5.957 6.510 6.510 7.087	31/2 31/2 31/2 31/2 31/2	16.69 17.53 18.40 19.29	43 51 41 5	21 26 20 25
213 213 216 27 215 215	5.940 6.213 6.492 6.777	Signal and so so	7 7 7½ 7½ 7½	7.087 7.548 8.171 8.171	3½ 3¼ 3¼ 3¼ 3¼	20.20 21.12 22.07 23.04	4½ 4¾ 5¼ 4¾ 4¾	19 22 26 21
3 3 3 3 3 3 3 3 3 3 3 3	7.069 7.670 8.296 8.946	33 37 4 4 43	71 71 71 71 71 71	8.641 9.305 9.993 10.706	3 3 3	24.03 26.08 28.20 30.42	5 51 43 43 43	22 21 20 20
1 (214 maj 47-jo	9.621 10.321 11.045 11.793	41 42 45 43 43	8 8 8 8 8 8	11.329 12.743 13.544 14.220	278 234 248 258	32.71 35.09 37.56 40.10	4½ 5¼ 5¼ 5	18 23 23 21
4 15	12.566	5	81/2	15.763	21/2	42.73	51	25

Lengths of Upset Ends above are best adapted for use with Turnbuckles of standard length, six inches between heads, as shown on page 378, and with Clevises shown on page 380. Lengths of Upset Ends for use with ordinary Right and Left Nuts, shown on page 379, may be one inch shorter than above.

### UPSET SCREW ENDS FOR SQUARE BARS.



Side of Square Bar.	Area of Body of Bar.	Diameter of Sorew.	Length of Upset.	Area at Root of Thread.	Number of Threads per Inch.	Weight per Foot of Bar.	Add for Upset.	Excess of Area at Root of Thread Over that of Body of Bar.
Inch.	Sq. Ins.	Inches.	Inches.	Sq. Ins.	mon.	Pounds.	Inches.	Per Cent.
1 9 16 5 8 11 16	.250 .316 .391 .473	34 778 1	41 41 41 41 41 41	.302 .420 .550	10 9 8 8	.850 1.076 1.328 1.607	4 5 5 3 3 4	21 33 41 17
3 13 16 15 16	.563 .660 .766 .879	110 110 110 100 100	43 43 5 5	.694 .893 1.057 1.057	7 7 6 6	1.913 2.245 2.603 2.989	4½ 5 5½ 4¼	23 35 38 20
$ \begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 3 \\ 1 \\ 3 \\ 1 \\ 6 \end{array} $	1.000 1.129 1.266 1.410	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5 5 1 5 1 5	1.295 1.515 1.515 1.744	5 1/2 5 5 5	3.400 3.838 4.303 4.795	434 52 44 43 43	29 34 20 24
$ \begin{array}{c} 1\frac{1}{4} \\ 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \end{array} $	1.563 1.723 1.891 2.066	17/8 17/8 2 21/8	512 5212 531 531	2.048 2.048 2.302 2.650	5 5 4 <sup>1</sup> / <sub>2</sub> 4 <sup>1</sup> / <sub>2</sub>	5.312 5.851 6.428 7.026	51 41 41 42 51	31 19 22 28
1½ 1½ 1½ 1½ 1½ 1½	2.250 2.441 2.641 2.848	214 214 230 230 230	5 <sup>3</sup> / <sub>4</sub> 5 <sup>3</sup> / <sub>4</sub> 6	2.650 3.023 3.419 3.419	4½ 4½ 4½ 4½ 4½	7.650 8.300 8.978 9.682	41 41 5 41	18 24 30 20
13 113 17 17 115 115	3.063 3.285 3.516 3.754	2225 225 225 225 225 225 225	6 61 61 61 61	3.715 4.155 4.155 4.619	4 4 4	10.410 11.170 11.950 12.760	4½ 5 4¼ 4½	21 26 18 23

Lengths of Upset Ends above are best adapted for use with Turnbuckles of standard length, six inches between heads, as shown on page 378, and with Clevises shown on page 380. Lengths of Upset Ends for use with ordinary Right and Left Nuts, shown on page 379, may be one inch shorter than above.

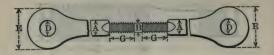
### UPSET SCREW ENDS FOR SQUARE BARS.



Side of Square Bar.	Area of Body of	Diameter of Screw.	Length of : Upset.	Area at Root of	Number of Threads	Weight per Foot of Bar.	Add for Upset.	Excess of Area at Root of Thread Over that of
A	Bar.	В	G	Thread.	per Inch.	0.000	opson	Body of Bar.
Inches.	Sq. Ins.	Inches.	Inches.	Sq. Ins.		Pounds.	Inches.	Per Cent.
$\begin{array}{c} 2 \\ 2\frac{1}{16} \\ 2\frac{1}{8} \\ 2\frac{3}{16} \end{array}$	4.000 4.254 4.516 4.785	27/8 27/8 3 3 31/8	6½ 6½ 6½ 6¾	5.108 5.108 5.428 5.957	4 4 3 <sup>1</sup> / <sub>2</sub> 3 <sup>1</sup> / <sub>2</sub>	13.60 14.46 15.35 16.27	5 41 41 5	28 20 20 24
$\begin{array}{c} 2\frac{1}{4} \\ 2\frac{5}{16} \\ 2\frac{3}{8} \\ 2\frac{7}{16} \end{array}$	5.063 5.348 5.641 5.941	314300300 300300	63 63 7 7	5.957 6.510 7.087 7.087	312 321 321 321 321 321	17.22 18.19 19.18 20.20	414 434 514 42	18 22 26 19
$\begin{array}{c} 2\frac{1}{2} \\ 2\frac{9}{16} \\ 2\frac{5}{6} \\ 2\frac{11}{16} \end{array}$	6.250 6.566 6.891 7.223	375   S   S   S   S   S   S   S   S   S	7 71 71 71 71	7.548 8.171 8.171 8.641	31 31 31 31 31	21.25 22.33 23.43 24.56	4 <del>1</del> 54 4 <u>1</u> 4 <u>3</u> 4 <u>3</u>	21 24 19 20
$\begin{array}{c} 2\frac{3}{4} \\ 2\frac{13}{16} \\ 2\frac{7}{8} \\ 2\frac{15}{16} \end{array}$	7.563 7.910 8.266 8.629	37/8 37/8 4 41/8	7½ 7½ 7½ 7½ 7½ 7½	9.305 9.305 9.993 10.706	3 3 3 3	25.71 26.90 28.10 29.34	54 42 43 5	23 18 21 24
3 3 3 3 3 4 3 3 3 3 3 3	9.000 9.766 10.563 11.391	453 425 425 425 425 425 425 425 425 425 425	7 <sup>3</sup> / <sub>4</sub> 8 8 8 <sub>1</sub>	10.706 12.087 12.743 13.544	27 27 23 23 23	30.60 33.20 35.92 38.73	4½ 5¼ 5 5	19 24 21 19
31500014710 300014710	12.250 13.141 14.063 15.016	478 5 518 514	81 81 81 82 84 84	15.068 15.763 16.658 17.572	25 21 21 22 21 21 21	41.65 44.68 47.82 51.05	5½ 5¼ 5 4¾	23 20 18 17
4	16.000	51	9	19.267	23	54.40	51	20

Lengths of Upset Ends above are best adapted for use with Turnbuckles of standard length, six inches between heads, as shown on page 378, and with Clevises shown on page 380. Lengths of Upset Ends for use with ordinary Right and Left Nuts, shown on page 379, may be one inch shorter than above.

#### UPSET SCREW ENDS FOR FLAT BARS.



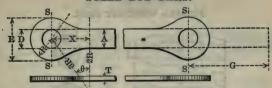
Width of Bar.	Thickness of Bar.	Diameter of Upset.	Area	Area at Root of	Length of Upset.	Add
A	T	B	Bar.	Thread.	G	Upset.
Inches.	Inch.	Inches.	Sq. Inches.	Sq. Inches,	Inches.	Inches.
2	1	2	2.00	2.30	51	6 .
2 3	1	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2.63	3.023	61	111
3	1	21	3.00	3.719	61	111
3 3 3 3 3	11	25	3.38	4.159	7	111
3	11	24	3.75	4.62	7	11
3	13	27	4.13	4.92	7	10
3	11	3	4.50	5.43	7	10
4	1	2½ 2½	3.00	3.719	61	123
4	1 1	28	3.50	4.159	7	12
4	1	24	4.00	4.62	7	11
4 4	14	8	4.50	5.43	7	11
4	14	31	5.00	6.51	71	11
4	18	31	5.50	6.51	71 71	11
9	19	01	6.00 6.50	7.54 7.54	73	10
, Ž	13	3½ 3½ 3½ 3½ 2½ 2½	7.00	8.64	73	91
5	17	93	3.75	4.62	72	11
5	: 1	3	4.38	5.43	7	11
5	18	31	5.00	6.51		104
5	11	31 31 31	5.63	6.51	7½ 7½	101
5	11	31	6.25	7.55	74	91
5	18	3	6.88	8.64	75	91
5	11	33	7.50	8.64	74	91 91
5	15		8.13	9.99		
5	13		8.75	9.99	21	
6	11	37	6.75	8.64	71	10
6	11	34	7.50	8.64	73	9
5555556666	17		8.25	9.99		
6	11		9.00	9.99		

For dimensions of heads corresponding to different-sized pins, see table of Eye Bars on page 377.

Shortest length of bar permissible on account of method of manufacture is 6'0" center to end.

The above length is used only for bars having heads 12½" diameter or less. When possible lengths of 7′0" are preferred.

#### STEEL EYE BARS.



Az = Area of Excess to form one Head = Plane Area of Head - AX. Az =  $\frac{(180 + 2\theta)}{360} \pi R^2 + \left(4 R^2 - \frac{A^2}{4}\right) \text{Tan.} \theta - .0698 R^2\theta$ .  $\frac{2R + \frac{A}{2}}{360} = \frac{2R + \frac{A}{2}}{360} = \frac{5Az}{360} = \frac{7.940848 - 10}{360} = \frac{360}{360} = \frac{360}{3$ 

3R

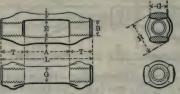
".0698 = 8.843855 - 10.

The control of the	lye Re-
2 4½ 1½ 33% 7½ 2 5½ 2½ 12½	
2 . 5½ 2¼ " 12½	
3	
9 1 21 9 " 361 10 361	
10   11/2   24/2   10/2	

The size of head given is the size of die. The size of finished head will overrun this about  $\frac{1}{2}$ . Eye Bars are Hydraulic Forged without the addition of extraneous metal and without buckles or welds. The heads on Eye Bars are finished of the same thickness "T" as body of bar.

## TURNBUCKLES.

### PRESSED WROUGHT IRON.



The Cleveland City Forge and Iron Co.

Di	Dimensions of Bar.						-		
Diameter of Serew.	Diameter of Bar.	Side of Square Bar.	L	T	A	E	F	H	G
Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
\$ 1 1 1 1 1 1 1 2 2 2 2 2 3 3 3 3 4 4 4 5 5	12 and 15 a 15	16 and 18 8 16 116 116 116 116 116 116 116 116	7½ 7½ 7½ 7½ 7½ 7½ 7½ 7½ 7½ 7½ 7½ 7½ 7½ 7	11/1/2 11	66666666666666666666699999	25 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	10.2.2.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.	11466 1146 11466 1	11/4 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6

Standard Lengths, 6, 9, 12, 15, 18, 24, 36, 48 and 72 inches between heads (A) for all sizes.

Lengths of Upset Ends shown on pages 372 to 375 inclusive are those best adapted for use with Turnbuckles of Standard Lengths, as above. Dimensions E. F. G and H depend upon the specifications of the Bars with which the Turnbuckles are to be used.

# RIGHT AND LEFT NUTS.



Diam-	Length	Diameter	Side	Length	Length	Diam-	Weig	
eter of Screw.	of Upset.	of Bar.	of Square Bar.	of Nut.	of Thread.	eter of Hex.	One Nut.	One Nut and Two Screw
В	G	A	A	L	T	W	-	Ends.
Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Pounds.	Pounds.
1 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2	444455555555666667777	5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	To 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9 9½ 9½ 9½	11 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2	11 1 2 2 2 2 2 2 2 2 2 3 3 3 3 3 3 3 3 4 4 4 4	14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	44444771111111111111111111111111111111
1110149014716 1111111111111111111111111111111111	445454 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	7 4 15 1 6 15 1 6 15 1 7 16 1 8 13 1 1 16 1 1 16	1 1 1 6 1 1 8 1 1 1 1 1 1 1 1 1 1 1 1 1	12 8½ 8½ 9 9 9 9 9 9½	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ম ম ম ম লাকলাকলাৰলাৰ নাকলাক	4 4 64 64 83 83 124 124	93 93 151 151 21 21 29 29 29 29

For Details of Upset Ends, see pages 372 to 375 inclusive. Length of Upset Ends for use with Right and Left Nuts may be made one inch shorter than the dimensions given in column "G" above.

#### CLEVISES.

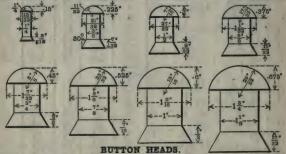


The Cleveland City Forge and Iron Co.

Diameter of Screw.	Length of Fork.	Length of Thread.			Di	am	ete	r of	Pi	n ir	I	ch	05.			USec	l with	ns to Speci ters I	fled
D	A	B	1	11/4	11/2	18/4	2	21/4	21/2	28/4	3	31/4	31/2	33/4	4	I	G	F	E
Ins.	Ins.	Ins.				Dia	am	eter	I	n I	nck	108.				Ins.	Ins.	Ins.	Ins.
8/4 7/8	51/2	11/8	23/4	23/4	28/4	3										28/4	11/2	1/2	17
1/8	51/2	13/8	23/4	28/4	3	31/	314									3	15/8	1/2	17
11/8	6	13/4		23/4	3	31/4	31/2	33/4								31/4	13/4	*	11
11/4	61/2	17/8		3	31/4	31/2	31/2	33/4	497							31/2	13/8	20	11
11/6	7 7	21/8		3/4	33/	4	43/6	43/8	48/4							33/4	2	5/8	11
15/8	7	21/2			33/4	4	48/8	48/4	51/4							4	21/8	5/8	23
13/4	8	25/8				48/8	48/4	51/4	51/4	51/4						48/8	21/4	11	3/4
2 8	9	3					51/4	51/4	58/	53/4	68/		111					_	
21/8	9	31/4						53/4	534	63/4	684	68/4				48/4	21/2	#	33
21/4	10	31/4						58/4	68/4	63/4	63/4	63/4				51/4	28/4	18	3/8
28/8	10	31/2						68/4	63/4	63/4	63/4	8	8			58/4	3	27	15
25/8	10	4							63/4	8	8	8	8	8	8	68/4	31/4	11	11
23/4	12	41/4							8	8	8	8	8	8	8	8	4	11	11/4
3/8	12	41/2	• • • •			• • • •				8	8	8 8	8	9	8	9	41/6	1.5	11/6

Dimension "H" is usually "I" larger than diameter of pin and "J" is made to suit the thickness of the pin plate. The above Clevises are designed for use with medium steel rods of 60000 to 68 000 pounds tensile strength per square inch. All clevis nuts with diameter "I" 8 inches or larger dimension "A" will be 12 inches.

# DIMENSIONS OF RIVET HEADS AFTER DRIVING.



Height of Head = % Diameter of Rivet. Radius of Head = % Diameter of Rivet + %.

COUNTERSUNK HEADS.

Diameter of Countersink Head same as Button Head. Angle of Countersink = 30°. In figuring Clearances for Rivet Heads allow for Heights as follows: %" for %" rivets, %" for %" rivets. All dimensions in inches.

# WEIGHTS, DIMENSIONS AND SAFE LOADS OF CHAINS.

As given by Standard Manufacturers.

Size.	C	omm	on Co	11.		Cr	ane.			Stud	Link	
Thickness of Link Bar.	Length of Link.	Width of Link.	Approximate Weight per Foot.	Safe Load in Thousand Lbs.	Length of Link.	Width of Link.	Approximate Weight per Foot.	Safe Load in Thousand Lbs.	Length of Link.	Width of Link.	Approximate Weight per Foot.	Safe Load in Thousand Lbs.
Ins.	Ins.	Ins.	Lbs,		Ins.	Ins.	Lbs.		Ins.	Ins.	Lbs.	
1 /4 1 /2 1 /2 1 /3 1 /4	13/8 11/2 13/4 21/8 21/4	7/8 11/4 11/4 11/2 11/6	.46 .75 1.10 1.55 2.00	.5 .8 1.3 1.8 2.3								
1/2 1/5 5/8 118	2½ 2½ 2½ 3¾ 3¾	17/8 21/8 21/4	2.60 3.25 4.00	3.3 4.0 4.8	31/8	21/8	4.0	6.9	3 3 <sup>3</sup> / <sub>8</sub> 3 <sup>3</sup> / <sub>4</sub> 4	13/4 2 21/4 21/2	2.3 3.0 4.0 4.8	4.8 5.9 6.3 8.5
*/4 †† ††	37/8 43/8	2 <del>11</del> 3½	5.90 8.0	6.8 9.3	35/8 41/8	21/2	6,3 8.0	9.6	43/8 43/4 5 53/8	23/4 3 31/4 31/2	5.7 6.7 7.3 8.5	10.1 11.9 14.0 15.8
1 1½ 1¼ 1¾ 1¾	5 5½ 6½	35/8 4 43/8	10.0 13.0 15.0	12.0 14.5 19.5	484 514 578 616	31/4 33/4 41/8 41/6	10.0 13.0 16.0 19.0	17.0 21.5 27.0 31.0	57/8 61/2 71/8 73/4	33/4 41/8 41/2 47/8	9.8 12.5 15.2 18.8	18.0 22.8 28.1 34.0
13/2 15/8 18/4 17/8					71/8 77/8 85/8 93/8	5 5½ 5 <sup>7</sup> / <sub>8</sub> 6 <sup>3</sup> / <sub>8</sub>	23.0 28.0 31.0 35.0	36.0 41.5 44.8 51.3	8½ 9¼ 10 10½	58/8 57/8 61/4 63/4	22.0 26.0 29.2 34.2	40.5 47.5 55.1 63.3
2 21/8 21/4 28/8 21/2					10½ 10½ 10½ 11½ 12 12½	63/4 71/8 75/8 8 83/8	40.0 47.0 53.0 58.5 65.0	58.3 65.8 73.7 82.0 90.9	111/8 12 13 13/2 14	71/4 73/4 81/4 83/4 9	40.0 44.2 50.0 54.2 80.0	72.0 81.3 91.1 101.5 112.5

Safe Loads based on one-half Proof Test, or one-fourth of the approximate breaking load of chain,

# BRIDGE PINS, NUTS AND PILOT NUTS.

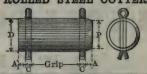


#### All Threads 8 per inch.

Nominal Diameter of Pin.	Turned Diameter of Pin.	Diameter of Thread.	Short Diameter of Nut.	Long Diameter of Nut.	Diameter of Holes
02 2 2 2 2	D	F	A	G	in Eye Bars.
Inches.	Inches.	Inches.	Inches.	Inches.	
11/4 12/4 21/4 21/4 21/4 31/4 31/4 31/4 31/4 41/4 41/4 41/4 4	1112223333444455566666666666666666666666666	1/4 1/2 1/2 1/2 2 2 2 2 2 2 2 3 3 4 4 4 4 4 4 4	2 21/2 21/2 3 3 31/2 4 4 41/2 41/2 5 5 5 6 6 6 6 6 7 7 7 7	2.231.72.4	D + 100

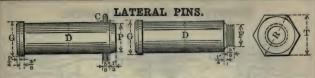
Allow 16" excess for each eye bar packed on the pin.

# COLD ROLLED STEEL COTTER PINS.



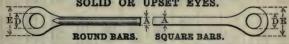
#### Dimensions of Pin in Inches.

Diameter of Pin.	D	1	11/4	11/2	13/4	2	21/4	21/2	23/4	3	31/4	31/2	33/4	4
Diameter of Reduced Point.	P	1 3/8	11/8	11/4	11/2	13/4	2	21/4	21/2	28/4	3	31/4	31/2	33/4
Lengths of Ends.	A	16	16	3/2.	1/2	3/2	1/2	1/2	1/2	7/8	7/8	7/8	7/8	7/8
Diameter of Cotter.	C	18	5 16	₩.	76	3/8	3/8	3/8	3/8	1/2	36	3/2	3/2	3/2
Diameter of Pin Hole.		110	15	100	113	216	25	200	218	316	3 5	3 0	318	416



Rough Diameter of Pin.	Nominal Diameter of Pin.	Finished Diameter of Pin.	Reduced Point.	Short Diameter of Nut.	Long Diameter of Nut.	Diameter of Thread.	Diameter of Cotter Pin.
Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inch.
	лионов.	AHOMOS.	THOROS.			дионов.	Inon,
11/2	11/4	116	1	15/8	17/8	- 1	13
13/4	11/2	175	1-/4	2	216	11/4	-
2	1%	128	172	21/3	21/8	11/3	-
21/4	21/	148	1%	272	278	173	2/
272	274	216	01/	272	2/8	172	3/8
23/4	272	011	274	372	478	2	4
21/	274	218	272	214	416	2	4
312	21/	218	274	414	23	214	44
38/	312	21	31/	416	5.4	212	44
4	33/4	3+1	31/2	416	53	216	45
-	D	- 6 511	-/-	D	- NT 1/11		

# COUNTER AND LATERAL RODS. SOLID OR UPSET EYES.



Diameter of Bar.	Diameter of Largest Head.	Diameter of Largest Pin.	Add for One Head.	Side of Square Bar.	Diameter of Largest Head.	Diameter of Largest Pin.	Add for One Head.
Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
7/6 1 1/4 11/4 11/4 11/4 11/4 11/4 11/4 21/4 2	214 414 414 5 5 514 6 6 614 714 8 8	114 214 214 224 234 234 3 3 3 3 4 4 4 4	9 18 16 20 18 22 20 18 21 21 19 21 21 21 22 22 34 25 24 22 24 25 24 24 25 25 26 27 27 28 28 28 28 28 28 28 28 28 28 28 28 28	1 11/4 11/4 11/4 11/4 11/4 11/4 11/4 2 21/4 22/4 22	414 414 5 5 5 5 6 6 6 6 7 7 7 8 8 8 8	21/2 22/4 23/4 33/4 33/4 33/4 4 4 4 4 4	16 14 18½ 16½ 18 16½ 18 16½ 18 16½ 18 16½ 19½ 19½ 21½ 21½ 21 19½ 22½ 23
*********				13/8	53/4	318	23 20
				11/2	31/2 41/2	21/4	20

For details of upset screw ends for round and square bars see pages 372 to 375.

# COUNTER AND LATERAL RODS. LOOP WELDED EYES.



Additional length of bar beyond center of pin required to make eye for square or round bars.

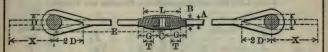
Diameter or Side of Bar.				Dia	meter	of Pi	n in I	nches.			
Inches.	34	1	11/4	11/2	13	2	21/4	21/2	23	3	31/4
* drucio col durio	5 <sup>3</sup> / <sub>4</sub> 6 <sup>3</sup> / <sub>4</sub>	63 71 72 8	7½ 8 8½ 9	8½ 9 9½ 10	$\begin{array}{c c} 9\frac{1}{2} \\ 10 \\ 10\frac{1}{4} \\ 10\frac{3}{4} \end{array}$	10½ 10¾ 11¼ 11¾ 11¾	11½ 11¾ 12¼ 12¾	12½ 12¾ 13¼ 13¼ 13½	13½ 13½ 14 14½	14 14½ 15 15½	15 15½ 16 16½
1 15 14 13 18		81/2	9½ 10 10¼	10½ 10¾ 11¼ 11¾	11½ 11¾ 12¼ 12¾ 12¾	12½ 12¾ 13¼ 13½ 13½	13½ 13½ 14 14½	14 14½ 15 15½	15 15½ 16 16½	16 16½ 16¾ 17¼	163 171 173 181
1½ 1½ 1½ 1¾ 1½ 1%				121	13½ 13½ 14	14 14½ 15 15½	15 15½ 16 16½	16 16½ 16¾ 17¼	163 171 173 181	173 181 183 191	18 <sup>3</sup> 19 <sup>1</sup> 19 <sup>1</sup> 20
2 2 2 2 2 3 2 8				• • • • •		16	163 171 18	17 <sup>3</sup> 18 <sup>1</sup> 18 <sup>3</sup> 19 <sup>1</sup>	183 194 193 204	19½ 20¼ 20¾ 21¼	20½ 21 21½ 21½ 22
21/2 25/3 25/4 27/6								193	20 <sup>3</sup> / <sub>4</sub> 21 <sup>1</sup> / <sub>4</sub> 21 <sup>3</sup> / <sub>4</sub>	213 221 223 223 231	223 234 234 241
3 3 3 3 4										233	24 <sup>3</sup> 25 <sup>1</sup> 25 <sup>3</sup>

Length in inches beyond center of pin required to form one eye = X.

FORMULÆ: When  $\frac{A}{2}$  = or < 1 X = 3.7 [D + A] + 1Length in inches beyond center of pin required to form one eye = X. A = Side or Diameter of Bar. D = D Diameter of Pin.Length in inches beyond center of pin required to form one eye = E -  $\frac{1}{2}$  C + X.

When  $\frac{A}{2} > 1$   $X = 3.7 [D + A] + \frac{A}{2}$ 

# COUNTER AND LATERAL RODS. LOOP WELDED EYES.



Additional length of bar beyond center of pin required to make eye for square or round bars.

Diameter or Side of Bar.				Dia	meter	of Pi	n in I	nches.			
Inches.	31/2	334	4	41	41/2	43	5	51	51/2	534	6
-(asiosierio	16 16 <sup>1</sup> / <sub>2</sub> 16 <sup>3</sup> / <sub>4</sub> 17 <sup>1</sup> / <sub>4</sub>	16½ 17½ 17¾ 18¼	17 <del>3</del> 18 <del>1</del> 18 <del>3</del> 19 <del>1</del>	18 <sup>3</sup> / <sub>19</sub> / <sub>1</sub> 19 <sup>1</sup> / <sub>2</sub> 20	19½ 20 20½ 21	20½ 21 21½ 21½ 22	21½ 22 22½ 22½ 22¾	$\begin{array}{c} 22\frac{1}{2} \\ 22\frac{3}{4} \\ 23\frac{1}{4} \\ 23\frac{3}{4} \end{array}$	23½ 23¾ 24¼ 24¾ 24¾	24½ 24¾ 25¼ 25¾ 25¾	251 251 26 261
1 1½ 1¼ 1¾ 18	173 184 183 194	18½ 19½ 19½ 20	19½ 20 20½ 21	20½ 21 21½ 21½ 22	21½ 22 22½ 22½ 22¾	22½ 22¾ 23¼ 23¾ 23¾	23½ 23¾ 24¼ 24¾ 24¾	24½ 24¾ 25¼ 25¾	25½ 25¾ 26 26½	26 26½ 27 27½	27 27½ 28 28½
1½5 158 1¾ 178	19½ 20 20½ 20½ 21	20½ 21 21½ 21½ 22	21½ 22 22½ 22½ 22¾	22½ 22¾ 23¼ 23¾ 23¾	23½ 23¾ 24¼ 24¾ 24¾	241 243 251 253	25½ 25¾ 26 26½	26 26½ 27 27½	27 27½ 28 28½	28 28½ 28¾ 29¼	284 294 294 294 304
2 2 2 2 4 2 3 2 3 2 3	21½ 22 22½ 22½ 23	$\begin{array}{c} 22\frac{1}{2} \\ 23 \\ 23\frac{1}{2} \\ 24 \end{array}$	23½ 23¾ 24½ 25	24½ 24¾ 25½ 25¾	25½ 25¾ 26¼ 26¾ 26¾	26 26½ 27¼ 27¾	27 27½ 28 28½	28 28½ 29 29½	28 <sup>3</sup> / <sub>29<sup>1</sup>/<sub>2</sub></sub> 30 30 <sup>1</sup> / <sub>2</sub>	29 <sup>3</sup> 30 <sup>1</sup> 30 <sup>3</sup> 31 <sup>1</sup>	30 <sup>3</sup> / <sub>4</sub> 31 <sup>3</sup> / <sub>4</sub> 31 <sup>3</sup> / <sub>4</sub> 32 <sup>1</sup> / <sub>4</sub>
21/215/80 3/47/8 2/2/8	$23\frac{1}{2}$ $24$ $24\frac{1}{2}$ $25\frac{1}{4}$	24½ 25 25½ 25½ 26	25½ 26 26½ 26½ 27	26½ 26¾ 27½ 28	27½ 27¾ 28¼ 28¾ 28¾	281 281 291 291 291	29 29 <del>1</del> 30 <del>1</del> 30 <del>1</del>	30 30½ 31 31½	31 31½ 32 32½	32 32½ 33 33½	323 331 333 343 342
क्षेत्र निवासिक स्थापन स्यापन स्थापन स्यापन स्थापन	25\\\ 26\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	26½ 27 27¾ 28¼ 28¼ 28¾	27½ 28 28½ 29½ 29½	28½ 29 29½ 30 30½	29½ 30 30½ 31 31½	30½ 30¾ 31¼ 31¾ 32½	31½ 31¾ 32½ 32¾ 32¾ 33¼	321 323 331 331 341 341	33 33½ 34 34¾ 35¼	34 34½ 35 35½ 36	35 35 <sup>1</sup> / <sub>3</sub> 36 36 <sup>1</sup> / <sub>3</sub> 37

For additional length required to form upset end and details of same see tables of Upset Ends, pages 372 to 375 inclusive.

For details of Turnbuckles, see page 378.

For details of Right and Left Nuts, see page 379.

# STANDARD STEEL WIRE NAILS AND SPIKES.

Sizes, Lengths and Approximate Number per Pound.

	Length.		Common		Brads.	rads.			Box.			Bar	
Size.	Ins.	Diam W. & M. G.	Inch.	No. per Lb.	Common B	Flooring Brads	Finishing.	Casing.	Smooth or Barbed Box.	Slating.	Shingle.	Heavy.	Light.
2d 3d 4d 5d 5d 7d 8d 9d 10d 12d 16d 20d 30d 40d 60d	1 11/4 11/2 18/4 2 21/4 21/2 28/4 3 31/4 31/2 4 41/2 5 51/2 6	15 14 12½ 12½ 11½ 11½ 10¼ 10¼ 9 8 6 5 4	.072 .080 .099 .099 .113 .1131 .131 .148 .148 .162 .192 .207 .225 .244 .263	876 568 316 271 181 161 106 90 69 03 40 31 24 18 14	876 568 316 271 181 161 106 59 63 49 31 24 18 14	157 139 99 90 69 54 43 31	1351 807 584 500 309 238 189 172 121 113 90 62	1010 635 473 406 236 210 145 132 94 87 71 52 46 35	1010 635 473 406 236 210 145 132 94 88 71 52 46 35	411 225 187 142 103	568 274 235 204 139 125 114 83	165 118 103 76 69 54 50 42 35 26 24 18 15	274 142 124 92 82 62 57 50 43 31 25 21 17
	설	Hir	ige.				111	96			Wi	re Spil	ces.
Size.	Length.	Wy.	Light,	Pence.	Clinch.	Fine.	Lining.	Barbed Roofing.	Barrel.	Tobacco.	Dian	eter.	No.
l'or	Ins.	Невту.	Lig	E-1	0	(Sa.)	E	A	B	F	W. & M. G.	Inch.	Lb.
	5/8						2077 1781	714 469	1615 1346 906	1			
2d Ex. Fine 2d 3d Ex. Fine 3d	1 11/8 11/4				710	1560 1351 1015 778	1558	411 365 251	775 700 568				ř.
4d 5d 6d	1½ 1¼ 1¾ 13/8 1½ 13/4	50	82	142 124	274 235 157	473		176 151 103	357	274 235 157			
7d 8d 9d	2 21/4 21/2 28/4	30	50	92 52 62	139					139			
10d 12d 16d	3 1/4 3 1/2	12 11 10	25 23 22	50 40 30	62 49					69	6 5	.192 .192 .207	33 30
20d 30d 40d 50d	4 41/2 5 51/2	9	19	23	37						3 2	.225 .244 .263 .283	23 17 13 10
60g	6 7 8										î	283 \$ 16 3/8 3/8 3/8 3/8	876543

# MISCELLANEOUS STEEL WIRE NAILS. Approximate Number per Pound.

				app	UAL	ша	LO IN	шье	r pe	I FC	unc					
ashburn k Moen Gauge.	eter ches.						Le	ngth	in	Incl	nes.					
Washbur & Moen Gauge.	Diameter in Inches.	T	8	1	38		1/2	5 8	1 3	1	7 8	1	13	1	11	11/3
000 00 00 1 1 2 3 4 4 5 6 6 7 7 8 9 10 11 12 13 14 15 16 16 16 17 18 18 18 18 18 18 18 18 18 18 18 18 18	362 3311 307 283 263 2244 225 207 1192 1177 162 1135 120 002 0080 0072 0080 0072 041 0041 0041 0042 0042 0042 0042 0042	2000237	702	2840 3504 4571 6233 8276 10668 15000 17777 22856		29 93 36 48 56 17 12 00 50	211 247 299 345 414 496 628 822 1072 1420 1752 2280 3116 4138 5334 7500 8888 838 11428	169 197 239 275 331 397 5022 658 857 1136 14022 1828 2495 3310 4267 6000 77111 9143	1: 1: 1: 2: 2: 2: 2: 3: 4: 5: 7	23   1 77   1 58   2 56   2 00   4 26   5	87 104 121 121 171 197 238 359 469 613 811 305 781 3364 409 33 359 409 305 781	55 68 76 90 106 122 149 177 200 248 314 411 538 710 87 87 87 87 87 84 444 444	55 55 56 57 77 77 77 77 77 77 77 77 77 77 77 77	50 58 67 80 94 111 133 153 153 184 2220 279 865 631 778 015 385 633 839 839	28 33 38 45 52 60 72 85 99 120 137 165 198 251 329 429 568 701 1246 1655 2133 3000	23 27 32 38 44 50 60 71 82 100 115 138 165 209 473 584 761 1038 1379 1778
ashburn k Moen Gauge.	ches.						Ler	ngth	in l	nch	es.					
Washbur & Moen Gauge.	Diameter in Inches.	14	2	21	$2\frac{1}{2}$	2	3	31/2	4	41/2	5	6	7	8	9	10
000 00 0 1 2 3 4 5 6 7 8	.362 .331 .307 .283 .263 .244 .225 .207 .192 .177 .162 .148	20 23 27 32 37 43 51 60 71 85 98 118	17 20 24 28 32 38 45 53 62 75 86 103	16 18 21 25 29 34 40 47 55 67 76 92	14 16 19 23 26 30 36 42 50 60 69 82	11 12 22 23 34 45 67	5 14 7 16 1 19 4 22 8 25 3 80 9 35 41 50 57 5 69	10 12 14 16 19 22 26 30 35 43 49 59	9 10 12 14 16 19 23 26 31 37 43 52	8 9 10 13 14 17 20 24 28 33 39 46	7 8 9 11 13 15 18 21 25 30 35 41	6 7 8 10 11 13 15 18 21 25 29	5 6 7 8 9 11 13 15 18	41 5 6 7 8 10 11	4 41 5 6 7 8 10	3½ 4 434 5½ 6½ 7½ 9
10 11 12	.135 .120 .105	142 179 235	124 157 204	110 139 182	125 164	11 14	4 105	71 90 117	82 79 103	55 70	50	W. &		1		12
13 14 15 16 17 18	.092 .080 .072 .063 .054	306 406 500 653 890 1182	268 350 438 571 779	238 315 389 508	214 284 350	19 25	5 178	153	200			00	-	31 33 41 5 6	444	3 3½ 4 4 4½ 5½

These approximate numbers are an average only, and the figures given may be varied either way, by changes in the dimensions of heads or points. Brads and no-head nails will have more to the pound than table shows, and large or thick-headed nails will have less.

98

10d

12d

16d

23/4

31/4

. 31/2

# CUT STEEL NAILS AND SPIKES.

Sizes, Lengths, and Approximate Number per Pound.

Sizes.	Length. Inches.	Common.	Cline	h. Fini	shing.	Casing . and Box.	Fencing.	Spikes.
2d	1	740	400	1	100			
3d	11/4	460	260	1 2	880			
4d	11/2	280	180		530	420		
50	13/4	210	125	1 3	350	300	100	
58	2	160	100		300	210	80	
7d	21/4	120	80		210	180	60	
58	21/2	88	68		168	130	52	1.0
90	23/4	73	52		130	107	38	
10d	3	60	48		104	- 88	26	
12d	31/4	46	40		96	70	20	
16d	31/2	33	34		86	52	18	17
208	4	23	24		76	38	. 16	14
25d	41/4	20						
50d	41/2	161/2				30		11
40d	5	12				26		9
50d	51/2	10		2 100	-	20		73/2
						20		172
60d	0	8				16		6
60d		1						
60d	0	1						6
101	61/2	8	Light	Sleting	Sive	Longth	. Flat Grip	6 5½ 5
60d Sizes.	0 6½ 7	Rarrel	Light Barrel.	Slating.	Size	Longth	- 1	6 5½ 5
101	6 61/2 7 Length.	Barrel.		Slating.	Size	Length Inches	Fine.	5½ 5½ 5
101	0 61/2 7 Length. Inches.	Barrel. 750 .		Slating.	Size	Length Inches	Fine.	5½ 5½ 5
101	0 6½ 7 Length. Inches.	Barrel. 750 . 600 .		Slating.		Length Inches	Fine.	5 5½ 5 Edge Gri
Sizes.	0 61/2 7 Length. Inches. 5/8 3/4 3/8	Barrel. 750 . 600 . 500 .			2d	Length Inches	1462 1300 1100	6 5½ 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
101	0 6½ 7 Length. Inches.	8	Barrel.	Slating.	2d 3d	Length Inches  34  76  1  1½	1462 1300 1100 800	6 5½ 5 5 ½ 5 5 Fine.
Sizes.	0 61/2 7 Length. Inches. 5/6 3/4 3/6 1 11/6	750 . 600 . 500 . 450 . 310	Barrel.	340	2d	Length Inches  34  76  1  1½	1462 1300 1100	6 5½ 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
Sizes.	0 63/2 7 Length. Inches. 5/8 3/4 3/6 1 13/4 13/4	750 600 500 450 310 280	Barrel.		2d 3d 4d	10 Length Inches  34 76 1 11/8 13/6	1462 1300 1100 800 650	6 5 ½ 5 5
Sires.	0 61/2 7 Length. Inches. 5/8 3/4 3/6 1 11/8 11/4 11/6	750 600 500 450 310 280 210	Barrel. 400 304	340	2d 3d 4d	Length Inches  34  76  1  1½	1462 1300 1100 800	6 5 ½ 5 5
Sizes.  2d  3d  4d	0 01/2 7  Length. Inches.  5/6 3/4 3/6 1 11/6 11/4 11/4 11/4	750 600 500 450 310 280	Barrel.	340 280	2d 3d 4d	16 Length Inches 7/5 1 1/8 13/6 Tobacco.	1462 1300 1100 800 650	6 5 ½ 5 5
8izes. 2d 3d 4d 5d	0 61/2 7 Length. Inches. 5/6 3/4 3/6 1 11/6 11/4 11/4 11/4 11/4 11/4 11/4	750 600 500 450 310 280 210	Barrel. 400 304	340	2d 3d 4d	16 Length Inches 34 76 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1402 1300 1100 800 650 Brads.	6 5½ 5 5 ½ 5 5 Fine.
Sizes.  2d  3d  4d	0 01/2 7  Length. Inches.  5/6 3/4 3/6 1 11/6 11/4 11/4 11/4	750 600 500 450 310 280 210	Barrel. 400 304	340 280	2d 3d 4d	16 Length Inches 7/5 1 1/8 13/6 Tobacco.	1462 1300 1100 800 650	6 5 ½ 5 5

62

50

40

27

72

60

SQUARE BOAT SPIKES.

Approximate Number in a Keg of 200 Pounds.

Size.	-1			Lei	ngth (	of Spi	ikeJ	inche	s.			
Inch.	8	4	5	6	7	8	9	10	11	12	14	16
1/4 5 16 3/8 7 16 1/2 5/8	3000 1660 1320	2375 1360 1140	2050 1230 940	1825 1175 800 600 450	990 650 590 375	880 600 510 335 260	525 400 300 240	475 360 275 220	320 260 205	280 240 190	175	160

WROUGHT SPIKES.

Approximate Number in a Keg of 150 Pounds.

Size.	-		1	Le	ngth	of Sy	ike-	Inch	es.			
· Inch.	3	31/2	4	41/2	5	6	7	8	9	1,0	11	12
1/4 5 16 3/8 10 1/2	2250	1890 1208	1650 1135		1380 930 742	1292 868 570	1161 662 482 445 306	635 455 384 256	573 424 300 240	391 270 222	249 203	236 180

# WOOD SCREWS.

Size	Diam-	Size	Diam-	Size	Diam-	Size	Diam-	Sine	Diam-	Size	Diam-
Num-	eter.	Num-	eter.	Num-	eter.	Num-	eter.	Num-	eter.	Num-	eter.
ber.	Inch.	ber.	Inch.	ber.	Inch.	ber.	Inch.	ber.	Inch.	ber.	Inch.
0 1 2 3 4	.056 .069 .082 .096 .109	5 6 7 8 9	.122 .135 .149 .162 .175	10 11 12 13 14	.188 .201 .215 .228 .241	15 16 17 18 19	.255 .268 .281 .293 .308	20 21 22 23 24	.321 .334 .347 .361 .374	25 26 27 28 29 30	.387 .401 .414 .427 .440 .453

# RAILROAD SPIKES.

Size Measured. Under Head.	Average Number per Keg of 200 Pounds	Quantity of Spikes Track. Ties 4 Spikes	Rail Used. Weight per Yard	
Inches.	OI 200 FOULUS	Pounds.	Kegs.	Pounds.
5½ × 5/8	300	7040	351/5	75 to 100
51/2 × 1/6	375	5870	291/3	45 " 75
5 X 78	400	5170	26	40 " 56
5 X 1/2	450	4660	231/3	35 " 40
41/2 X 1/2	530	3960	20	30 " 35
4 X 1/2	600	3520	17%	25 " 35
4½ X 78	680	3110	151/2	
4 × 5%	720	2910	143/4	20 " 30
31/2 × 1/6	900	2350	11	20 * 30 20 * 30 16 * 25 16 * 25
4 × 3/8	1000	2090	101/2	16 " 25
$3\frac{1}{2} \times \frac{3}{8}$	11190	1780	9	16 " 20
3 × 3/8	1240	1710	81/2	16 " 20
21/2 X 3/8	1342	1575	77/8	12 " 16

# DIMENSIONS, WEIGHTS AND PROPERTIES OF STANDARD PIPE.

Dia	ameter in Inch	108.	Weight per Foot.	Moment of Inertia.	Section Modulus.	Radius of Gyration.		
Nominal,	External.	Internal.	Pounds.	Inches.4	Inches.3	Inches.		
BLA	CK OR	BALVANI	ZED STAI	NDARD W	EIGHT PI	PE.		
100-44-17-00-45-19-40-40-40-40-40-40-40-40-40-40-40-40-40-	.405	.269	.244	.001	.005	.12		
	.540	.364	.424	.003	.012	.16		
	.675	.493	.567	.007	.022	.21		
	.840	.622	.850	.017	.041	.26		
	1.050	.824	1.130	.037	.071	.33		
$1\\ 1\frac{1}{4}\\ 1\frac{1}{2}\\ 2\\ 2\frac{1}{2}$	1.315	1.049	1.678	.09	.13	.42		
	1.660	1.380	2.272	.19	.23	.54		
	1.900	1.610	2.717	.31	.36	.62		
	2.375	2.067	3.652	.67	.56	.79		
	2.875	2.469	5.793	1.53	1.06	.95		
$3 \\ 3\frac{1}{2} \\ 4 \\ 4\frac{1}{2} \\ 5$	3.500	3.068	7.575	3.02	1.72	1.16		
	4.000	3.548	9.109	4.79	2.39	1.34		
	4.500	4.026	10.790	7.23	3.21	1.51		
	5.000	4.506	12.538	10.4	4.2	1.68		
	5.563	5.047	14.617	15.2	5.5	1.88		
6 7 8 8	6.625 7.625 8.625 8.625 9.625	6.065 7.023 8.071 7.981 8.941	18.974 23.544 24.696 28.554 33.907	28.1 46.5 63.4 72.5 107.6	8.5 12.2 14.7 16.8 22.4	2.25 2.59 3.31 2.94 3.28		
10	10.750	10.192	31.201	125.9	23.4	3.70		
10	10.750	10.020	40.483	160.9	29.9	3.67		
10	10.750	10.136	34.240	137.1	25.5	3.69		
11	11.750	11.000	45.557	217.0	36.9	4.02		
11	12.750	12.090	43.773	248.5	40.0	3.91		
12	12.750	12.000	49.562	285.4	44.7	4.38		
13	14.00	13.25	54.568	372.8	53.3	4.82		
14	15.00	14.25	58.573	461.0	61.5	5.23		
15	16.00	15.25	62.579	562.0	70.3	5.53		
	STANDARD EXTRA STRONG PIPE.							
Top-14-min the mid-	.405	.215	.314	.001	.006	.11		
	.540	.302	.535	.004	.014	.15		
	.675	.423	.738	.009	.026	.20		
	.840	.546	1.087	.020	.048	.25		
	1.050	.742	1.473	.045	.085	.32		

# DIMENSIONS, WEIGHTS AND PROPERTIES OF STANDARD PIPE (CONTINUED).

	OF B	LANDA	AD FIF.	(CONTI	NUED).	1
Dia	ameter in Incl	hes.	Weight	Moment	Section	Radius
	1		per Foot.	Inertia.	Modulus.	Gyration.
· Nominal.	External.	Internal.	Pounds.	Inches.4	Inches.3	Inches.
	STANDA	RD EXT	RA STRO	NG PIPE	(CONTINUE	D).
1	1.315	.957	2.171	.11	.16	.41
11/4	1.660	1.278	2.996	.24	.29	.52
11	1.900	1.500	3.631	.39	.46	.61
2	2.375	1.939	5.022	.87	.73	.77
$2\frac{1}{2}$	2.875	2.323	7.661	1.92	1.34	.92
3	3.500	2.900	10.252	3.89	2.23	1.14
31	4.000	3.364	12.505	6.28	3.14	1.29
4	4.500	3.826	14.983	9.6	4.3	1.48
41	5.000	4.290	17.611	14.1	5.6	1.65
5	5.563	4.813	20.778	20.7	7.4	1.84
6	6.625	5.761	28.573	40.5	12.2	2.19
7	7.625	6.625	38.048	71.4	18.7	2.53
8	8.625	7.625	43.388	105.7	24.5	2.88
9	9.625	8.625	48.728	149.4	31.0	3.23
10	10.750	9.75	54.735	212.0	39.3	3.63
11	11.750	10.75	60.075	280.1	47.7	3.98
12	12.750	11.75	65.415	360.7	56.6	4.33
	STANDA	RD DOU	BLE EXT	RA STRON	G PIPE.	1
		E - 30 I				
1 2 3 4	.840	.252	1.714	.024	.058	.22
34	1.050	.434	2.440	.058	.110	.28
1	1.315	.599	3.659	.14	.21	.36
114	1.660	.896	5.214	.34	.41	.47
$1\frac{1}{2}$	1.900	1.100	6.408	.57	.67	.55
$\tilde{2}^{2}$ .	2.375	1.503	9.029	1.31	1.10	.70
$\frac{2}{2\frac{1}{2}}$	2.875	1.771	13.695	2.87	2.00	.84
3	3.500	2.300	18.583	6.0	3.4	1.05
31	4.000	2.728	22.850	9.8	4.9	1.03
4	4.500	3.152	27.541	15.3	6.8	1.37
41/2	5.000	3.580	32.530	22.6	9.0	1.54
5	5.563	4.063	38.552	33.7	12.3	1.72
. 6	6.625	4.897	53.160	66.3	20.0	2.08
7	7.625	5.875	62.079	107.5	28.2	2.41
8	8.625	6.875	72.424	162.0	37.6	2.76
24 2 .						-

WROUGHT IRON WELDED STEAM, GAS AND WATER PIPE.

	DIAMETER.			Weight	CHEUMP	ERENCE.	Lineal Feet to 1 Sq.	
Nominal.	Inside.	Outside.	Thickness.	per Foot.	Internal.	External.		rface.
Inches.	Inches.	Inches.	Inches.	Pounds.	Inches.	Inches.	Inside.	Outside.
1/8	.269	.405	.068	.244	.85	1.27	14.13	9.45
1/8	.364	.540	.088	.424	1.14	1.70	10.52	7.06
3/8 1/2 8/4	.493	.675	.091	.567	1.55	2.12	7.74	5.66
1/2	.622	.840	.109	.850	1.95	2.64	6.15	4.55
8/4	.824	1.050	.113	1.130	2.59	3.30	4.63	3.64
1	1.049	1.315	.133	1.678	3.30	4.13	3.64	2.91
11/4	1.380	1.660	.140	2.272	4.34	5.22	2.77	2.30
11/2	1.610	1.900	.145	2.717	5.06	5.97	2.37	2.01
2	2.067	2.375	.154	3.652	6.49	7.46	1.85	1.61
21/2	2.469	2.875	.203	5.793	7.76	9.03	1.55	1.33
3	3.068	3.500	.216	7.575	9.64	11.00	1.24	1.09
31/2	3.548	4.000	.226	9.109	11.15	12.57	1.08	.95
4	4.026	4.500	.237	10.790	12.65	14.14	195	.85
41/2	4.506	5.000	.247	12.538	14.16	15.71	.85	.76
5	5.047	5.563	.258	14.617	15.86	17.48	.76	.69
0	6.065	6.625	.280	18.974	19.05	20.81	.63	.58
7 .	7.023	7.625	.301	23.544	22.06	23.95	.54	.50
8	8.071	8.625	.277	24.696	25.36	27.10	.47	.44
8	7.981	8.625	.322	28.554	25.07	27.10	.48	.44
9	8.941	9.625	.342	33.907	28.09	30.24	.43	.40
10	10.192	10.750	.279	31.201	32.02	33.77	.37	.36
10	10.136	10.750	.307	34.240	31.84	33.77	.38	.36
10	10.020	10.750	.365	40.483	31.48	33.77	.38	.36
11	11.000	11.750	.375	45.557	34.56	36.91	.35	.33
12	12.090	12.750	.330	43.773	37.98	40.06	.32	.30
12	12.000	12.750	.375	49.562	37.70	40.06	.32	.30
13	13.250	14.000	.375	54.568	41.63	43.98	.29	.27
14	14.250	15.000	.375	58.573	44.77	47.12	.27	.25
15	15.250	16.000	.375	62.579	47.91	50.27	.25	.24

Nominal	AR	EA.	Lineal Feet	No. of	Contents to 1	COUPLINGS	
Diameter.	Internal.	External.	containing	Threads	Lineal Foot.	Outside Diam	Length.
Inches.	Sq. Inches.	Sq. Inches.	1 Cubic Foot.	perInch.	Gallons.	Inches.	Inches.
1/8	.06	.13	2540.00	27	.003	.59	.81
3/4	.10	123	1384.00	18	.005	.72	.94
8/8	.19	.36	754.40	18	.010	184	1.06
1/2	.30	.55	473.90	14	.016	1.00	1.31
3/4	.53	.87	270.00	14	.028	1.33	1.56
1	.87	1.35	166.60	111/2	.045	1.56	1.81
11/4	1.50	2.16	96.28	111/2	.078	1.95	2,13
11/2	2.04	2.84	70.73	111/2	.106	2.22	2.38
2	3.35	4.43	42.91	111/2	.174	2.75	2.63
21/2	4.78	6.49	30.08	8	.249	3.28	2.88
. 3	7.38	9.62	19.48	8	.380	3.94	3.13
31/2	9.88	12.57	14.57	8	.514	4.44	3.68
4	12.72	15.90	11.31	8	.661	5.00	3.63
41/2	15.93	19.63	9.03	8	.828	5.50	3.63
5 .	19.99	24.30	7.20	8	1.040	6.22	4.13
6	28.87	34.47	4.98	8	1.500	7.31	4.13
7	38.71	45.66	3.72	8	2.010	8.31	4.13
8	51.16	58.43	2.82	8	2.660	9.31	4.63
8	50.03	58.43	2.88	8	2.610	9.31	4.63
0	62.79	72.76	2.29	8	3.260	10.38	5.13
10	. 81.47	90.76	1.77	8	4.230	11.66	6.13
10	80.33	90.76	1.78	8	4.190	11.66	6.13
10	78.86	90.76	1.83	8	4.100	11.66	6.13
11	95.03	108.43	1.52	8	4.940	12.66	6.13
12	114.63	127.68	1.25	80 80 80 80 80 80 80 80 80 80 80 80 80 8	5.960	13.88	6.13
12	113.10	127.68	1.27	8	5.880	13.88	6.13
13	137.89	153.94	1.04	8	7.160	15.06	6.13
14	159.48	176.71	.90	8	8.280	16.38	6.13
15	182.65	201.06	1 .79	1 8	9.490	17.38	6.13

# MANUFACTURERS' STANDARD SPECIFICATIONS.

REVISED APRIL 22, 1919

#### STRUCTURAL STEEL.

#### Grades.

1. These specifications cover three classes of structural steel, namely:

Class A steel, to be used for railway bridges and ships.

Class B steel, to be used for buildings, highway bridges, train sheds and similar structures.

Class C steel, to be used for structural rivets.

#### I. MANUFACTURE.

#### Process.

2. Steel for Classes A and C shall be made by the open-hearth process. Steel for Class B may be made either by the open-hearth or by the Bessemer process.

#### II. CHEMICAL PROPERTIES AND TESTS.

#### Chemical Composition.

3. The steel shall conform to the following requirements as to chemical composition:

Elements Considered.	Class A Steel.	Class B Steel.	Class C Steel.
Phosphorus, max., per cent.:			
Basic open hearth	0.04	0.06	0.04
Acid open hearth	0.06	0.08	0.04
Bessemer		0.10	
Sulphur, max., per cent	0.06		0.05

### Ladle Analyses.

4. To determine whether the material conforms to the requirements specified in section 3, an analysis shall be made by the manufacturer from a test ingot taken during the pouring of each melt. A copy of this analysis shall be given to the purchaser or his representative, if requested.

# Check Analyses.

5. A check analysis of Class A and Class C steel may be made by the purchaser from finished material representing each melt, in which case an excess of 25 per cent, above the requirements specified in section 3 shall be allowed.

#### III. PHYSICAL PROPERTIES AND TESTS.

#### Tension Tests.

6. The steel shall conform to the following requirements as to tensile properties:

Properties Considered.	Class A Steel.	Class B Steel.	Class C Steel.
Tensile strength, lb. per sq. in. Yield point, minimum, lb. per	55,000-65,000	55,000-65,000*	46,000-56,000
sq. in	0.5 tens. str.	0.5 tens. str.	0.5 tens. str.
Elongation in 8 in., min., per cent	1,400,000† tens. str.	1,400,000† tens. str.	1,400,000 tens. str.
Elongation in 2 in., min., per cent. (Fig. 2)	22	22	

<sup>\*</sup>See section 8. †See section 9.

#### Yield Point.

7. The yield point shall be determined by the drop of the beam of the testing machine.

#### Modification in Tensile Strength.

 Class B steel may have tensile strength up to 70,000 lb. maximum, provided the elongation is not less than the percentage required for 65,000 lb. tensile strength.

#### Modifications in Elongation.

- 9. (a) For material over ¾ in. in thickness, a deduction of 1 from the percentage of elongation in 8 in. specified for Classes A and B in section 6 shall be made for each increase of ¼ in. in thickness above ¾ in., to a minimum of 18 per cent.
- (b) For material under \( \frac{1}{6} \) in. in thickness, a deduction of 2.5 from the percentage of elongation in 8 in. specified for Classes A and B in section 6 shall be made for each decrease of \( \frac{1}{16} \) in. in thickness below \( \frac{1}{16} \) in.

#### Character of Fracture.

10. All broken tension test specimens shall show a silky fracture.

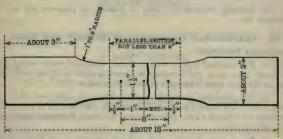
#### Bend Tests.

11. (a) The test specimen for plates, shapes and bars shall bend cold through 180 deg. without fracture on the outside of the bent portion, as follows: For material  $\frac{1}{2}$  in. and under in thickness, flat on itself; for material over  $\frac{1}{2}$  in. up to  $\frac{1}{2}$  in. in thickness, around a pin the diameter of which is equal to  $\frac{1}{2}$  times the thickness of the specimen; and for material over  $\frac{1}{2}$  in. in thickness, around a pin the diameter of which is equal to twice the thickness of the specimen.

- (b) The test specimen for pins and rollers shall bend cold through 180 deg, around a 1-in, pin without fracture on the outside of the bent portion.
- (c) A rivet rod shall bend cold through 180 deg. flat on itself without fracture on the outside of the bent portion.
  - (d) Bend tests may be made by pressure or by blows.

#### Test Specimens.

- 12. (a) Tension and bend test specimens shall be taken from the finished rolled or forged product, and shall not be annealed or otherwise treated, except as specified in section 13.
- (b) Tension and bend test specimens for plates, shapes and bars, except as specified in paragraph (c), shall be of the full thickness of material as rolled, and with both edges milled to the form and dimensions shown in Fig. 1, or may have both edges parallel.



Frg. 1.

- (c) Tension and bend test specimens for plates and bars (except eye-bar flats) over 1½ in. in thickness or diameter may be turned or planed to a diameter or thickness of at least ¾ in. for a length of at least 9 in.
- (d) Tension and bend test specimens for pins and rollers shall be taken parallel to the axis, 1 in. from the surface of the bar. Tension test specimens shall be of the form and dimensions shown in Fig. 2. Bend test specimens shall be 1 in. by ½ in. in section.

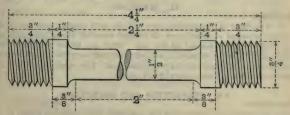


Fig. 2.

(e) Rivet bars shall be tested in full-size section as rolled.

#### Annealed Specimens.

13. Test specimens for material which is to be annealed or otherwise treated before use shall be cut from properly annealed or similarly treated short lengths of the full section of the piece.

#### Number of Tests.

- 14. (a) At least one tension test and one bend test shall be made from each melt. If material from one melt differs 3% in. or more in thickness, tests shall be made from both the thickest and the thinnest material rolled.
- (b) If any test specimen develops flaws, or if an 8-in. tension test specimen breaks outside the middle third of the gage length, or if a 2-in. tension test specimen breaks outside the gage length, it may be discarded and another specimen substituted therefor.
- (c) Material intended for fillers or ornamental purposes will not be subject to test.

# IV. PERMISSIBLE VARIATIONS IN WEIGHT AND GAGE. Permissible Variations.

- 15. (a) The sectional area or weight of each structural shape and of each rolled-edge plate up to and including 36 inches in width shall not vary more than 2.5 per cent. from theoretical or specified amounts.
- (b) The thickness or weight of each universal plate over 36 in. in width, and of each sheared plate, shall conform to the schedules of permissible variations for sheared plates, Manufacturers' Standard Practice, appended to these specifications.
- (c) The weights of angles, tees, zees and channels of bar sizes, and the dimensions of rounds, squares, hexagons and flats, shall conform to the Manufacturers' Standard Practice governing the allowable variations in size and weight of hot-rolled bars.

#### V. FINISH.

#### Finish.

16. The finished material shall be free from injurious defects and shall have a workmanlike finish.

#### VI. MARKING.

#### Marking.

17. The name of the manufacturer and the melt number shall be legibly marked, stamped or rolled upon all finished material, except that each pin and roller shall be stamped on the end. Rivet and lattice steel and other small pieces may be shipped in securely fastened bundles, with the above marks legibly stamped on attached metal tags. Test specimens shall have their melt numbers plainly marked or stamped.

### VII. INSPECTION AND REJECTION.

### Inspection.

18. The inspector representing the purchaser shall have free entry, at all times while work on the contract of the purchaser is being performed, to all parts of the manufacturer's works which concern the manufacture of the

material ordered. The manufacturer shall afford the inspector, free of cost, all reasonable facilities to satisfy him that the material is being furnished in accordance with these specifications. All tests and inspection shall be made at the place of manufacture prior to shipment, and shall be so conducted as not to interfere unnecessarily with the operation of the works.

#### Rejection.

19. Material which, subsequent to the above tests at the mills and its-acceptance there, develops weak spots, brittleness, cracks or other imperfections, or is found to have injurious defects, may be rejected at the shop, and shall then be replaced by the manufacturer at his own cost.

### BOILER STEEL.

#### Grades.

 There shall be three grades of steel for boilers, namely: flange, firebox, and boiler rivet.

#### I. MANUFACTURE.

#### Process.

2. The steel shall be made by the open-hearth process.

#### II. CHEMICAL PROPERTIES AND TESTS.

#### Chemical Composition.

The steel shall conform to the following requirements as to chemical composition:

Elements Considered.	Flange Steel.	Firebox Steel.	Boiler Rivet Steel.
Manganese, per cent	0.30 to 0.60	0.30 to 0.50	0.30 to 0.50
Basic	0.04	0.035	0.04
Acid	0.05	0.04	0.04
Sulphur, max., per cent	0.05	0.04	0.045

### Ladle Analyses.

4. To determine whether the material conforms to the requirements specified in section 3, an analysis shall be made by the manufacturer from a test ingot taken during the pouring of each melt. A copy of this analysis shall be given to the purchaser or his representative.

# Check Analyses.

5. A check analysis may be made by the purchaser from a broken tension test specimen representing each plate as rolled, and this analysis shall conform to the requirements specified in section 3.

#### III. PHYSICAL PROPERTIES AND TESTS.

#### Tension Tests.

6. The steel shall conform to the following requirements as to tensile properties:

Properties Considered.	Flange Steel.	Firebox Steel.	Boiler Rivet Steel.
Tensile strength, lb. per sq. in  Yield point, min., lb. per	55,000-65,000	52,000-60,000	45,000-55,000
sq. in	0.5 tens. str.	0.5 tens. str.	0.5 tens. str.
Elongation in 8 in., min., per cent	1,450,000* tens. str.	1,450,000* tens. str.	1,450,000 tens. str.

<sup>\*</sup> See section 8.

#### Yield Point.

7. The yield point shall be determined by the drop of the beam of the testing machine.

# Modifications in Elongation.

- 8. (a) For plates over  $\frac{3}{4}$  in. in thickness, a deduction of 0.5 from the specified percentage of elongation will be allowed for each increase of  $\frac{1}{4}$  in. in thickness above  $\frac{3}{4}$  in., to a minimum of 20 per cent.
- (b) For plates under  $\frac{5}{16}$  in. in thickness, a deduction of 2.5 from the percentage of elongation specified in section 6 shall be made for each decrease of  $\frac{1}{16}$  in. in thickness below  $\frac{5}{16}$  in.

#### Bend Tests.

- 9. (a) Cold-bend tests shall be made on the material as rolled.
- (b) Quench-bend test specimens, before bending, shall be heated to a light cherry red as seen in the dark (about 1200 deg. F.), and quenched in water the temperature of which is about 80 deg. F.
- (c) Specimens for cold-bend and quench-bend tests of flange and firebox steel shall bend through 180 deg. without fracture on the outside of the bent portion, as follows: For material  $\frac{1}{2}$  in. and under in thickness, flat on themselves; for material over  $\frac{1}{2}$  in. up to  $\frac{1}{2}$  in. in thickness, around a pin the diameter of which is equal to the thickness of the specimen; and for material over  $\frac{1}{2}$  in. in thickness, around a pin the diameter of which is equal to  $\frac{1}{2}$  times the thickness of the specimen.
- (d) Specimens for cold-bend and quench-bend tests of boiler rivet steel shall bend cold through 180 deg, flat on themselves without fracture on the outside of the bent portion.
  - (e) Bend tests may be made by pressure or by blows.

#### Test Specimens.

- 10. (a) Tension and bend test specimens for plates shall be taken from the finished product, and shall be of the full thickness of material as rolled. Tension test specimens shall be of the form and dimensions shown in Fig. 1. Bend test specimens shall be  $1\frac{1}{2}$  in. to  $2\frac{1}{2}$  in. wide, and shall have the sheared edges milled or planed.
- (b) The tension and bend test specimens for rivet bars shall be of the full-size section of material as rolled.

#### Number of Tests.

- 11. (a) One tension, one cold-bend, and one quench-bend test shall be made from each plate as rolled.
- (b) Two tension, two cold-bend, and two quench-bend tests shall be made for each melt of rivet steel.
- (c) If any test specimen develops flaws, or if a tension test specimen breaks outside the middle third of the gage length, it may be discarded and another specimen substituted therefor.

# IV. PERMISSIBLE VARIATIONS IN WEIGHT AND GAGE. Permissible Variations.

- 12. (a) The thickness or weight of each sheared plate shall conform to the schedule of permissible variations, Manufacturers' Standard Practice, appended to these specifications.
- (b) The dimensions of rivet bars shall conform to the Manufacturers' Standard Practice governing allowable variations in the size of hot-rolled bars.

#### V. FINISH.

#### Finish.

13. The finished material shall be free from injurious defects and shall have a workmanlike finish.

#### VI. MARKING.

#### Marking.

14. The melt or slab number, name of the manufacturer, grade, and the minimum tensile strength for its grade as specified in section 6 shall be legibly stamped on each plate. The melt or slab number shall be legibly stamped on each test specimen representing that melt or slab.

#### VII. INSPECTION AND REJECTION.

### Inspection.

15. The inspector representing the purchaser shall have free entry, at all times while work on the contract of the purchaser is being performed, to all parts of the manufacturer's works which concern the manufacture of the material ordered. The manufacturer shall afford the inspector, free of cost, all reasonable facilities to satisfy him that the material is being furnished in accordance with these specifications. All tests and inspection shall be made at the place of manufacture prior to shipment, and shall be so conducted as not to interfere unnecessarily with the operation of the works.

#### Rejection.

16. Material which, subsequent to the above tests at the mills and its acceptance there, develops weak spots, brittleness, cracks or other imperfections, or is found to have injurious defects, may be rejected at the shop, and shall then be replaced by the manufacturer at his own cost.

### MANUFACTURERS' STANDARD PRACTICE.

# PERMISSIBLE VARIATIONS IN WEIGHT AND THICKNESS OF SHEARED PLATES.

#### WHEN ORDERED TO WEIGHT.

One cubic inch of rolled steel is assumed to weigh 0.2833 pound.

When ordered to weight per square foot, the weight of each lot\* in each shipment shall not vary from the weight ordered more than the amount given in the following table:

2-12	Permi					Veights				
Ordered Weight  Lbs. per Sq. Ft.	Under 48 In.		48 in. incl. to 60 in. excl.		60 in, incl. to 72 in, excl.		72 in. incl. to 84 in. excl.		84 in. incl. 50 96 in. excl.	
	Over.	Under.	Over.	Under.	Over.	Under.	Over.	Under.	Over.	Under.
Under 5	5	3	5.5	3	6	3	7	3		
5 incl. to 7.5 excl.	4.5	3	5	3	5.5	3	6	3		
7.5 " " 10 "	4	3	4.5	3	5	3	5.5	3	0	3
10 " " 12.5 "	3.5	2.5	4	3	4.5	3	5	3	5.5	8
12.5 " " 15 "	3	2.5	3.5	2.5	4	3	4.5	3	5	3
15 " " 17.5 "	2.5	2.5	3	2.5	3.5	2.5	4	3	4.5	3
17.5 " " 20 "	2.5	2	2.5	2.5	3	2.5	3.5	2.5	4	3
20 " " 25 "	2	2	2.5	2	2.5	2.5	3	2.5	3.5	2.5
25 # # 30 #	2	2	2	2	2.5	2	2.5	2.5	3	2.5
30 " " 40 "	2	2	2	2	2	2	2.5	2	2.5	2.5
40 or over	2	2	2	2	2	2	2	2	2.5	2

Note:—The weight per square foot of individual plates shall not vary from the ordered weight by more than  $1\frac{1}{3}$  times the amount given in this table.

<sup>\*</sup>The term "lot" applied to this table means all of the plates of each group width and group weight.

#### MANUFACTURERS' STANDARD PRACTICE.

# PERMISSIBLE VARIATIONS IN WEIGHT AND THICKNESS OF SHEARED PLATES.

#### WHEN ORDERED TO WEIGHT.

One cubic inch of rolled steel is assumed to weigh 0.2833 pound.

When ordered to weight per square foot, the weight of each lot\* in each shipment shall not vary from the weight ordered more than the amount given in the following table:

96 in. incl. to 108 in. excl.		108 in. incl. to 120 in. excl.		120 in. incl. to 132 in. excl.		132 in. or over.		Ordered Weight  Lbs. per Sq. Ft.			
Over.	Under.	Over.	Under.	Over.	Under.	Over.	Under.				
								Uno	ler 5	-	
								5	incl	. to 7.5	excl.
7	3	8	3					7.8	"	" 10	æ
6	3	7	3	8	8	9	8	10	а	" 12.5	a
5.5	3	6	3	7	3	8	3	12.8		<b>4</b> 15	α
5	3	5.5	3	6	3	7	3	15	4	<b>4</b> 17.5	44
4.5	3	5	3	. 5.5	3	6	3	17.8	5 4	<sup>4</sup> 20	46
4	3	4.5	3	5	3	5.5	3	20	æ	<sup>4</sup> 25	44
3.5	3	4	3	4.5	3	5	3	25	æ	<b>4</b> 30	æ
3	2.5	3.5	3	4	3	4.5	3	30	ш	" 40	4
2.5	2.5	3	2.5	3.5	3	4	3	40	or ov	rer	

NOTE:—The weight per square foot of individual plates shall not vary from the ordered weight by more than 11/3 times the amount given in this table.

<sup>\*</sup> The term "lot" applied to this table means all of the plates of each group width and group weight.

#### MANUFACTURERS' STANDARD PRACTICE.

# PERMISSIBLE VARIATIONS IN WEIGHT AND THICKNESS OF SHEARED PLATES (CONTINUED).

#### WHEN ORDERED TO THICKNESS.

One cubic inch of rolled steel is assumed to weigh 0.2833 pound.

When ordered to thickness, the thickness of each plate shall not vary more than 0.01 inch under that ordered. The overweight of each lot\* in each shipment shall not exceed the amount given in the following table:

		nissible E Widths G							
Ordered Thickness Inch.	Under 48 in.	48 in. incl. to 60 in. excl.	60 in. incl. to 72 in. excl.	72 in. incl. to 84 in. excl.	84 in. incl. to 96 in. excl.	96 in. incl. to 108 in. excl.	108 in. incl. to 120 in. excl.	120 in. incl. to 132 in. excl.	132 in.
Under 1/8	9	10	12	14					
1/8 incl. to 3/8 excl.	8	-0	10	12					
36 " " 1/4 "	7	8	9	10	12				
7/4 " " 5 "	6	7	8	9	10	12	14	16	10
5 " " 8/8 "	5	0	7	8	9	10	12	14	17
3/8 4 4 7 4	4.5	5	6	7	8 .	9	10	12	15
7 4 4 1/2 4	4	4.5	5	6	7	8	9	10	13
1/2 " " 5/8 "	3.5	4	4.5	5	6	7	8	9	11
5/8 " " 3/4 "	3	3.5	4	4.5	5	8	7	8	9
3/4 " " 1 "	2.5	3	3.5	4	4.5	5	8	7	8
1 or over	2.5	2.5	3	3.5	4	4.5	5	6	7

<sup>\*</sup> The term "lot" applied to this table means all of the plates of each group width and group thickness.

#### WOODEN BEAMS AND COLUMNS.

The results of a series of studies of wooden beams and columns of various kinds of American timber are contained in the Proceedings of the Fifth Annual Convention of the Association of Railway Superintendents of Bridges and Buildings, October, 1895, at which the Committee on Strength of Bridge and Trestle Timbers presented a report, portions of which have been used in preparing certain of the tables on the following pages, but as noted thereon the arrangement and values in many cases have been modified by later information from various sources.

The publications of the Forestry Division of the United States Department of Agriculture, Bulletins Nos. 8 and 12, and Circular No. 15, contain reports of tests of American woods, and deductions drawn therefrom. Extracts and tables from these reports are given on the following pages.

The tables of safe loads for wooden beams and tables of strength of wooden columns given on the following pages have been specially calculated for this book, using the information regarding the properties of the various species contained in the reports above referred to, as modified in some cases by later data.

In order that information on this subject will be more complete, tables are given herein showing structural timber stress values, as published in the United States Forestry Service Bulletin, No. 108, and also those recommended by the American Railway Engineering and Maintenance of Way Association, Bulletin No. 107.

# Explanation of the Tables of Safe Loads in Pounds, Uniformly Distributed, for Rectangular Wooden Beams One Inch Thick, Pages 416 to 421 Inclusive.

#### General.

For convenience in use, three of these tables have been prepared from which the safe loads of the various species can be obtained, either directly or by proportion as stated in the footnotes.

The values given in the tables are the safe loads in pounds uniformly distributed, including the weight of the beam itself, for rectangular beams one inch thick for spans from four to forty feet and for depths from four to twenty-four inches. The safe load for a beam of any thickness may be found by multiplying the values given in the tables by the thickness of the beam in inches.

The last column of each of the three Tables of Safe Loads for

Rectangular Wooden Beams gives a coefficient of deflection, by means of which the deflection for any beam may be obtained, corresponding to the given span and safe load, by dividing the coefficient by the depth of the beam in inches, which will give approximately the deflection in inches under the given conditions.

In each table the deflection coefficient is given for only one species of wood, as shown, but the deflections for other species may be obtained from these by proportion as explained hereafter.

For the reason that wood has no well-defined limit or modulus of elasticity the deflections obtained by the use of the coefficients are only approximate and will vary, according to the moisture content of the wood and the character of the loading. The deflections thus obtained are, therefore, useful only as a general indication of the amount of bending to be expected under the given conditions and are not exact as in the case of materials like steel, which has a well-defined limit and modulus of elasticity.\*

The safe loads for other species of woods than those stated in the headings of the tables may be obtained from those given, by direct proportion, dependent upon the ratio of their allowable unit stress as compared with that for which the table is figured, as stated in the foot-notes at the bottom of the tables.

\* NOTE.—"A series of tests, undertaken at the College of Forestry at Cornell University, seems to demonstrate that, at least in coniferous wood, a definite elastic limit for any particular piece can be easily shown, and, that it coincides with the theoretically calculated elastic limit upon the bases of compression tests and their application, according to Neely's formula."

### Explanation of the Table of Safe Loads for Rectangular Beams of White Pine, Cedar, Spruce or Eastern Fir.

The values for the various species of woods, which are included in this table are calculated for an allowable fibre stress, for flexure, of 700 pounds per square inch.

The deflection coefficients are given for white pine and are based upon a modulus of elasticity of 1 000 000 pounds per square inch.

The lower dotted line crossing the table indicates the limits of spans for which the deflection will exceed  $\frac{1}{360}$  of the span for the kind of wood for which the deflection coefficient is given. For spans below the line the safe loads given in the tables will produce a deflection greater than  $\frac{1}{360}$  of the span, while those above the line will produce less than this, which is the usual limit of deflection in order to prevent cracking of plastered ceilings. Similarly,

the upper dotted line indicates the limit of deflection for the kind of wood for which the deflection coefficient is given, corresponding to a modulus of elasticity of 500 000 pounds per square inch, which should be considered in cases where the deflection should be more closely limited.

The coefficients of deflection for Cedar corresponding to moduli of 700 000 and 350 000 may be obtained by multiplying those of the table by <sup>1</sup>/<sub>2</sub> and <sup>2</sup>/<sub>2</sub> respectively, and for Spruce and Eastern Fir corresponding to moduli of 1 200 000 and 600 000 by

multiplying those of the table by \$ and \$ respectively.

The full zig-zag line in the table gives the limits of the safe loads corresponding to the allowable shearing stress along the neutral axis of the beam. The safe loads above the line, which are based upon the extreme fibre strains, will produce shearing stresses along the axis or with the grain in excess of that allowable, which, in the case of White Pine and the other woods of this table, is 100 pounds per square inch.

The position of this line, which indicates the limit of safe loads for shearing along the neutral axis, was determined by the aid

of the following formula:

$$W = \frac{4bds}{3}$$

in which

W = safe load in pounds uniformly distributed.

d = depth of beam in inches.

b = breadth of beam in inches.

s = allowable shear in the direction of the grain in pounds per square inch.

# Explanation of the Table of Safe Loads for Rectangular Beams of Short-leaf Yellow Pine.

The table is calculated for an allowable fibre stress, for flexure, of 1 000 pounds per square inch.

The deflection coefficients are figured for a modulus of elasticity of 1 200 000 pounds per square inch, but may be used for other moduli, after obtaining the corresponding coefficients by proportion as heretofore explained.

The lower dotted line across the table indicates the limits of spans for which the safe load will produce deflections greater than  $\frac{1}{880}$  of the length of the beam. Values above the line will give less deflection than this, and those below will give greater, based on a modulus of 1 200 000 pounds per square inch. Similarly, the upper dotted line indicates the limit of deflection corresponding to a modulus of elasticity of 600 000 pounds per square inch.

The full zig-zag line across the table indicates the limiting spans and loads based on the allowable intensity of shearing stress along the neutral axis of the beam. The values above the full zig-zag line correspond to shearing stresses greater than the allowable stress in the direction of the grain for Short-leaf Yellow Pine, while those below the line correspond to shearing stresses less than that allowable, which, in this case, is assumed to be 100 pounds per square inch.

# Explanation of Tables of Safe Loads for Rectangular Beams of White Oak and Long-leaf Yellow Pine.

This table is computed for an allowable fibre stress of 1 200 pounds per square inch, for flexure, and the deflection coefficients are calculated for a modulus of elasticity of 1 500 000 pounds per square inch.

The limit for a deflection of  $\frac{1}{10}$  of the span is indicated by the lower dotted zig-zag line on the tables, the values below which correspond to deflections greater than, and those above to deflections less than, the limiting deflections. The upper dotted zig-zag line similarly indicates the limits of deflection for a modulus of elasticity of 750 000 pounds per square inch.

The lower full zig-zag line indicates the limit of allowable shearing stress along the axis corresponding to the allowable intensity, for Yellow Pine, of 150 pounds per square inch.

Similarly, the upper full zig-zag line indicates the limits for shearing along the axis for White Oak based on an allowable intensity of 200 pounds per square inch.

### BEARING AT POINTS OF SUPPORT.

Care should be taken in designing to provide sufficient bearing at the points of support so that the allowable intensity of compression across the grain, as given in the tables on pages 409 to 415, is not exceeded.

This may be obtained, where necessary, by the use of corbels or bearing plates of harder wood arranged so as to give a large bearing area against the softer beam. The following statements are made in Bulletin No. 12, U. S. Department of Agriculture, Division of Forestry:

#### RECOMMENDED PRACTICE.

"Since the strength of timber varies very greatly with the moisture contents (see Bulletin 8 of the Forestry Division), the economical designing of such structures will necessitate their being separated into groups according to the maximum moisture contents in use.

### MOISTURE CLASSIFICATION.

"Class A (moisture contents, 18 per cent.)—Structures freely exposed to the weather, such as railway trestles, uncovered bridges, etc.

"Class B (moisture contents, 15 per cent.)—Structures under roof but without side shelter, freely exposed to outside air, but protected from rain, such as roof trusses of open shops and sheds, covered bridges over streams, etc.

"Class C (moisture contents, 12 per cent.)—Structures in buildings unheated, but more or less protected from outside air, such as roof trusses of barns, enclosed shops and sheds, etc.

"Class D (moisture contents, 10 per cent.)—Structures in buildings at all times protected from the outside air, heated in the winter, such as roof trusses in houses, halls, churches, etc.

"For long-leaf pine add to all the values given in the tables, except those for moduli of elasticity, tension and shearing, for Class B, 15 per cent.; for Class C, 40 per cent.; and for Class D, 55 per cent. For the other species add to these values, for Class B, 8 per cent.; for Class C, 18 per cent., and for Class D, 25 per cent."

Based upon the above classification of structures, the two following tables have been figured to facilitate calculations of allowable loads for wooden beams and columns.

Proportion of the Values given in the "Tables of Safe Loads for Wooden Beams," Pages 416 to 421 inclusive, to be used in order to obtain the Safe Loads for the various classes of structures referred to above.

	Yellow Pine.
1.00 1.08 1.18 1.25	1.00 1.15 1.40
20	1.

Safety Factors to be applied to the Values given in the Table of "Strength of Solid Wooden Columns," Pages 422 and 423, in order to obtain the Safe Loads for the various classes of structures referred to above.

Classes.	Yellow Pine.	All Others.
Class A	0.20	0.20
Class C	0.28	0.24

# SPECIFIC GRAVITY AND WEIGHT PER FOOT FOR VARIOUS KINDS OF TIMBER.

30 49.9 38 23.7	
	2 ,1.90
38.0	8 3.17
31.8	0.01
31.8	4 2.65
50 31.2	
10   24.9	1 2100
	1 2000
	0 0000
	0 1000
	10 24.9 16 28.7 16 23.1 16 41.2 19 24.9

The specific gravities and weights given above are the averages of a large number of determinations by various authorities, for woods containing less than 15 per cent. of moisture or such as are commercially known as dry timber. The weights of green or unseasoned woods will be from 20 to 40 per cent. greater than those given in the above table.

# SAFE UNIT STRESSES FOR TIMBER.

RECOMMENDED IN BULLETIN No. 12, U. S. DEPARTMENT OF AGRICULTURE, DIVISION OF FORESTRY.

Safe Unit Stresses at 18% Moisture.

Species.	Modulus of Strength at Rupture per Square Inch.	Modulus of Elasticity per Square Inch.	Resilience per Cubic Inch.	Grushing Strength Endwise per Square Inch.	570	Strength per Square Inch.	Strength per Square Inch
	Lbs.	Lbs.	Lbs.	Lbs.	Lbs.	Lbs.	Lbs.
Long-leaf Pine (Pinus palustris) D Short-leaf Pine (Pinus	1550	720000	1.30	1000	215	12000	125
echinata) D	1300	600000	1.30	840	215	9000	100
		000000	1.00	010	NIO	2000	100
White Pine (Pinus stro- bus) Norway Pine (Pinus res-	880	435000	1.00	700	147	7000	75
	1090	566000		760	143		
inosa)		900000		100	140		
Colorado Pine (Pinus ponderosa)	980	444000		630	180		
Douglas Fir (Pseudot-					100		
suga douglasii)	1320	690000		880	167		
Redwood (Sequoia sem-							
pervirens)	*1440	†226000		650	115		
		[220000		000	110		
Red Cedar (Juniperus	4000	995000		700	950		
virginiana)	1000	335000		700	250		
Bald Cypress (Taxo-				-	100	0000	70
dium distichum) D	1000	450000	1.10	675	120	6000	60
White Oak (Quercus				1		-	
alba) D		550000	1.25	800	400	10000	200
Factor of Safety		2	1	5	3	1	4
a deces of careey	0				1		

The values marked "D" were obtained from experiments made by the Forestry Division. The other values were obtained from various sources, chiefly the 10th Census Report, but so modified as to give results comparable with Forestry Division values. To arrive at true average values of strength multiply safe loads by factor of safety given in each column. The value for resilience and tensile strength are the ultimate values. The former is practically never used in designing. The latter is a factor impossible to develop in practice, since the piece will always fail in some other way, usually by shearing.

The crushing strength across the grain in above is based upon a crushing of 3 per cent, of the cross sectional height of the piece.

<sup>\*</sup> This value is certainly too large.

<sup>† &</sup>quot; " " small.—ED.

# AVERAGE TESTED STRENGTH VALUES OF STRUCTURAL TIMBERS WITH ORDINARY DEFECTS.

	112		Bene	ling.
Kind of Timber.	Condition.	Average Moisture Content,	Fibre Stress at Mastic Limit.	Modulus of Rupture.
		Per Cent.	Lbs. per Sq. In.	Lbs. per Sq. In.
Long-leaf Pine (Pinus	Green	27.6	3734	6140
Palustris).	Air Seasoned	19.2	3691	5749
Douglas Fir (Pseudo-	Green	33.2	3968	5983
	Air Seasoned	17.3	4563	6372
Short-leaf Pine (Pinus	Green	46.4	3237	5548
Echinata).	Air Seasoned	15.9	4675	6573
	Green	51.3	3324	4948
	Air Seasoned	17.9	3503	5856
	Green	34.4	3040	5084
Tæda).	Air Seasoned	17.9	3517	6118
Tamarack (Larix Lari-		42.0	2813	4556
cina).	Air Seasoned	21.5	3730	5498
Western Hemlock (Tsuga	Green	47.6	3516	5296
Heterophylla).	Air Seasoned	17.7	4398	6420
Redwood (Sequoia Sem-		87.5	3760	4472
	Air Seasoned	20.9	3442	3891
	Green	49.0	2492	3864
Resinosa).	Air Seasoned	15.7	4069	6054

The above table presents the average results of an extensive series of tests The above table presents the average results of an extensive series of tests on structural timbers as conducted by the United States Forestry Service and published in Bulletin No. 108, issued September 23, 1912. Many engineering handbooks and other publications dealing with timber quote results of tests made only on small thoroughly seasoned specimens, free from defects. Such values may be from one and one-half to two times as high as stresses developed in large timbers and joists.

The above tabulations, with the exception of those in final column headed "Shear," are based upon tests of structural size timbers having such defects as are ordinarily to be found. The "Shear" column values, owing to the method of testing, were obtained from small specimens and it will be seen that the shearing stresses developed are much higher than the calculated.

that the shearing stresses developed are much higher than the calculated shearing stresses in beams that failed by horizontal shear. The difference is doubtless due to the fact that on account of checks and shakes, the actual area resisting shear is likely to be much less than the calculated area used in the formula for horizontal shear. Since large timbers almost invariably form checks during seasoning, it is not safe, in designing timber beams, to use shearing stresses higher than those determined for beams that failed in horizontal shear.

# AVERAGE TESTED STRENGTH VALUES OF STRUCTURAL TIMBERS WITH ORDINARY DEFECTS.

Beno	ding.		Comp		Shear.	
Modulus			Parallel to Gra	in.	Perpendicular to Grain,	Shearing
of Elasticity.	*Horizontal Shear.	Crushing Strength at Elastic Limit.	Crushing Strength at Maximum Load.	Modulus of Masticity.	Crushing Strength at Elastic Limit.	Strength (Small Specimens).
1000 Lbs. per Sq. In.	Lbs. per Sq. In.	Lbs. per Sq. In.	Lbs. per Sq. In.	1000 Lbs. per Sq. In.	Lbs. per Sq. In.	Lbs. per Sq. In.
1463	353	3480	4800		568	973
1705	272	3480	4800		572	984
1517	166	2770	3495	1414	570	765
1549 1473	221 332	3271 2460	4258 3435	1038 1548	639 351	822 704
1726	364	4070	6030	1951	796	1135
1301	288	2675	3510	1575	456	700
1487	340	2010	5746	10,0	597	905
1387	335	2050	2940	548	500	630
1487	434	3011	4292	1206	655	1115
1220	261	2400	3230	1373		668
1341	299	3349	4320	1351		879
1445	288	2905	3355	1617	434	630
1737	307	4840	5814	2140	473	924
1042	302	3194	3882	1240	434	742
890			4276		525	671
1133	232	2065	2555	1002		589
1418	278	3047	4228	1367		1145

<sup>\*</sup>Only those pieces which failed first by horizontal shear are included in this column.

The averages for the bending tests are the results of tests on timbers ranging in cross section from 4 by 10 inches to 8 by 16 inches, over a 15-ft, span.

A comparison of the results of tests on air seasoned material with those on green material shows that, in general, all of the mechanical properties are increased by seasoning. Increase in strength of wood fibre, due to drying, is, in the case of large timbers, largely offset by a weakening of the timber due to the formation of checks. If the moisture content of a seasoned timber is increased, it loses strength rapidly, and if thoroughly soaked with water will become slightly weaker than when green. On this account, it is not safe in practice to depend upon any increase of strength in timbers, due to seasoning. When, however, large beams are seasoned with ordinary care, it is safe to assume that they are not weaker than when green.

# UNIT STRESSES FOR STRUCTURAL TIMBER.

(Expressed in Pounds per Square Inch.)

	1	Bending		Shearing.				
Kind of Timber.	Extr Fibre		Modulus of Elasticity	Para to Gr		Longitudinal Shear in Beams.		
	Average Ultimate.	Safe Stress.	in Thou- sands.	Average Ultimate.	Safe Stress.	Average Ultimate.	Safe Stress.	
Douglas Fir	6100	1200	1510	690	170	270	110	
Long-leaf Pine Short-leaf Pine White Pine	6500 5600 4400	1300 1100 900	1610 1480 1130	720 710 400	180 170 100	300 330 180	120 130 70	
Spruce Norway Pine Tamarack Western Hemlock	4800 4200 4600 5800	1000 800 900 1100	1310 1190 1220 1480	600 *590 670 630	150 130 170 160	170 250 260 *270	70 100 100 100	
Redwood Bald Cypress Red Cedar White Oak	5000 4800 4200 5700	900 900 800 1100	800 1150 800 1150	300 500  840	80 120 210	270	110	

Note.—These unit stresses are for a green condition of timber and are to \* Partially air-dry.

The above table gives the ultimate and safe unit stress values for structural timber as adopted by the American Railway Engineering and Maintenance of Way Association, upon recommendation of their Committee on Wooden Bridges and Trestles, Convention of 1909; and published in the Association's "Bulletin No. 107," 1909, and "Manual," 1911.

They state that the working unit stresses given in this table are intended for railroad bridges and trestles. For highway bridges and trestles, the unit stresses may be increased twenty-five (25) per cent. For buildings and similar structures, in which the timber is protected from the weather and practically free from impact, the unit stresses may be increased fifty (50) per cent. To compute the deflection of a beam under long continued loading instead of that when the load is first applied, only fifty (50) per cent. of the corresponding modulus of elasticity given in the tables is to be employed.†

The safe unit stresses were determined by carefully considering both the average ultimate stresses, which represent the best results now available, as well as the unit stresses which have been in use in designing wooden bridges and trestles, and have been demonstrated by extensive practice to be safe.

<sup>†</sup> Timber has no well-defined modulus of elasticity.--Ep.

# UNIT STRESSES FOR STRUCTURAL TIMBER.

(Expressed in Pounds per Square Inch.)

		(	Compress	ion.		Ratio
	Perpendicular to Grain.		Parallel to Grain.		Long Columns over	of Length to Stringer
Elastic Limit.	Safe Stress.	Average Ultimate.	Safe Stress.	15 Diams, Safe Stress.	15 Diameters. Safe Stress.	Depth.
630	310	3600	1200	.900	$1200 \ (1 - \frac{L}{60D})$	10
520	260	3800	1300	980	1300 ( " )	10
340	170	3400	1100	830	1100 ( " )	10
290	150	3000	1000	750	1000 ( " )	10
370	180	3200	1100	830	1100 ( " )	
	150	*2600	800	600	800 ( " )	
	220	*3200	1000	750	1000 ( " )	
440	220	3500	1200	900	1200 ( " )	
400	150	3300	900	680	900 ( " )	
340	170	3900	1100	830	1100 ( " )	
470	230	2800	900	680	900 ( " )	
920	450	3500	1300	980	1300 ( " )	12

be used without increasing the live load stresses for impact. L = length in inches. D = least side or diameter in inches.

The relation between the strength of the lowest 10 per cent. group of tests and the average strength for each series, the relation between the elastic limit and the ultimate strength, as well as the fact that the live load stresses are not to be increased for impact, are all to be taken into account in determining the general relation between the safe stress and the average ultimate stress; it being always remembered that it is more rational to relate the safe unit stress to the elastic limit of the material than to its ultimate strength.

As large columns not over 15 diameters in length may not develop more than 70 per cent. of the strength of short blocks, the column formulas are arranged to give approximately these relative values at the given limit of length when L, the length of the column in inches, equals 15 times its least diameter D, also expressed in inches.

It is expected that these unit stresses will be revised at intervals of a few years, whenever new results of timber tests are published, or when the experience of bridge engineers who have adapted them shall indicate that revision is desirable.

# AVERAGE ULTIMATE BREAKING UNIT

	Ten	sion.
Kind of Timber.	With Grain.	Across Grain.
White Oak. White Pine. White Pine. Southern Long-leaf or Georgia Yellow Pine. Douglas Fir. Short-leaf Yellow Pine. Red Pine (Norway Pine) Spruce and Eastern Fir. Hemlock. Cypress. Cedar. Chestnut. California Redwood. California Spruce.	12000 7000 12000 8000 8000 8000 6000 7000 8500 7000	2000 500 600 500 500 500

# AVERAGE SAFE ALLOWABLE WORKING UNIT

Kind of Timber.	Tension.	
	With Grain.	Across Grain.
· Factor of Safety.	Ten.	Ten.
White Oak White Pine. Southern Long-leaf or Georgia Yellow Pine. Douglas Fir. Short-leaf Yellow Pine. Red Pine (Norway Pine). Spruce and Eastern Fir. Hemlock. Cypress. Cedar. Chestnut. California Redwood. California Spruce.	1200 700 1200 800 800 800 800 600 700 850 700	200 50 60 50 50 50 50

The above tables are based on those recommended by the committee on intendents of Bridges and Buildings at their Fifth Annual Convention in by later data from various sources.

#### STRESSES, IN POUNDS PER SQUARE INCH.

C	ompression	-117	Tran	sverse.	Shea	ring.
With	Grain.					
Mnd Bearing.	Columns Under 15 Diams,	Across Grain.	Extreme Fibre Stress.	Modulus of Elasticity.	With Grain.	Across Grain.
7000 5500 7000 5700 6000 5000 6000	\$000 \$500 \$500 \$500 \$4500 \$4000 \$4000 \$4000 \$4000 \$4000 \$4000 \$4000 \$4000	2000 700 1400 800 1000 500 700 600 700 900 600	7000 4000 7000 5000 6000 5000 4000 3500 4000 4000 4500 5000	1500000 1000000 1500000 1400000 1200000 1200000 900000 700000 1000000 1200000 1200000	800 400 600 500 400 400 350 400 600 400	4000 5000 5000 4000 3000 2500 1500 2000

#### STRESSES, IN POUNDS PER SQUARE INCH.

Ce	ompression.		Tran	sverse.	Shea	ring.	
With Grain,  End Bearing. Columns Under 15 Diams.		Across Grain.	Grain. Stress.		With Grain.	Across Grain,	
Five.	Five.	Four.	Six.	Two.	Four.	Four.	
1400 1100 1400 1100 1200 1000 1200	1000 700 1000 800 800 800 800 800 800 800 800	500 200 350 200 250 200 200 150 200 200 250 150	1200 700 1200 800 1000 800 700 600 800 700 800 750 800	750000 500000 750000 800000 665000 450000 450000 450000 350000 600000	200 100 150 130 100 100 100 100 150 100	1000 500 1250 1000 750 600 400 500	

<sup>&</sup>quot;Strength of Bridge and Trestle Timbers" of the Association of Railway Super-October, 1895, but the arrangement and values in many cases are now modified

#### SAFE LOAD IN POUNDS FOR RECTANGULAR OF WHITE PINE, CEDAR

Allowable fibre stress 700 pounds per square inch. Safety factor 6.

Safe loads for other safety factors may be obtained as follows:

Span				Dep	th of	Bean	a in I	nche	3.	1		Deflection Coefficient for White Pine
Feet.	4	5	6	7	8	9	10	11	12	13	14	V
ă	311	486	700	953	1244	1575	1944	2352	2800	3286	3811	.34
5	249	389	560	762	996	1260	1556	1882	2240	2629	3049	.53
6	207	324	467	635	830	1050	1296	1569	1867	2191	2541	.76
7	178	278	400	544	711	900	1111	1344	1600	1878	2178	1.03
8	156	243	350	476	622	788	972	1176	1400	1643	1906	1.34
5	138	216	311	423	553	700	864	1046	1244	1460	1094	1.70
10	124	194	280	381	498	630	778	941	1120	1314	1524	2.10
11	113	177	255	346	453	573	707	856	1018	1195		2.54
12	103	162	233	318	415	525	648	784	933	1095	1270	3.02
13	96	150	215	293	383	485	598	724	862	1011	1173	3.55
14	89	139	200	272	356	450	556	672	800	939	1089	4.12
15	83	130	187	254	332	420	519	627	747	876	1016	4.73
16	78	122	175	238	311	394	486	588	700	821	953	5.38
17	78	114	165	224	293	371	458	554	659	773	897	6.07
18	69	108	156	212	277	350	432	523	622	730	847	6.80
19	65	102	147	201	262	332	409	495	589	692	802	7.58
20		97	140	191	249	315	289	471	560	657	762	8.40
21		93	133	182	237	300	370	448	533	626	726	9.26
22		88	127	173	226	286	354	428	509	597	693	10.16
23		85	122	166	216	274	338	409	487	572	663	11.11
24			117	159	207	263	324	392	467	548	635.	12.10
25		111-1	112	152	199	252	311	376	448	526	010	13.13
26			108	147	191	242	209	362	431	506	586	14.20
27			104	141	184	233	288	349	415	487	565	15.31
28			100	136	178	225	278	336	400	469	544	16.46
29			97	131	172	217	268	325	386	453	526	17.66
30			93	127	166	210	259	314	373	438	508	18.90
31			90	123	161	203	251	304	361	424	492	20.18
32			88	119	156	197	243	294	350	411	476	21.50
33			85	115	151	191	236	285	339	398	462	22.87
34				112	146	185	229	277	329	387	448	24.28
35		-	-	109	142	180	222	260	320	376	436	25.73

#### UNIFORMLY DISTRIBUTED BEAMS ONE INCH THICK AND SPRUCE OR EASTERN FIR.

Modulus of rupture 4 200 pounds per square inch.

New safe load = Safe load from table  $\times \frac{6}{\text{New factor}}$ 

Span			1	Depth	of B	eam i	n Inch	les.		,	Deflection Coefficient for White Pine
Feet.	15	16	17	18	19	20	21	22	23	24	V
9	1944	2212	2498	2800	3120	3457	3811	4183	4571	4978	1.70
10	1750	1991	2248	2520	2808	3111	3430	3764	4114	4480	2.10
11	1601	1810	2044	2291	2552	2828	3118	3422	3740	4073	2.54
12	1458	1659	1873	2100	2340	2593	2858	3137	2428	3733	3.02
13	1346	1531	1729	1938	2160	2393	2638	2896	3165	3446	3.55
14	1250	1422	1606	1800	2056	2222	2450	2689	2939	3200	4.12
15	1167	1328	1499	1680	1872	2074	2287	2510	2743	2987	4.73
16	1094	1244	1405	1575	1755	1944	2144	2353	2571	2800	5.38
17	1029	1171	1322	1482	1652	1830	2018	2214	2420	2635	6.07
18	972	1106	1249	1400	1560	1728	1906	2091		2489	6.80
19	921	1048	1183	1326	1478	1637	1805	1981	2165	2358	7.58
20	875	996	1124	1260	1404	1556	1715	1882	2057	2240	8.40
21	833	948	1070	1200	1337	1481	1633	1793	1959	2133	9.26
22	795	905	1022	1145	1276	1414	1559	1711	1870	2036	10.16
23	761	866	977	1096	1221	1353	1491	1637	1789	1948	11.11
24	729	830	937	1050	1170	1296	1429	1569	1714	1867	12.10
25	700	796	899	1008	1123	1244	1372	1506	1645	1792	13.13
26	673	766		989	1080	1197	1319	1448	1582	1723	14.20
27	648	737	833	933	1040	1152	1270	1394	1524	1659	15.31
28	625	711	803		1003	1111	1225	1344	1469	1600	16.46
29	603	687	775	869	968	1073	1183	1298	1419	1545	17.66
30	583	664	749	840	936	1037	1143	1255	1371	1493	18.90
31	565	642	725	813	906	1004	1106	1214	1327	1445	20.18
32	547	622	703	787	877	972	1072	1176	1286	1400	21.50
33	534	603	681	764	850	943	1039	1141	1247	1358	22.87
34	515	586	661	741	826	915	1009	1107	1210	1318	24.28
35	500	500	642	720	802	889	980	1076	1176	1280	25.73
36	486	553	624	700	780	864	953	1046	1143	1244	27.22
37	473	538	608	681	759	841	927	1017	1112	1211	28.75
38	460	524	592	663	739	819	903	991	1083	1179	30.32
39	449	511	576	646	720	798	880	985	1055	1149	31.94
40	438	498	562	630	702	778	858	941	1029	1120	33.60

#### SAFE LOADS IN POUNDS FOR RECTANGULAR OF SHORT-LEAF

Allowable fibre stress 1 000 pounds per square inch. Safety factor 6.

Safe loads for other safety factors may be obtained as follows:

Span in				Dep	th of	Bean	n in I	nches				Deflection Coefficient
Feet.	4	5	6	7	8	9	10	11	12	13	14	V
4	444	694	1000	1361	1778	2250	2778	3361	4000	4694	5444	.40
5	356	556	800	1039	1422	1800	2222	2689	3200	3756	4356	163
6	296	463	667	907	1185	1500	1852	2241	2667	3130	3630	190
7	254	397	571	778	1016	1286	1587	1921	2286	2683	3111	1.23
8	222	347	500	681	889	1125	1389	1681	2000	2347	2722	1.60
9	198	309	444	005	790	1000	1235	1494	1778	2086	2420	2.03
10	178	278	400	544	711	900	1111	1344	1600	1878	2178	2.50
11	162	253	364	495	646	818	1010	1222	1455	1707	1980	3.03
12	148	231	333	454	593	750	926	1120	1333	1565	1815	3.60
13	137	214	308	419	547	692	855	1034	1231	1444	1675	4.23
14	127	198	286	389	508	643	794	960	1143	1341	1556	4.90
15	119	185	267	363	474	600	741	896	1067	1252	1452	5.63
16	111	174	250	340	444	503	694	840		1174	1361	6.40
17	105	163	235	320	418	529	654	791	UAL	1105	1281	7.23
18	99	154	222	302	395	500	617	747	889	1043		8.10
19	94	146	211	287	374	474	585	708	842	988	1146	9.03
20	89	139	200	272	356	450	556	672	800	539	1089	10.00
21	85	132	190	259	339	429	529	640	762	894	1037	11.03
22	81	126	182	247	323	409	505	611	727	854	990	12.10
23	77	121	174	237	309	391	483	585	696	816	947	13.23
24		116	162	227	296	375	463	560	667	782	907	14.40
25		111	160	218	284	360	444	538	640	751	871	15.63
26		107	154	209	274	346	427	517	615	722	838	16.90
27		103	148	202	263	333	412	498	593	695	807	18.23
28	-	99	143	194	254	321	397	480	571	671	778	19.60
29	-		138	188	245	310	383	464	552	648	751	21.03
30			133	181	237	300	370	448	533	626	726	22.50
31			129	176	229	290	358	434	516	608	703	24.03
32			125	170	222	281	347	420	500	587	681	25.60
33			121	165	215	273	337	407	485	569	860	27.23
34		-	118	160	209	265	327	395	471	552	641	28.90
35	1		114	156	203	257	317	384	457	537	602	30.63

Safe loads for any fibre stress may be readily obtained from this table by proportion.

#### UNIFORMLY DISTRIBUTED, BEAMS ONE INCH THICK, YELLOW PINE.

Modulus of rupture 6 000 pounds per square inch. New safe load = Safe load from table  $\times \frac{6}{\text{New factor}}$ .

Span		Depth of Beam in Inches.									Deflection Coefficient
Feet.	15	16	17	18	19	20	21	82	23	24	V
9	2778	3160	3568	4000	4457	4938	5444	5975	6531	7111	2.03
10	2500	2844	3211	3600	4011	4444	4900	5378	5878	6400	2.50
11	2273	2586	2919	3273	3646	4040	4455	4889	5343	5818	3.03
12	2083	2370	2676	2000	3343	3704	4083	4481	4898	5333	3.60
13	1923	2188	2470	2769	3085	3419	3769	4137	4521	4923	4.23
14	1786	2032	2294	2571	2865	3175	3500	3841	4198	4571	4.90
15	1667	1896	2141	2400	2674	2963	3267	3585	3919	4267	5.63
16	1563	1778	2007	2250	2507	2778	3062	3361	3674	4000	6.40
17	1471	1673	1889	2118	2359	2614	2882	3163	2458	3785	7.23
18	1389	1580	1789	2000	2228	2469	2722	2988	3265	3556	8.10
19	1316	1497	1690	1895	2111	2839	2579	2830	3094	3368	9.03
20	1250	1422	1606	1800	2008	2222	2450	2689	2939	3200	10.00
21	1190	1354	1520	1714	1910	2116	2333	2561	2799	3048	11.03
22	1136	1293	1460	1636	1823	2020	2227	2444	2672	2909	12.10
23	1087	1237	1396	1565	1744	1932	2130	2338	2556	2783	13.23
24	1042	1185	1338	1500	1671	1852	2042	2241	2449	2667	14.40
25	1000	1138	1284	1440	1604	1778	1960	2131	2351	2560	15.63
26	962	1094	1235	1385	1543	1709	1885	2068	2261	2462	16.90
27	926	1053	1189	1333	1486	1646	1815	1992	2177	2370	18.23
28	893	1016	1147	1286	1433	1587	1750	1921	2099	2286	19.60
29	862	981	1107	1241	1383	1533	1690	1854	2027	2207	21.03
30	833	948	1070	1200	1337	1481	1633	1793	1959	2133	22.50
31	806	918	1036	1161	1294	1434	1581	1735	1896	2065	24.03
32	781	889	1003	1125	1253	1389	1531	1681	1837	2000	25.60
33	758	862	973	1091	1215	1347	1485	1630	1781	1939	27.23
34	735	837	944	1059	1180	1307	1441	1582	1728	1882	28.90
35	714	813	917	1029	1146	1270	1400	1537	1677	1829	30.63
36	694	780	894	1000	1114	1235	1361	1494	1633	1778	32.40
37	676	769	868	973	1084	1201	1324	1453	1589	1730	34.23
38	658	749	845	947	1056	1169	1289	1415	1547	1684	36.10
39	641	729	823	923	1028	1140	1256	1379	1507	1641	38.03
40	625	711	803	900	1003	1111	1225	1344	1469	1600	40.00

Safe loads for beams of California Redwood, 34 of above.

#### SAFE LOADS IN POUNDS FOR RECTANGULAR OF WHITE OAK AND

Allowable fibre stress 1 200 pounds per square inch. Safety factor 6.

Safe loads for other safety factors may be obtained as follows:

Span in				Dep	th of	Bear	n in I	nche	s.			Deflection
Feet.	4	5	6	7	8	9	10	11	12	13	14	V
4	533	833	1200	1633	2133	2700	3333	4033	4800	5633	6533	138
5	427	667	960	1307	1707	2160	2667	3227	3840	4507	5227	180
6	356	556	800	1089	1422	1800	2222	2689	3200	3756	4356	186
7	305	476	686	933	1219	1543	1905	2305	2743	3219	3733	1.18
8	267	417	600	817	1067	1350	1667	2017	2400	2817	3267	1.54
9	237	370	533		948	1200	1481	1793	2133	2504	2904	1.94
									2100			2.02
10	213	333	480	653	853	1080	1333	1613	1920	2253	2613	2.40
11	194	303	436	594	776	982	1212	1467	1745	2048	2376	2.90
12	178	278	400	544	711	900	1111	1344	1600	1878	2178	3.46
13	164	256	369	503	656		1026	1241	1477	1733	2010	4.06
14	152	238	343	467	610	771	952	1152	1371	1610	1867	4.70
15	142	222	320	436	569	720	889	1076	1280	1502	1742	5.40
16	133	208	300	408	533	675	833	1008	1200	1408	1633	6.14
17	125	196	282	384	502	635	784	949	1129	1325	1537	0.94
18	119	185	267	363	474	600	741	896	1067	1252	1452	7.78
19	112	175	253	344	449	568	702	849	1011	1186	1375	8.66
20	107	167	240	327	427	540	667	807	960	1127	1307	9.60
21	102	159	229	311	406	514	635	768	914	1073	1244	10.58
22	97	152	218	297	388	491	606	733	873	1024	1188	11.62
23	93	145	209	284	371	470	580	701	835	980	1136	12.70
24	89	139	200	272	356	450	556	672	800	939	1089	13.82
25	85	133	192	261	341	432	533	645	768	901	1045	15.00
26		128	185	251	328	415	513	621	738	867	1005	16.22
27		123	178	242	316	400	494	598	711	835	968	17.50
28		119	171	233	305	386	476	576	886	805	933	18.82
29		115	166	225	294	372	460	556	662	777	901	20.18
20		111	160	218	284	360	444	538	640	751	871	21.60
31		108	155	211	275	348	430	520	619	727	843	23.36
32			150	204	267	338	417	504	600	704	817	24.58
33			145	198	259	327	404	489	582	683	792	26.14
34			141	192	251	318	392	475	565	663	769	27.74
35			137	187	244	309	381	461	549	644	747	29.40

Safe loads for beams of Douglas Fir, Red Pine (Norway Pine), Cypress, Chestnut and California Spruce, % of above.

#### UNIFORMLY DISTRIBUTED, BEAMS ONE INCH THICK, LONG-LEAF YELLOW PINE.

Modulus of rupture 7 200 pounds per square inch. New safe load = Safe load from table  $\times \frac{6}{\text{New factor}}$ 

Span		Depth of Beam in Inches.									Deflection Coefficient
Feet.	15	16	17	18	19	20	21	22	28	24	V
9	3333	3793	4281	4800	5348	5926	6533	7170	7837	8533	1.94
10	3000	3413	3853	4320	4813	5333	5880	6453	7053	7680	2.40
11	2727	3103	3503	3927	4376	4848	5356	5867	6412	6982	2.90
12	2500		3211	3600	4011	4444	4900	5378	5878	6400	3.46
13	2308	2626	2964	3323	3703	4103	4523	4964	5426	5908	4.06
14	2143	2438	2752	3086	3438	3810		4610	5038	5486	4.70
15	2000	2276	2569	2880	3209	3556	3920	4302	4702	5120	5.40
16	1875	2133	2408	2700	3008	3333	3675	4033	4433	4800	9.14
17	1765	2008	2267	2541	2831	3137	3459	3796	4149	4518	6.94
18	1667	1896	2141	2400	2674	2963	3267	3585	3819	4267	7.78
19	1579	1796	2027	2274	2533	2807	3095	3396	3712	4042	8.66
20	1500	1707	1927	2160	2407	2667	2940	3227	3527	3840	9.60
21	1429	1625	1835	2057	2292	2540	2800	3073	3359	3657	10.58
22	1364	1552	1752	1964	2188	2424	2678	2933	3206	3491	11.62
23	1304	1484	1675	1878	2093	2319	2557	2806	3067	3339	12.70
24	1250	1422	1606	1800	2006	2222	2450	2689	2939	3200	13.82
25	1200	1365	1541	1728	1925	2133	2352	2581	2821	3072	15.00
26	1154	1313	1482	1662	1851	2051	2262	2482	2713	2954	16.22
27	1111	1264	1427	1600	1783	1975	2178	2390	2612	2844	17.50
28	1071	1219	1376	1543	1719	1905	2100	2305	2519	2743	18.82
29	1034	1177	1329	1400	1660	1839	2028	2225	2432	2648	20.18
30	1000	1138	1284	1440	1604	1778	1960	2151	2351	2560	21.60
31	968	1101	1243	1394	1553	1720	1897	2082	2275	2477	23.06
32	938	1067	1204	1350	1504	1667	1838	2017	2217	2400	24.58
33	909	1034	1168	1309	1459	1616	1785	1956	2137	2327	26.14
34	882	1004	1133	1271	1416	1569	1729	1898	2075	2259	27.74
35	857	975	1101	1234	1375	1524	1680	1844	2013	2194	29.40
. 36	833	948	1070	1200	1337	1481	1633	1793	1959	2133	31.10
37	811	923	1041	1168	1301	1441	1589	1744	1906	2076	32.86
38	789	893	1014	1137	1267	1404	1547	1698	1856	2021	34.66
39	769	875	988	1108	1234	1368	1508	1655	1809	1969	36.50
40	750	853	963	1080	1203	1333	1470	1613	1763	1920	38.40

Safe loads for beams of Hemlock, 1/2 of above.

### STRENGTH OF SOLID WOODEN COLUMNS OF DIFFERENT KINDS OF TIMBER.

For various values of  $\frac{1}{d}$ .

1 = length of column in inches. d = least diameter in inches. Based on the Formula of the U. S. Department of Agriculture, Division of Forestry.

$$P = F \times \frac{700 + 15c}{700 + 15c + c^2}$$

P = ultimate strength in pounds per square inch.

F = ultimate crushing strength of timber.  $c = \frac{1}{d}$ 

Values of F are those given in table on pages 414 and 415 herein.

	Ultimate	Ultimate Strength in Pounds per Square Inch:									
	White Oak and Southern Long-leaf or Georgia Yellow Pine.	Douglas Fir and Short-leaf Yellow Pine.	Red Pine (Norway Pine), Spruce or Eastern Fir, Hemlock, Cypress, Chestnut, California Redwood and Cali- fornia Spruce.	White Pine and Cedar.							
T	5000	4500	4000	3500							
1 d											
2	4973	4475	3978	3481							
3	4940	4446	3952	3458							
4	4897	4407	3918	3428							
5	4844	4359	3875	3391							
6	4782	4304	3826	3347							
7	4713	4242	3770	3299							
8	4638	4174	3710	3247							
9	4558	4102	3646	3190							
10	4474	4026	3579	3132							
11	4386	3948	3509	3070							
12	4297	3867	3438	3008							
13	4206	3785	3365	2944							
14	4114	3703	3291	2880							
15	4022	3620	3217	2815							
16	.3930	3537	3144	2751							
17	3838	3455	3071	2687							
18	3748	3373	2998	3624							
19	3659	3293	2927	2561							

For safety factors for various classes of structures to be used in connection with the above table, see p. 408.

### STRENGTH OF SOLID WOODEN COLUMNS OF DIFFERENT KINDS OF TIMBER.

For various values of  $\frac{1}{d}$ 

1 = length of column in inches. d = least diameter in inches.

BASED ON THE FORMULA OF THE U. S. DEPARTMENT OF AGRICULTURE, DIVISION OF FORESTRY.

 $P = F \times \frac{700 + 15c}{700 + 15c + c^2}$ 

P = ultimate strength in pounds per square inch.

F = ultimate crushing strength of timber.  $c = \frac{1}{d}$ 

Values of F are those given in table on pages 414 and 415 herein.

	Ultimate Strength in Pounds per Square Inch.								
	White Oak and Southern Long-leaf or Georgia Yellow Pine.	Douglas Fir and Short-leaf Yellow Pine.	Red Pine (Norway Pine), Spruce or Eastern Fir, Hemlock, Cypress, Chestnut, California Redwood and Cali- fornia Spruce.	White Pine and Cedar.					
F	5000	4500	4000	3500					
1 d									
20	3571	3214	2857	2500					
21	3486	3137	2788	2440					
22	3402	3061	2721	2381					
23	3320	2988	2656	2324					
24	3240	2916	2592	2268					
25	3162	2846	2529	2213					
26	3086	2777	2469	2160					
27	3013	2711	2410	2109					
28	2941	2647	2353	2059					
29	2872	2585	2298	2010					
30	2805	2524	2244	1963					
32	2677	2409	2142	1874					
34	2557	2301	2046	1790					
36	2445	2200	1956	1711					
38	2340	2106	1872	1638					
40	2241	2017	1793	1569					
42	2149	1934	1719	1505					
44	2063	1857	1650	1444					
46	1982	1784	1586	1388					
48	1907	1716	1525	1335					
50	1835	1652	1468	1285					

For safety factors for various classes of structures to be used in connection with the above table, see p. 408.

The Basis for Specific Gravities is Pure Water at 62 Degrees Fah.,  Barometer 30 Inches.	Average Specific Gravity,	Average Weight of One Cubic Foot.
Weight of One Cubic Foot, 62.355 Pounds.	Water=1.	Pounds.
Acid, acetic, 90%	1.062	66.3
" fluoric, 58%	1.20	75
muriatic (hydrochloric), 40%	1.20	75
" nitric, 35% phosphoric, 72%	1.217 1.558	76 97.2
* sulphuric, 97%	1.841	115
Air, atmospheric at 60 degrees F., under pressure of one atmosphere, or 14.7 pounds per square inch, weighs 1/815 as much as water	.00123	.0765
Alabaster	100120	160
Alcohol, commercial	.833	52
Alder wood	.68	42
Alum	.53	33
Aluminum bronze, 10%	7.70	480
" 5%	8.26 2.74	516 170.9
" " Cast	2.85	178.1
" " rolled	2.76	172.1
pure, annealed	2.66	165.9
" Cast	2.56 2.68	159.6
" rolled	2.70	167.1 168
" wrought	2.67	167
Ammonia, liquid, 29%	.897	56
Anthracite, 1.3 to 1.84; of Penna., 1.3 to 1.7	1.5	93.5
broken, of any size, loose		52 to 57
moderately shaken. heaped bushel, loose, 77 to 83 pounds. a ton loose occupies 40 to 43 cubic		56 to 60
" a ton loose occupies 40 to 43 cubic feet		
Antimony, cast	6.70	418
" native	6.67	416
Apple wood	.76	47
Arsenic	5.67	354
Asbestos	2.40	149
Ash, American white, dry (see note p. 433)	.61	38
" perfectly dry (see note p. 423)	.752	47
Ashes of soft coal, solidly packed		40 to 45
Asphaltum, 1 to 1.8.	1.4	87.3
Bamboo wood	.35	22
Barley		40
Basalt	2.86	178
Beech wood.	.73	46
Beer, lager.	1.034	64.5
Deer, lager	1.002	1 01.0

The Brais for Specific Gravities is Pure Water at 62 Degrees Fah.,  Barometer 30 Inches  Weight of One Cubic Foot, 62.355 Pounds.	Average Specific Gravity. Water=1.	Average Weight of One Cubic Foot. Pounds.
Beeswax	.965	60.2
Benzine		50
Birch wood	.65	41
Bismuth	9.78	611
Bleaching powder		31
Bluestone		150
Borax		110
Boxwood	.97	60
Brass, cu. 67, zn. 33, cast	8.32	519
" high yellow plates	8.59	535
" Muntz metal	8.22	512
" Naval rolled	8.51	530 527
wire	8.56	533
Brick, best pressed	0.00	150
" common and hard		125
" soft inferior		100:
Brickwork, at 125 pounds per cubic foot, 1 cubic yard		
equals 1.507 tons, and 17.92 cubic feet		
equal 1 ton		
coarse, inferior, soft		100
medium quality		125 140
pressed brick, the joints		-
Bronze, cu. 90, tin 10	8.67 8.75	541 546
* Tobin	8.38	523
Butter	.94	59
Butternut wood	.45	28
Butternut wood	.40	20
Calcite		170
		98
Calcium	1.57	
Camphor	.99	61.7
Caoutchouc	.96	60
Carbon	2.15	134
Carpet		12
Caustic soda		88
Cedar, American		35
Cement barrel, 15-30 pounds, average 20 pounds		
" mortar, Portland, 1: 2½		135
" natural, per barrel, net, 282 pounds " bag, net, 94 pounds		
Portland, loose		
" packed, as in barrels		
" per bag, net, 94 pounds		
p		

The Basis for Specific Gravities is Pure Water at 62 Degrees Fah.,  Barometer 30 Inches.  Weight of One Cubic Foot, 62.355 Pounds.	Average Specific Gravity. Water=1.	Average Weight of One Cubic Foot. Pounds.
Weight of One Onbie Foot, 62.355 Pounds.  Cement, Portland, per barrel, net, 376 pounds.  " standard proportioning.  a set.  Chalk.  Charcoal of pines and oaks.  Cheese.  Cherry wood, perfectly dry (see note p. 433)  Chestnut.  Chromium.  Cider.  Cinders (coal ashes and clinkers)  Cinnabar.  Citron.  Clay, dry in lump, loose.  " hard, ordinary.  " potters', dry, 1.8 to 2.1.  Coal, anthracite (see Anthracite).  " bituminous, a heaped bushel, loose, 70 to 78.  " broken, of any size, loose.  " a moderately shaken.  " " 1.2 to 1.5.  " " 1 ton occupies 43 to 48 cubic feet.  " lignite.  Cobalt.  Coke.  " loose, a heaped bushel, 35 to 42.	Gravity. Water=1.  2.85 2.5  .672 .66 6.8 1.02  8.81 .73	Cubic Foot.
Concrete, cinder, with Portland cement	8.7 8.93 8.93 8.82 8.89 8.89 8.9	112 150 150 148 143 143 155 557 557 557 549 555 554 555

Corn.         31           Cornmeal.         37           Cortundum, pure, 3.8 to 4.         3.9           Cotton goods.         11–33           Crockery.         40           Cypress wood.         .46         29           Dogwood.         .76         47           Dolomite.         180           Earth, common loam, perfectly dry, loose.         72 to 80           """ shaken         82 to 92           """ shaken         90 to 100           """ shaken         90 to 100           """ shaken         75 to 90           """ shak	The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. , Weight of One Cubic Foot, 62.355 Pounda.	Average Specific Gravity. Water=1.	Average Weight of One Cubic Foot. Pounds.
Cornmeal.         37           Cortundum, pure, 3.8 to 4         3.9           Cotton goods         11–33           Crockery         40           Cypress wood         .46         29           Dogwood         .76         47           Dolomite         180           Earth, common loam, perfectly dry, loose         72 to 80           Earth, common loam, perfectly dry, loose         72 to 80           Earth, common loam, perfectly dry, loose         72 to 80           Earth, common loam, perfectly dry, loose         72 to 80           Earth, common loam, perfectly dry, loose         72 to 80           Earth, common loam, perfectly dry, loose         72 to 80           Earth, common loam, perfectly dry, loose         70 to 76           Earth, common loam, perfectly dry, loose         70 to 76           Earth, common loam, perfectly dry, loose         70 to 76           Earth, composition         82 to 92           Earth, composition         82 to 92           Earth, composition         82 to 92           Earth, composition         83           Earth, composition         83           Earth, composition         80           Earth, composition         80           Earth, common window			
Corundum, pure, 3.8 to 4			
Cotton goods.		20	31
Crockery.         40           Cypress wood.         46           Dogwood.         .76         47           Dolomite.         180           Earth, common loam, perfectly dry, loose.         72 to 80           """"""""""""""""""""""""""""""""""""		0.0	11_22
Dogwood			
Dogwood		46	
Dolomite	Cypicos wood	.10	20
Dolomite	Demond	70	APT
Earth, common loam, perfectly dry, loose. 72 to 80  " " " shaken 82 to 92  " " " a more moist, loose. 70 to 76  " " " " shaken 75 to 90  " " " " " shaken 75 to 90  " " " " " shaken 75 to 90  " " " " " shaken 75 to 90  " " " " " " shaken 75 to 90  " " " " " " " " " " " " " " " " " " "		.70	
" " " shaken. 82 to 92 " " " " rammed. 90 to 100 " " " " slightly moist, loose. 70 to 76 " " " " shaken. 75 to 90 " " " " shaken. 104 to 112 "	Dolomite		190
" " " shaken. 82 to 92 " " " " rammed. 90 to 100 " " " " slightly moist, loose. 70 to 76 " " " " shaken. 75 to 90 " " " " shaken. 104 to 112 "			70.00
"" " " " " " " " " " " " " " " " " " "			
" " " " " " " " " " " " " " " " " " "	" " " rammed		
## ## ## ## ## ## ## ## ## ## ## ## ##	" " slightly moist, loose		70 to 76
" " " " as soft flowing mud	more moist, loose		
" " a soft flowing mud.	" " " nacked		
The following content of the first of the	" as soft flowing mud		
Ebony wood, American	" well pressed.		
" Indian			72
Eggs 1.09 Elder wood			
Elder wood	Indian		75
Elm wood, perfectly dry (see note p. 433)56 35  Fat—beef, hog and mutton92 57 Feldspar			
Fat—beef, hog and mutton       .92       57         Feldspar       .160       .55       34         Fir wood       .55       34       .55       34       .55       .26       .162       .162       .162       .26       .162       .26 <td></td> <td></td> <td></td>			
Feldspar         160           Fir wood         .55         34           Flax         90         90           Flint         2.6         162           Flour, compact         40         40           a loose         30         30           Gamboge         1.22         76           Gasoline (motor)         .7175         44 to 47           Glass, common window         2.52         157           " crown or plate         160         188           " flint         3.70         230           Glassware in boxes         60	Elm wood, perfectly dry (see note p. 433)	.50	35
Feldspar         160           Fir wood         .55         34           Flax         90         90           Flint         2.6         162           Flour, compact         40         40           a loose         30         30           Gamboge         1.22         76           Gasoline (motor)         .7175         44 to 47           Glass, common window         2.52         157           " crown or plate         160         188           " flint         3.70         230           Glassware in boxes         60	the second secon	-	
Fir wood     .55     34       Flax     90       Flint     2.6     162       Flour, compact     40       " loose     30       Gamboge     71-75     44 to 47       Glass, common window     2.52     157       " crown or plate     160     188       " flint     3.70     230       Glassware in boxes     60		.92	57
Flax         90           Flint         2.6         162           Flour, compact         40         30           Gamboge         30         30           Gasoline (motor)         71-75         44 to 47           Glass, common window         2.52         15           " crown or plate         160         188           " flint         3.70         230           Glassware in boxes         60			160
Flint   2.6   162   Flour, compact   40   40   30   30		.55	
Flour, compact.			2.0
" loose.     30       Gamboge.     1.22     76       Gasoline (motor).     .71–.75     44 to 47       Glass, common window.     2.52     157       " crown or plate     160     188       " crystal     188     188       " flint.     3.70     230       Glassware in boxes     60		2.6	
Gamboge     1.22     76       Gasoline (motor).     .7175     44 to 47       Glass, common window.     2.52     15       " crown or plate.     160       " crystal.     188       " flint.     3.70     230       Glassware in boxes.     60	Flour, compact		
Gasoline (motor)       .7175       44 to 47         Glass, common window       2.52       157         " crown or plate       160         " crystal       188         " flint       3.70       230         Glassware in boxes       60	100Se.,		30
Gasoline (motor)       .7175       44 to 47         Glass, common window       2.52       157         " crown or plate       160         " crystal       188         " flint       3.70       230         Glassware in boxes       60			
Glass, common window     2.52     157       " crown or plate     160       " crystal     188       " flint     3.70     230       Glassware in boxes     60			
" crown or plate     160       " crystal     188       " flint     3.70     230       Glassware in boxes     60	Gasoline (motor)		
" crystal	" crown or plate		
" flint	* crystal		
Glassware in boxes	* flint	3.70	
		2.69	168

The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches.	Average Specific Gravity.	Average Weight of One Cubic Foot.
Weight of One Cubic Foot, 62.355 Pounds.	Water=1.	Pounds.
Gneiss, in loose piles		96
Gold, cast, pure or 24-karat	19.258	1204
" pure, hammered	19.5	1217
* standard 22-k. (gold 11, copper 1)	17.5	1090
Granite, solid	2.72	170
" broken		96 165
dressed		154
dry		138
Graphite		130
Gravel		120
and sand		90-130
Greenstone, trap, 2.8 to 3.2.	3.00	187
Gum arabic	1.45	90
	.92	57
Gum wood		56
Gunpowder, loose	.90 1.00	62.4
" shaken " solid	1.55-1.80	97-113
Gutta-percha	.98	61
Gypsum, plaster of Paris or stucco mixed with water	.00	01
into a stiff mass, such as mortar, set and		
dried out		77
" rock, natural, free from surface water, not		
calcined in block form		140-145
" crushed, not calcined, all to pass through 1-inch ring		90-100
ground, 90% to pass through 100-mesh screen		30-100
dried of all free moisture, not calcined.		
known as "land plaster"		75-80
same, but calcined, known as "stucco" or		
"plaster of Paris"—loose		55-65
well shaken down or in bins		65-75
Hackmatack wood (American larch) (tamarack)	.59	37
Hay, baled		24
Hazel wood	.60	38
Hemlock wood	.40	25
Hemp		90
Hickory wood, perfectly dry (see note p. 433)	.85	53
Holly wood.	.76	47
Honey	1.45	91
Hornbeam wood	.76	47
		190
Hornblende		65.7
Human blood	1.054	1 00.7

The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches.	Average Specific Gravity.	Average Weight of One Cubic Foot.	
Weight of One Cubic Foot, 62.355 Pounds.	Water=1.	Pounds.	
Hydrogen	.00008	.0052	
Ice, .917 to .922	.92	57.4	
India rubber	.93	58	
Indigo	1.01	63	
Iron, cast, 6.9 to 7.4	7.15	446	
" grey cast	7.08	442	
" foundry, cold	7.21	450	
" " molten	6.94 7.86	433	
" white cast	7.65	477	
" wire	7.77	485	
" wrought	7.69	480	
Jasmine wood, Spanish	.77	48	
	.56	35	
Juniper wood	.00	00	
Larch wood	.56	35	
	.95	59	
Lard	11.37	1	
Lead, cast	11.37	708	
sheet	11.43	712	
Leather, dry	.86	54	
greased	1.02	64	
" in bales		16-23	
Lignite		80	
Lignum-vitæ wood (dry)	.65-1.33	41 to 83	
Lime	1.03	64	
" quick	1.5	95	
ground, thoroughly shaken, per struck			
bushel 93¾ pounds well shaken, per struck bushel		75	
80 pounds		64	
Limestone and marble	2.6	164.4	
broken	1.61	100	
solid,	2.70	168	
Linden wood	.60	38	
Loam	1.23	77	
Locust wood, dry (see note p. 433)	.71	44	
Logwood	.91	. 57.	
Lye		110	
	-		
Magnesite		100	
	1	190	

Magnesium	The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. J	Average Specific Gravity.	Average Weight of One Cubic Foot.
Mahogany wood, Spanish, dry (see note p. 433)       .85       .53         Manganese       8.00       500         Maple wood, dry (see note p. 433)       .79       49         Marble (see Limestone).       .79       49         Marl.       .140       .79       49         Marl ()       .140       .79       49         Marl ()       .140       .79       49         Masonry debris       .90       .90	Weight of One Cubic Foot, 62.355 Pounds.		Pounds.
Mahogany wood, Spanish, dry (see note p. 433)       .85       .53         Manganese       8.00       500         Maple wood, dry (see note p. 433)       .79       49         Marble (see Limestone).       .79       49         Marl.       .140       .79       49         Marl ()       .140       .79       49         Marl ()       .140       .79       49         Masonry debris       .90       .90			,
## Honduras, dry (see note. p. 433)56	Magnesium	1.74	109
## Honduras, dry (see note. p. 433)56	Mahogany wood, Spanish, dry (see note p. 433)		
Maple wood, dry (see note p. 433)	" Honduras, dry (see note. p. 433)		
Marble (see Limestone).         140           Marl.         90           Marl.         90           " of brickwork (see Brickwork).         90           " granite or limestone, well dressed.         165           " " well-scabbled mortar rubble, about ½ of mass will be mortar rubble.         154           " " roughly scabbled mortar rubble, about ½ to ½ of mass will be mortar rubble.         150           " " scabbled dry rubble.         125           " sandstone, ½ less than granite.         150           Mastic wood.         85         53           Mercury, at 32° F.         13.62         349           " at 68° F.         13.5         346           Mica, 2.75 to 3.1.         2.93         183           Milk.         1.03         64.5           Mortar, hardened, 1.4 to 1.9.         1.65         103           Muck (decayed vegetable matter, manure, etc.)         .92         57           Mud, dry, close.         80 to 110         10 to 130           " wet, moderately pressed         110 to 130           " fluid         104 to 120           Mulberry wood         .73         46           Nickel, cast.         8.99         541           " ilive, perfectly dry, .88-1.02 (see note p. 43			
Marl       140         Masonry debris       90         " of brickwork (see Brickwork).       90         " " granite or limestone, well dressed.       165         " " well-scabbled mortar rubble, about ½ of mass will be mortar rubble, about ½ to ¾ of mass will be mortar rubble.       154         " " a " a scabbled dry rubble.       150         " " sandstone, ½ less than granite.       150         Mastic wood.       .85       53         Mercury, at 32° F.       13.62       349         " a to 68° F.       13.5       346         Mica, 2.75 to 3.1       2.93       183         Milk       1.03       64.5         Molybdenum       8.50       532         Mortar, hardened, 1.4 to 1.9       1.65       103         Muck (decayed vegetable matter, manure, etc.)       .92       57         Mud, dry, close.       80       to 110         " wet, moderately pressed       110 to 130         " " fluid       104 to 120         Mulberry wood       .73       46         Nickel, cast       8.29       516         " " silver (52 cu. + 26 zn. + 22 ni.)       8.44         Satistiver (52 cu. + 26 zn. + 22 ni.)       8.45         Oak wood, heart of old		.79	49
Masonry debris			
" of brickwork (see Brickwork). " " granite or limestone, well dressed. " " well-scabbled mortar rubble, about ½ of mass will be mortar subble. " " roughly scabbled mortar rubble. about ½ to ½ of mass will be mortar scabbled dry rubble. " " roughly scabbled mortar rubble, about ½ to ½ of mass will be mortar scabbled dry rubble. " " scabbled dry rubble. " " scabbled dry rubble. " scabbled dry rubble. " sandstone, ½ less than granite.  Mastic wood.  Mercury, at 32° F. 13.62 349 " at 68° F. 13.5 346 Mica, 2.75 to 3.1 2.93 183 Milk. 1.03 64.5 Molybdenum 8.50 532 Mortar, hardened, 1.4 to 1.9. 1.65 103 Muck (decayed vegetable matter, manure, etc.) .92 57 Mud, dry, close. 80 to 110 " wet, moderately pressed 110 to 130 " " fluid 104 to 120 Mulberry wood73 46  Nickel, cast. 8.29 516 " " silver (52 cu. +26 zn. +22 ni.) 8.49 541 " " " live, perfectly dry, .88-1.02 (see note p. 433) .95 359.3 " " red, black, perfectly dry .32 to 45 " silver, perfectly dry, .88-1.02 (see note p. 433) .95 359.3 " " red, black, perfectly dry .32 to 45 " white .34  Oats0012a, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed,	Marl		
" granite or limestone, well dressed			90
## about ½ for mass will be mortar well-scabbled dry rubble, about ½ to ½ of mass will be mortar rubble, about ½ to ½ of mass will be mortar rubble, about ½ to ½ of mass will be mortar rubble, about ½ to ½ of mass will be mortar rubble, about ½ to ½ of mass will be mortar rubble, about ½ to ½ of mass will be mortar rubble, about ½ to ½ of mass will be mortar rubble, about ½ for mortar rubble, abo	" of brickwork (see Brickwork). " "granite or limestone well dressed		165
" " well-scabbled dry rubble	" well-scabbled mortar rubble,		
## or woughly scabbled mortar rubble, about ¼ to ¾ of mass will be mortar rubble.  ## a " scabbled dry rubble			
About   150   150   150   150   150   150   150   150   150   125   150   125   150   125   150   125   150   15	well-scappied dry ruppie		138
### ### ### ### #### #################	Toughty scappied mortal rupple,		
" " sandstone, ⅓ less than granite.  Mastic wood	mortar		
Mastic wood.     .85     53       Mercury, at 32° F.     13.62     349       " at 68° F.     13.5     346       Mica, 2.75 to 3.1     2.93     183       Milk     1.03     64.5       Molybdenum     8.50     532       Mortar, hardened, 1.4 to 1.9     1.65     103       Muck (decayed vegetable matter, manure, etc.)     .92     57       Mud, dry, close.     80 to 110     10 to 130       " wet, moderately pressed     110 to 130     104 to 120       Mulberry wood     .73     46       Nickel, cast     8.29     516       " rolled     8.69     541       " sliver (52 cu. + 26 zn. + 22 ni.)     8.44     52       Nitrogen     .00125     .0782       Oak wood, heart of old     1.17     73       " " live, perfectly dry, .88-1.02 (see note p. 433)     .95     59.3       " " et, black, perfectly dry     32 to 45       Oats     .0012a     .91       Oats     .002a, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed.     27			125
Mercury, at 32° F.       13.62       849         at 68° F.       13.5       346         Mica, 2.75 to 3.1.       2.93       183         Milk       1.03       64.5         Molybdenum       8.50       532         Mortar, hardened, 1.4 to 1.9.       1.65       103         Muck (decayed vegetable matter, manure, etc.)       .92       57         Mud, dry, close       80 to 110       110 to 130         " wet, moderately pressed       110 to 130       104 to 120         Mulberry wood       .73       46         Nickel, cast       8.29       516         " rolled       8.69       541         " silver (52 cu. + 26 zn. + 22 ni.)       8.44       527         Nitrogen       .00125       .0782         Oak wood, heart of old       1.17       73         " at live, perfectly dry, .88-1.02 (see note p. 433)       .95       59.3         " are, black, perfectly dry       32 to 45       52         Oats       .0012s, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed,       27			
## at 68° F.   13.5   846  Mica, 2.75 to 3.1   2.93   183  Milk   1.03   64.5  Molybdenum   8.50   532  Mortar, hardened, 1.4 to 1.9   1.65   103  Muck (decayed vegetable matter, manure, etc.)   92   57  Mud, dry, close   80 to 110  ## wet, moderately pressed   110 to 130  ## fluid   104 to 120  Mulberry wood   73   46  Nickel, cast   8.69   541  ## rolled   8.69   541  ## silver (52 cu. +26 zn. +22 ni.)   8.44   527  Nitrogen   .00125   .0782  Oak wood, heart of old   1.17   73   59.3  ## a red, black, perfectly dry   .88-1.02 (see note p. 433)   .95   59.3  ## a red, black, perfectly dry   .84   .52  Oats   .0012a, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed,   .77			
Mica, 2.75 to 3.1.       2.93       183         Milk       1.03       64.5         Molybdenum       8.50       532         Mortar, hardened, 1.4 to 1.9.       1.65       103         Muck (decayed vegetable matter, manure, etc.)       .92       57         Mud, dry, close       80 to 110       80 to 110         " wet, moderately pressed       110 to 130       104 to 120         Mulberry wood       .73       46         Nickel, cast       8.29       516         " rolled       8.69       541         " sliver (52 cu. + 26 zn. + 22 ni.)       8.44       527         Nitrogen       .00125       .0782         Oak wood, heart of old       1.17       73         " " live, perfectly dry, .88-1.02 (see note p. 433)       .95       59.3         " " erd, black, perfectly dry       32 to 45       52         Oats       cota, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed,       27	Mercury, at 32° F		
Milk       1.03       64.5         Molybdenum       8.50       532         Mortar, hardened, 1.4 to 1.9       1.65       103         Muck (decayed vegetable matter, manure, etc.)       .92       57         Mud, dry, close       80 to 110       80 to 110         " wet, moderately pressed       110 to 130       104 to 120         Mulberry wood       .73       46         Nickel, cast       8.29       516         " rolled       8.69       541         " silver (52 cu. + 26 zn. + 22 ni.)       8.44       527         Nitrogen       .00125       .0782         Oak wood, heart of old       1.17       73         " live, perfectly dry, .88-1.02 (see note p. 433)       .95       35.9.3         " a red, black, perfectly dry       32 to 45       52         Oats       27       27         Oil—bone, colza, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed,       27			
Molybdenum		1.03	64.5
Mortar, hardened, 1.4 to 1.9.         1.65         103           Muck (decayed vegetable matter, manure, etc.)         .92         57           Mud, dry, close.         .80 to 110         .80 to 110           " wet, moderately pressed         .110 to 130           " fluid         .104 to 120           Mulberry wood         .73         46           Nickel, cast.         8.29         516           " rolled         8.69         541           " silver (52 cu. + 26 zn. + 22 ni.)         8.44         527           Nitrogen         .00125         .0782           Oak wood, heart of old         1.17         73           " " live, perfectly dry, .88-1.02 (see note p. 433)         .95         59.3           " " erd, black, perfectly dry         32 to 45         52           Oats         .002a, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed,         27			. 532
Muck (decayed vegetable matter, manure, etc.)         .92         57           Mud, dry, close         .80 to 110         110 to 130           " wet, moderately pressed         .110 to 130           " fluid         .104 to 120           Mulberry wood         .73         46           Nickel, cast         8.29         516           " rolled         8.69         541           " silver (52 cu.+26 zn.+22 ni.)         8.44         527           Nitrogen         .00125         .0782           Oak wood, heart of old         1.17         73           " a live, perfectly dry, .88-1.02 (see note p. 433)         .95         35 9.3           " a red, black, perfectly dry         32 to 45         52           Oats         27         27           Oil—bone, colza, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed.         27			103
Mud, dry, close.       80 to 110         " wet, moderately pressed.       110 to 130         " fluid.       104 to 120         Mulberry wood.       .73         Nickel, cast.       8.29         " rolled.       8.69         " silver (52 cu. + 26 zn. + 22 ni.)       8.44         Nitrogen.       .00125         Oak wood, heart of old.       1.17         " live, perfectly dry, .88-1.02 (see note p. 433)       .95         " red, black, perfectly dry       32 to 45         " white       .84         Oats.       .95         Oil—bone, colza, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed,       27		.92	. 57
" wet, moderately pressed			80 to 110
Mulberry wood       .73       46         Nickel, cast       8.29       516         " rolled       8.69       541         " silver (52 cu.+26 zn.+22 ni.)       8.44       527         Nitrogen       .00125       .0782         Oak wood, heart of old       1.17       73         " live, perfectly dry, .88-1.02 (see note p. 433)       .95       35.9.3         " red, black, perfectly dry       32 to 45       52         Oats       27         Oil—bone, colza, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed,       27	" wet, moderately pressed		
Nickel, cast			
Nickel, cast       8.29       516         " rolled       8.69       541         " silver (52 cu. + 26 zn. + 22 ni.)       8.44       527         Nitrogen       .00125       .0782         Oak wood, heart of old       1.17       73         " live, perfectly dry, .88-1.02 (see note p. 433)       .95       359.3         " red, black, perfectly dry       32 to 45         Oats       .84       52         Oats       .95       .95         " white       .84       52         Oats       .95       .97         " mustard seed, neatsfoot, paraffin, rape seed,       27	Mulberry wood	.73	46
Nickel, cast       8.29       516         " rolled       8.69       541         " silver (52 cu. + 26 zn. + 22 ni.)       8.44       527         Nitrogen       .00125       .0782         Oak wood, heart of old       1.17       73         " live, perfectly dry, .88-1.02 (see note p. 433)       .95       359.3         " red, black, perfectly dry       32 to 45         Oats       .84       52         Oats       .95       .95         " white       .84       52         Oats       .95       .97         " mustard seed, neatsfoot, paraffin, rape seed,       27			
" silver (52 cu. + 26 zn. + 22 ni.)	Nickel, cast		
Oak wood, heart of old	" rolled		
Oak wood, heart of old       1.17       73         " live, perfectly dry, .88-1.02 (see note p. 433)       .95       32 to 45         " white       .84       52         Oats       .27         Oil—bone, colza, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed,       27		0.00	
" " red, black, perfectly dry	Nitrogen	.00125	.0782
" " red, black, perfectly dry			
" " red, black, perfectly dry	Oak wood, heart of old	1.17	73
0ats	" " live, perfectly dry, .88–1.02 (see note p. 433)		
Oats		84	
Oil—bone, colza, cylinder, engine, 500° fire test, mustard seed, neatsfoot, paraffin, rape seed,		101	
mustard seed, neatsfoot, paraffin, rape seed,			
tallow	mustard seed, neatsfoot, paraffin, rape seed,		
burning (Perosone) 150° and 300° 283   51.7	tallow	.90	
During (Acrosche), 100 and 000	burning (kerosene), 150° and 300°	.83	51.7

Oil, cotton seed         96         60.2         4 to 49         44 to 49         57.4         44 to 49         58.8         18.8         19.4         58.8         19.4         58.8         19.4         58.8         19.4         58.8         19.1         57.4         19.1         57.4         19.1         57.4         19.1         57.4         19.1         57.4         19.1         57.4         19.1         57.4         19.1         57.4         19.1         57.4         19.1         57.2         19.1         57.2         19.1         57.2         19.1         57.2         19.2	The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds.	Average Specific Gravity. Water=1.	Average Weight of One Cubic Foot. Pounds.
Paper, calendered       50-70         " strawboard newspaper       33-44         " writing or wrapping       70-90         Paraffine       .89       55.5         Pear wood       .66       41         Peat.       .50         Petroleum       .878       54.8         Phosphate rock       200         Pine wood, white       .40       25         " yellow, Northern       .55       34         " Southern       .72       45         Pitch       1.15       71.7         Plaster       .53       3         " of Paris (see Gypsum).       21.5       1342         Plum wood       .78       49         Poplar wood, dry (see note p. 433)       .47       29         " white Spanish       .53       33         Porcelain       2.40       149         Potassium       .87       54         Potatoes, in pile       .45         Proof spirit       .93       58         Pumice stone       .63       39         Quartz       2.65       165         Rags in bales       .15-36         Redwood       .48       30	# gasoline (motor) # lard # linseed # mineral lubricating. # Navy sperm # olive. # petroleum # signal # turpentine. # whale	.7175 .92 .94 .91 .87 .91 .88 .85 .87	44 to 49 57.4 58.8 57 54 57 55 53 54 58
" strawboard newspaper       33-44         " writing or wrapping.       70-90         Paraffine       .89       55.5         Pear wood       .66       41         Peat.       .50       50         Petroleum.       .878       54.8         Phosphate rock.       .200       200         Pine wood, white.       .40       25         " yellow, Northern       .55       34         " " Southern       .72       45         Pitch.       1.15       71.7         Plaster.       .53       3         " of Paris (see Gypsum).       1.15       71.7         Platinum.       21.5       1342         Plum wood.       .78       49         Poplar wood, dry (see note p. 433)       .47       29         " white Spanish.       .53       33         Porcelain.       2.40       149         Potassium.       .87       54         Potatoes, in pile.       .45       45         Proof spirit.       .93       58         Pumice stone.       .63       39         Quartz.       2.65       165         Rags in bales.       .63       30 <td>Oxygen</td> <td>.00143</td> <td>.0895</td>	Oxygen	.00143	.0895
Pear wood         .66         41           Peat         .50           Petroleum         .878         54.8           Phosphate rock         .200           Pine wood, white         .40         25           " yellow, Northern         .55         34           " Southern         .72         45           Pitch         1.15         71.7           Plaster         .53         53           " of Paris (see Gypsum).         21.5         1342           Plum wood.         .78         49           Poplar wood, dry (see note p. 433)         .47         29           " white Spanish         .53         33           Porcelain         2.40         149           Potassium         .87         54           Potatoes, in pile         .45         45           Proof spirit         .93         58           Pumice stone         .63         39           Quartz         2.65         165           Rags in bales         .15–36           Redwood         .48         30           Rope         .42	" strawboard newspaper		33-44 70-90
Peat.         50           Petroleum         .878         54.8           Phosphate rock         200           Pine wood, white.         .40         25           " yellow, Northern         .55         34           " Southern         .72         45           Pitch         1.15         71.7           Plateser.         .53         3           " of Paris (see Gypsum).         21.5         1342           Plum wood.         .78         49           Poplar wood, dry (see note p. 433)         .47         29           " white Spanisin         .53         33           Porcelain         2.40         149           Potassium         .87         54           Potatoes, in pile         .45         45           Proof spirit         .93         58           Pumice stone         .63         39           Quartz         2.65         165           Rags in bales         .15-36           Redwood         .48         30           Rope         .42		100	
Petroleum.         .878         54.8           Phosphate rock.         200           Pine wood, white.         .40         25           " yellow, Northern         .55         34           " Southern         .72         45           Pitch.         1.15         71.7           Plaster.         .53         53           " of Paris (see Gypsum).         21.5         1342           Plum wood.         .78         49           Poplar wood, dry (see note p. 433)         .47         29           " white Spanish         .53         33           Porcelain         2.40         149           Potassium.         .87         54           Potatoes, in pile.         .45         58           Proof spirit.         .93         58           Pumice stone.         .63         39           Quartz.         2.65         165           Rags in bales         15–36           Redwood         .48         30           Rope.         .42			
Phosphate rock         200           Pine wood, white.         40         25           " a yellow, Northern         .55         34           " a Southern         .72         45           Pitch         1.15         71.7           Plaster         .53         1342           " of Paris (see Gypsum).         21.5         1342           Plum wood         .78         49           Poplar wood, dry (see note p. 433)         .47         29           " white Spanish         .53         33           Porcelain         2.40         149           Potassium         .87         54           Potatoes, in pile         .45         45           Proof spirit         .93         58           Pumice stone         .63         39           Quartz         2.65         165           Rags in bales         .15-36           Redwood         .48         30           Rope         .42		.878	
" yellow, Northern			200
" Southern   .72   45     Pitch	Pine wood, white	.40	
Pitch.     1.15     71.7       Plaster.     53       " of Paris (see Gypsum).     21.5     1342       Plum wood.     .78     49       Poplar wood, dry (see note p. 433)     .47     29       " white Spanish.     .53     33       Porcelain.     2.40     149       Potassium.     .87     54       Potatoes, in pile.     45     58       Pumice stone.     .63     39       Quartz.     2.65     165       Rags in bales.     15-36       Redwood.     .48     30       Rope.     .42	yellow, Northern		
Plaster     53       " of Paris (see Gypsum).     21.5       Platinum.     21.5       Plum wood.     .78       49     49       Poplar wood, dry (see note p. 433)     .47       29     .53       33     .53       Porcelain.     2.40       149     .87       Potassium.     .87       54     .45       Proof spirit.     .93       58     .63       29     .63       39     .63       Quartz.     2.65       Rags in bales.     .15-36       Redwood.     .48       30       Rope     .42	Southern		
" of Paris (see Gypsum).  Platinum			
Plum wood.     .78     49       Poplar wood, dry (see note p. 433)     .47     29       " white Spanish     .53     33       Porcelain     2.40     149       Potassium     .87     54       Potatoes, in pile     45       Proof spirit     .93     58       Pumice stone     .63     39       Quartz     2.65     165       Rags in bales     15-36       Redwood     .48     30       Rope     .42	" of Paris (see Gypsum).		93
Poplar wood, dry (see note p. 433)	Platinum	21.5	1342
" white Spanish		.78	49
Porcelain.         2.40         149           Potassium.         .87         54           Potatoes, in pile.         .45           Proof spirit.         .93         58           Pumice stone.         .63         39           Quartz.         2.65         165           Rags in bales.         .15-36         Redwood.         .48         30           Rope.         .42         .42         .43         .43	Poplar wood, dry (see note p. 433)	.47	29
Potassium.         .87         54           Potatoes, in pile.         .45         .45           Proof spirit.         .93         58           Pumice stone.         .63         39           Quartz.         2.65         165           Rags in bales.         .15-36         .30           Redwood.         .48         30           Rope.         .42	white Spanish		
Potatoes, in pile.       45         Proof spirit.       .93       58         Pumice stone.       .63       39         Quartz.       2.65       165         Rags in bales.       15–36       15–36         Redwood       .48       30         Rope.       .42			
Proof spirit.       .93       58         Pumice stone.       .63       39         Quartz.       2.65       165         Rags in bales.       .15–36       Redwood.       .48       30         Rope.       .42       .42       .43       .43       .43		.87	42
Pumice stone.       .63       39         Quartz.       2.65       165         Rags in bales.       .15–36       Redwood.       .48       30         Rope.       .42       .42       .43       .43       .43		00	
Quartz.       2.65       165         Rags in bales.       15–36       165         Redwood.       .48       30         Rope.       .42			
Rags in bales. 15–36 Redwood .48 30 Rope42		.03	00
Redwood	Quartz	2.65	165
Rope			15-36
2		.48	30
Rosin			42
	Rosin	1.10	68.6

The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches.	Average Specific Gravity.	Average Weight of One Cubic Foot.
Weight of One Cubic Foot, 62.355 Pounds.	Water=1.	Pounds.
Rubber		60 95 50
	2.41	45 68 90 to 106 118 to 129 117 144 151
Sassafras wood	.48	30
Shales, red or black, 2.4 to 2.8	2.6	162 8-32
Silver	10.5	655
Slag		160 to 180
" furnace, granulated	2.8	53 175
Snow, fresh-fallen moistened, compacted by rain	2.0	5 to 12 15 to 50
Soapstone, 2.65 to 2.8	2.73	170
Soda ash		62
Sodium	.97	61
Spelter, 6.8 to 7.2	7.00	437.5
Spermaceti	.94	59
Spruce wood.	.50	31.2 28.7
Starch		95
Starch (in barrels)		23
Steam at 212° F	.0006	.0368
Steel	7.85	489.6
Straw, baled		24
Sugar, stored.	1.60	100 42
Sulphur	2.00	125
Sumac wood		39
Sycamore wood, perfectly dry (see note p. 433)	.59	37
Tale		170
Tallow	.94	58.6
Tar	1.15	71.7

The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds.	Average Specific Gravity. Water=1.	Average Weight of One Cubic Foot. Pounds.
Teak wood	.82	51
Tile (see page 69).	.02	0.2
Tin. cast. 7.2 to 7.5	7.35	459
" pure	7.29	455
Tobacco		28
Trap rock, compact	3.02	188
" " in pile		190
Tungsten	19.1	1192
Turf	.40	25
Vanadium	5.5	343
Vapor, alcohol	.00198	.122
" turpentine spirits	.00615	.378
" water	1.33	83
Vinegar.	1.08	67.4
Vinegal	1.00	07.2
Walnut wood, black, perfectly dry (see note below)	.61	38
Water, pure rain, distilled, at 32° F., Bar. 30 inches.		62.417
" " " " 62° F " 30 "	1	62.355
" " " " 212° F., " 30 " sea, 1.026 to 1.030	1.028	59.7 64.08
Wax, bees-	.97	61
Wheat	.91	39-44
White metal (Babbitts)	7.32	456
Willow wood	.54	34
Wine	.99	62
Wool, in bales	.00	15-22
/		13-22
		10 88
Yew wood	.79	49
Zinc, cast	6.86	428
" pure	7.15	446
" rolled	7.19	449

NOTE.—Green timbers usually weigh from one-fifth to nearly one-half more than dry; ordinary building timbers, tolerably seasoned, one-sixth more.

For specific gravities of woods not given in this table, see page 408.

#### STANDARD DECIMAL GAUGE.

Standard Decimal Gauge	Thickness in Fractions	Approximate Thickness	1	Square Foot Avoirdupois.
In Inches.	of an Inch.	in Millimetres.	IRON.  Basis—480  Pounds  per Cubic Foot.	STEEL. Basis—489.6 Founds per Cubic Foot.
.002	1-500	.05080010	.08	.0816
.004	1-250	.10160020	.16	.1632
.006	3-500	.15240030	.24	.2448
.008	1-125	.20320041	.32	.3264
.010	1-100	.25400051	.40	.4080
.012 .014 .016 .018	3-250 7-500 2-125(1+) 9-500 1-50	.80480061 .85560071 .40640081 .45720091 .50800102	.48 .56 .64 .72 .80	.4896 .5712 .6528 .7344 .8160
.022 .025 .028 .032 .036	11-500 1-40 7-250 4-125(1+) 9-250	.55880112 .68500127 .71120142 .81280163 .91440188	.88 1.00 1.12 1.28 1.44	1.0200 1.1424 1.3056 1.4688
.040	1-25	1.01600203	1.60	1.6820
.045	9-200	1.14300229	1.80	1.8360
.050	1-20	1.27000254	2.00	2.0400
.055	11-200	1.39700280	2.20	2.2440
.060	3-50 (1-)	1.52400305	2.40	2.4480
.065	13-200	1.65100330	2.60	2.6520
.070	7-100	1.77800356	2.80	2.8560
.075	3-40	1.90500381	3.00	3.0600
.080	2-25	2.03200406	3.20	3.2640
.085	17-200	2.15900432	3.40	3.4680
.090	9-100	2.25600457	3.60	3.6720
.095	19-200	2.41300483	3.80	3.8760
.100	1-10	2.54000508	4.00	4.0800
.110	11-100	2.79400559	4.40	4.4880
.125	1-8	3.17500630	5.00	5.1000
.135	27-200	8.42900686	5.40	5.5080
.150	3-20	8.81000762	6.00	6.1200
.165	33-200	4.19100838	6.60	6.7320
.180	9-50	4.57200914	7.20	7.8440
.200	1-5	5.08001016	8.00	8.1600
.220	11-50	5.58801118	8.80	8.9760
.240	6-25	6.09601219	9.60	9.7920
.250	1-4	6.85001270	10.00	10.2000

#### WIRE AND SHEET METAL GAUGES.

In Decimals of an Inch.

Number of Gauge.	Birmingham or Stubs Iron Wire Gauge (B. W. G.)	American or Brown & Sharpe Wire Gauge.	United States Standard Cauge, for Sheet and Plate Iron and Steel.	Washburn & Moen Manufacturing Co. and John A. Roebling's Sons Co. Wire Gauge.	Trenton Iron Co. Wire Gauge.	American Screw Co. Screw Wire Gauge.	British Imperial or English Legal Standard Wire Gauge.	New Birmingham Standard Sheet and Hoop Gauge (B. G.)
7/0 6/0 5/0 4/0 3/0 00	.454 .425 .380 .340	.460000 .409642 .364796	.5 .46875 .4375 .40625 .375 .34375 .3125	.4600 .4300 .3938 .3625 .3310	.450 .400 .360 .330	.0315 .0447	.464 .432 .400 .372 .348	.6656 .625 .5883 .5416 .500 .4452
12345	.300 .264 .259 .238 .220 .203 .180	289297 .257627 .29423 .204307 .181940 .162023 .144285	28125 265625 25 234375 21875 203125 .1875	2830 2625 .2437 2263 .2070 .1920 .1770	285 265 245 225 205 .190 .175	.0710 10842 .0973 .1105 .1236 .1368 .1500	.300 .276 .252 .232 .212 .192 .176	.3532 .3147 .2804 .250 .2225 .1981 .1764
1 84 5 67 89 10 11 12 13 14 15	.165 .148 .134 .120 .109 .095 .023 .072	.128490 .114423 .101897 .090742 .080808 .071962 .064084	.171875 .15625 .140625 .125 .109375 .09375 .078125	.1620 .1483 .1350 .1205 .1055 .0915 .0800 .0720	.160 .145 .130 .1175 .105 .0925 .0806	.1631 .1763 .1894 .2026 .2158 .2289 .2421 .2552	.160 .144 .128 .116 .104 .092 .080 .072	.1570 .1398 .1250 .1113 .0991 .0882 .0785
16 17 18 19 20	.065 .053 .049 .042 .035 .032	.050821 .045257 .040303 .035890 .031961 .028462 .025346	0625 05625 .05 .04375 .0375 .034375	.0625 .0540 .0475 .0410 .0348 .03175	.061  0525  045  040  035  031  028	2684 2616 .2947 .3079 .3210 .3342 .3474	.064 .056 .048 .040 .036 .032	.0625 .0556 .0495 .0440 .0392 .0349
21 22 23 24 25 26 27 28 29 20	.025 .022 .020 .018 .016 .014 .013	.022572 .020101 .017900 .015941 .014195 .012641 .011257	.028125 .025 .021875 .01875 .0171875 .015625 .0140625	.0258 .0230 .0204 .0181 .0173 .0162 .0150 .0140	.025 .0225 .020 .018 .017 .016 .015	.3605 .3737 .3868 .4000 .4132 .4263 .4396 .4526	.024 1022 .020 .018 .0164 .0148 .0136	.02782 .02476 .02204 .01961 .01745 .015625 .0139 .0123
31 32 33 34 35	.012 .010 .009 .008 .007 .005	.008928 .007950 .007080 .006305 .005615	.0109375 .01015625 .009375 .00859375 .0076125	.0132 .0128 .0118 .0104 .0095	.013 .012 .011 .010 .0095	.4658 .4790 .4921 .5053 .5184	.0124 .0116 .0108 .0100 .0092 .0084 .0076	.0123 .0110 .0098 .0087 .0077 .0069 .0061
86 87 88 89 40		.004453 .003965 .003531 .003144	.006640625 .00625	.0085 .0080 .0075	.0085 .008 .0075	.5448 .5579 .5711 .5842	.0060	.0048 .0043 .00386

## WEIGHTS OF SHEETS AND PLATES OF STEEL, WROUGHT IRON, COPPER AND BRASS.

American or Browne & Sharpe Gauge.

Number	Thickness		Weight per	Square Foot.	
of Gauge.	in Inches.	Steel.	Iron.	Copper.	Brass.
0000	.460000	18.7680	18.4000	20.8380	19.6880
	.409642	16.7134	16.3857	18.5568	17.5827
	.864796	14.8837	14.5918	16.5253	15.6188
01234	.324861	13.2543	12.9944	14.7162	13.9041
	.289297	11.8033	11.5719	13.1052	12.3819
	.257627	10.5112	10.3051	11.6705	11.0264
	.229423	9.3605	9.1769	10.3929	9.8193
	.204307	8.3357	8.1723	9.2551	8.7448
5	.181940	7.4232	7.2776	8.2419	7.7870
6	.162023	6.6105	6.4809	7.3396	6.9346
7	.144285	5.8868	5.7714	6.5361	6.1754
8	.128490	5.2424	5.1396	5.8206	5.4994
9	.114423	4.6685	4.5769	5.1834	4.8973
10	.101897	4.1574	4.0759	4.6159	4.3612
11	.090742	3.7023	8.6297	4.1106	8.8838
12	.080808	3.2970	8.2323	3.6606	8.4586
13	.071962	2.9360	2.8785	3.2599	8.0800
14	.064084	2.6146	2.5634	2.9030	2.7428
15	.057068	2.3284	2.2827	2.5852	2.4425
16	.050821	2.0735	2.0328	2.3022	2.1751
17	.045257	1.8465	1.8103	2.0501	1.9370
18	.040303	1.6444	1.6121	1.8257	1.7250
19	.035890	1.4643	1.4356	1.6258	1.5361
20 21 22 28 28 24	.031961 .028462 .025346 .022572 .020101	1.3040 1.1612 1.0341 .92094 .82012	1.2784 1.1385 1.0138 90288 .80404	1.4478 1.2893 1.1482 1.0225 .91058	1.3679 1.2182 1.0848 .96608 .86032
25	.017900	.78032	.71600	.81087	.76612
26	.015941	.65039	.63764	.72213	.68227
27	.014195	.57916	.56780	.64303	.60755
28	.012641	.51575	.50564	.57264	.54108
29	.011257	.45929	.45028	.50994	.48180
80	.010025	40902	.40100	.45413	.42907
81	.008928	186426	.85712	.40444	.88212
82	.007950	.32436	.81800	.86014	.34026
88	.007080	.28886	.28320	.32072	.30302
84	.006305	.26724	.25220	.28562	.26985
35	.005615	.22909	.22460	.25486	.24032
36	.005000	.20400	.20000	.22650	.21400
37	.004453	.18168	.17812	.20172	.19059
88	.003965	.16177	.15860	.17961	.16970
89	.003531	.14406	.14124	.15995	.15113
40	.003144	.12828	.12576	.14242	.13456

For weights of steel plates  $\gamma_8$ " and over in thickness, see "Table of Weights of Flat Rolled Bars," pages 475 to 486 inclusive.

## WEIGHTS OF SHEETS AND PLATES OF STEEL, WROUGHT IRON, COPPER AND BRASS.

Birmingham Wire Gauge (B. W. G.)

Number	Thickness		Weight per	Square Foot.	
Gange.	in Inches.	Steel.	Iron.	Copper.	Brass.
0000	.454	18.5232	18.16	20.5662	19.4312
000	.425	17.3400	17.00	19.2525	18.1900
00	.380	15.5040	15.20	17.2140	16.2640
0	.340	13.8720	13.60	15.4020	14.5520
1	.300	12.2400	12.00	13.5900	12.8400
2	.284	11.5872	11.36	12.8652	12.1552
3	.259	10.5672	10.36	11.7327	11.0852
4	.238	9.7104	9.52	10.7814	10.1864
5	.220	8.9760	8.80	9.966	9.4160
6	.208	8.2824	8.12	9.1959	8.6884
7	.180	7.3440	7.20	8.1540	7.7040
8	.165	6.7320	6.60	7.4745	7.0620
9	.148	6.0384	5.92	6.7044	6.8344
10	.184	5.4672	5.86	6.0702	5.7852
11	.120	4.8960	4.80	5.4360	5.1860
12	.109	4.4472	4.36	4.9377	4.6652
13	.095	3.8760	3.80	4.3035	4.0660
14	.088	3.3864	8.82	8.7599	8.5524
15	.072	2.9376	2.88	3.2616	8.0816
16	.065	2.6520	2.60	2.9445	2.7820
17	.058	2.8664	2.32	2.6274	2.4824
18	.049	1.9992	1.96	2.2197	2.0972
19	.042	1.7136	1.68	1.9026	1.7976
20 21 22 23 24	.085 .082 .028 .025	1.4280 1.3056 1.1424 1.0200 .8976	1.40 1.28 1.12 1.00	1.5855 1.4496 1.2684 1.1325 .9966	1.4980 1.8696 1.1984 1.0700 -9416
25 26 27 28 29	.020 .018 .016 .014 .013	.8160 .7344 .6528 .5712 .5304	.80 .72 .64 .56	.9060 .8154 .7248 .6342 .5889	.8560 .7704 .6848 .5992 .5564
80	.012	.4896	.48	.5436	.5186
81	.010	.4080	.40	.4530	.4280
82	.009	.8672	.36	.4077	.8852
83	.008	.8264	.82	.3624	.8424
84	.007	.2856	.28	.3171	.2996
85	.005	.2040	.20	.2265	.2140
86	.004	.1632	.16	.1812	.1712
Specific Grawinght of	avities	7.85 489.6 .2888	7.70 480.0 .2778	8.72 548.6 3146	5.24 513.6 .2972

## COMBINED TABLE OF SIZES IN THE PRINCIPAL WIRE GAUGES.

Values printed in bold-faced type are exact; values not exact are rounded off to four significant figures, except diameters of the American (B. & S.) Wire Gauge and of the Metric Wire Gauge in the column headed "Diameter, inches," are given to 0.001 inch for the larger sizes and to 0.0001 inch for the smaller. This represents the usual degree of accuracy in the measurement of wires.

1	Diamete	r	V	Vire G	auge N	lumber	rs		Cross S	ection	
Mils	Mm.	Ins.	American (B. & S.)	Washburn & Moen	Birmingham (Stubs')	British	Metric	Sq. Ins.	Sq. Mils	Circular Mils	Sq. Mm.
500 490 464	12.70 12.45 11.79	1500 1490 .464		7-0				.1963 .1886 .1691	188 600	<b>250 000</b> <b>240 100</b> 215 300	126.7 121.7 109.1
461.5 460 454	11.70 11.68 11.53	.4615 .460 .454	4-0					.1673 .1662 .1619	166 200	213 000 211 600 206 100	107.9 107.2 104.4
432 430.5 425	10.97 10.93 10.80	.432 .4305 .425		5-0	3-0	5-0		.1466 .1456 .1419	145 600	186 600 185 300 180 600	94.56 93.91 91.52
409.6 400 393.8	10.40 10.16 10.00	.410 [400 [3938		4-0		4-0		.1318 .1257 .1218	125 700	167 800 160 000 155 100	85.03 81.07 78.58
393.7 380 372	10.0 9.652 9.449	.3937 .380 .372			2-0	3-0	100	.1217 .1134 .1087	113 400	155 000 144 400 138 400	78.54 73.17 70.12
364.8 362.5 354.3	9.266 9.208 9.0	.365 13625 .354	2-0	3-0				.1045 .1032 .098 61	103 200	133 100 131 400 125 500	67.43 66.58 63.62
348 340 331	8.839 8.636 8.407	.348 .340 .331		2-0	0			.095 11 .090 79 .086 05	90 790	121 100 115 600 109 600	61.36 58.58 55.52
324.9 324 315	8.251 8.230 <b>8.0</b>	.325 1324 .315	0			0		.082 89 .082 45 .077 91		105 500 105 000 99 200	53.48 53.19 50.27
306.5 300 289.3	7.785 7.620 7.348	.3065 .300 .289	1	0	1	X		.073 78 .070 69 .065 73	73 780 70 690 65 730	93 940 90 000 83 690	47.60 45.60 42.41
	1	П									

I	iameter		N	7ire G	auge N	lumber	8		Cross S	ection	
Mils	Mm.	Ins.	American (B. & S.)	Washburn & Moen	Birmingham (Stubs')	British Standard	Metric	Sq. Ins.	Sq. Mils	Circular Mils	Sq. Mm.
284 283 276	7.214 7.188 7.010	.284 .283 .276		1		2		.063 35 .062 90 .059 83	63 350 62 900 59 830	80 660 80 090 76 180	40.87 40.58 38.60
275.6 262.5 259	7.0 6.668 6.579	.276 .2625 .259		2	3		70	.059 65 .054 12 .052 69	59 650 54 120 52 690	75 950 68 910 67 080	38.48 34.92 33.99
257.6 252 243.7	6.544 6.401 6.190	.258 .252 .2437	2	3		3		.052 13 .049 88 .046 64	52 130 49 880 46 640	66 370 63 500 59 390	33.63 32.18 30.09
238 .236.2 232	6.045 6.0 5.893	.238 .236 .232			4	A	60	.044 49 .043 83 .042 27	44 490 43 830 42 270	56 640 55 800 53 820	28.70 28.27 27.27
229.4 225.3 220	5.827 5.723 5.588	.229 .2253 .220	3	4	5			.041 34 .039 87 .038 01	41 340 39 870 38 010	52 630 50 760 48 400	26.67 25.72 24.52
212 207 204.3	5.385 5.258 5.189	.212 .207 .204	4	5		5		.035 30 .033 65 .032 78	35 300 33 650 32 780	44 940 42 850 41 740	22.77 21.71 21.15
203 196.8 192	5.156 5.0 4.877	.203 .197 .192	1		6	6	50	.032 37 .030 43 .028 95	32 370 30 430 28 950	41 210 38 750 36 860	20.88 19.63 18.68
181.9 180 177.2	4.621 4.572 <b>4.5</b>	.182 .180 .177	5		7		45	.026 00 .025 45 .024 65	26 000 25 450 24 650	32 400	16.77 16.42 15.90
177 176 165	4.496 4.470 4.191	.177 .176 .165		7	8	7		.024 61 .024 33 .021 38	24 610 24 330 21 380	30 980	15.70
162 160 157.5	4.115 4.064 <b>4.0</b>	.162 .160 .157	6	8		8	40	.020 62 .020 11 .019 48	20 620 20 110 19 480	25 600	12.97
148,3 148 144.3	3.767 3.759 3.665	.1483 .148 .144	7	9	9			.017 27 .017 20 .016 35	17 270 17 200 16 350	21 900	11.10
144 137.8 135	3.658 3.5 3.429	.144 .138 .135		. 10		. 9	35	.016 29 .014 91 .014 31	16 290 14 910 14 310	18 990	9.621
134 128.5 128	3.404 3.264 3.251	.128	8	·]	. 10	10		.014 10 .012 97 .012 87	14 10 12 97 12 87	16 510	8.366

I	Diameter		W	Vire G	auge N	umber	8		Cross S	Section	
Mils	Mm.	Ins.	American (B. & S.)	Washburn & Moen	Birmingham (Stubs')	British Standard	Metric	Sq. Ins.	Sq. Mils	Circular Mils	Sq. Mm.
120.5 120 118.1	3.061 3.048 3.0	.1205 .120 .118			11			.011 40 .011 31 .010 96	11 400 11 310 10 960	14 520 14 400 13 950	7.358 7.297 7.069
116 114.4 109	2.946 2.906 2.769	.116 .114 .109	9		12	11		.010 57 .010 28 .009 331	10 570 10 280 9331	13 460 13 090 11 880	6.818 6.634 6.020
105.5 104 101.9	2.680 2.642 2.588	.1055 .104 .102	10	12		12		.008 742 .008 495 .008 155	8742 8495 8155	11 130 10 820 10 380	5.640 5.481 5.261
98.42 95 92	2.5 2.413 2.337	.098 .095 .092			13	13	25	.007 609 .007 088 .006 648	7609 7088 6648	9687 9025 8464	4.909 4.573 4.289
91.5 90.74 <b>53</b>	2.324 2.305 2.108	.0915 .091 .083	11	19				.006 576 .006 467 .005 411	6576 6467 5411	8372 8234 <b>6889</b>	4.242 4.172 3.491
80.81 80 78.74	2.053 2.032 <b>2.0</b>	.081 .080 .079	12	14		14		.005 129 .005 027 .004 869	5129 5027 4869	6530 6400 6200	3.309 3.243 3.142
72 71.96 70.87	1.829 1.828 1.8	.072 .072 .071	13		15	15	18	.004 072 .004 067 .003 944	4072 4067 3944	5184 5178 5022	2.627 2.624 2.545
65 64.08 64	1.651 1.628 1.626	.065 .064 .064	14		16			.003 318 .003 225 .003 217	3318 3225 3217	4225 4107 4096	2.141 2.081 2.075
62.99 62.5 58	1.6 1.588 1.473	.063 .0625 .058		16	17		16	.003 116 .003 068 .002 642	3068	3968 3906 3364	2.011 1.979 1.705
57.07 56 55.12	1.450 1.422 1.4	.057 .056 .055				17		.002 558 .002 463 .002 386	2463	3257 3136 3038	1.650 1.589 1.539
54 50.82 49	1.372 1.291 1.245	.054 .051 .049	16	17	18			.002 290 .002 028 .001 886	2028	2916 2583 2401	1.478 1.309 1.217
48 47.5 47.24	1.219 1.207 1.2	.048 .0475 .047		18		18		.901 810 .001 772 .001 753	1772	2304 2256 2232	1.167 1.143 1.131
45.26 42 41	1.150 1.067 1.041	.045 .042 .041	17	19	19			.001 609 .001 385 .001 320		2048 1764 1681	1.038 0.8938 0.8518

I	Diamete	r	v	Vire G	auge N	lumber	18	L. 11	Cross S	Section	
Mils	Mm.	Ins.	American (B. & S.)	Washburn & Moen	Birmingham (Stubs')	British Standard	Metric	Sq. Ins.	Sq. Mils	Circular Mils	Sq. Mm.
40.3 40 39.37	1.024 1.016 1.0	.040 .040 .039	18			19	10	.001 276 .001 257 .001 217	1276 1257 1217	1624 1600 1550	.8231 .8107 .7854
36 35.89 35.43	.9144 .9116	.036 .036 .035	19				9	.001 018 .001 012 .0 <sub>3</sub> 9861	1018 1012 986.1	1296 1288 1255	.6567 .6527 .6362
35 34.8 32	.8890 .8839 .8128	.035 .0349 .032		20	20			.0 <sub>3</sub> 9621 .0 <sub>3</sub> 9511 .0 <sub>3</sub> 8042	962.1 951.1 804.2	1225 1211 1024	.6207 .6136 .5189
31.96 31.7 31.5	.8118 .8052 LBO	.032 .0317 .031	20	21			8	.0 <sub>3</sub> 8023 .0 <sub>3</sub> 7892 .0 <sub>3</sub> 7791	802.3 789.2 779.1	1022 1005 992	.5176 .5092 .5027
28.6 28.46 28	.7264 .7229 .7112	.0286 .0285 .028	21		22			.0 <sub>3</sub> 6424 .0 <sub>3</sub> 6363 .0 <sub>3</sub> 6158	642.4 636.3 615.8	818 810.1 <b>784</b>	.4145 .4105 .3973
27.56 25.8 25.35	.70 .6553 .6438	.0276 .0258 .0253		23			7	0 <sub>3</sub> 5965 .0 <sub>3</sub> 5228 .0 <sub>3</sub> 5046	596.5 522.8 504.6	759.5 665.6 642.4	.3848 .3373 .3255
25 24 23.62	.6350 .6096	.025 .024 .0236			23	23		.0 <sub>3</sub> 4909 .0 <sub>3</sub> 4524 .0 <sub>3</sub> 4383	490.9 452.4 438.3	625 576 558	.3167 .2919 .2827
23 22.57 22	.5842 .5733 .5588	.023 .0226	23		24			.0 <sub>3</sub> 4155 .0 <sub>3</sub> 4001 .0 <sub>3</sub> 3801	415.5 400.1 380.1	529 509.5 484	.2675 .2582 .2452
20.1 20.1 20	.5182 .5106 .5080	.0204 .0201	24	25	25			.0 <sub>3</sub> 3269 .0 <sub>3</sub> 3173 .0 <sub>2</sub> 3142	326.9 317.3 314.2	416.2 404 400	.2109 .2047 .2027
19.68 18.1 18	.4597 .4572	.0197 .0181 .018			26		5	.0 <sub>3</sub> 3043 .0 <sub>3</sub> 2573 .0 <sub>3</sub> 2545	304.3 257.3 254.5	387.5 327.6 <b>324</b>	.1963 .1660 .1642
17.9 17.72 17.3	.4547 .45 .4394	.0179 .0177 .0173	25				4-5	.0 <sub>3</sub> 2517 .0 <sub>3</sub> 2465 .0 <sub>3</sub> 2351	251.7 246.5 235.1	320.4 313.9 299.3	.1624 .1590 .1517
16.4 16.2 16	.4166 .4115 .4064	.0164 .0162 .016			27			.0 <sub>3</sub> 2112 .0 <sub>3</sub> 2061 .0 <sub>3</sub> 2011	211.2 206.1 201.1	269 262.4 <b>256</b>	.1363 .1330 .1297
15.94 15.75 <b>15</b>	4049 40 3810	.0159 .0157 .015	26				28	.0 <sub>3</sub> 1996 .0 <sub>3</sub> 1948 .0 <sub>3</sub> 1767	199.6 194.8 176.7	254.1 248 225	.1288 .1257 .1140

I	Diamete		M	Tire Ga	auge N	umber	g		Cross S	Section	
Mils	Mm.	Ins.	American (B. & S.)	Washburn & Moen	Birmingham (Stubs')	British Standard	Metric	Sq. Ins.	Sq. Mils	Circular Mils	Sq. Mm.
14.8 14.2 14	.3759 .3606 .3556	.0148 .0142 .0140	27	30	28	28		.0 <sub>3</sub> 1720 .0 <sub>3</sub> 1583 .0 <sub>3</sub> 1539	172.0 158.3 153.9	219 201.5 196	.1110 .1021 .099 32
13.78 13.6 13.2	.35 .3454 .3353	.0138 .0136 .0132				29		.0 <sub>3</sub> 1491 .0 <sub>3</sub> 1453 .0 <sub>3</sub> 1368	149.1 145.3 136.8	189.9 185 174.2	.096 21 .093 72 .088 29
13 12.8 12.64	.3302 .3251 .3211	.0130 .0128 .0126	28	32	29			.0 <sub>3</sub> 1327 .0 <sub>3</sub> 1287 .0 <sub>3</sub> 1255	132.7 128.7 125.5	163.8 159.8	.085 63 .083 02 .080 98
12.4 12 11.81	.3150 .3048	.0124 .0120 .0118			30	30	3	.0 <sub>3</sub> 1208 .0 <sub>3</sub> 1131 .0 <sub>3</sub> 1096	120.8 113.1 109.6	153.8 144 139.5	.077 91 .072 97 .070 69
11.8 11.6 11.26	.2997 .2946 .2859	.0118 .0116 .0113						.0 <sub>3</sub> 1094 .0 <sub>3</sub> 1057 .0 <sub>4</sub> 9954	109.4 105.7 99.54	139.2 134.6 126.7	.070 55 .068 18 .064 22
10.8 10.4 10.03	.2743 .2642 .2546	.0108 .0104 .0100		34		32		.0 <sub>4</sub> 9161 .0 <sub>4</sub> 8495 0 <sub>4</sub> 7894	91.61 84.95 78.94	116.6 108.2 100.5	.059 10 .054 81 .050 93
9.842 9.5	.2540 .25 .2413	.0100 .0098 .0095		35		33	2-5	.0 <sub>4</sub> 7854 .0 <sub>4</sub> 7609 .0 <sub>4</sub> 7088	78.54 76.09 70.88	96.87 90.25	.050 67 .049 09 .045 73
9.2 9 8.928	.2337 .2286 .2268	.0092 .0090 .0089	31	36	32	34		.046648 .046362 .046260	66.48 63.62 62.60	84.64 81 79.7	.042 89 .041 04 .040 39
8.5 8.4 8	.2159 .2134 .2032	10085 10084 10080		37	33	35		.0 <sub>4</sub> 5675 .0 <sub>4</sub> 5542 .0 <sub>4</sub> 5027	56.75 55.42 50.27	72.25 70.56 64	.036 61 .035 75 .032 43
7.95 7.874 <b>7.6</b>	.2019 .20 .1930	.0080 .0079				36	2	.0 <sub>4</sub> 4964 .0 <sub>4</sub> 4869 .0 <sub>4</sub> 4536	49.64 48.69 45.36	63.21 62.00 <b>57.76</b>	.032 03 .031 42 .029 27
7.5 7.087 7.08	.1905 .18 .1798	.0075 .0071 .0071	33	39			1.8	.0 <sub>4</sub> 4418 .0 <sub>4</sub> 3944 .0 <sub>4</sub> 3937	44.18 39.44 39.37	<b>56.25</b> 50.22 50.13	.028 50 .025 45 .025 40
7 6.8 6.6	.1778 .1727 .1676	.0070 .0068 .0066				37		.0 <sub>4</sub> 3848 .0 <sub>4</sub> 3632 .0 <sub>4</sub> 3421	38.48 36.32 34.21	49 46.24 43.56	.024 83 .023 43 .022 07
6.305 6.299 <b>6.2</b>	.1601 .16 .1575	.0063 .0063	34	42			1-6	.0 <sub>4</sub> 3122 .0 <sub>4</sub> 3116 .0 <sub>4</sub> 3019	31.22 31.16 30.19	39.75 39.68 38.44	.020 14 .020 11 .019 48

1	Diamete	r	Vi	7ire Ga	auge N	umber	s		Cross	Section	
Mils	Mm.	Ins.	American (B. & S.)	Washburn & Moen	Birmingham (Stubs')	British Standard	Metric	Sq. Ins.	Sq. Mils	Circular Mils	Sq. Mm.
5.906 5.8	.1524 .15 .1473	.0050 .0059 .0058		43			1.5	.0 <sub>4</sub> 2827 .0 <sub>4</sub> 2739 .0 <sub>4</sub> 2642	28.27 27.39 26.42	36 34.87 33.64	.018 24 .017 67 .017 05
5.615 5.512 <b>5.5</b>	.1426 .14 .1397	.0056 .0055 .0055	35	45				.0 <sub>4</sub> 2476 .0 <sub>4</sub> 2386 .0 <sub>4</sub> 2376	24.76 23.86 23.76	31.52 30.38 30.25	.015 97 .015 39 .015 33
5.2 5 4.8	.1321 .1270 .1219	.0052 .0050 .0048	36	46 47 48	35	39 40		.0 <sub>4</sub> 2124 .0 <sub>4</sub> 1963 .0 <sub>4</sub> 1810	21.24 19.63 18.10	27.04 25 23.04	.013 70 .012 67 .011 67
4.724 4.6 4.453	.12 .1168 .1131	.0047 .0046 .0045	37	49			1.2	.0 <sub>4</sub> 1753 .0 <sub>4</sub> 1662 .0 <sub>4</sub> 1557	17.53 16.62 15.57	22.32 21.16 19.83	.011 31 .010 72 .010 05
4.4 4 3.965	.1118 .1016 .1007	.0044 .0040 .0040	38	50	36	41 42		.041521 .041257 .041235	15.21 12.57 12.35	19.36 16 15.72	.009 810 .008 107 .007 967
3.937 3.6 3.531	.10 .091 44 .089 69	.0039 .0036 .0035	39			43	1	.0 <sub>4</sub> 1217 .0 <sub>4</sub> 1018 .0 <sub>5</sub> 9793	12.17 10.18 9.793	15.50 12.96 12.47	.007 854 .006 567 .006 318
3.2 3.145 2.800	.081 28 .079 87 .071 13	.0032 .0031 .0028	40 41			44		.0 <sub>5</sub> 8042 .0 <sub>5</sub> 7766 .0 <sub>5</sub> 6159	8.042 7.766 6.159	10.24 9.888 7.842	.005 189 .005 010 .003 973
2.8 2.494 2.4	.071 12 .063 34 .060 96	.0028 .0025 .0024	42			46		.0 <sub>5</sub> 6158 .0 <sub>5</sub> 4884 .0 <sub>5</sub> 4524	6.158 4.884 4.524	7.84 6.219 5.76	.003 973 .003 151 .002 919
2.221 2 1.978	.056 41 .050 80 .050 23	.0022 .0020 .0020	43			47		.0 <sub>6</sub> 3873 .0 <sub>5</sub> 3142 .0 <sub>6</sub> 3072	3.873 3.142 3.072	4.932 4 3.911	.002 499 .002 027 .001 982
1.969 1.761 <b>1.6</b>	.044 73 .040 64	.0020 .0018 .0016	45			48	0:5	.0 <sub>5</sub> 3044 .0 <sub>5</sub> 2436 .0 <sub>5</sub> 2011	3.044 2.436 2.011	3.875 3.102 <b>2.56</b> 0	.001 963 .001 572 .001 297
1.568 1.397 1.243	.039 84 .035 47 .031 59	.0016 .0014 .0012	46 47 48					.0 <sub>5</sub> 1932 .0 <sub>5</sub> 1532 .0 <sub>5</sub> 1215	1.932 1.532 1.215	2.460 1.951 1.547	.001 246 :0 <sub>3</sub> 9884 .0 <sub>3</sub> 7838
1.2 1.107 1	.030 48 .028 13 .025 40	.0012 .0011 .0010	49	• • •,• •		49 50		.0 <sub>5</sub> 1131 .0 <sub>6</sub> 9635 .0 <sub>6</sub> 7854	1.131 .9635 .7854	1.44 1.227 1	.0 <sub>3</sub> 7297 .0 <sub>3</sub> 6216 .0 <sub>3</sub> 5067
.9863	.025 05	.0010	50					.067641	.7641	.9728	.034929

#### DECIMAL EQUIVALENTS OF NON-BINARY FRACTIONS

(Denominators 7 to 19.) '

Nu-					DENOM	INATOR				
mer- ator	7	9	11	12	13	14	15	17	18	19
1	.1429	.1111	.0909	.0833	.0769	.0714	.0667	.0588	.0556	.0526
2	.2857	.2222	.1818	.1667	.1538	.1429	.1333	.1176	.1111	.1053
8	.4286	.3333	.2727	.2500	.2308	.2143	.2000	.1765	.1667	.1579
4	.5714	.4444	.3636	.3333	.3077	.2857	.2667	.2353	.2222	.2105
-	P149	EEEO	AKAK	4107	2016	0571	9999	0041	.2778	0000
									.3333	
	.8571								.3889	
									.4444	
U			.818%	.7500	.6923	.6429	.6000	.5294	.5000	.4737
10			0001	0000	2000	M140	0000			×000
									.5556	
11									.6111	
				_					.6667	
13									.7222	
14							.9333	.8235	.7778	.7368
15									.8333	
16								.9412	.8889	.8421
17									.9444	.8947
18										.9474

#### SQUARE ROOTS AND CUBE ROOTS OF FRACTIONS

Frac- tion	Square Root	Cube Root	Frac- tion	Square Root	Cube Root	Frac- tion	Square Root	Cube Root
1 2	.70711	.79370	67	.92582	.94991	12	.28868	.43679
1 socios	.57735	.69336	18	.35355	.50000	12 7 12	.76376	.74690
	.50000	.62996	- cocs cocs cocs co	.61237	.72112	112	.95743	.97141
484	.86603	.90856	87	.93541	.95647	16	.25000	.89685
16056	.40825	.55032	10	.33333	.48075	$\frac{3}{16}$ $\frac{5}{16}$	.43301	.67860
6	.37796	.52275	192949	.47140	.60571	7 16 9 16	.66144	.75915
79	.58452	.65863	5 9	.74536	.82207	116	.82916	88259
7 4	.65465	.75395	uja vja ala	.88192	.91963	13 16 15	.90138	.93313
5	.84515	.89390						

## DECIMAL EQUIVALENTS OF NON-BINARY FRACTIONS

(Denominators 21 to 31.)

NUMBRATOR		DENOMINATOR									
NOWE	21	22	28	24	28	27	28	29	80	81	
2 3	.0952 .1429	.0909 .1364	.0870	.0833 .1250	.0385 .0769 .1154 .1538	.0741	.0714		.0667	.0645	
5 6 7	.2381 .2857 .3888	.2273 .2727 .3182	.2174 .2609 .3043	.2083 .2500 .2917	.1923 .2308 .2692	.1852 .2222 .2593	.1786 .2143 .2500	.1724 .2069 .2414	.1667 .2000 .2338	.1613 .1935 .2258	
10	.4286	.4091	.3913		.3462	.3704	.3214	.2759 .3103 .3448 .3793	.8888	.2903	
12 18	.5714 .6190	.5455 .5909	.5217 .5652	.5000 .5417	.4615	.4444 .4815	.4286 .4643	.4138	.4000 .4333	.3871 .4194	
16 17 18	.7619 .8095 .8571	.7273 .7727 .8182	.6957 .7391 .7826	.6667 .7083 .7500	.6538	.5926 .6296 .6667	.5714 .6071 .6429	.5172 .5517 .5862 .6207 .6552		.5161 .5484 .5806	
20 21 22	.9524	.9091	.8696	.8333 .8750	.7692 .8077 .8462	.7407	.7143 .7500 .7857	.6897 .7241	.6667 .7000 .7333	.6452 .6774 .7097	
24 25 26					.9281	.8889 .9259 .9630	.8571 .8929 .9286	.8276 .8621 .8966	.8000 .8333 .8667	.7742 .8065 .8387	
27 28 29							.9643		.9000 .9333 .9667	.9032	

## DECIMALS OF A FOOT FOR EACH 1 OF AN INCH.

	1					
Inch.	0"	1"	2"	3"	4"	5"
0	0	.0833	.1667	.2500	.3333	.4167
1 64 32 32 64 1 16	.0013 .0026 .0039 .0052	.0846 .0859 .0872 .0885	.1680 .1693 .1706 .1719	.2513 .2526 .2539 .2552	.3346 .3359 .3372 .3385	.4180 .4193 .4206 .4219
5 64 3 32 7 64 8	.0065 .0078 .0091 .0104	.0898 .0911 .0924 .0937	.1732 .1745 .1758 .1771	.2565 .2578 .2591 .2604	.3398 .3411 .3424 .3437	.4232 .4245 .4258 .4271
$\begin{array}{r} \frac{9}{64} \\ \frac{5}{32} \\ \frac{11}{64} \\ \frac{3}{16} \end{array}$	.0117 .0130 .0143 .0156	.0951 .0964 .0977 .0990	.1784 .1797 .1810 .1823	.2617 .2630 .2643 .2656	.3451 .3464 .3477 .3490	.4284 .4297 .4310 .4323
13 64 7 32 164 1	.0169 .0182 .0195 .0208	.1003 .1016 .1029 .1042	.1836 .1849 .1862 .1875	.2669 .2682 .2695 .2708	.3503 .3516 .3529 .3542	.4336 .4349 .4362 .4375
17 64 9 32 19 64 5	.0221 .0234 .0247 .0260	.1055 .1068 .1081 .1094	.1888 .1901 .1914 .1927	.2721 .2734 .2747 .2760	.3555 .3568 .3581 .3594	.4388 .4401 .4414 .4427
214 614 223 24 83 8	.0273 .0286 .0299 .0312	.1107 .1120 .1133 .1146	.1940 .1953 .1966 .1979	.2773 .2786 .2799 .2812	.3607 .3620 .3633 .3646	.4440 .4453 .4466 .4479
25 64 13 32 27 64 7	.0326 .0339 .0352 .0365	.1159 .1172 .1185 .1198	.1992 .2005 .2018 .2031	.2826 .2839 .2852 .2865	.3659 .3672 .3685 .3698	.4492 .4505 .4518 .4531
29 64 15 32 34 12	.0378 .0391 .0404 .0417	.1211 .1224 .1237 .1250	.2044 .2057 .2070 .2083	.2878 .2891 .2904 .2917	.3711 .3724 .3737 .3750	.4544 .4557 .4570 .4583

# DECIMALS OF A FOOT FOR EACH $\frac{1}{64}$ OF AN INCH.

Inch.	6"	7"	8"	9"	10"	11"
O	.5000	.5833	.6667	.7500	.8333	.9167
$ \begin{array}{r} \frac{1}{64} \\ \frac{1}{32} \\ \frac{3}{64} \\ \frac{1}{16} \end{array} $	.5013 .5026 .5039 .5052	.5846 .5859 .5872 .5885	.6680 .6693 .6706 .6719	.7513 .7526 .7539 .7552	.8346 .8359 .8372 .8385	.9180 .9193 .9206 .9219
5 64 3 32 7 64 1 8	.5065 .5078 .5091 .5104	.5898 .5911 .5924 .5937	.6732 .6745 .6758 .6771	.7565 .7578 .7591 .7604	.8398 .8411 .8424 .8437	.9232 .9245 .9258 .9271
9 64 5 32 11 64 3 16	.5117 .5130 .5143 .5156	.5951 .5964 .5977 .5990	.6784 .6797 .6810 .6823	.7617 .7630 .7643 .7656	.8451 .8464 .8477 .8490	.9284 .9297 .9310 .9323
13 64 7 32 15 64	.5169 .5182 .5195 .5208	.6003 .6016 .6029 .6042	.6836 .6849 .6862 .6875	.7669 .7682 .7695 .7708	.8503 .8516 .8529 .8542	.9336 .9349 .9362 .9375
17 64 9 32 19 64 5	.5221 .5234 .5247 .5260	.6055 .6068 .6081 .6094	.6888 .6901 .6914 .6927	.7721 .7734 .7747 .7760	.8555 .8568 .8581 .8594	.9388 .9401 .9414 .9427
21 64 11 32 23 64 3 8	.5273 .5286 .5299 .5312	.6107 .6120 .6133 .6146	.6940 .6953 .6966 .6979	.7773 .7786 .7799 .7812	.8607 .8620 .8633 .8646	.9440 .9453 .9466 .9479
25 64 13 32 27 64 7	.5326 .5339 .5352 .5365	.6159 .6172 .6185 .6198	.6992 .7005 .7018 .7031	.7826 .7839 .7852 .7865	.8659 .8672 .8685 .8698	.9492 .9505 .9518 .9531
29 64 15 32 31 64	.5378 .5391 .5404 .5417	.6211 .6224 .6237 .6250	.7044 .7057 .7070 .7083	.7878 .7891 .7904 .7917	.8711 .8724 .8737 .8750	.9544 .9557 .9570 .9583

## DECIMALS OF A FOOT FOR EACH $\frac{1}{64}$ OF AN INCH.

Inch.	0"	1"	2"	3"	4"	5"
33 64 17 32 36 64 9	.0430 .0443 .0456 .0469	.1263 .1276 .1289 .1302	.2096 .2109 .2122 .2135	.2930 .2943 .2956 .2969	.3763 .3776 .3789 .3802	.4596 .4608 .4622 .4635
37 64 19 32 39 64 58	.0482 .0495 .0508 .0521	.1315 .1328 .1341 .1354	.2148 .2161 .2174 .2188	.2982 .2995 .3008 .3021	.3815 .3828 .3841 .3854	.4648 .4663 .4674
\$1 84 82 43 64 16	.0534 .0547 .0560 .0573	.1367 .1380 .1393 .1406	.2201 .2214 .2227 .2240	.3034 .3047 .3060 .3073	.3867 .3880 .3893 .3906	.4701 .4714 .4721 .4740
45 64 23 32 47 64 3	.0586 .0599 .0612 .0625	.1419 .1432 .1445 .1458	.2253 .2266 .2279 .2292	.3086 .3099 .3112 .3125	.3919 .3932 .3945 .3958	.4758 .4766 .4778 .4792
49 64 25 32 51 64 13 16	.0638 .0651 .0664 .0677	.1471 .1484 .1497 .1510	.2305 .2318 .2331 .2344	.3138 .3151 .3164 .3177	.3971 .3984 .3997 .4010	.4808 .4818 .483
53 64 32 55 64 78	.0690 .0703 .0716 .0729	.1523 .1536 .1549 .1562	.2357 .2370 .2383 .2396	.3190 .3203 .3216 .3229	.4023 .4036 .4049 .4062	.485 .487 .488 .489
57-649-350-645-6-1-6	.0742 .0755 .0768 .0781	.1576 .1589 .1602 .1615	.2409 .2422 .2435 .2448	.3242 .3255 .3268 .3281	.4076 .4089 .4102 .4115	.4909 .4929 .4939 .4949
61 81 82 63 64	.0794 .0807 .0820	.1628 .1641 .1654	.2461 .2474 .2487	.3294 .3307 .3320	.4128 .4141 .4154	.496: .4974 .498

# DECIMALS OF A FOOT FOR EACH $\frac{1}{64}$ OF AN INCH.

Inch.	6"	7"	8"	9"	10"	11"
33 64 17 82 36 64 9	.5430 .5443 .5456 .5469	.6263 .6276 .6289 .6302	.7096 .7109 .7122 .7135	.7930 .7943 .7956 .7969	.8763 .8776 .8789 .8802	.9596 .9609 .9622 .9635
37 646 322 364 58	.5482 .5495 .5508 .5521	.6315 .6328 .6341 .6354	.7148 .7161 .7174 .7188	.7982 .7995 .8008 .8021	.8815 .8828 .8841 .8854	.9648 .9661 .9674 .9688
41 64 21 82 43 43 64 11	.5534 .5547 .5560 .5573	.6367 .6380 .6393 .6406	.7201 .7214 .7227 .7240	.8034 .8047 .8060 .8073	.8867 .8880 .8893 .8906	.9701 9714 .9727 .9740
45 64 23 327 47 64	.5586 .5599 .5612 .5625	.6419 .6432 .6445 .6458	.7253 .7266 .7279 .7292	.8086 .8099 .8112 .8125	.8919 .8932 .8945 .8958	.9753 .9766 .9779 .9792
49 044 255 322 564 13 16	.5638 .5651 .5664 .5677	.6471 .6484 .6497 .6510	.7305 .7318 7331 .7344	.8138 .8151 .8164 .8177	.8971 .8984 .8997 .9010	.9805 .9818 .9831 .9844
53 647 325 677 8	.5690 .5703 .5716 .5729	.6523 .6536 .6549 .6562	.7357 .7370 .7383 .7396	.8190 .8203 .8216 .8229	.9023 .9036 .9049 .9062	.9857 .9870 .9883 .9896
57 64 29 54 54 15 16	.5742 .5755 .5768 .5781	.6576 .6589 .6602 .6615	.7409 .7422 .7435 .7448	.8242 .8255 .8268 .8281	.9076 .9089 .9102 .9115	.9909 .9922 .9935 .9948
61 64 31 32 63 64 1	.5794 .5807 .5820	.6628 .6641 .6654	.7461 .7474 .7487	.8294 .8307 .8320	.9128 .9141 .9154	.9961 .9974 .9987

# DECIMALS OF AN INCH FOR EACH $\frac{1}{64}$ TH. WITH MILLIMETRE EQUIVALENTS.

Frac-	1/64ths	Decimal	Millime- tres	Frac-	1 64ths	Decimal	Millime- tres
1 32  1 16	1 2 3 4	.015625 .03125 .046875 .0625	0.397 0.794 1.191 1.588	17 32  9 16	33 34 35 36	.515625 .53125 .546875 .5625	13.097 13.494 13.891 14.288
$\frac{\frac{3}{32}}{\frac{3}{2}}$ $\frac{1}{8}$	5 6 7 8	.078125 .09375 .109375 .125	1.984 2.381 2.778 3.175	19 32  5/8	37 38 39 40	.578125 .59375 .609375 .625	14.684 15.081 15.478 15.875
$\begin{array}{c} \cdot \cdot \cdot \\ \frac{5}{32} \\ \cdot \cdot \cdot \\ \frac{3}{16} \end{array}$	10 11 12	.140625 .15625 .171875 .1875	3.572 3.969 4.366 4.763	21 32  11 16	41 42 43 44	.640625 .65625 .671875 .6875	16.272 16.669 17.066 17.463
$\begin{array}{c} \cdot \cdot \cdot \\ \frac{7}{32} \\ \cdot \cdot \cdot \\ \frac{1}{4} \end{array}$	13 14 15 16	.203125 .21875 .234375 .25	5.159 5.556 5.953 6.350	· · · · · · · · · · · · · · · · · · ·	45 46 47 48	.703125 .71875 .734375 .75	17.859 18.256 18.653 19.050
9 32  5	17 18 19 20	.265625 .28125 .296875 .3125	6.747 7.144 7.541 7.938	25 32  13 16	49 50 51 52	.765625 .78125 .796875 .8125	19.447 19.844 20.241 20.638
11 32  3/8	21 22 23 24	.328125 .34375 .359375 .375	8.334 8.731 9.128 9.525	· · · · · · · · · · · · · · · · · · ·	53 54 55 56	.828125 .84375 .859375 .875	21.034 21.431 21.828 22.225
$\frac{13}{32}$ $\frac{7}{16}$	25 26 27 28	.390625 .40625 .421875 .4375	9.922 10.319 10.716 11.113	29 32  15	57 58 59 60	.890625 .90625 .921875 .9375	22.622 23.019 23.416 23.813
1/2	29 30 31 32	.453125 .46875 .484375	11.509 11.906 12.303 12.700	1 31 32	61 62 63 64	.953125 .96875 .984375	24.209 24.606 25.003 25.400

## WEIGHTS AND AREAS OF SQUARE AND ROUND BARS AND CIRCUMFERENCES OF ROUND BARS.

One cubic foot of steel weighs 489.6 lbs.

The following tables of weights of rounds, squares, flats, etc., are theoretical only. The various sizes made by us are listed elsewhere herein under appropriate headings, and the weights of rolled steel are subject to variation in accordance with mill practice for the different classes of products.

Thickness or Biameter in Inches.    Veight of    Bar in Inches.   Bar inches.   Bar inches.   Bar inches.						
In Inches.   One Foot Long.   One Foot Long.   In Sq. Inches.   In Sq. Inches.   In Inches.   Inches.   In Inches.   Inches. Inches.   Inches. Inches. Inches.   Inches. Inches. Inches. Inches. Inches.   Inches. Inches.	Thickness	-		-		
16	or Diameter	of Bar	of Bar	of Bar	of Bar	of O Bar
100   100	in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	<u>i</u>					
\$\frac{7}{64}\$         .041         .032         .0120         .0094         .3436           \$\frac{1}{64}\$         .053         .042         .0156         .0123         .3927           \$\frac{7}{64}\$         .067         .053         .0198         .0155         .4418           \$\frac{7}{64}\$         .083         .065         .0244         .0192         .4909           \$\frac{7}{64}\$         .100         .079         .0295         .0232         .5400           \$\frac{3}{14}\$         .120         .094         .0352         .0276         .5891           \$\frac{1}{14}\$         .140         .110         .0413         .0324         .6381           \$\frac{1}{14}\$         .140         .110         .0413         .0324         .6381           \$\frac{1}{12}\$         .163         .128         .0479         .0376         .6872           \$\frac{1}{14}\$         .240         .188         .0706         .0554         .8345           \$\frac{1}{14}\$         .240         .188         .0706         .0554         .8345           \$\frac{1}{12}\$         .332         .261         .0977         .0767         .9818           \$\frac{1}{12}\$         .362         .	64					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	33					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	64 .	.041	.032	.0120	.0094	.3436
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	.053	.042	.0156	.0123	.3927
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	\ <u>9</u>	,067	.053	.0198	.0155	.4418
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	.100	.079	.0295	.0232	.5400
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3.	.120	.094	.0352	.0276	.5891
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	13					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7 32	.163	.128		.0376	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	15 64	.187	.147	.0549	.0431	.7363
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	.212	167	.0625	.0491	.7854
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	17					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9 22					.8836
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10 64	.300	.235	.0881	.0692	.9327
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		332	261	0977	0767	9818
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	16 21					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	23	.439	.345	.1292	.1014	1.1290
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	478	376	1406	1104	1.1781
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	25					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						1.2763
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	27 64	.605	.475	.1780	.1398	1.3254
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7	651	511	1914	.1503	1.3745
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	16					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	15					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	31	.798	.627	.2346	.1843	1.5217
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	.850	.668	.2500	.1963	1.5708
	33					
35   1.017   .799   .2991   .2349   1.7181	17/32					
	35	1.017	.799	.2991	.2349	1.7181

Thickness	Weight	Weight	Area	Area	Circumference
or Diameter	of Bar	of Bar	of Bar	of Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
9 16	1.076	.845	.3164	.2485	1.7672
37 64	1.136	.893	.3342	.2625	1.8162
32 39 64	1.199	.941	.3525	.2769	1.8653
64	1.200	.002	.0710	.2010	TOTAL
5 8	1.328	1.043	.3906	.3068	1.9635
61	1.395	1.096	.4104	.3223	2.0126
31	1.464	1.150	.4307	.3382	2.0617
62	1.535	1.205	.4514	.3545	2.1108
116	1.607	1.262	.4727	.3712	2.1599
46 64 23 32 47 64	1.681	1.320	.4944	.3883	2.2089
23	1.756	1.380	.5166	.4057	2.2580
64	1.834	1.440	.5393	.4236	2.3071
3	1.913	1.502	.5625	.4418	2.3562
13	2.245	1.763	.6602	.5185	2.5526
13 16 7	2.603	2.044	.7656	.6013	2.7489
15 16	2.988	2.347	.8789	.6903	2.9453
1	3.400	2.670	1.0000	.7854	3.1416
1	3.838	3.015	1.1289	.8866	3.3380
10	4.303	3.380	1.2656	.9940	3.5343
16 28 3 16	4.795	3.766	1.4102	1.1075	3.7306
1	5.313	4.172	1.5625	1.2272	3.9270
1 4 5 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1	5.857	4.600	1.7227	1.3530	4.1234
3	6.428	5.049	1.8906	1.4849	4.3197
7 16	7.026	5.518	2.0664	1.6230	4.5161
1	7.650	6.008	2,2500	1.7671	4.7124
1 2 16	8.301	6.519	2.4414	1.9175	4.9088
5 8	8.978	7.051	2.6406	2.0739	5.1051
116 116	9.682	7.604	2.8477	2.2365	5.3015
3.	10.41	8.178	3.0625	2,4053	5.4978
13 16	11.17	8.773	3.2852	2.5802	5.6942
8	11.95	9.388	3.5156	2.7612	5.8905
15 16	12.76	10.02	3.7539	2.9483	6.0869

Thickness	Weight	Weight	Area	Area	Gircumference
or Diameter	of Bar	of Bar	of Bar	of Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
2	13.60	10.68	4.0000	3.1416	6.2832
	14.46	11.36	4.2539	3.3410	6.4796
16 18 3 16	15.35	12.06	4.5156	3.5466	6.6759
	16.27	12.78	4.7852	3.7583	6.8723
14 5 16 38	17.21	13.52	5.0625	3.9761	7.0686
1,6	18.18	14.28	5.3477	4.2000 4.4301	7.2650
8 7 16	19.18	15.06 15.87	5.6406 5.9414	4.4301	7.4613
16	20.20	10.07	0.0111	T.0001	1.0077
1 2 9 16 5 8	21.25	16.69	6.2500	4.9087	7.8540
16	22.33	17.53	6.5664	5.1573	8.0504
5 8	23.43	18.40	6.8906	5.4119	8.2467
16	24.56	19.29	7.2227	5.6727	8.4431
3	25.71	20.19	7.5625	5.9396	8.6394
3 13 16	26.90	21.12	7.9102	6.2126	8.8358
15 15 16	28.10	22.07	8.2656	6.4918	9.0321
16	29.34	23.04	8.6289	6.7771	9.2285
3	30.60	24.03	9.0000	7.0686	9.4248
16	31.89	25.05	9.3789	7.3662	9.6212
1 16 18 8 3 16	33.20	26.08	9.7656	7.6699	9.8175
16	34.55	27.13	10.160	7.9798	10.014
1	35.92	28.21	10.563	8.2958	10.210
16	37.31	29.30	10.973	8.6179	10.407
16 16 3 8 7	38.73	30.42	11.391	8.9462	10.603
16	40.18	31.55	11.816	9.2806	10.799
1 1	41.65	32.71	12.250	9.6211	10.996
1 2 9 10 . 5	43.15	33.89	12.691	9.9678	11.192
58	44.68	35.09	13.141	10.321	11.388
116	46.23	36.31	13.598	10.680	11.585
1 13 13 13 13 13 13 13 13 13 13 13 13 13	47.82	37.55	14.063	11.045	11.781
13	49.42	38.81	14.535	11.416	11.977
7	51.05	40.10	15.016	11.793	12.174
16	52.71	41.40	15.504	12.177	12.370

Thickness	Weight	Weight	Area	Area	Circumference
or Diameter	of Bar	of Bar	of Bar	of Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
4	54.40	42.73	16,000	12.566	12.566
1 1 6	56.11	44.07	16.504	12.962	12.763
18	57.85 59.62	45.44 46.83	17.016 17.535	13.364 13.772	12.959 13.155
16					
1 8 16	61.41	48.24 49.66	18.063 18.598	14.186	13.352 13.548
16 3 8 7 16	65.08	51.11	19.141	15.033	13.745
16	66.95	52.58	19.691	15.466	13.941
1 2 16	68.85	54.07	20.250	15.904	14.137
16 5 8	70.78	55.59 57.12	20.816 21.391	16.349	14.334
11 16	74.71	58.67	21.973	17.257	14.726
34	76.71	60.25	22.563	17.721	14.923
13 16	78.74	61.85 63.46	23.160 23.766	18.190	15.119
7 15 16	82.89	65.10	24.379	19.147	15.512
5	85.00	66.76	25,000	19.635	15.708
16	87.14	68.44	25.629	20.129	15.904
16	89.30 91.49	70.14 71.86	26.266 26.910	20.629 21.135	16.101
-					
1 5 10	93.71 95.96	73.60 75.37	27.563 28.223	21.648 22.166	16.493
8	98.23	77.15	28.891	22.691	16.886
16	100.5	78.95	29.566	23.221	17.082
· ½ 9 1,6		80.78	30.250	23.758 24.301	17.279
16 5 8	105.2	82.62	30.941	24.301	17.672
118	110.0	86.38	32.348	25.406	17.868
3 13 16	112.4	88.29	33.063	25.967	18.064
18 2	114.9	90.22 92.17	33.785 34.516	26.535 27.109	18.261
18 16	119.9	94.14	35.254	27.688	18.653

Thickness	Weight	Weight	Area	Area	Circumference
or Diameter	of Bar	of Bar	of Bar	of Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
8	122.4	96.13	36.000	28.274	18.850
16	125.0 127.6	98.15 100.2	36.754 37.516	28.867 29.465	19.046
18 3 16	130.2	102.2	38.285	30.069	19.439
1 2	132.8	104.3	39,063	30.680	19.635
16	135.5	106.4	39.848	31.296	19.831
16 16 38 77	138.2	108.5 110.7	40.641	31.919 32.548	20.028
16	140.9	110.7	41.441	32,348	20.224
1/2 9 1/6	143.7	112.8	42.250	33.183	20.420
16	146.5 149.2	115.0 117.2	43.066	33.824 34.472	20.617 20.813
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	152.1	119.4	44.723	35.125	21.009
3	154.9	121.7	45,563	35,785	21.206
13 13	157.8	123.9	46.410	36.451	21.402
1	160.7	126.2	47.266	37.122	21.599
15	163.6	128.5	48.129	37.800	21.795
7	166.6	130.8	49.000	38.485	21.991
16	169.6 172.6	133.2 135.6	49.879 50.766	39.175 39.871	22.188 22.384
16	175.6	138.0	51.660	40.574	22.580
	7 20 2	7404	F0 F00	47.000	
16 3 8 16	178.7 181.8	140.4 142.8	52.563 53.473	41.283	22.777 22.973
38	184.9	145.2	54.391	42.718	23.169
16	188.1	147.7	55.316	43.446	23.366
1/2	191.3	150.2	56.250	44.179	23.562
16	194.5	152.7	57.191	44.918	23.758
16 5 8 116	197.7	155.3 157.8	58.141 59.098	45.664 46.415	23.955 24.151
13	204.2	160.4 163.0	60.063	47.173 47.937	24.347 24.544
3 13 16 7 7 15	210.9	165.6	62.016	48.707	24.740
15	214.2	168.2	63.004	49.483	24.936

Thickness	Weight	Weight	Area	Arca	Direumference
or Diameter	of Bar	of Bar	of Bar	of Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
8	217.6	170.9	64.000	50.266	25.133
16 28 3 3 16	221.0	173.6	65.004	51.054	25.329
8 3	224.5	176.3 179.0	66.016 67.035	51.849 52.649	25.526 25.722
16	241.0	170.0	07.000	04.040	20.122
1	231.4	181.8	68.063	53.456	25.918
16	234.9	184.5	69.098	54.269	26.115
307	238.5 242.1	187.3 190.1	70.141 71.191	55.088 55.914	26.311 26.507
716	242.1	190.1	71.191	55.914	20.507
1	245.7	192.9	72.250	56.745	26.704
1 2 9 16	249.3	195.8	73.316	57.583	26.900
8	252.9	198.6	74.391	58.426 59.276	27.096
116	256.6	201.5	75.473	59.276	27.295
3	260.3	204.4	76.563	60.132	27.489
13	264.0	207.4	77.660	60.994	27.685
8	267.8	210.3	78.766	61.863	27.882
15 16	271.6	213.3	79.879	62.737	28.078
9	275.4	216.3	81.000	63.617	28.274
16	279.2	219.3	82.129	64.504	28.471
18	283.1	222.3	83.266	65.397	28.667
16	287.0	225.4	84,410	66.296	28,863
1	290.9	228.5	85.563	67.201	29.060
1 5 16	294.9	231.6	86.723	68.112	29.256
3 7 16	298.8	234.7	87.891	69.029	29.453
16	302.8	237.8	89.066	69.953	29.649
1	306.9	241.0	90.250	70.882	29.845
18 16	310.9	244.2	91.441	71.818	30.042
5 11 16	315.0	247.4	92.641	72.760	30.238
16	319.1	250.6	93.848	73.708	30.434
3	323.2	253.8	95.063	74.662	30.631
13 16 2 8	327.4	257.1	96.285	75.622	30.827
78	331.6	260.4	97.516	76.589 77.561	31.023
15	335.8	263.7	98.754	17.561	01.440

(CONCLUDED.)

Thickness	Weight	Weight	Area	Area	Circumference
or Diameter	of Bar	of Bar	of Bar	of Bar	of Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
10	340.0	267.0 270.4	100.00 101.25	78.540 79.525	31.416 31.612
16	348.6	273.8	102.52	80.516	31.809
1 16 1 8 3 16	352.9	277.1	103.79	81.513	32.005
1 5 16 3 8 7	357.2 361.6	280.6 284.0	105.06 106.35	82.516 83.525	32.201 32.398
3	366.0	287.4	107.64	84.541	32.594
7	370.4	290.9	108.94	85.563	32.790
16	374.9	294.4	110.25	86.590	32.987
16	379.3	297.9	111.57	87.624	33.183
111	383.8 388.4	301.5 305.0	112.89 114.22	88.664 89.710	33.380 33.576
118	900.4	303.0	114.22	30.710	00.070
2	392.9	308.6	115.56	90.763	33.772
13 16 7	397.5	312.2	116.91	91.821	33.969
18	402.1	315.8	118.27	92.886	34.165
18	406.7	319.5	119.63	93.957	34.361
11	411.4	323.1	121.00	95.033	34.558
16	416.1	326.8	122.38	96.116	34.754
1 8 3 16	420.8	330.5	123.77	97.206	34.950
16	425.5	334.3	125.16	98.301	35.147
1	430.3	338.0	126,56	99,402	35,343
1 8 16	435.1	341.7	127.97	100.51	35.539
3 8 7 16	439.9	345.5	129.39	101.62	35.736
16	444.8	349.3	130.82	102.74	35.932
1	449.7	353.2	132.25	103.87	36.128
1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6	454.6	357.0	133.69	105.00	36.325
5 11 16	459.5	360.9	135.14	106.14	36.521
16	464.4	364.8	136.60	107.28	36.717
3	469.4	368.7	138.06	108.43	36.914
13 18	474.4	372.6	139.54	109.59	37.110
18	479.5	376.6	141.02	110.75	37.307
15	484.5	380.5	142.50	111.92	37.503

## WEIGHTS OF SQUARE AND ROUND BARS PER RUNNING INCH.

One cubic inch of steel weighs 0.2833 lb.

	1	1		1	1
Thickness or Dismeter in Inches.	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.	Thickness or Diameter in Inches.	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.
16 8 8 16	.01		2 16 18 3 16	1.13 1.21 1.28 1.36	.89 .95 1.01 1.07
7 16 130 7 16	.02 .03 .04 .05	.01 .02 .03 .04	14 16 38 7	1.43 1.52 1.60 1.68	1.13 1.19 1.26 1.32
16 5 8 11 16	.07 .09 .11 .13	.06 .07 .09 .11	12 9 16 5 8 11	1.77 1.86 1.95 2.05	1.39 1.46 1.54 1.61
13 16 7 8 15 16	.16 .19 .22 .25	.13 .15 .17 .20	3 13 16 78 15 16	2.14 2.24 2.34 2.44	1.69 1.76 1.84 1.92
1 16 25 3 16	.28 .32 .36 .40	.22 .25 .28 .31	3 16 18 3 3 16	2.55 2.66 2.77 2.88	2.01 2.09 2.18 2.26
16 16 16 7 16	.44 .49 .54 .58	.35 .38 .42 .46	16 38 7 16	2.99 3.11 3.23 3.35	2.35 2.44 2.53 2.63
1 9 16 6 8 11 16	.64 .69 .75 .81	.50 .54 .59 .63	10 16 5 11 16	3.47 3.60 3.72 3.85	2.73 2.82 2.92 3.03
13 13 10 7 8 15	.87 .94 1.00 1.06	.68 .73 .78 .84	3 13 16 7 8 15	3.98 4.12 4.25 4.39	3.13 3.23 3.34 3.45

Thickness or Diameter in Inches,	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.	Thickness or Diameter in Inches.	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.
4 16 8 8 16	4.53 4.68 4.82 4.97	3.57 3.67 3.79 3.90	6 16 18 18 18	10.20 10.41 10.63 10.85	8.01 8.18 8.35 8.52
5 16 3 8 7	5.12 5.27 5.42 5.58	4.02 4.14 4.26 4.38	5 16 3 8 7	11.07 11.29 11.51 11.74	8.69 8.87 9.04 9.22
100	5.74 5.90 6.06 6.23	4.51 4.63 4.76 4.89	16 5 5 7 11 16	11.97 12.20 12.43 12.67	9.40 9.58 9.77 9.95
3 16 7 15 16	6.39 6.56 6.73 6.91	5.02 5.15 5.29 5.42	3 13 16 7 8 16 16	12.91 13.15 13.39 13.64	10.14 10.33 10.52 10.71
5 16 8 3 16	7.08 7.26 7.44 7.62	5.56 5.70 5.84 5.99	7 16 18 8 3 16	13.88 14.13 14.38 14.64	10.90 11.10 11.30 11.50
16 3 8 7	7.81 8.00 8.19 8.38	6.13 6.28 6.43 6.58	16 16 38 7 16	14.89 15.15 15.41 15.67	11.70 11.90 12.10 12.31
10 16 8 116	8.57 8.77 8.96 9.16	6.73 6.88 7.04 7.20	12 9 16 58 11 16	15.94 16.20 16.47 16.74	12.52 12.73 12.94 13.15
34 13 16 2 8 18 16	9.37 9.57 9.78 9.99	7.36 7.52 7.68 7.84	3 4 13 16 7 8 15 16	17.02 17.29 17.57 17.85	13.36 13.58 13.80 14.02

Thickness or Diameter in Inches.	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.	Thickness or Diameter in Inches.	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.
8 16 8 3 16	18.11 18.42 18.70 18.99	14.24 14.46 14.69 14.92	10 16 18 8 3 16	28.33 28.69 29.04 29.41	22.25 22.53 22.81 23.09
14 5 16 3 8 7	19.28 19.58 19.87 20.17	15.14 15.38 15.61 15.84	16 38 7	29.77 30.13 30.50 30.87	23.38 23.66 23.95 24.24
16 5 8 16 16	20.47 20.77 21.08 21.38	16.08 16.31 16.55 16.79	9 16 5 8 11 16	31.24 31.61 31.98 32.36	24.53 24.82 25.12 25.42
34 13 16 7 8 16 16	21.69 22.00 22.31 22.63	17.04 17.28 17.53 17.77	3 16 7 8 15 16	32.74 33.12 33.51 33.89	25.71 26.01 26.32 26.62
9 116 18 18 116	22.95 23.27 23.59 23.91	18.02 18.27 18.53 18.78	11 16 18 3 16	34.28 34.67 35.06 35.46	26.92 27.23 27.54 27.85
. 16 3 8 7	24.24 24.57 24.90 25.23	19.04 19.30 19.56 19.82	16 16 38 7	35.86 36.26 36.66 37.06	28.16 28.48 28.79 29.11
16 56 81 16	25.57 25.91 26.25 26.59	20.08 20.35 20.61 20.88	16 56 11 16	37.47 37.88 38.29 38.70	29.43 29.75 30.07 30.39
13 13 17 8 16	26.93 27.28 27.63 27.98	21.15 21.42 21.70 21.97	3 13 16 7 8 15	39.12 39.53 39.95 40.37	30.72 31.04 31.38 31.71

Thickness or Diameter in Inches.	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.	Thickness or Diameter in Inches.	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.
12 18 18 18 18	40.80 41.65 42.52 43.39	32.04 32.71 33.39 34.08	16	72.53 73.67 74.81 75.97	56.96 57.86 58.76 59.66
*(r*v)con(***-\100	44.27 45.16 46.06 46.96	34.77 35.47 36.17 36.88	¥∰24 15 15 55 4€ F- 85	77.13 78.31 79.49 80.68	60.58 61.50 62.43 63.36
13	47.88 48.81 49.74 50.68	37.60 38.33 39.06 39.80	17	81.88 83.09 84.30 85.53	64.30 65.25 66.21 67.17
T(24 s)(00 m)+# T-100	51.63 52.59 53.56 54.54	40.55 41.31 42.07 42.84	च्चीटव as co os -स र- so	86.77 88.01 89.26 90.52	68.14 69.12 70.10 71.09
14	55.53 56.53 57.53 58.54	43.62 44.39 45.18 45.98	18	91.79 93.07 94.36 95.66	72.09 73.10 74.11 75.13
*(reusions) *rigo	59.57 60.60 61.64 62.69	46.78 47.59 48.41 49.23	Alica rol concil 4 4-loo	96.96 98.28 99.60 100.94	76.15 77.19 78.22 79.27
15	63.75 64.81 65.89 66.97	50.06 50.90 51.75 52.60	19	102.28 103.63 104.99 106.35	80.32 81.39 82.45 83.53
right solidaries rico	68.07 69.17 70.28 71.40	53.46 54.32 55.20 56.08	Trice unicoccipi e-jeo	107.73 109.12 110.51 111.91	84.61 85.70 86.79 87.89

Thickness or Diameter in Inches.	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.	Thickness or Diameter in Inches.	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.
20	113.33 114.75 116.18 117.62	89.00 90.12 91.24 92.37	24	163.19 164.89 166.61 168.33	128.16 129.50 130.85 132.20
*(carcino e) de do	119.06 120.52 121.98 123.46	93.51 94.65 95.80 96.96	≠dearolocolete-joo	170.06 171.80 173.55 175.31	133.57 134.93 136.30 137.68
21	124.94 126.43 127.93 129.44	98.13 99.30 100.48 101.66	25 design	177.07 178.85 180.63 182.42	139.07 140.46 141.86 143.27
म्बंद्धा क्षेत्र क्षेत्र क्षेत्र	130.96 132.49 134.03 135.57	102.85 104.05 105.26 106.47	Trace and control of the Prices	184.23 186.04 187.86 189.68	144.68 146.11 147.54 148.97
22	137.12 138.69 140.26 141.84	107.69 108.92 110.15 111.40	26	191.52 193.37 195.22 197.09	150.41 151.86 153.32 154.78
	143.43 145.03 146.63 148.25	112.64 113.90 115.16 116.43	##(carcho es)-41joo	198.96 200.84 202.73 204.63	156.25 157.73 159.22 160.71
23	149.88 151.51 153.15 154.81	117.71 118.99 120.28 121.58	27	206.54 208.45 210.38 212.31	162.21 163.71 165.22 166.74
edirection or in the color or	156.46 158.13 159.81 161.49	122.88 124.19 125.51 126.83	#devojeo coj-tr-jeo	214.26 216.21 218.17 220.14	168.27 169.80 171.34 172.89

Thickness or Diameter in Inches,	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.	Thickness or Diameter in Inches.	Weight of Bar One Inch Long.	Weight of Bar One Inch Long.
28	222.12 224.11 226.10 228.11	174.44 176.01 177.57 179.15	32	290.11 292.39 294.67 296.95	227.85 229.63 231.42 233.22
reference or in the reference	230.12 232.15 234.18 236.22	180.73 182.32 183.91 185.52	Micercia cojet-i-a	299.25 301.56 303.87 306.20	235.02 236.83 238.65 240.48
29	238.27 240.33 242.39 244.47	187.13 188.74 190.37 192.00	33	308.53 310.87 313.22 315.58	242.31 244.15 245.99 247.85
Tression of 47-io	246.56 248.65 250.75 252.86	193.64 195.28 196.93 198.59	•dcanieo coj-at-ico	317.95 320.33 322.71 325.11	249.71 251.57 253.45 255.33
30 18 14 38	254.98 257.11 259.25 261.40	200.25 201.93 203.61 205.29	34	327.51 329.93 332.35 334.78	257.22 259.11 261.01 262.92
1 22500 3144710	263.55 265.72 267.89 270.07	206.99 208.69 210.39 212.11	##CHOICE CO #ET-lace	337.22 339.66 342.12 344.59	264.84 266.76 268.69 270.63
31	272.27 274.47 276.68 278.89	213.83 215.56 217.29 219.03	35	347.06 349.54 352.04 354.54	272.57 274.52 276.48 278.44
referencia prijestejao	281.12 283.36 285.60 287.85	220.78 222.54 224.30 226.07	rejetusjæ rojetrijas	357.05 359.57 362.09 364.63	280.41 282.39 284.38 286.37

## WEIGHTS OF CIRCULAR STEEL PLATES. POUNDS.

Diameters 35 to 134 ins.; Thicknesses  $\frac{3}{16}$  to 1 inch.

			mki	kness, Inch	00		
Diameter in	3		5 1	3	es 7 1	4 1	9
Inches	16	4	16	8	16	2	16
35	51.1	68.1	85.2	102.2	119.3	136.3	153.3
36	54.1	72.1	90.1	108.1	126.2	144.2	162.2
37	57.1	76.2	95.2	114.2	133.3	152.3	171.4
38	60.2	80.3	100.4	120.5	140.6	160.7	180.7
39	63.5	84.6	105.8	126.9	148.1	169.2	190.4
40	66.8	89.0	111.3	133.5	155.8	178.0	200.3
41	70.1	93.5	116.9	140.3	163.7	187.0	210.4
42	73.6	98.1	122.7	147.2	171.7	196.3	220.8
43	77.1	102.9	128.6	154.3	180.0	205.7	231.4
44	80.8	107.7	134.6	161.6	188.5	215.4	242.3
45	84.5	112.6	140.8	169.0	197.1	225.3	253.5
48	88.3	117.7	147.1	176.6	206.0	235.4	264.9
47	92.2	122.9	153.6	184.3	215.1	245.8	276.5
48	96.1	128.2	160.2	192.3	224.3	256.4	288.4
49	100.2	133.6	167.0	200.4	233.8	267.1	300.5
50	104.3	139.1	173.9	208.6	243.4	278.2	312.9
51	108.5	144.7	180.9	217.0	253.2	289.4	325.6
52	112.8	150.4	188.0	225.6	263.3	300.9	338.5
53	117.2	156.3	195.3	234.4	273.5	312.5	351.6
54	121.7	162.2	202.8	243.3	283.9	324.4	365.0
55	126.2	168.3	210.4	252.4	294.5	336.6	378.6
56	180.8	174.5	218.1	261.7	305.3	348.9	392.5
57	135.6	180.7	225.9	271.1	316.3	361.5	406.7
58	140.4	187.1	233.9	280.7	327.5	374.3	421.1
59	145.2	193.7	242.1	290.5	338.9	387.3	435.7
60	150.2	200.3	250.3	300.4	350.5	400.6	450.6
61	155.3	207.0	258.8	310.5	362.3	414.0	465.8
62	160.4	213.9	267.3	320.8	374.2	427.7	481.2
63	165.6	220.8	276.0	331.2	386.4	441.6	496.8
64	170.9	227.9	284.8	341.8	398.8	455.7	512.7
65	176.8	235.0	293.8	352.6	411.8	470.1	528.9
66	181.8	242.3	302.9	363.5	424.1	484.7	545.3
67	187.3	249.7	312.2	374.6	487.0	499.5	561.9
68	192.9	257.2	321.6	385.9	450.2	514.5	578.8
69	198.6	264.9	331.1	397.3	463.5	529.7	595.9
70	204.4	272.6	340.7	408.9	477.0	545.2	613.3
71	210.3	280.4	350.6	420.7	490.8	560.9	631.0
72	216.3	288.4	360.5	432.6	504.7	576.8	648.9
78	222.3	296.5	370.6	444.7	518.8	592.9	667.0
74	228.5	304.6	380.8	457.0	533.1	609.3	685.4
75	284.7	312.9	391.2	469.4	547.6	625.9	704.1
76	241.0	321.3	401.7	482.0	562.3	642.7	723.0
77	247.4	329.8	412.3	494.8	577.2	659.7	742.1
78	253.9	338.5	423.1	507.7	592.3	676.9	761.6
79	260.4	347.2	434.0	520.8	607.6	694.4	781.2
80	267.0	356.0	445.1	534.1	623.1	712.1	801.1
81	273.8	365.0	456.3	547.5	638.8	730.0	821.3
82	280.6	374.1	467.6	561.1	654.6	748.1	841.7
88	287.4	383.3	479.1	574.9	670.7	766.5	862.3
84	294.4	392.5	490.7	588.8	686.9	785.1	883.2

## WEIGHTS OF CIRCULAR STEEL PLATES. POUNDS.

Diameters 35 to 134 ins.; Thicknesses 3 to 1 inch.

16 0 7 11011											
-	11	Th 3	ickness, Inch	nes 7	15		Diameter in				
5 8	16	4	16	8	16	1	Inches				
170.4	187.4	204.4	221.5	238.6	255.6	272.6	35				
180.2	198.3	216.3	234.3	252.4	270.3	288.3	86				
190.4	209.4	228.3	247.5	266.6	285.6	304.6	37				
200.8	220.9	241.0	261.0	281.2	301.2	321.3	38				
211.5	232.7	253.9	275.0	296.2	317.3	338.4	39				
222.5	244.8	267.0	289.3	311.6	333.8	356.0	40				
233.8	257.2	280.6	303.9	327.5	350.7	374.1	41				
245.3	269.9	294.4	318.9	343.4	368.0	392.5	42				
257.2	282.9	308.6	334.3	360.0	385.8	411.5	48				
269.3	296.2	323.1	350.1	377.0	403.9	430.9	44				
281.6	309.8	338.0	366.1	394.3	422.4	450.6	45				
294.3	323.7	353.2	382.6	412.1	441.4	470.9	46				
307.2	338.0	368.7	399.4	430.2	460.8	491.5	47				
320.4	352.5	384.5	416.5	448.6	480.6	512.7	48				
333.9	367.3	400.7	434.1	467.6	500.9	534.8	49				
347.7	382.5	417.2	452.0	486.8	521.6	556.3	50				
361.7	397.9	434.1	470.2	506.4	542.6	578.7	51				
376.1	413.7	451.8	488.9	526.6	564.1	601.7	52				
390.7	429.7	468.8	507.9	547.0	586.0	625.1	53				
405.6	446.1	486.7	527.3	567.8	608.4	648.9	54				
420.7	462.8	504.9	546.9	589.0	631.1	673.2	55				
436.2	479.8	523.4	567.0	610.7	654.3	697.9	56				
451.9	497.1	542.2	587.4	632.6	677.8	723.0	57				
467.9	514.7	561.4	608.2	655.0	701.8	748.6	58				
484.1	532.6	581.0	629.4	677.8	726.2	774.7	59				
500.7	550.8	600.8	650.9	701.0	751.0	801.1	60				
517.5	569.3	621.0	672.8	724.5	776.3	828.1	61				
534.6	588.1	641.6	695.1	758.5	800.9	855.4	62				
552.0	607.2	662.4	717.6	772.8	828.0	883.2	63				
569.7	626.6	683.6	740.6	797.6	854.5	911.4	64				
587.6	646.4	705.1	763.9	822.6	881.4	940.2	65				
605.8	666.4	727.0	787.6	848.1	908.7	969.3	66				
624.3	686.8	749.2	811.6	874.0	936.5	999.0	67				
643.1	707.4	771.7	836.0	900.3	964.7	1029	68				
662.2	728.4	794.6	860.8	927.1	993.3	1060	69				
681.5	749.6	817.8	885.9	954.1	1023	1091	70				
701.1	771.2	841.3	919.4	985.5	1052	1122	71				
721.0	793.1	865.2	937.8	1010	1082	1154	72				
741.2	815.3	889.4	963.5	1038	1112	1186	73				
761.6	837.8	913.9	990.0	1066	1143	1219	74				
782.3	860.6	938.8	1017	1096	1174	1252	75				
803.3	883.7	964.0	1045	1125	1205	1286	76				
824.6	907.1	989.5	1072	1155	1237	1320	77				
846.2	930.8	1015	1100	1185	1270	1354	78				
868.0	954.8	1042	1129	1216	1302	1389	79				
890.1	979.1	1068	1158	1247	1336	1425	80				
912.5	1004	1095	1187	1278	1369	1460	81				
935.2	1029	1122	1216	1310	1403	1497	82				
958.1	1054	1150	1246	1342	1438	1533	83				
981.4	1080	1178	1276	1374	1472	1571	84				

# WEIGHTS OF CIRCULAR STEEL PLATES. POUNDS.

Diameters 35 to 134 ins.; Thicknesses 3 to 1 inch.

	10											
Diameter in	8	-	Thi 5	ckness, Inc	hes 7	-	9					
Inches	16	4	16	8	18	2	18					
85 86	301.5	401.9	502.4 514.3	602.9	703.4	803.9 822.9	904.4					
87	315.8	421.1	526.4	631.6	736.9	842.2	947.4					
88	323.1 330.5	430.8	538.5 550.8	646.2 661.0	753.9 771.2	861.6 881.3	969.8					
90	338.0 345.5	450.6	563.3 575.9	675.9	788.6 806.2	901.2	1014					
92	353.2	470.9	588.6	706.3	824.0	921.4	1060					
93 94	360.9	481.2 491.6	601.5	721.7	842.0 860.2	962.3 983.1	1083 1106					
95 96	376.6 384.5	502.1	627.6	753.1 769.1	878.6 897.2	1004 1025	1130 1154					
97	392.6	523.4	640.9 654.3	785.2	916.0	1047	1178					
98	400.7	534.3 545.8	667.9 681.6	801.4 817.9	935.0 954.2	1069 1091	1202 1227					
100 101	417.2 425.6	556.3 567.5	695.4 709.4	834.5 851.3	973.6	1113 1135	1252 1277					
102	434.1	578.8	723.5	868.2	1013	1158	1302 1328					
103 104	442.7	590.2 601.7	737.8 752.1	885.3 902.6	1033 1053	1180 1203	1328 1354					
105 106	460.0 468.8	613.3 625.1	766.7 781.4	920.0 937.6		1227 1250	1380 1406					
107	477.7	636.9	796.2	955.4	1115	1274	1433					
108 109	486.7	648.9 661.0	811.1 826.2	973.3 991.5	1136 1157	1298 1322	1460					
110 111	504.9 514.1	673.2 685.4	841.4 856.8	1010 1028	1178	1346 1371	1515 1542					
112	523.4	697.9	872.3 888.0	1047	1221	1396	1570					
113 114	532.8	710.4	903.7	1066 1085	1243 1265	1421 1446	1598 1627					
115 116	551.8 561.4	735.7 748.6	919.7	1104	1288 1310	1472	1655 1684					
117	571.2	761.6	951.9		1333	1523	1714					
118 119	581.0 590.9	774.6	968.3 984.8	1162 1182	1356 1379	1549 1576	1743 1773					
120 121	600.8	801.1 814.5	1001	1202 1222	1402	1602 1629	1803 1833					
122 123	621.0	828.0	1035	1242 1263	1449 1473	1656 1683	1863 1894					
124	641.6	841.7 855.4	1069	1283	1497	1711	1925					
125 126	651.9 662.4	869.3 883.2		1304 1325	1521 1546	1789	1956					
127	673.0	897.3	1122	1346	1570 1595	1795	2019					
128 129	683.6 694.3	911.5 925.8	1157	1367 1389	1620	1852	2051 2083					
130 131	705.1	940.2	1175	1410 1432	1645 1671	1880 1909	2115 2148					
132	727.0	954.7	1212	1454	1696 1722	1939	2181 2214					
133 134	738.1 749.2	984.1 998.9		1498	1748	1998	2248					

### WEIGHTS OF CIRCULAR STEEL PLATES.

#### POUNDS.

Diameters 35 to 134 ins.; Thicknesses  $\frac{3}{16}$  to 1 inch.

m**											
			hickness, Inc				Diameter in				
8	11	8 4	$\begin{array}{c c} 13 \\ \hline 16 \end{array}$	7 8	15	1	Inches				
1005	1105	1206	1307	1407	1509	1608	85				
1029	1132	1284	1338	1441	1548	1646	86				
1053	1158	1263	1369	1474	1580	1685	87				
1077	1185	1293	1400	1508	1616	1724	88				
1102	1212	1322	1438	1543	1653	1763	89				
1127	1239	1352	1465	1577	1690	1808	90				
1152	1267	1382	1498	1613	1728	1848	91				
1177	1295	1413	1531	1648	1766	1884	92				
1203	1323	1444	1564	1684	1804	1925	93				
1229	1352	1475	1598	1721	1843	1967	94				
1255	1381	1506	1632	1757	1883	2008	95				
1282	1410	1538	1666	1795	1928	2051	96				
1309	1440	1570	1701	1832	1963	2094	97				
1336	1469	1603	1737	1870	2004	2137	98				
1368	1499	1636	1772	1908	2045	2181	99				
1391	1530	1669	1808	1947	2086	2225	100				
1419	1561	1708	1844	1986	2128	2270	101				
1447	1592	1786	1881	2026	2171	2315	102				
1476	1628	1771	1918	2066	2213	2361	103				
1504	1655	1805	1956	2106	2256	2407	104				
1533	1687	1840	1998	2147	2300	2458	105				
1563	1719	1875	2032	2188	2344	2500	106				
1592	1752	1911	2070	2229	2889	2548	107				
1622	1785	1947	2109	2271	2433	2596	108				
1652	1818	1983	2148	2313	2479	2644	109				
1688	1851	2020	2188	2356	2524	2698	110				
1714	1885	2056	2228	2399	2570	2742	111				
1745	1919	2094	2268	2443	2617	2791	112				
1776	1954	2131	2309	2486	2664	2842	118				
1808	1988	2169	2350	2531	2711	2892	114				
1839	2023	2207	2391	2575	2759	2948	115				
1872	2059	2246	2433	2620	2807	2994	116				
1904	2094	2285	2475	2665	2856	8046	117				
1937	2130	2324	2518	2711	2905	8099	118				
1970	2167	2363	2560	2757	2954	3151	119				
2003 2036 2070 2104 2139	2208 2240 2277 2315 2352	2408 2444 2484 2525 2566	2604 2647 2691 2735 2780	2804 2851 2898 2946 2994	3004 3054 3105 3156 3208	8204 8258 3312 3367 8422	120 121 122 123 123 124				
2178	2391	2608	2825	3042	3260	3477	125				
2208	2429	2650	2871	3091	3312	3538	126				
2243	2468	2692	2916	3141	3365	3589	127				
2279	2507	2734	2962	3190	3418	3646	128				
2314	2546	2777	3009	3240	3472	3703	129				
2351	2586	2821	3056	3291	3526	3761	130				
2387	2625	2864	3103	3342	3580	3819	131				
2423	2666	2908	3150	3393	3685	3877	132				
2460	2706	2952	3198	3444	3690	3936	133				
2497	2747	2997	3247	8496	3746	3996	134				

For Thicknesses from \(\frac{1}{16}\) in. to 2 in. and Widths from 1 in. to 12\frac{3}{4}\) in.

Thickness in Inches.	1"	11/2"	11/2"	13"	2"	21"	2½"	23"	12"
16 18 3 16	.063 .125 .188 .250	.078 .156 .234 .313	.094 .188 .281 .375	.109 .219 .328 .438	.125 .250 .375 .500	.141 .281 .422 .563	.156 .313 .469 .625	.172 .344 .516 .688	.750 1.50 2.25 3.00
5 16 3 8 7 16	.313 .375 .438 .500	.391 .469 .547 .625	.469 .563 .656 .750	.547 .656 .766 .875	.625 .750 .875 1.00	.703 .844 .984 1.13	.781 .938 1.09 1.25	.859 1.03 1.20 1.38	3.75 4.50 5.25 6.00
9 16 5 11 10 3	.563 .625 .688 .750	.703 .781 .859 .938	.844 .938 1.03 1.13	.984 1.09 1.20 1.31	1.13 1.25 1.38 1.50	1.27 1.41 1.55 1.69	1.41 1.56 1.72 1.88	1.55 1.72 1.89 2.06	6.75 7.50 8.25 9.00
18 16 7 8 15 16	.813 .875 .938 1.00	1.02 1.09 1.17 1.25	1.22 1.31 1.41 1.50	1.42 1.53 1.64 1.75	1.63 1.75 1.88 2.00	1.83 1.97 2.11 2.25	2.03 2.19 2.34 2.50	2.23 2.41 2.58 2.75	9.75 10.50 11.25 12.00
1 1/16 1 1/8 1 1/8 1 1/6 1 1/4	1.06 1.13 1.19 1.25	1.33 1.41 1.48 1.56	1.59 1.69 1.78 1.88	1.86 1.97 2.08 2.19	2.13 2.25 2.38 2.50	2.39 2.53 2.67 2.81	2.66 2.81 2.97 3.13	2.92 3.09 3.27 3.44	12.75 13.50 14.25 15.00
$ \begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array} $	1.31 1.38 1.44 1.50	1.64 1.72 1.80 1.88	1.97 2.06 2.16 2.25	2.30 2.41 2.52 2.63	2.63 2.75 2.88 3.00	2.95 3.09 3.23 3.38	3.28 3.44 3.59 3.75	3.61 3.78 3.95 4.13	15.75 16.50 17.25 18.00
$1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4}$	1.56 1.63 1.69 1.75	1.95 2.03 2.11 2.19	2.34 2.44 2.53 2.63	2.73 2.84 2.95 3.06	3.13 3.25 3.38 3.50	3.52 3.66 3.80 3.94	3.91 4.06 4.22 4.38	4.30 4.47 4.64 4.81	18.75 19.50 20.25 21.00
113 17 115 115 2	1.81 1.88 1.94 2.00	2.27 2.34 2.42 2.50	2.72 2.81 2.91 3.00	3.17 3.28 3.39 3.50	3.63 3.75 3.88 4.00	4.08 4.22 4.36 4.50	4.53 4.69 4.84 5.00	4.98 5.16 5.33 5.50	21.75 22.50 23.25 24.00

Thickness in Inches.	3"	31"	311"	33"	4"	41"	41/1	43"	12"
16	.188	.203	.219	.234	.250	.266	.281	.297	.750
18	.375	.406	.438	.469	.500	.531	.563	.594	1.50
8	.563	.609	.656	.703	.750	.797	.844	.891	2.25
16	.750	.813	.875	.938	1.00	1.06	1.13	1.19	3.00
5 16 3 8 7 16 1 2	.938 1.13 1.31 1.50	1.02 1.22 1.42 1.63	1.09 1.31 1.53 1.75	1.17 1.41 1.64 1.88	1.25 1.50 1.75 2.00	1.33 1.59 1.86 2.13	1.41 1.69 1.97 2.25	1.48 1.78 2.08 2.38	3.75 4.50 5.25 6.00
9 16 5 8 11 16 3 4	1.69 1.88 2.06 2.25	1.83 2.03 2.23 2.44	1.97 2.19 2.41 2.63	2.11 2.34 2.58 2.81	2.25 2.50 2.75 3.00	2.39 2.66 2.92 3.19	2.53 2.81 3.09 3.38	2.67 2.97 3.27 3.56	6.75 7.50 8.25 9.00
13 16 7 8 15 16	2.44 2.63 2.81 3.00	2.64 2.84 3.05 3.25	2.84 3.06 3.28 3.50	3.05 3.28 3.52 3.75	3.25 3.50 3.75 4.00	3.45 3.72 3.98 4.25	3.66 3.94 4.22 4.50	3.86 4.16 4.45 4.75	9.75 10.50 11.25 12.00
$1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4}$	3.19	3.45	3.72	3.98	4.25	4.52	4.78	5.05	12.75
	3.38	3.66	3.94	4.22	4.50	4.78	5.06	5.34	13.50
	3.56	3.86	4.16	4.45	4.75	5.05	5.34	5.64	14.25
	3.75	4.06	4.38	4.69	5.00	5.31	5.63	5.94	15.00
$\begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array}$	3.94	4.27	4.59	4.92	5.25	5.58	5.91	6.23	15.75
	4.13	4.47	4.81	5.16	5.50	5.84	6.19	6.53	16.50
	4.31	4.67	5.03	5.39	5.75	6.11	6.47	6.83	17.25
	4.50	4.88	5.25	5.63	6.00	6.38	6.75	7.13	18.00
$\begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4} \end{array}$	4.69	5.08	5.47	5.86	6.25	6.64	7.03	7.42	18.75
	4.88	5.28	5.69	6.09	6.50	6.91	7.31	7.72	19.50
	5.06	5.48	5.91	6.33	6.75	7.17	7.59	8.02	20.25
	5.25	5.69	6.13	6.56	7.00	7.44	7.88	8.31	21.00
$1\frac{13}{16} \\ 1\frac{7}{8} \\ 1\frac{15}{16} \\ 2$	5.44	5.89	6.34	6.80	7.25	7.70	8.16	8.61	21.75
	5.63	6.09	6.56	7.03	7.50	7.97	8.44	8.91	22.50
	5.81	6.30	6.78	7.27	7.75	8.23	8.72	9.20	23.25
	6.00	6.50	7.00	7.50	8.00	8.50	9.00	9.50	24.00

Thickness in Inches.	5"	51"	51"	53"	6"	61"	6½"	63"	12"
16 18 3 16	.313 .625 .938 1.25	.328 .656 .984 1.31	.344 .688 1.03 1.38						.750 1.50 2.25 3.00
5 16 9 7 16 12	1.56 1.88 2.19 2.50	1.64 1.97 2.30 2.63	1.72 2.06 2.41 2.75	1.80 2.16 2.52 2.88	1.88 2.25 2.63 3.00	1.95 2.34 2.73 3.13	2.03 2.44 2.84 3.25	2.11 2.53 2.95 3.38	3.75 4.50 5.25 6.00
9 16 5 11 16	2.81 3.13 3.44 3.75	2.95 3.28 3.61 3.94	3.09 3.44 3.78 4.13	3.23 3.59 3.95 4.31	3.38 3.75 4.13 4.50	3.52 3.91 4.30 4.69	3.66 4.06 4.47 4.88	3.80 4.22 4.64 5.06	6.75 7.50 8.25 9.00
13 16 7 8 15 16 1	4.06 4.38 4.69 5.00	4.27 4.59 4.92 5.25	4.47 4.81 5.16 5.50	4.67 5.03 5.39 5.75	4.88 5.25 5.63 6.00	5.08 5.47 5.86 6.25	5.28 5.69 6.09 6.50	5.48 5.91 6.33 6.75	9.75 10.50 11.25 12.00
1 1 6 1 8 1 8 1 6 1 2 1 6 1 2 1 6 1 2 1 6 1 2 1 6 1 2 1 6 1 2 1 6 1 2 1 6 1 2 1 6 1 6	5.31 5.63 5.94 6.25	5.58 5.91 6.23 6.56	5.84 6.19 6.53 6.88	6.11 6.47 6.83 7.19	6.38 6.75 7.13 7.50	6.64 7.03 7.42 7.81	6.91 7.31 7.72 8.13	7.17 7.59 8.02 8.44	12.75 13.50 14.25 15.00
$ \begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array} $	6.56 6.88 7.19 7.50	6.89 7.22 7.55 7.88	7.22 7.56 7.91 8.25	7.55 7.91 8.27 8.63	7.88 8.25 8.63 9.00	8.20 8.59 8.98 9.38	8.53 8.94 9.34 9.75	8.86 9.28 9.70 10.13	15.75 16.50 17.25 18.00
$\begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4} \end{array}$	7.81 8.13 8.44 8.75	8.20 8.53 8.86 9.19	8.59 8.94 9.28 9.63	8.98 9.34 9.70 10.06	9.38 9.75 10.13 10.50	9.77 10.16 10.55 10.94	10.16 10.56 10.97 11.38	10.55 10.97 11.39 11.81	18.75 19.50 20.25 21.00
$1\frac{13}{16} \\ 1\frac{7}{8} \\ 1\frac{15}{16} \\ 2$		9.52 9.84 10.17 10.50	9.97 10.31 10.66 11.00	10.78	11.63	12.11	12.19 12.59	12.23 12.66 13.08 13.50	21.75 22.50 23.25 24.00

Thickness in Inches,	7"	71"	71"	73"	8"	81"	811"	83"	12"
16	.438	.453	.469	.484		.516	.531	.547	.750
8	.875	.906	.938	.969		1.03	1.06	1.09	1.50
3	1.31	1.36	1.41	1.45		1.55	1.59	1.64	2.25
16	1.75	1.81	1.88	1.94		2.06	2.13	2.19	3.00
5 16 3 3 8 7 16	2.19 2.63 3.06 3.50	2.27 2.72 3.17 3.63	2.34 2.81 3.28 3.75	2.42 2.91 3.39 3.88	2.50 3.00 3.50 4.00	2.58 3.09 3.61 4.13	2.66 3.19 3.72 4.25	2.73 3.28 3.83 4.38	3.75 4.50 5.25 6.00
16 5 8 11 16 3 4	3.94 4.38 4.81 5.25	4.08 4.53 4.98 5.44	4.22 4.69 5.16 5.63	4.36 4.84 5.33 5.81	4.50 5.00 5.50 6.00	4.64 5.16 5.67 6.19	4.78 5.31 5.84 6.38	4.92 5.47 6.02 6.56	6.75 7.50 8.25 9.00
136	5.69	5.89	6.09	6.30	6.50	6.70	6.91	7.11	9.75
78	6.13	6.34	6.56	6.78	7.00	7.22	7.44	7.66	10.50
156	6.56	6.80	7.03	7.27	7.50	7.73	7.97	8.20	11.25
1	7.00	7.25	7.50	7.75	8.00	8.25	8.50	8.75	12.00
$ \begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $	7.44	7.70	7.97	8.23	8.50	8.77	9.03	9.30	12.75
	7.88	8.16	8.44	8.72	9.00	9.28	9.56	9.84	13.50
	8.31	8.61	8.91	9.20	9.50	9.80	10.09	10.39	14.25
	8.75	9.06	9.38	9.69	10.00	10.31	10.63	10.94	15.00
$ \begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array} $	9.19	9.52	9.84	10.17	10.50	10.83	11.16	11.48	15.75
	9.63	9.97	10.31	10.66	11.00	11.34	11.69	12.03	16.50
	10.06	10.42	10.78	11.14	11.50	11.86	12.22	12.58	17.25
	10.50	10.88	11.25	11.63	12.00	12.38	12.75	13.13	18.00
$ \begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4} \end{array} $	10.94	11.33	11.72	12.11	12.50	12.89	13.28	13.67	18.75
	11.38	11.78	12.19	12.59	13.00	13.41	13.81	14.22	19.50
	11.81	12.23	12.66	13.08	13.50	13.92	14.34	14.77	20.25
	12.25	12.69	13.13	13.56	14.00	14.44	14.88	15.31	21.00
113 17 115 115 2	12.69 13.13 13.56 14.00	13.14 13.59 14.05 14.50	13.59 14.06 14.53 15.00	14.05 14.53 15.02 15.50	14.50 15.00 15.50 16.00	14.95 15.47 15.98 16.50	15.41 15.94 16.47 17.00	15.86 16.41 16.95 17.50	21.75 22.50 23.25 24.00

Thickness in Inches.	9"	91/	91/2"	93"	10"	101"	10½"	103"	12"
16 16 18 3 16	.563 1.13 1.69 2.25	.578 1.16 1.73 2.31	.594 1.19 1.78 2.38	.609 1.22 1.83 2.44	.625 1.25 1.88 2.50	.641 1.28 1.92 2.56	.656 1.31 1.97 2.63	.672 1.34 2.02 2.69	.750 1.50 2.25 3.00
5 16 3 8 7 15 1 2	2.81 3.38 3.94 4.50	2.89 3.47 4.05 4.63	2.97 3.56 4.16 4.75	3.05 3.66 4.27 4.88	3.13 3.75 4.38 5.00	3.20 3.84 4.48 5.13	3.28 3.94 4.59 5.25	3.36 4.03 4.70 5.38	3.75 4.50 5.25 6.00
16 5 8 11 16 3 4	5.06 5.63 6.19 6.75	5.20 5.78 6.36 6.94	5.34 5.94 6.53 7.13	5.48 6.09 6.70 7.31	5.63 6.25 6.88 7.50	5.77 6.41 7.05 7.69	5.91 6.56 7.22 7.88	6.05 6.72 7.39 8.06	6.75 7.50 8.25 9.00
13 16 7 8 15 16	7.31 7.88 8.44 9.00	7.52 8.09 8.67 9.25	7.72 8.31 8.91 9.50	7.92 8.53 9.14 9.75	8.13 8.75 9.38 10.00	8.33 8.97 9.61 10.25	8.53 9.19 9.84 10.50	8.73 9.41 10.08 10.75	9.75 10.50 11.25 12.00
$1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4}$	9.56 10.13 10.69 11.25	9.83 10.41 10.98 11.56	10.09 10.69 11.28 11.88	10.36 10.97 11.58 12.19	10.63 11.25 11.88 12.50	10.89 11.53 12.17 12.81	11.16 11.81 12.47 13.13	11.42 12.09 12.77 13.44	12.75 13.50 14.25 15.00
$\begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array}$	11.81 12.38 12.94 13.50	12.14 12.72 13.30 13.88	12.47 13.06 13.66 14.25	12.80 13.41 14.02 14.63	13.13 13.75 14.38 15.00	13.45 14.09 14.73 15.38	13.78 14.44 15.09 15.75	14.11 14.78 15.45 16.13	15.75 16.50 17.26 18.00
$\begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4} \end{array}$	14.06 14.63 15.19 15.75	14.45 15.03 15.61 16.19	14.84 15.44 16.03 16.63	16.45	15.63 16.25 16.88 17.50	16.02 16.66 17.30 17.94	16.41 17.06 17.72 18.38	16.80 17.47 18.14 18.81	18.75 19.50 20.25 21.00
$1\frac{13}{16} \\ 1\frac{7}{8} \\ 1\frac{15}{16} \\ 2$	16.31 16.88 17.44 18.00	16.77 17.34 17.92 18.50	17.22 17.81 18.41 19.00	18.28 18.89	18.13 18.75 19.38 20.00	18.58 19.22 19.86 20.50	19.69 20.34	19.48 20.16 20.83 21.50	21.75 22.50 23.25 24.00

(CONCLUDED.)

Thickness in Inches,	11"	1117"	11½"	113"	12"	121"	121"	123″
16 16 8 8 16 14	.688 1.38 2.06 2.75	.703 1.41 2.11 2.81	.719 1.44 2.16 2.88	.734 1.47 2.20 2.94	.750 1.50 2.25 3.00	.766 1.53 2.30 3.06	.781 1.56 2.34 3.13	.797 1.59 2.39 3.19
56	3.44	3.52	3.59	3.67	3.75	3.83	3.91	3.98
38	4.13	4.22	4.31	4.41	4.50	4.59	4.69	4.78
87	4.81	4.92	5.03	5.14	5.25	5.36	5.47	5.58
16	5.50	5.63	5.75	5.88	6.00	6.13	6.25	6.38
9 16 5 8 11 16 3	6.19 6.88 7.56 8.25	6.33 7.03 7.73 8.44	6.47 7.19 7.91 8.63	6.61 7.34 8.08 8.81	6.75 7.50 8.25 9.00	6.89 7.66 8.42 9.19	7.03 7.81 8.59 9.38	7.17 7.97 8.77 9.56
$1 \frac{\frac{13}{16}}{\frac{7}{8}}$ $1 \frac{15}{16}$	8.94	9.14	9.34	9.55	9.75	9.95	10.16	10.36
	9.63	9.84	10.06	10.28	10.50	10.72	10.94	11.16
	10.31	10.55	10.78	11.02	11.25	11.48	11.72	11.95
	11.00	11.25	11.50	11.75	12.00	12.25	12.50	12.75
$ \begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $	11.69	11.95	12.22	12.48	12.75	13.02	13.28	13.55
	12.38	12.66	12.94	13.22	13.50	13.78	14.06	14.34
	13.06	13.36	13.66	13.95	14.25	14.55	14.84	15.14
	13.75	14.06	14.38	14.69	15.00	15.31	15.63	15.94
$\begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array}$	14.44	14.77	15.09	15.42	15.75	16.08	16.41	16.73
	15.13	15.47	15.81	16.16	16.50	16.84	17.19	17.53
	15.81	16.17	16.53	16.89	17.25	17.61	17.97	18.33
	16.50	16.88	17.25	17.63	18.00	18.38	18.75	19.13
$\begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4} \end{array}$	17.19	17.58	17.97	18.36	18.75	19.14	19.53	19.92
	17.88	18.28	18.69	19.09	19.50	19.91	20.31	20.72
	18.56	18.98	19.41	19.83	20.25	20.67	21.09	21.52
	19.25	19.69	20.13	20.56	21.00	21.44	21.88	22.31
113 17 115 115 2	19.94 20.63 21.31 22.00	20.39 21.09 21.80 22.50	20.84 21.56 22.28 23.00	21.30 22.03 22.77 23.50	21.75 22.50 23.25 24.00	22.20 22.97 23.73 24.50	22.66 23.44 24.22 25.00	23.11 23.91 24.70 25.50

to find the area of 15%"  $\times$  0.50 = 13.34 square inches areas of plates of any width greater than I

## WEIGHTS OF FLAT ROLLED STRIPS, HOOP OR BAND STEEL.

Pounds per Lineal Foot.

Thicknesses by Birmingham Wire Gauge.

One cubic foot of steel weighs 489.6 pounds, For widths from ½ inch to ¾ inch and thicknesses from No. 19 to No. 11 B.W.G.

POF WIGE	For widths from 1/2 inch to 1/2 inch and thicknesses from No. 19 to No. 11 B.W.G.										
Width in Inches.	No. 19.	No. 18.	No. 17.	No. 16.	No. 15.	No. 14.	No. 13.	No. 12.	No. 11.		
	.042 In.	.049 In.	.058 In.	.065 In.	.072 In.	.083 In.	.095 In.	.109 In.	.120 In.		
17764 932 1964	.036 .038 .040 .042	.042 .044 .047 .049	.049 .052 .055 .059	.055 .059 .062 .066	.061 .065 .069 .073	.071 .075 .079 .084	.081 .086 .091 .096	.093 .098 .104 .110	.102 .108 .115 .121		
Testoring old	.045	.052	.062	.069	.077	.088	.101	.116	.128		
	.047	.055	.065	.073	.080	.093	.106	.122	.134		
	.049	.057	.068	.076	.084	.097	.111	.127	.140		
	.051	.060	.071	.079	.088	.101	.116	.133	.147		
18 5445524 744 2467-13 746	.054 .056 .058 .060	.062 .065 .068 .070	.074 .077 .080 .083	.083 .086 .090 .093	.092 .096 .099 .103	.106 .110 .115 .119	.121 .126 .131 .136	.139 .145 .151 .156	.153 .159 .166 .172		
7 00 4 00 1 1 0 0 1 1 0 0 0 0 0 0 0 0 0 0	.062	.073	.086	.097	.107	.123	.141	.162	.179		
	.065	.075	.089	.100	.111	.128	.146	.168	.185		
	.067	.078	.092	.104	.115	.132	.151	.174	.191		
	.069	.081	.096	.107	.119	.137	.156	.180	.198		
ado de ago	.071	.083	.099	.111	.122	.141	.162	.185	.204		
	.074	.086	.102	.114	.126	.146	.167	.191	.210		
	.076	.089	.105	.117	.130	.150	.172	.197	.217		
	.078	.091	.108	.121	.134	.154	.177	.203	.223		
9 107 40 2014	.080	.094	.111	.124	.138	.159	.182	.208	.230		
	.083	.096	.114	.128	.142	.163	.187	.214	.236		
	.085	.099	.117	.131	.145	.168	.192	.220	.242		
	.087	.102	.120	.135	.149	.172	.197	.226	.249		
58 44 4 2 3 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	.089	.104	.123	.138	.153	.176	.202	.232	.255		
	.091	.107	.126	.142	.157	.181	.207	.237	.261		
	.094	.109	.129	.145	.161	.185	.212	.243	.268		
	.096	.112	.132	.148	.164	.190	.217	.249	.274		
16 5 4 5 5 7 7 4 5 5 4 5 4 5 4 5 4 5 4 5 5 4 5 5 4 5 5 6 5 6	.098	.115	.136	.152	.168	.194	.222	.255	.281		
	.100	.117	.139	.155	.172	.198	.227	.261	.287		
	.103	.120	.142	.159	.176	.203	.232	.266	.293		
	.105	.122	.145	.162	.180	.207	.237	.272	.300		
	.107	.125	.145	.166	.184	.212	.242	.278	.306		

Pounds per Lineal Foot.

One cubic foot of steel weighs 489.6 pounds. For thicknesses from  $\frac{1}{16}$  inch to  $\frac{1}{16}$  inch and widths from  $\frac{1}{16}$  inch to 1 inch.

Thickness in Inches.	1"	17"	32"	19"	5 "	21" 84"	117	23° 64	3"
16 64 37 64	.053 .066 .080 .093	.056 .071 .085 .099	.060 .075 .090 .105	.063 .079 .095 .110	.066 .083 .100 .116	.070 .087 .105 .122	.073 .091 .110 .128	.076 .095 .115 .134	.080 .100 .120 .139
8 9 64 32 11 64	.106 .120 .133 .146	.113 .127 .141 .155	.120 .134 .149 .164	.126 .142 .158 .173	.133 .149 .166 .183	.139 .157 .174 .192	.146 .164 .183 .201	.153 .172 .191 .210	.159 .179 .199 .219
3 16 13 6 7 32 16 6 4	.159 .173 .186 .199	.169 .183 .198 .212	.179 .194 .209 .224	.189 .205 .221 .237	.199 .216 .232 .249	.209 .227 .244 .261	.219 .237 .256 .274	.229 .248 .267 .286	.239 .259 .279 .299
17 64 9 32 19 64	.213 .226 .239 .252	.226 .240 .254 .268	.239 .254 .269 .284	.252 .268 .284 .300	.266 .282 .299 .315	.279 .296 .314 .331	.292 .310 .329 .347	.305 .325 .344 .363	.319 .339 .359 .379
8 6 -44 1 246 1 23 24 6	.266 .279 .292 .305	.282 .296 .310 .325	.299 .314 .329 .344	.315 .331 .347 .363	.332 .349 .365 .382	.349 .366 .383 .401	.365 .383 .402 .420	.382 .401 .420 .439	.398 .418 .438 .458
5)-4-5)-4-5)-4-7-1-4-1	.319 .332 .345 .359	.339 .353 .367 .381	.359 .374 .388 .403	.379 .394 .410 .426	.398 .415 .432 .448	.418 .436 .453 .471	.438 .457 .475 .493	.458 .477 .496 .515	.478 .498 .518 .538
1 6 0 14 6 14 1 240 14 6 14 1 20 14 6 14	.372 .385 .398 .412	.395 .409 .423 .437	.418 .433 .448 .463	.442 .457 .473 .489	.465 .481 .498 .515	.488 .506 .523 .540	.511 .530 .548 .566	.535 .554 .573 .592	.558 .578 .598 .618
100 00 00 00 00 00 00 00 00 00 00 00 00	.425 .438 .452 .465 .478	.452 .466 .480 .494 .508	.478 .493 .508 .523 .538	.505 .520 .536 .552 .567	.531 .548 .564 .581 .598	.558 .575 .593 .610 .628	.584 .603 .621 .639 .657	.611 .630 .649 .668 .687	.638 .657 .677 .697 .717

### Pounds per Lineal Foot.

		ł.			, ,	t	1		1
Thickness in Inches.	25" 64"	13 h	27" 64"	716"	29" 64"	15" 32"	81# 64	1/2"	12"
1 16 5 64 3 32 7 64	.083 .104 .125 .145	.086 .108 .129 .151	.090 .112 .134 .157	.093 .116 .139 .163	.096 .120 .144 .169	.100 .125 .149 .174	.103 .129 .154 .180	.106 .133 .159 .186	2.55 3.19 3.83 4.46
88 9 6 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	.166 .187 .208 .228	.173 .194 .216 .237	.179 .202 .224 .247	.186 .209 .232 .256	.193 .217 .241 .265	.199 .224 .249 .274	.206 .232 .257 .283	.212 .239 .266 .292	5.10 5.74 6.38 7.01
3 1.6 1.6 7 7 3 1.5 6 4	.249 .270 .291 .311	.259 .281 .302 .324	.269 .291 .314 .336	.279 .302 .325 .349	.289 .313 .337 .361	.299 .324 .349 .374	.309 .335 .360 .386	.319 .345 .372 .398	7.65 8.29 8.93 9.56
14 17 84 32 194	.332 .353 .374 .394	.345 .367 .388 .410	.359 .381 .403 .426	.372 .395 .418 .442	.385 .409 .433 .457	.398 .423 .448 .473	.412 .437 .463 .489	.425 .452 .478 .505	10.20 10.84 11.48 12.11
561412234	.415 .436 .457 .477	.432 .453 .475 .496	.448 .471 .493 .515	.465 .488 .511 .535	.481 .506 .530 .554	.498 .523 .548 .573	.515 .540 .566 .592	.531 .558 .584 .611	12.75 13.39 14.03 14.66
ত্যাত ত্যাল তাল ক্র	.498 .519 .540 .560	.518 .540 .561 .583	.538 .560 .583 .605	.558 .581 .604 .628	.578 .602 .626 .650	.598 .623 .647 .672	.618 .643 .669 .695	.638 .664 .691 .717	15.30 15.94 16.58 17.21
7 169 145 145 145 145 145 145 145 145 145 145	.581 .602 .623 .643	.604 .626 .647 .669	.628 .650 .672 .695	.651 .674 .697 .721	.674 .698 .722 .746	.697 .722 .747 .772	.721 .746 .772 .798	.744 .770 .797 .823	17.85 18.49 19.13 19.76
100 00 14 1 100 00 10 00	.664 .685 .706 .726 .747	.691 .712 .734 .755 .777	.717 .740 .762 .784 .807	.744 .767 .790 .813 .837	.770 .794 .818 .843 .867	.797 .822 .847 .872 .896	.823 .849 .875 .901 .926	.850 .877 .903 .930 .956	20.40 21.04 21.68 22.31 22.95

#### Pounds per Lineal Foot.

Thickness in Inches.	38"	17"	35" 64"	9 "	37" 64	19"	39# 64	5#	12"
16 64 3 32 7 64	.110 .137 .164 .192	.113 .141 .169 .198	.116 .145 .174 .203	.120 .149 .179 .209	.123 .154 .184 .215	.126 .158 .189 .221	.129 .162 .194 .227	.133 .166 .199 .232	2.55 3.19 3.83 4.46
89 64 82 83 84	.219 .247 .274 .301	.226 .254 .282 .310	.232 .261 .291 .320	.239 .269 .299 .329	.246 .276 .307 .338	.252 .284 .315 .347	.259 .291 .324 .356	.266 .299 .332 .365	5.10 5.74 6.38 7.01
3 18 18 64 7 32 154	.329 .356 .383 .411	.339 .367 .395 .423	.349 .378 .407 .436	.359 .388 .418 .448	.369 .399 .430 .461	.379 .410 .442 .473	.388 .421 .453 .486	.398 .432 .465 .498	7.65 8.29 8.93 9.56
144 144 150 150 150 150 150 150 150 150 150 150	.438 .466 .493 .520	.452 .480 .508 .536	.465 .494 .523 .552	.478 .508 .538 .568	.491 .522 .553 .584	.505 .536 .568 .599	.518 .550 .583 .615	.531 .564 .598 .631	10.20 10.84 11.48 12.11
5 16 12 26 13 24 24 24 24 24 24 24 24 24 24 24 24 24	.548 .575 .603 .630	.564 .593 .621 .649	.581 .610 .639 .668	.598 .628 .657 .687	.614 .645 .676 .706	.631 .662 .694 .725	.647 .680 .712 .745	.664 .697 .730 .764	12.75 13.39 14.03 14.66
240 - 140 040	.657 .685 .712 .740	.677 .706 .734 .762	.697 .726 .755 .784	.717 .747 .777 .807	.737 .768 .799 .829	.757 .789 .820 .852	.777 .809 .842 .874	.797 .830 .863 .896	15.30 15.94 16.58 17.21
7 16 0)45 12 144 246 140 250	.767 .794 .822 .849	.790 .818 .847 .875	.813 .843 .872 .901	.837 .867 .896 .926	.860 .891 .921 .952	.883 .915 .946 .978	.906 .939 .971 1.00	.930 .963 .996 1.03	17.85 18.49 19.13 19.76
38 647 132 355 64 16	.877 .904 .931 .959 .986	.903 .931 .960 .988 1.02	.930 .959 .988 1.02 1.05	.956 .986 1.02 1.05 1.08	.983 1.01 1.04 1.07 1.11	1.01 1.04 1.07 1.10 1.14	1.04 1.07 1.10 1.13 1.17	1.06 1.10 1.13 1.16 1.20	20.40 21.04 21.68 22.31 22.95

Pounds per Lineal Foot.

Thickness in Inches.	<del>11</del> "	21" 32"	48"	11"	468	23" 32"	47°	3"	12"
16 54 3 32 7 64	.136 .170 .204 .238	.139 .174 .209 .244	.143 .178 .214 .250	.146 .183 .219 .256	.149 .187 .224 .261	.153 .191 .229 .267	.156 .195 .234 .273	.159 .199 .239 .279	2.55 3.19 3.83 4.46
8 9 6 4 5 3 3 1 1 6 4	.272 .306 .340 .374	.279 .314 .349 .383	.286 .321 .357 .393	.292 .329 .365 .402	.299 .336 .374 .411	.305 .344 .382 .420	.312 .351 .390 .429	.319 .359 .398 .438	5.10 5.74 6.38 7.01
3 16 133 64 7 33 64	.408 .442 .476 .510	.418 .453 .488 .523	.428 .464 .500 .535	.438 .475 .511 .548	.448 .486 .523 .560	.458 .496 .535 .573	.468 .507 .546 .585	.478 .518 .558 .598	7.65 8.29 8.93 9.56
174 9 32 194	.545 .579 .613 .647	.558 .593 .628 .662	.571 .607 .642 .678	.584 .621 .657 .694	.598 .635 .672 .710	.611 .649 .687 .725	.624 .663 .702 .741	.638 .677 .717 .757	10.20 10.84 11.48 12.11
5 16 244 132 245 4	.681 .715 .749 .783	.697 .732 .767 .802	.714 .750 .785 .821	.730 .767 .804 .840	.747 .784 .822 .859	.764 .802 .840 .878	.780 .819 .858 .897	.797 .827 .877 .916	12.75 13.39 14.03 14.66
este solvente rive	.817 .851 .885 .919	.837 .872 .906 .941	.857 .892 .928 .964	.877 .913 .950 .986	.896 .934 .971 1.01	.916 .955 .993 1.03	.936 .975 1.01 1.05	.956 .996 1.04 1.08	15.30 15.94 16.58 17.21
7 160 120 137 138 16	.953 .987 1.02 1.06	.976 1.01 1.05 1.08	.999 1.04 1.07 1.11	1.02 1.06 1.10 1.13	1.05 1.08 1.12 1.16	1.07 1.11 1.15 1.18	1.09 1.13 1.17 1.21	1.12 1.16 1.20 1.24	17.85 18.49 19.13 19.76
23 84 117 32 15 04 09	1.09 1.12 1.16 1.19 1.23	1.12 1.15 1.19 1.22 1.26	1.14 1.18 1.21 1.25 1.28	1.17 1.21 1.24 1.28 1.31	1.20 1.23 1.27 1.31 1.34	1.22 1.26 1.30 1.34 1.37	1.25 1.29 1.33 1.37 1.40	1.28 1.31 1.35 1.39 1.43	20.40 21.04 21.68 22.31 22.95

Pounds per Lineal Foot.

Thickness in Inches.	49//	25// 32	51//	13"	53"	37"	55//	7''	12"
16 5 64 3 32 7 64	.163 .203 .244 .285	.166 .208 .249 .291	.169 .212 .254 .296	.173 .216 .259 .302	.176 .220 .264 .308	.179 .224 .269 .314	.183 .228 .274 .320	.186 .232 .279 .325	2.55 3.19 3.83 4.46
1 8 9 64 5 32 11 64	.325 .366 .407 .447	.332 .374 .415 .457	.339 .381 .423 .466	.345 .388 .432 .475	.352 .396 .440 .484	.359 .403 .448 .493	.365 .411 .457 .502	.372 .418 .465 .511	5.10 5.74 6.38 7.01
3 16 13 64 7 32 15 64	.488 .529 .569 .610	.498 .540 .581 .623	.508 .550 .593 .635	.518 .561 .604 .647	.528 .572 .616 .660	.538 .583 .628 .672	.548 .594 .639 .685	.558 .604 .651 .697	7.65 8.29 8.93 9.56
1 4 17 64 9 32 19 64	.651 .691 .732 .773	.664 .706 .747 .789	.677 .720 .762 .804	.691 .734 .777 .820	.704 .748 .792 .836	.717 .762 .807 .852	.730 .776 .822 .867	.744 .790 .837 .883	10.20 10.84 11.48 12.11
5 16 21 64 11 32 23 64	.813 .854 .895 .936	.830 .872 .913 .955	.847 .889 .931 .974	.863 .906 .950 .993	.880 .924 .968 1.01	.897 .941 .986 1.03	.913 .959 1.00 1.05	.930 .976 1.02 1.07	12.75 13.39 14.03 14.66
3 8 25 64 13 32 27 64	.976 1.02 1.06 1.10	.996 1.04 1.08 1.12	1.02 1.06 1.10 1.14	1.04 1.08 1.12 1.17	1.06 1.10 1.14 1.19	1.08 1.12 1.17 1.21	1.10 1.14 1.19 1.23	1.12 1.16 1.21 1.26	15.30 15.94 16.58 17.21
7 16 29 64 15 32 31 64	1.14 1.18 1.22 1.26	1.16 1.20 1.25 1.29	1.19 1.23 1.27 1.31	1.21 1.25 1.30 1.34	1.23 1.28 1.32 1.36	1.26 1.30 1.35 1.39	1.28 1.32 1.37 1.42	1.30 1.35 1.40 1.44	17.85 18.49 19.13 19.76
12 33 64 132 355 64 9	1.30 1.34 1.38 1.42 1.46	1.33 1.37 1.41 1.45 1.49	1.35 1.40 1.44 1.48 1.52	1.38 1.42 1.47 1.51 1.55	1.41 1.45 1.50 1.54 1.58	1.43 1.48 1.52 1.57 1.61	1.46 1.51 1.55 1.60 1.64	1.49 1.53 1.58 1.63 1.67	20.40 21.04 21.68 22.31 22.95

Pounds per Lineal Foot.

									1
Thickness in Inches.	57''	29//	59//	15"	61//	31"	63"	1"	12"
16 5 64 3 3 7 64	.189 .237 .284 .331	.193 .241 .289 .337	.196 .245 .294 .343	.199 .249 .299 .349	.203 .253 .304 .354	.206 .257 .309 .360	.209 .262 .314 .366	.213 .266 .319 .372	2.55 3.19 3.83 4.46
64 5 32 11 64	.379 .426 .473 .520	.385 .433 .481 .529	.392 .441 .490 .538	.398 .448 .498 .548	.405 .456 .506 .557	.412 .463 .515 .566	.418 .471 .523 .575	.425 .478 .531 .584	5.10 5.74 6.38 7.01
3 16 13 64 7 22 15	.568 .615 .662 .710	.578 .626 .674 .722	.588 .637 .686 .735	.598 .648 .697 .747	.608 .658 .709	.618 .669 .721 .772	.628 .680 .732 .784	.638 .691 .744 .797	7.65 8.29 8.93 9.56
17 64 9 32 19 64	.757 .804 .852 .899	.770 .818 .867 .915	.784 .833 .882 .931	.797 .847 .896 .946	.810 .861 .911 .962	.823 .875 .926 .978	.837 .889 .941 .994	.850 .903 .956 1.01	10.20 10.84 11.48 12.11
5 16 21 64 11 32 23 64	.946 .994 1.04 1.09	.963 1.01 1.06 1.11	.980 1.03 1.08 1.13	.996 1.05 1.10 1.15	1.01 1.06 1.11 1.17	1.03 1.08 1.13 1.18	1.05 1.10 1.15 1.20	1.06 1.12 1.17 1.22	12.75 13.39 14.03 14.66
38 25 64 132 24	1.14 1.18 1.23 1.28	1.16 1.20 1.25 1.30	1.18 1.22 1.27 1.32	1.20 1.25 1.30 1.35	1.22 1.27 1.32 1.37	1.24 1.29 1.34 1.39	1.26 1.31 1.36 1.41	1.28 1.33 1.38 1.43	15.30 15.94 16.58 17.21
7 16 29 64 132 84	1.33 1.37 1.42 1.47	1.35 1.40 1.44 1.49	1.37 1.42 1.47 1.52	1.40 1.44 1.49 1.54	1.42 1.47 1.52 1.57	1.44 1.49 1.54 1.60	1.46 1.52 1.57 1.62	1.49 1.54 1.59 1.65	17.85 18.49 19.13 19.76
102 8 4 103 6 4 103 103 104 105 105 105 105 105 105 105 105 105 105	1.51 1.56 1.61 1.66 1.70	1.54 1.59 1.64 1.69 1.73	1.57 1.62 1.67 1.71 1.76	1.59 1.64 1.69 1.74 1.79	1.62 1.67 1.72 1.77 1.82	1.65 1.70 1.75 1.80 1.85	1.67 1.73 1.78 1.83 1.88	1.70 1.75 1.81 1.86 1.91	20.40 21.04 21.68 22.31 22.95

#### Pounds per Lineal Foot.

One cubic foot of steel weighs 489.6 pounds. For Thicknesses from  $\chi_{5}^{1}$  in. to 2 ins. and Widths from 1 in. to 12¾ ins.

Thickness in Inches.	1"	11/4"	112"	13"	2"	21"	2½"	23"	12"
16 16 2 8 3 16 1	.213 .425 .638 .850	.266 .531 .797 1.06	.319 .638 .956 1.28	.372 .744 1.12 1.49	.425 .850 1.28 1.70	.478 .956 1.43 1.91	.531 1.06 1.59 2.13	.584 1.17 1.75 2.34	2.55 5.10 7.65 10.20
* 16 3 8 7 16	1.06 1.28 1.49 1.70	1.33 1.59 1.86 2.13	1.59 1.91 2.23 2.55	1.86 2.23 2.60 2.98	2.13 2.55 2.98 3.40	2.39 2.87 3.35 3.83	2.66 3.19 3.72 4.25	2.92 3.51 4.09 4.68	12.75 15.30 17.85 20.40
9 16 5 8 11 16 3 4	1.91 2.13 2.34 2.55	2.39 2.66 2.92 3.19	2.87 3.19 3.51 3.83	3.35 3.72 4.09 4.46	3.83 4.25 4.68 5.10	4.30 4.78 5.26 5.74	4.78 5.31 5.84 6.38	5.26 5.84 6.43 7.01	22.95 25.50 28.05 30.60
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.76 2.98 3.19 3.40	3.45 3.72 3.98 4.25	4.14 4.46 4.78 5.10	4.83 5.21 5.58 5.95	5.53 5.95 6.38 6.80	6.22 6.69 7.17 7.65	6.91 7.44 7.97 8.50	7.60 8.18 8.77 9.35	33.15 35.70 38.25 40.80
1 1 6 1 8 1 8 1 1 6 1 1 4	3.61 3.83 4.04 4.25	4.52 4.78 5.05 5.31	5.42 5.74 6.06 6.38	6.32 6.69 7.07 7.44	7.23 7.65 8.08 8.50	8.13 8.61 9.08 9.56	9.03 9.56 10.09 10.63	9.93 10.52 11.10 11.69	43.35 45.90 48.45 51.00
$ \begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array} $	4.46 4.68 4.89 5.10	5.58 5.84 6.11 6.38	6.69 7.01 7.33 7.65	7.81 8.18 8.55 8.93	8.93 9.35 9.78 10.20	10.04 10.52 11.00 11.48	11.16 11.69 12.22 12.75	12.27 12.86 13.44 14.03	53.55 56.10 58.65 61.20
$ \begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4} \end{array} $	5.31 5.53 5.74 5.95	6.64 6.91 7.17 7.44	7.97 8.29 8.61 8.93	9.30 9.67 10.04 10.41	10.63 11.05 11.48 11.90	11.95 12.43 12.91 13.39	13.28 13.81 14.34 14.88	14.61 15.19 15.78 16.36	63.75 66.30 68.85 71.40
1 <sup>13</sup> / <sub>16</sub> 1 <sup>7</sup> / <sub>8</sub> 1 <sup>15</sup> / <sub>16</sub>	6.16 6.38 6.59 6.80	7.70 7.97 8.23 8.50	9.24 9.56 9.88 10.20	10.78 11.16 11.53 11.90	12.33 12.75 13.18 13.60	13.87 14.34 14.82 15.30	15.41 15.94 16.47 17.00	16.95 17.53 18.12 18.70	73.95 76.50 79.05 81.60

### Pounds per Lineal Foot.

-									1
Thickness in Inches.	3"	31"	31/2	33"	4"	44"	41"	43"	12"
16 3 16	.638	.691	.744	.797	.850	.903	.956	1.01	2.55
	1.28	1.38	1.49	1.59	1.70	1.81	1.91	2.20	5.10
	1.91	2.07	2.23	2.39	2.55	2.71	2.87	3.03	7.65
	2.55	2.76	2.98	3.19	3.40	3.61	3.83	4.04	10.20
5 16 3 8 7 16	3.19 3.83 4.46 5.10	3.45 4.14 4.83 5.53	3.72 4.46 5.21 5.95	3.98 4.78 5.58 6.38	4.25 5.10 5.95 6.80	4.52 5.42 6.32 7.22	4.78 5.74 6.69 7.65	5.05 6.06 7.07 8.08	12.75 15.30 17.85 20.40
16 5 8 11 13 3	5.74 6.38 7.01 7.65	6.22 6.91 7.60 8.29	6.69 7.44 8.18 8.93	7.17 7.97 8.77 9.56	7.65 8.50 9.35 10.20	8.13 9.03 9.93 10.84	8.61 9.56 10.52 11.48	9.08 10.09 11.10 12.11	22 95 25.50 28.05 30.60
13 16 7 8 15 15 16	8.29 8.93 9.56 10.20	8.98 9.67 10.36 11.05	9.67 10.41 11.16 11.90	10.36 11.16 11.95 12.75	11.05 11.90 12.75 13.60	11.74 12.64 13.55 14.45	12.43 13.39 14.34 15.30	13.12 14.13 15.14 16.15	33.15 35.70 38.25 40.80
1 1 8 1 1 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10.84	11.74	12.64	13.55	14.45	15.35	16.26	17.16	43.35
	11.48	12.43	13.39	14.34	15.30	16.26	17.21	18.17	45.90
	12.11	13.12	14.13	15.14	16.15	17.16	18.17	19.18	48.45
	12.75	13.81	14.88	15.94	17.00	18.06	19.13	20.19	51.00
1 1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	13.39	14.50	15.62	16.73	17.85	18.97	20.08	21.20	53.55
	14.03	15.19	16.36	17.53	18.70	19.87	21.04	22.21	56.10
	14.66	15.88	17.11	18.33	19.55	20.77	21.99	23.22	58.65
	15.30	16.58	17.85	19.13	20.40	21.68	22.95	24.23	61.20
1 ½ 1 ½ 1 ½ 1 ½ 1 ½ 1 ½ 1 ½ 1 ½ 1 ½ 1 ½	15.92	17.27	18.59	19.92	21.25	22.58	23.91	25.23	63.75
	16.58	17.96	19.34	20.72	22.10	23 48	24.86	26.24	66.30
	17.21	18.65	20.08	21.52	22.95	24.38	25.82	27.25	68.85
	17.85	19.34	20.83	22.31	23.80	25.29	26.78	28.26	71.40
1 1 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	18.49	20.03	21.57	23.11	24.65	26.19	27.73	29.27	73.95
	19.13	20.72	22.31	23.91	25.50	27.09	28.69	30.28	76.50
	19.76	21.41	23.06	24.70	26.35	28.00	29.64	31.29	79.05
	20.40	22.10	23.80	25.50	27.20	28.90	30.60	32.30	81.60

#### Pounds per Lineal Foot.

Thickness in Inches.	5"	51"	51/2"	53"	6"	61"	61"	63"	12"
16 18 3 16 4	1.06 2.13 3.19 4.25	1.12 2.23 3.35 4.46	1.17 2.34 3.51 4.68	1.22 2.44 3.67 4.89	1.28 2.55 3.83 5.10	1.33 2.66 3.98 5.31	1.38 2.76 4.14 5.53	1.43 2.87 4.30 5.74	2.55 5.10 7.65 10.20
5 16 3 8 7 16	5.31 6.38 7.44 8.50	5.58 6.69 7.81 8.93	5.84 7.01 8.18 9.35	6.11 7.33 8.55 9.78	6.38 7.65 8.93 10.20	6.64 7.97 9.30 10.63	6.91 8.29 9.67 11.05	7.17 8.61 10.04 11.48	12.75 15.30 17.85 20.40
9 16 5 8 11 16 3	9.56 10.63 11.69 12.75	10.04 11.16 12.27 13.39	10.52 11.69 12.86 14.03	11.00 12.22 13.44 14.67	11.48 12.75 14.03 15.30	11.95 13.28 14.61 15.94	12.43 13.81 15.19 16.58	12.91 14.34 15.78 17.21	22.95 25.50 28.05 30.60
13 16 7 8 15 16	13.81 14.88 15.94 17.00	14.50 15.62 16.73 17.85	15.19 16.36 17.53 18.70	15.88 17.11 18.33 19.55	16.58 17.85 19.13 20.40	17.27 18.59 19.92 21.25	17.96 19.34 20.72 22.10	18.65 20.08 21.52 22.95	33.15 35.70 38.25 40.80
1 1 6 1 8 1 3 1 6 1 1 4	18.06 19.13 20.19 21.25	18.97 20.08 21.20 22.31	19.87 21.04 22.21 23.38	20.77 21.99 23.22 24.44	21.68 22.95 24.23 25.50	22.58 23.91 25.23 26.56	23.48 24.86 26.24 27.63	24.38 25.82 27.25 28.69	43.35 45.90 48.45 51.00
$ \begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array} $	22.31 23.38 24.44 25.50	23.43 24.54 25.66 26.78	24.54 25.71 26.88 28.05	25.66 26.88 28.10 29.33	26.78 28.05 29.33 30.60	27.89 29.22 30.55 31.88	29.01 30.39 31.77 33.15	30.12 31.56 32.99 34.43	53.55 56.10 58.65 61.20
$\begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4} \end{array}$	26.56 27.63 28.69 29.75	27.89 29.01 30.12 31.24	29.22 30.39 31.56 32.73	30.55 31.77 32.99 34.21	31.88 33.15 34.43 35.70	33.20 34.53 35.86 37.19	34.53 35.91 37.29 88.68	35.86 37.29 38.73 40.16	63.75 66.30 68.85 71.40
1 <sup>13</sup> / <sub>16</sub> 1 <sup>7</sup> / <sub>8</sub> 1 <sup>15</sup> / <sub>16</sub> 2	30.81 31.88 32.94 34.00	32.35 33.47 34.58 35.70	33.89 35.06 36.23 37.40	35.43 36.66 37.88 39.10	36.98 38.25 39.53 40.80	38.52 39.84 41.17 42.50	40.06 41.44 42.82 44.20	41.60 43.03 44.47 45.90	73.95 76.50 79.05 81.60

### Pounds per Lineal Foot.

Thickness in Inches.	7"	71"	$7\frac{1}{2}''$	73"	8"	81"	81/	83"	12"
16	1.49	1.54	1.59	1.65	1.70	1.75	1.81	1.86	2.55
18	2.98	3.08	3.19	3.29	3.40	3.51	3.61	3.72	5.10
3	4.46	4.62	4.78	4.94	5.10	5.26	5.42	5.58	7.65
16	5.95	6.16	6.38	6.59	6.80	7.01	7.23	7.44	10.20
5 16 3 8 7 16 12	7.44 8.93 10.41 11.90	7.70 9.24 10.78 12.33	7.97 9.56 11.16 12.75	8.23 9.88 11.53 13.18	8.50 10.20 11.90 13.60	8.77 10.52 12.27 14.03	9.03 10.84 12.64 14.45	9.30 11.16 13.02 14.88	12.75 15.30 17.85 20.40
9 16 5 8 11 16 3	13.39 14.88 16.36 17.85	13.87 15.41 16.95 18.49	14.34 15.94 17.53 19.13	14.82 16.47 18.12 19.76	15.30 17.00 18.70 20.40	15.78 17.53 19.28 21.04	16.26 18.06 19.87 21.68	16.73 18.59 20.45 22.31	22.95 25.50 28.05 30.60
13 16 7 8 15 16	19.34 20.83 22.31 23.80	20.03 21.57 23.11 24.65	20.72 22.31 23.91 25.50	21.41 23.06 24.70 26.35	22.10 23.80 25.50 27.20	22.79 24.54 26.30 28.05	23.48 25.29 27.09 28.90	24.17 26.03 27.89 29.75	33.15 35.70 38.25 40.80
$ \begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $	25.29	26.19	27.09	28.00	28.90	29.80	30.71	31.61	43.35
	26.78	27.73	28.69	29.64	30.60	31.56	32.51	33.47	45.90
	28.26	29.27	30.28	31.29	32.30	33.31	34.32	35.33	48.45
	29.75	30.81	31.88	32.94	34.00	35.06	36.13	37.19	51.00
$ \begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array} $	31.24	32.35	33.47	34.58	35.70	36.82	37.93	39.05	53.55
	32.73	33.89	35.06	36.23	37.40	38.57	39.74	40.91	56.10
	34.21	35.43	36.66	37.88	39.10	40.32	41.54	42.77	58.65
	35.70	36.98	38.25	39.53	40.80	42.08	43.35	44.63	61.20
$ \begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4} \end{array} $	37.19	38.52	39.84	41.17	42.50	43.83	45.16	46.48	63.75
	38.68	40.06	41.44	42.82	44.20	45.58	46.96	48.34	66.30
	40.16	41.60	43.03	44.47	45.90	47.33	48.77	50.20	68.85
	41.65	43.14	44.63	46.11	47.60	49.09	50.58	52.06	71.40
$ \begin{array}{c} 1\frac{13}{16} \\ 1\frac{7}{8} \\ 1\frac{15}{16} \\ 2 \end{array} $	43.14	44.68	46.22	47.76	49.30	50.84	52.38	53.92	73.95
	44.63	46.22	47.81	49.41	51.00	52.59	54.19	55.78	76.50
	46.11	47.76	49.41	51.05	52.70	54.35	55.99	57.64	79.05
	47.60	49.30	51.00	52.70	54.40	56.10	57.80	59.50	81.60

### Pounds per Lineal Foot.

Thickness in Inches.	9"	91"	$9\frac{1}{2}''$	93"	10"	101/4	101/2"	103"	12"
1 16 1 8 3 16 1	1.91 3.83 5.74 7.65	1.97 3.93 5.90 7.86	2.02 4.04 6.06 8.08	2.07 4.15 6.22 8.29	2.13 4.25 6.38 8.50	2.18 4.36 6.53 8.71	2.23 4.46 6.69 8.93	2.28 4.57 6.85 9.14	2.55 5.10 7.65 10.20
5 16 3 8 7 16 12	9.56 11.48 13.39 15.30	9.83 11.79 13.76 15.73	10.09 12.11 14.13 16.15	10.36 12.43 14.50 16.58	10.63 12.75 14.88 17.00	10.89 13.07 15.25 17.43	11.16 13.39 15.62 17.85	11.42 13.71 15.99 18.28	12.75 15.30 17.85 20.40
9 16 5 8 11 16 3	17.21 19.13 21.04 22.95	17.69 19.66 21.62 23.59	18.17 20.19 22.21 24.23	18.65 20.72 22.79 24.86	19.13 21.25 23.38 25.50	19.60 21.78 23.96 26.14	20.08 22.31 24.54 26.78	20.56 22.84 25.13 27.41	22.95 25.50 28.05 30.60
13 16 7 8 15 16	24.86 26.78 28.69 30.60	25.55 27.52 29.48 31.45	26.24 28.26 30.28 32.30	26.93 29.01 31.08 33.15	27.63 29.75 31.88 34.00	28.32 30.49 32.67 34.85	29.01 31.24 33.47 35.70	29.70 31.98 34.27 36.55	33.15 35.70 38.25 40.80
$ \begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $	32.51 34.43 36.34 38.25	33.42 35.38 37.35 39.31	34.32 36.34 38.36 40.38	35.22 37.29 39.37 41.44	36.13 38.25 40.38 42.50	37.03 39.21 41.38 43.56	37.93 40.16 42.39 44.63	38.83 41.12 43.40 45.69	43.35 45.90 48.45 51.00
$ \begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array} $	40.16 42.08 43.99 45.90	41.28 43.24 45.21 47.18	42.39 44.41 46.43 48.45	43.51 45.58 47.65 49.73	44.63 46.75 48.88 51.00	45.74 47.92 50.10 52.28	46.86 49.09 51.32 53.55	47.97 50.26 52.54 54.83	53.55 56.10 58.65 61.20
$ \begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4} \end{array} $	47.81 49.73 51.64 53.55	49.14 51.11 53.07 55.04	50.47 52.49 54.51 56.53	51.80 53.87 55.94 58.01	53.13 55.25 57.38 59.50	54.45 56.63 58.81 60.99	55.78 58.01 60.24 62.48	57.11 59.39 61.68 63.96	63.75 66.30 68.85 71.40
$\begin{array}{c} 1\frac{13}{16} \\ 1\frac{7}{8} \\ 1\frac{15}{16} \\ 2 \end{array}$	55.46 57.38 59.29 61.20	57.00 58.97 60.93 62.90	58.54 60.56 62.58 64.60	60.08 62.16 64.23 66.30	61.63 63.75 65.88 68.00	63.17 65.34 67.52 69.70	64.71 66.94 69.17 71.40	66.25 68.53 70.82 73.10	73.95 76.50 79.05 81.60

### Pounds per Lineal Foot.

(CONCLUDED.)

Thick- ness in Inches.	11"	1114"	1112"	113"	12"	121"	$12\frac{1}{2}"$	123"
16 18 3 16 14	2.34 4.68 7.01 9.35	2.39 4.78 7.17 9.56	2.44 4.89 7.33 9.78	2.50 4.99 7.49 9.99	2.55 5.10 7.65 10.20	2.60 5.21 7.81 10.41	2.66 5.31 7.97 10.63	2.71 5.42 8.13 10.84
5 16. 3 8 7 16	11.69 14.03 16.36 18.70	11.95 14.34 16.73 19.13	12.22 14.66 17.11 19.55	12.48 14.98 17.48 19.98	12.75 15.30 17.85 20.40	13.02 15.62 18.22 20.83	13.28 15.94 18.59 21.25	13.55 16.26 18.97 21.68
9 16 5 8 11 16	21.04 23.38 25.71 28.05	21.52 23.91 26.30 28.69	21.99 24.44 26.88 29.33	22.47 24.97 27.47 29.96	22.95 25.50 28.05 30.60	23.43 26.03 28.63 31.24	23.91 26.56 29.22 31.88	24.38 27.09 29.80 32.51
13 16 78 15 15	30.39 32.73 35.06 37.40	31.08 33.47 35.86 38.25	31.77 34.21 36.66 39.10	32.46 34.96 37.45 39.95	33.15 35.70 38.25 40.80	33.84 36.44 39.05 41.65	34.53 37.19 39.84 42.50	35.22 37.93 40.64 43.35
1 1 1 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	39.74 42.08 44.41 46.75	40.64 43.03 45.42 47.81	41.54 43.99 46.43 48.88	42.45 44.94 47.44 49.94	43.35 45.90 48.45 51.00	44.25 46.86 49.46 52.06	45.16 47.81 50.47 53.13	46.06 48.77 51.48 54.19
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	49.09 51.43 53.76 56.10	50.20 52.59 54.98 57.38	51.32 53.76 56.21 58.65	52.43 54.93 57.43 59.93	53.55 56.10 58.65 61.20	54.67 57.27 59.87 62.48	55.78 58.44 61.09 63.75	56.90 59.61 62.32 65.03
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	58.44 60.78 63.11 65.45	59.77 62.16 64.55 66.94	61.09 63.54 65.98 68.43	62.42 64.92 67.42 69.91	63.75 66.30 68.85 71.40	65.08 67.68 70.28 72.89	66.41 69.06 71.72 74.38	67.73 70.44 73.15 75.86
113 1 18 1 15 1 15 2	67.79 70.13 72.46 74.80	69.33 71.72 74.11 76.50	70.87 73.31 75.76 78.20	72.41 74.91 77.40 79.90	73.95 76.50 79.05 81.60	75.49 78.09 80.70 83.30	77.03 79.69 82.34 85.00	78.57 81.28 83.99 86.70

For Diameters from  $\frac{1}{10}$  to 100, advancing by Tenths.

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
0.0 .1 .2 .3 .4	.007854 .031416 .070686 .12566	.31416 .62832 .94248 1.2566	4.0 .1 .2 3 .4	12.5664 13.2025 13.8544 14.5220 15.2053	12.5664 12.8805 13.1947 13.5088 13.8230
.5 .6 .7 .8	.19635 .28274 .38485 .50265 .63617	1.5708 1.8850 2.1991 2.5133 2.8274	.5 .6 .7 .8	15.9043 16.6190 17.3494 18.0956 18.8574	14.1372 14.4513 14.7655 15.0796 15.3938
1.0 .1 .2 .3 .4	.7854 .9503 1.1310 1.3273 1.5394	3.1416 3.4558 3.7699 4.0841 4.3982	5.0 .1 .2 .3 .4	19.6350 20.4282 21.2372 22.0618 22.9022	15.7080 16.0221 16.3363 16.6504 16.9646
.5 .6 .7 .8	1.7671 2.0106 2.2698 2.5447 2.8353	4.7124 5.0265 5.3407 5.6549 5.9690	.5 .6 .7 .8 .9	23.7583 24.6301 25.5176 26.4208 27.3397	17.2788 17.5929 17.9071 18.2212 18.5354
2.0 .1 .2 .3	3.1416 3.4636 3.8013 4.1548 4.5239	6.2832 6.5973 6.9115 7.2257 7.5398	6.0 .1 .2 .3 .4	28.2743 29.2247 30.1907 31.1725 32.1699	18.8496 19.1637 19.4779 19.7920 20.1062
.5 .6 .7 .8	4.9087 5.3093 5.7256 6.1575 6.6052	7.8540 8.1681 8.4823 8.7965 9.1106	.5 .6 .7 .8	33.1831 34.2119 35.2565 36.3168 37.3928	20.4204 20.7345 21.0487 21.3628 21.6770
3.0 .1 .2 .3 .4	7.0686 7.5477 8.0425 8.5530 9.0792	9.4248 9.7389 10.0531 10.3673 10.6814	7.0 .1 .2 .3 .4	38.4845 39.5919 40.7150 41.8539 43.0084	21.9911 22.3053 22.6195 22.9336 23.2478
.5 .6 .7 .8	9.6211 10.1788 10.7521 11.3411 11.9459	10.9956 11.3097 11.6239 11.9381 12.2522	.5 .6 .7 .8	44.1786 45.3646 46.5663 47.7836 49.0167	23.5619 23.8761 24.1903 24.5044 24.8186

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
8.0 .1 .2 .3 .4	50.2655 51.5300 52.8102 54.1061 55.4177	25.1327 25.4469 25.7611 26.0752 -26.3894	12.0 .1 .2 .3 .4	113.0973 114.9901 116.8987 118.8229 120.7628	37.6991 38.0133 38.3274 38.6416 38.9557
.5 .6 .7 .8	56.7450 58.0880 59.4468 60.8212 62.2114	26.7035 27.0177 27.3319 27.6460 27.9602	.5 .6 .7 .8	122.7185 124.6898 126.6769 128.6796 130.6981	39.2699 39.5841 39.8982 40.2124 40.5265
9.0 .1 .2 .3 .4	63.6173 65.0388 66.4761 67.9291 69.3978	28.2743 28.5885 28.9027 29.2168 29.5310	13.0 .1 .2 .3 .4	132.7323 134.7822 136.8478 138.9291 141.0261	40.8407 41.1549 41.4690 41.7832 42.0973
.5 .6 .7 .8	70.8822 72.3823 73.8981 75.4296 76.9769	29.8451 30.1593 30.4734 30.7876 31.1018	.5 .6 .7 .8	143.1388 145.2672 147.4114 149.5712 151.7468	42.4115 42.7257 43.0398 43.3540 43.6681
10.0 .1 .2 .3 .4	78.5398 80.1185 81.7128 83.3229 84.9487	31.4159 31.7301 32.0442 32.3584 32.6726	14.0 .1 .2 .3 .4	153.9380 156.1450 158.3677 160.6061 162.8602	43.9823 44.2965 44.6106 44.9248 45.2389
.5 .6 .7 .8	86.5901 88.2473 89.9202 91.6088 93.3132	32.9867 33.3009 33.6150 33.9292 34.2434	.5 .6 .7 .8	165.1300 167.4155 169.7167 172.0336 174.3662	45.5531 45.8673 46.1814 46.4956 46.8097
11.0 .1 .2 .3 .4	95.0332 96.7689 98.5203 100.2875 102.0703	34.5575 34.8717 35.1858 35.5000 35.8142	15.0 .1 .2 .3 .4	176.7146 179.0786 181.4584 183.8539 186.2650	47.1239 47.4380 47.7522 48.0664 48.3805
.5 .6 .7 .8	103.8689 105.6832 107.5132 109.3588 111.2202	36.1283 36.4425 36.7566 37.0708 37.3850	.5 .6 .7 .8	188.6919 191.1345 193.5928 196.0668 198.5565	48.6947 49.0088 49.3230 49.6372 49.9513

Diameter.	Area.	Circumference.	Diameter.	Area,	Circumference.
16.0 .1 .2 .3 .4	201.0619 203.5831 206.1199 208.6724 211.2407	50.2655 50.5796 50.8938 51.2080 51.5221	20.0 .1 .2 .3 .4	314.1593 317.3087 320.4739 323.6547 326.8513	62.8319 63.1460 63.4602 63.7743 64.0885
.5 .6 .7 .8	213.8246 216.4243 219.0397 221.6708 224.3176	51.8363 52.1504 52.4646 52.7788 53.0929	.5 .6 .7 .8	330.0636 333.2916 336.5353 339.7947 343.0698	64.4026 64.7168 65.0310 65.3451 65.6593
17.0 .1 .2 .3 .4	226.9801 229.6583 232.3522 235.0618 237.7871	53.4071 53.7212 54.0354 54.3496 54.6637	21.0 .1 .2 .3 .4	346.3606 349.6671 352.9893 356.3273 359.6809	65.9734 66.2876 66.6018 66.9159 67.2301
.5 .6 .7 .8	240.5282 243.2849 246.0574 248.8456 251.6494	54.9779 55.2920 55.6062 55.9203 56.2345	.5 .6 .7 .8	363.0503 366.4354 369.8361 373.2526 376.6848	67.5442 67.8584 68.1726 68.4867 68.8009
18.0 .1 .2 .3 .4	254.4690 257.3043 260.1553 263.0220 265.9044	56.5487 56.8628 57.1770 57.4911 57.8053	22.0 .1 .2 .3 .4	380.1327 383.5963 387.0756 390.5707 394.0814	69.1150 69.4292 69.7434 70.0575 70.3717
.5 .6 .7 .8	268.8025 271.7163 274.6459 277.5911 280.5521	58.1195 58.4336 58.7478 59.0619 59.3761	.5 .6 .7 .8	397.6078 401.1500 404.7078 408.2814 411.8706	70.6858 71.0000 71.3142 71.6283 71.9425
19.0 .1 .2 .3 .4	283.5287 286.5211 289.5292 292.5530 295.5925	59.6903 60.0044 60.3186 60.6327 60.9469	23.0 .1 .2 .3 .4	415.4756 419.0963 422.7327 426.3848 430.0526	72.2566 72.5708 72.8849 73.1991 73.5133
.5 .6 .7 .8	298.6477 301.7186 304.8052 307.9075 311.0255	61.2611 61.5752 61.8894 62.2035 62.5177	.5 .6 .7 .8	433.7361 437.4354 441.1503 444.8809 448.6273	73.8274 74.1416 74.4557 74.7699 75.0841

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.		
24.0 .1 .2 .3 .4	452.3893 456.1671 459.9606 463.7698 467.5946	75.3982 75.7124 76.0265 76.3407 76.6549	28.0 .1 .2 .3 .4	615.7522 620.1582 624.5800 629.0175 633.4707	87.9646 88.2788 88.5929 88.9071 89.2212		
.5 .6 .7 .8	471.4352 475.2916 479.1636 483.0513 486.9547	76.9690 77.2832 77.5973 77.9115 78.2257	.5 .6 .7 .8	637.9397 642.4243 646.9246 651.4406 655.9724	89.5354 89.8495 90.1637 90.4779 90.7920		
25.0 .1 .2 .3 .4	490.8739 494.8087 498.7592 502.7255 506.7075	78.5398 78.8540 79.1681 79.4823 79.7965	29.0 .1 .2 .3 .4	660.5199 665.0830 669.6619 674.2565 678.8668	91.1062 91.4203 91.7345 92.0487 92.3628		
.5 .6 .7 .8	510.7052 514.7185 518.7476 522.7924 526.8529	80.1106 80.4248 80.7389 81.0531 81.3672	.5 .6 .7 .8	683.4927 688.1345 692.7919 697.4650 702.1538	92.6770 92.9911 93.3053 93.6195 93.9336		
26.0 .1 .2 .3 .4	530.9292 535.0211 539.1287 543.2521 547.3911	81.6814 81.9956 82.3097 82.6239 82.9380	30.0 .1 .2 .3 .4	706.8583 711.5786 716.3145 721.0662 725.8336	94.2478 94.5619 94.8761 95.1903 95.5044		
.5 .6 .7 .8	551.5459 555.7163 559.9025 564.1044 568.3220	83.2522 83.5664 83.8805 84.1947 84.5088	.5 .6 .7 .8	730.6167 735.4154 740.2299 745.0601 749.9060	95.8186 96.1327 96.4469 96.7611 97.0752		
27.0 .1 .2 .3 .4	572.5553 576.8043 581.0690 585.3494 589.6455	84.8230 85.1372 85.4513 85.7655 86.0796	31.0 .1 .2 .3 .4	754.7676 759.6450 764.5380 769.4467 774.3712	97.3894 97.7035 98.0177 98.3319 98.6460		
.5 .6 .7 .8	593.9574 598.2849 602.6282 606.9871 611.3618	86.3938 86.7080 87.0221 87.3363 87.6504	.5 .6 .7 .8	779.3113 784.2672 789.2388 794.2260 799.2290	98.9602 99.2743 99.5885 99.9026 100.2168		

Diameter.	Area.	Gircumfarenca.	Diameter.	Area	Circumference.
32.0 .1 .2 .3 .4	804.2477 809.2821 814.3322 819.3980 824.4796	100.5310 100.8451 101.1593 101.4734 101.7876	36.0 .1 .2 .3 .4	1017.8760 1023.5387 1029.2172 1034.9113 1040.6211	113.0973 113.4115 113.7257 114.0398 114.3540
.5 .6 .7 .8	829.5768 834.6897 839.8184 844.9628 850.1229	102.1018 102.4159 102.7301 103.0442 103.3584	.5 .6 .7 .8	1046.3467 1052.0880 1057.8449 1063.6176 1069.4060	114.6681 114.9823 115.2965 115.6106 115.9248
33.0 .1 .2 .3 .4	855,2986 860,4902 865,6973 870,9202 876,1588	103.6726 103.9867 104.3009 104.6150 104.9292	37.0 .1 .2 .3 .4	1075.2101 1081.0299 1086.8654 1092.7166 1098.5835	116.2389 116.5531 116.8672 117.1814 117.4956
.5 .6 .7 .8	881.4131 886.6831 891.9688 897.2703 902.5874	105.2434 105.5575 105.8717 106.1858 106.5000	.5 .6 .7 .8	1104.4662 1110.3645 1116.2786 1122.2083 1128.1538	117.8097 118.1239 118.4380 118.7522 119.0664
34.0 .1 .2 .3 .4	907.9203 913.2688 918.6331 924.0131 929.4088	106.8142 107.1283 107.4425 107.7566 108.0708	38.0 .1 .2 .3 .4	1134.1149 1140.0918 1146.0844 1152.0927 1158.1167	119.3805 119.6947 120.0088 120.3230 120.6372
.5 .6 .7 .8	934.8202 940.2473 945.6901 951.1486 956.6228	108.3849 108.6991 109.0133 109.3274 109.6416	.5 .6 .7 .8 .9	1164.1564 1170.2118 1176.2830 1182.3698 1188.4723	120.9513 121.2655 121.5796 121.8938 122.2080
35.0 .1 .2 .3 .4	962.1127 967.6184 973.1397 978.6768 984.2296	109.9557 110.2699 110.5841 110.8982 111.2124	39.0 .1 .2 .3 .4	1194.5906 1200.7246 1206.8742 1213.0396 1219.2207	122.5221 122.8363 123.1504 123.4646 123.7788
.5 .6 .7 .8	989.7980 995.3822 1000.9821 1006.5977 1012.2290	111.5265 111.8407 112.1549 112.4690 112.7832	.5 .6 .7 .8	1225.4175 1231.6300 1237.8582 1244.1021 1250.3617	124.0929 124.4071 124.7212 125.0354 125.3495

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference
40.0 .1 .2 .3 .4	1256.6371 1262.9281 1269.2348 1275.5573 1281.8955	125.6637 125.9779 126.2920 126.6062 126.9203	44.0 .1 .2 .3 .4	1520.5308 1527.4502 1534.3853 1541.3360 1548.3025	138.2301 138.5442 138.8584 139.1726 139.4867
.5 .6 .7 .8	1288.2493 1294.6189 1301.0042 1307.4052 1313.8219	127.2345 127.5487 127.8628 128.1770 128.4911	.5 .6 · .7 .8	1555.2847 1562.2826 1569.2962 1576.3255 1583.3705	139.8009 140.1150 140.4292 140.7434 141.0575
41.0 .1 .2 .3	1320.2543 1326.7024 1333.1663 1339.6458 1346.1410	128.8053 129.1195 129.4336 129.7478 130.0619	45.0 .1 .2 .3 .4	1590.4313 1597.5077 1604.5999 1611.7077 1618.8313	141.3717 141.6858 142.0000 142.3141 142.6283
.5 .6 .7 .8	1352.6520 1359.1786 1365.7210 1372.2791 1378.8529	130.3761 130.6903 131.0044 131.3186 131.6327	.5 .6 .7 .8	1625.9705 1633.1255 1640.2962 1647.4826 1654.6847	142.9425 143.2566 143.5708 143.8849 144.1991
42.0 .1 .2 .3 .4	1385.4424 1392.0476 1398.6685 1405.3051 1411.9574	131.9469 132.2611 132.5752 132.8894 133.2035	46.0 .1 .2 .3 .4	1661.9025 1669.1360 1676.3852 1683.6502 1690.9308	144.5133 144.8274 145.1416 145.4557 145.7699
.5 .6 .7 .8	1418.6254 1425.3092 1432.0086 1438.7238 1445.4546	133.5177 133.8318 134.1460 134.4602 134.7743	.5 .6 .7 .8	1698.2272 1705.5392 1712.8670 1720.2105 1727.5696	146.0841 146.3982 146.7124 147.0265 147.3407
43.0 .1 .2 .3 .4	1452.2012 1458.9635 1465.7415 1472.5352 1479.3446	135.0885 135.4026 135.7168 136.0310 136.3451	47.0 .1 .2 .3 .4	1734.9445 1742.3351 1749.7414 1757.1634 1764.6012	147.6549 147.9690 148.2832 148.5973 148.9115
.5 .6 .7 .8	1486.1697 1493.0105 1499.8670 1506.7392 1513.6272	136.6593 136.9734 137.2876 137.6018 137.9159	.5 .6 .7 .8	1772.0546 1779.5237 1787.0086 1794.5091 1802.0254	149.2257 149.5398 149.8540 150.1681 150.4823

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference,
48.0 .1 .2 .3 .4	1809.5574 1817.1050 1824.6684 1832.2475 1839.8423	150.7964 151.1106 151.4248 151.7389 152.0531	52.0 .1 .2 .3 .4	2123.7166 2131.8926 2140.0843 2148.2917 2156.5149	163.3628 163.6770 163.9911 164.3053 164.6195
.5 .6 .7 .8	1847.4528 1855.0790 1862.7210 1870.3786 1878.0519	152.3672 152.6814 152.9956 153.3097 153.6239	.5 .6 .7 .8	2164.7537 2173.0082 2181.2785 2189.5644 2197.8661	164.9336 165.2478 165.5619 165.8761 166.1903
49.0 .1 .2 .3 .4	1885.7410 1893.4457 1901.1662 1908.9024 1916.6543	153.9380 154.2522 154.5664 154.8805 155.1947	53.0 .1 .2 .3 .4	2206.1834 2214.5165 2222.8653 2231.2298 2239.6100	166.5044 166.8186 167.1327 167.4469 167.7610
.5 .6 .7 .8	1924.4218 1932.2051 1940.0041 1947.8189 1955.6493	155.5088 155.8230 156.1372 156.4513 156.7655	.5 .6 .7 .8	2248.0059 2256.4175 2264.8448 2273.2879 2281.7466	168.0752 168.3894 168.7035 169.0177 169.3318
50.0 .1 .2 .3 .4	1963.4954 1971.3572 1979.2348 1987.1280 1995.0370	157.0796 157.3938 157.7080 158.0221 158.3363	54.0 .1 .2 .3 .4	2290.2210 2298.7112 2307.2171 2315.7386 2324.2759	169.6460 169.9602 170.2743 170.5885 170.9026
.5 .6 .7 .8	2002.9617 2010.9020 2018.8581 2026.8299 2034.8174	158.6504 158.9646 159.2787 159.5929 159.9071	.5 .6 .7 .8	2332.8289 2341.3976 2349.9820 2358.5821 2367.1979	171.2168 171.5310 171.8451 172.1593 172.4734
51.0 .1 .2 .3 .4	2042.8206 2050.8395 2058.8742 2066.9245 2074.9905	160.2212 160.5354 160.8495 161.1637 161.4779	55.0 .1 .2 .3 .4	2375.8294 2384.4767 2393.1396 2401.8183 2410.5126	172.7876 173.1018 173.4159 173.7301 174.0442
.5 .6 .7 .8	2083.0723 2091.1697 2099.2829 2107.4118 2115.5563	161.7920 162.1062 162.4203 162.7345 163.0487	.5 .6 .7 .8	2419.2227 2427.9485 2436.6899 2445.4471 2454.2200	174.3584 174.6726 174.9867 175.3009 175.6150

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference
56.0 .1 .2 .3 .4	2463.0086 2471.8129 2480.6330 2489.4687 2498.3201	175.9292 176.2433 176.5575 176.8717 177.1858	60.0 .1 .2 .3	2827.4334 2836.8660 2846.3143 2855.7784 2865.2582	188.4956 188.8097 189.1239 189.4380 189.7522
.5 .6 .7 .8	2507.1873 2516.0701 2524.9687 2533.8830 2542.8129	177.5000 177.8141 178.1283 178.4425 178.7566	.5 .6 .7 .8	2874.7536 2884.2648 2893.7917 2903.3343 2912.8925	190.0664 190.3805 190.6947 191.0088 191.3230
57.0 .1 .2 .3 .4	2551.7586 2560.7200 2569.6971 2578.6899 2587.6984	179.0708 179.3849 179.6991 180.0133 180.3274	61.0 .1 .2 .3 .4	2922.4666 2932.0563 2941.6617 2951.2828 2960.9196	191.6372 191.9513 192.2655 192.5796 192.8938
.5 .6 .7 .8	2596.7227 2605.7626 2614.8182 2623.8896 2632.9766	180.6416 180.9557 181.2699 181.5841 181.8982	.5 .6 .7 .8	2970.5722 2980.2404 2989.9244 2999.6241 3009.3394	193.2079 193.5221 193.8363 194.1504 194.4646
58.0 .1 .2 .3 .4	2642.0794 2651.1979 2660.3321 2669.4820 2678.6475	182.2124 182.5265 182.8407 183.1549 183.4690	62.0 .1 .2 .3 .4	3019.0705 3028.8173 3038.5798 3048.3580 3058.1519	194.7787 195.0929 195.4071 195.7212 196.0354
.5 .6 .7 .8	2687.8289 2697.0259 2706.2386 2715.4670 2724.7112	183.7832 184.0973 184.4115 184.7256 185.0398	.5 .6 .7 .8	3067.9616 3077.7869 3087.6279 3097.4847 3107.3571	196.3495 196.6637 196.9779 197.2920 197.6062
59.0 .1 .2 .3	2733.9710 2743.2465 2752.5378 2761.8448 2771.1675	185.3540 185.6681 185.9823 186.2964 186.6106	63.0 .1 .2 .3 .4	3117.2453 3127.1492 3137.0687 3147.0040 3156.9550	197.9203 198.2345 198.5487 198.8628 199.1770
.5 .6 .7 .8	2780.5058 2789.8599 2799.2297 2808.6152 2818.0165	186.9248 187.2389 187.5531 187.8672 188.1814	.5 .6 .7 .8	3166.9217 3176.9041 3186.9023 3196.9161 3206.9456	199.4911 199.8053 200.1195 200.4336 200.7478

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference
64.0 .1 .2 .3 .4	3216.9909 3227.0518 3237.1285 3247.2208 3257.3289	201.0620 201.3761 201.6902 202.0044 202.3186	68.0 .1 .2 .3 .4	3631.6811 3642.3704 3653.0753 3663.7960 3674.5324	213.6283 213.9425 214.2566 214.5708 214.8849
.5 .6 .7 .8	3267.4527 3277.5922 3287.7474 3297.9183 3308.1049	202.6327 202.9469 203.2610 203.5752 203.8894	.5 .6 .7 .8	3685.2845 3696.0523 3706.8358 3717.6351 3728.4500	215.1991 215.5133 215.8274 216.1416 216.4556
65.0 .1 .2 .3 .4	3318.3072 3328.5253 3338.7590 3349.0084 3359.2736	204.2035 204.5177 204.8318 205.1460 205.4602	69.0 .1 .2 .3	3739.2807 3750.1270 3760.9890 3771.8668 3782.7603	216.7699 217.0841 217.3982 217.7124 218.0265
.5 .6 .7 .8	3369.5545 3379.8510 3390.1633 3400.4913 3410.8350	205.7743 206.0885 206.4026 206.7168 207.0310	.5 .6 .7 .8	3793.6695 3804.5944 3815.5349 3826.4913 3837.4633	218.3407 218.6548 218.9690 219.2832 219.5973
66.0 .1 .2 .3 .4	3421.1944 3431.5695 3441.9603 3452.3668 3462.7891	207.3451 207.6593 207.9734 208.2876 208.6017	70.0 .1 .2 .3 .4	3848.4510 3859.4544 3870.4735 3881.5084 3892.5589	219.9115 220.2256 220.5398 220.8540 221.1681
.5 .6 .7 .8	3473.2270 3483.6807 3494.1500 3504.6351 3515.1359	208.9159 209.2301 209.5442 209.8584 210.1725	.5 .6 .7 .8	3903.6252 3914.7072 3925.8048 3936.9182 3948.0473	221.4823 221.7964 222.1106 222.4248 222.7389
67.0 .1 .2 .3 .4	3525.6523 3536.1845 3546.7324 3557.2960 3567.8753	210.4867 210.8009 211.1150 211.4292 211.7433	71.0 .1 .2 .3 .4	3959.1921 3970.3526 3981.5288 3992.7208 4003.9284	223.0531 223.3672 223.6814 223.9956 224.3097
.5 .6 .7 .8	3578.4704 3589.0811 3599.7075 3610.3497 3621.0075	212.0575 212.3717 212.6858 213.0000 213.3141	.5 .6 .7 .8	4015.1517 4026.3908 4037.6455 4048.9160 4060.2022	224.6239 224.9380 225.2522 225.5664 225.8805

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
72.0 .1 .2 .3 .4	4071.5041 4082.8216 4094.1549 4105.5039 4116.8687	226.1947 226.5088 226.8230 227.1371 227.4513	76.0 .1 .2 .3 .4	4536.4598 4548.4057 4560.3673 4572.3446 4584.3376	238.7610 239.0752 239.3894 239.7035 240.0177
.5 .6 .7 .8	4128.2491 4139.6452 4151.0570 4162.4846 4173.9278	227.7655 228.0796 228.3938 228.7079 229.0221	.5 .6 .7 .8	4596.3464 4608.3708 4620.4110 4632.4668 4644.5384	240.3318 240.6460 240.9602 241.2743 241.5885
73.0 .1 .2 .3 .4	4185.3868 4196.8615 4208.3518 4219.8579 4231.3797	229.3363 229.6504 229.9646 230.2787 230.5929	77.0 .1 .2 .3 .4	4656.6257 4668.7287 4680.8474 4692.9818 4705.1319	241.9026 242.2168 242.5310 242.8451 243.1592
.5 .6 .7 .8	4242.9172 4254.4704 4266.0393 4277.6240 4289.2243	230.9071 231.2212 231.5354 231.8495 232.1637	.5 .6 .7 .8	4717.2977 4729.4792 4741.6765 4753.8894 4766.1180	243.4734 243.7876 244.1017 244.4159 244.7301
74.0 .1 .2 .3 .4	4300.8403 4312.4721 4324.1195 4335.7827 4347.4616	232.4779 232.7920 233.1062 233.4203 233.7345	78.0 .1 .2 .3 .4	4778.3624 4790.6225 4802.8982 4815.1897 4827.4969	245.0442 245.3584 245.6725 245.9867 246.3009
.5 .6 .7 .8	4359.1562 4370.8664 4382.5924 4394.3341 4406.0915	234.0487 234.3628 234.6770 234.9911 235.3053	.5 .6 .7 .8	4839.8198 4852.1584 4864.5127 4876.8828 4889.2685	246.6150 246.9292 247.2433 247.5575 247.8717
75.0 .1 .2 .3 .4	4417.8647 4429.6535 4441.4580 4453.2783 4465.1142	235.6194 235.9336 236.2478 236.5619 236.8761	79.0 .1 .2 .3 .4	4901.6699 4914.0871 4926.5199 4938.9685 4951.4328	248.1858. 248.5000 248.8141 249.1283 249.4425
.5 .6 .7 .8	4476.9659 4488.8332 4500.7163 4512.6151 4524.5296	237.1902 237.5044 237.8186 238.1327 238.4469	.5 .6 .7 .8	4963.9127 4976.4084 4988.9198 5001.4469 5013.9897	249.7566 250.0708 250.3849 250.6991 251.0133

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
80.0 .1 .2 .3 .4	5026.5482 5039.1224 5051.7124 5064.3180 5076.9394	251.3274 251.6416 251.9557 252.2699 252.5840	84.0 .1 .2 .3 .4	5541.7694 5554.9720 5568.1902 5581.4242 5594.6738	263.8938 264.2079 264.5221 264.8363 265.1504
.5 .6 .7 .8	5089.5764 5102.2292 5114.8977 5127.5818 5140.2817	252.8982 253.2124 253.5265 253.8407 254.1548	.5 .6 .7 .8	5607.9392 5621.2203 5634.5171 5647.8296 5661.1578	265.4646 265.7787 266.0929 266.4071 266.7212
81.0 .1 .2 .3 .4	5152.9973 5165.7286 5178.4756 5191.2384 5204.0168	254.4690 254.7832 255.0973 255.4115 255.7256	85.0 .1 .2 .3 .4	5674.5017 5687.8613 5701.2367 5714.6277 5728.0344	267.0354 267.3495 267.6637 267.9779 268.2920
.5 .6 .7 .8 .9	5216.8109 5229.6208 5242.4463 5255.2876 5268.1446	256.0398 256.3540 256.6681 256.9823 257.2964	.5 .6 .7 .8	5741.4569 5754.8951 5768.3489 5781.8185 5795.3038	268.6062 268.9203 269.2345 269.5486 269.8628
82.0 .1 .2 .3 .4	5281.0172 5293.9056 5306.8097 5319.7295 5332.6650	257.6106 257.9248 258.2389 258.5531 258.8672	86.0 .1 .2 .3 .4	5808.8048 5822.3215 5835.8539 5849.4020 5862.9659	270.1770 270.4911 270.8053 271.1194 271.4336
.5 .6 .7 .8	5345.6162 5358.5832 5371.5658 5384.5641 5397.5782	259.1814 259.4956 259.8097 260.1239 260.4380	.5 .6 .7 .8	5876.5454 5890.1406 5903.7516 5917.3782 5931.0206	271.7478 272.0619 272.3761 272.6902 273.0044
83.0 .1 .2 .3	5410.6079 5423.6534 5436.7146 5449.7914 5462.8840	260.7522 261.0663 261.3805 261.6947 262.0088	87.0 .1 .2 .3 .4	5944.6787 5958.3525 5972.0419 5985.7471 5999.4680	273.3186 273.6327 273.9469 274.2610 274.5752
.5 .6 .7 .8	5475.9923 5489.1163 5502.2560 5515.4115 5528.5826	262.3230 262.6371 262.9513 263.2655 263.5796	.5 .6 .7 .8	6013.2047 6026.9570 6040.7250 6054.5088 6068.3082	274.8894 275.2035 275.5177 275.8318 276.1460

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference
88.0 .1 .2 .3 .4	6082.1234 6095.9542 6109.8008 6123.6631 6137.5410	276.4602 276.7743 277.0885 277.4026 277.7168	92.0 .1 .2 .3	6647.6100 6662.0692 6676.5441 6691.0347 6705.5410	289.0265 289.3407 289.6548 289.9690 290.2832
.5 .6 .7 .8	6151.4347 6165.3441 6179.2692 6193.2101 6207.1666	278.0309 278.3451 278.6593 278.9734 279.2876	.5 .6 .7 .8	6720.0630 6734.6007 6749.1542 6763.7233 6778.3081	290.5978 290.9115 291.2256 291.5398 291.8540
89.0 .1 .2 .3 .4	6221.1388 6235.1268 6249.1304 6263.1498 6277.1848	279.6017 279.9159 280.2301 280.5442 280.8584	93.0 .1 .2 .3 .4	6792.9087 6807.5249 6822.1569 6836.8046 6851.4680	292.1681 292.4823 292.7964 293.1106 293.4248
.5 .6 .7 .8	6291.2356 6305.3021 6319.3843 6333.4822 6347.5958	281.1725 281.4867 281.8009 282.1150 282.4292	.5 .6 .7 .8	6866.1471 6880.8419 6895.5524 6910.2786 6925.0205	293.7389 294.0531 294.3672 294.6814 294.9956
90.0 .1 .2 .3 .4	6361.7251 6375.8701 6390.0308 6404.2073 6418.3994	282.7433 283.0575 283.3717 283.6858 284.0000	94.0 .1 .2 .3	6939.7781 6954.5515 6969.3405 6984.1453 6998.9657	295.3097 295.6239 295.9380 296.2522 296.5663
.5 .6 .7 .8	6432.6073 6446.8308 6461.0701 6475.3251 6489.5958	284.3141 284.6283 284.9425 285.2566 285.5708	.5 .6 .7 .8	7013.8019 7028.6538 7043.5214 7058.4047 7073.3037	296.8805 297.1947 297.5088 297.8230 298.1371
91.0 .1 .2 .3 .4	6503.8822 6518.1843 6532.5021 6546.8356 6561.1848	285.8849 286.1991 286.5132 286.8274 287.1416	95.0 .1 .2 .3 .4	7088.2184 7103.1488 7118.0949 7133.0568 7148.0343	298.4513 298.7655 299.0796 299.3938 299.7079
.5 .6 .7 .8	6575.5497 6589.9304 6604.3267 6618.7388 6633.1666	287.4557 287.7699 288.0840 288.3982 288.7124	.5 .6 .7 .8	7163.0276 7178.0365 7193.0612 7208.1016 7223.1577	300.0221 300.3363 300.6504 300.9646 301.2787

(CONCLUDED.)

Diameter.	Area.	Circumference,	Diameter.	Area.	Circumference.
96.0	7238.2294	301.5929	98.0	7542.9639	307.8761
.1	7253.3169	301.9071	.1	7558.3656	308.1902
.2	7268.4201	302.2212	.2	7573.7830	308.5044
.3	7283.5391	302.5354	.3	7589.2161	308.8186
.4	7298.6737	302.8495	.4	7604.6648	309.1327
.5	7313.8240	303.1637	.5	\$7620.1293	309.4469
.6	7328.9901	303.4779	.6	7635.6095	309.7610
.7	7344.1718	303.7920	.7	7651.1054	310.0752
.8	7359.3693	304.1062	.8	7666.6170	310.3894
.9	7374.5824	304.4203	.9	7682.1443	310.7035
97.0	7389.8113	304.7345	99.0	7697.6874	311.0177
.1	7405.0559	305.0486	.1	7713.2461	311.3318
.2	7420.3162	305.3628	.2	7728.8205	311.6460
.3	7435.5921	305.6770	.3	7744.4107	311.9602
.4	7450.8838	305.9911	.4	7760.0166	312.2743
.5 .6 .7 .8	7466.1913 7481.5144 7496.8532 7512.2077 7527.5780	306.3053 306.6194 306.9336 307.2478 307.5619	.5 .6 .7 .8	7775.6381 7791.2754 7806.9284 7822.5971 7838.2815	312.5885 312.9026 313.2168 313.5309 313.8451
			100.0	7853.9816	314.1593

To find from the table areas or circumferences for larger diameters than those given.

#### CASE I.

For diameters greater than 100 and less than 1001:

Take from the table the area or circumference for a circle the diameter of which is one-tenth of the given diameter.

To obtain the required area or circumference, multiply the area so found by 100 and the circumference so found by 10.

For Example.—What is the area and circumference corresponding to a diameter of 459?

From the tables the area and circumference for diameter 45.9 are 1 654.6847 and 144.1991. Therefore 165 468.47 and 1 441.991 are the area and circumference required.

#### CASE II.

For diameters greater than 1000:

Divide the given diameter by any convenient factor which will give as a quotient a diameter found in the table, and take from the table the area or circumference for this diameter.

To obtain the required area or circumference multiply the area so found by the square of the factor and the circumference so found by the factor.

For Example.-What is the area and circumference corresponding to a

diameter of 1 983?

1 983  $\div$  3 = 661. From the tables and Case I the area and circumference for diameter 661 are 343 156.95 and 2 076.593. Therefore 343 156.95  $\times$  9 = 3 088 412.55 = area required, and 2 076.593  $\times$  3 = 6 229.779 = circumference required.

Diameters  $\frac{1}{16}$  to 100.

Diameter.	Area	Circumference.	Diameter.	Area.	Circumference.
- do - do - de cio - de cojo o o de cio	.0031 .0123 .0491 .1104 .1963 .3068 .4418	.1963 .3927 .7854 1.1781 1.5708 1.9635 2.3562 2.7489	TI PROPERTY OF THE PROPERTY OF	19.6350 20.6290 21.6476 22.6907 23.7583 24.8505 25.9673 27.1086	15.7080 16.1007 16.4934 16.8861 17.2788 17.6715 18.0642 18.4569
	.7854 .9940 1.2272 1.4849 1.7671 2.0739 2.4053 2.7612	3.1416 3.5343 3.9270 4.3197 4.7124 5.1051 5.4978 5.8905		28.2744 29.4648 30.6797 31.9191 33.1831 34.4717 35.7848 37.1224	18.8496 19.2423 19.6350 20.0277 20.4204 20.8131 21.2058 21.5985
কুল কুৰ লাভ কুমেতাত লাকান্ত	3.1416 3.5466 3.9761 4.4301 4.9087 5.4119 5.9396 6.4918	6.2832 6.6759 7.0686 7.4613 7.8540 8.2467 8.6394 9.0321	শ্বিক শ্বিকার্যক শ্বিক্তাক ব্যক্তিক বিশ্বক	38.4846 39.8713 41.2826 42.7184 44.1787 45.6636 47.1731 48.7071	21.9912 22.3839 22.7766 23.1693 23.5620 23.9547 24.3474 24.7401
	7.0686 7.6699 8.2958 8.9462 9.6211 10.3206 11.0447 11.7933	9.4248 9.8175 10.2102 10.6029 10.9956 11.3883 11.7810 12.1737		50.2656 51.8487 53.4563 55.0884 56.7451 58.4264 60.1322 61.8625	25.1328 25.5255 25.9182 26.3109 26.7036 27.0963 27.4890 27.8817
-dood-delente-delente	12.5664 13.3641 14.1863 15.0330 15.9043 16.8002 17.7206 18.6655	12.5664 12.9591 13.3518 13.7445 14.1372 14.5299 14.9226 15.3153	1/30 m(1/1/10)(5 m(1/1/10)(50 c)(1/1/17/10)	63.6174 65.3968 67.2008 69.0293 70.8823 72.7599 74.6621 76.5889	28.2744 28.6671 29.0598 29.4525 29.8452 30.2379 30.6306 31.0233

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
10	78.540 80.516 82.516 84.541 86.590 88.664 90.763 92.886	31.4160 31.8087 32.2014 32.5941 32.9868 33.3795 33.7722 34.1649	15	176.715 179.673 182.655 185.661 188.692 191.748 194.828 197.933	47.1240 47.5167 47.9094 48.3021 48.6948 49.0875 49.4802 49.8729
11	95.033 97.205 99.402 101.623 103.869 106.139 108.434 110.754	34.5576 34.9503 35.3430 35.7357 36.1284 36.5211 36.9138 37.3065	16	201.062 204.216 207.395 210.598 213.825 217.077 220.354 223.655	50,2656 50,6583 51,0510 51,4437 51,8364 52,2291 52,6218 53,0145
12 de rideste ricucio sia rio	113.098 115.466 117.859 120.277 122.719 125.185 127.677 130.192	37.6992 38.0919 38.4846 38.8773 39.2700 39.6627 40.0554 40.4481	17	226.981 230.331 233.706 237.105 240.529 243.977 247.450 250.948	53.4072 53.7999 54.1926 54.5853 54.9780 55.3707 55.7634 56.1561
13 de de sie de	132.733 135.297 137.887 140.501 143.139 145.802 148.490 151.202	40.8408 41.2335 41.6262 42.0189 42.4116 42.8043 43.1970 43.5897	18	254.470 258.016 261.587 265.183 268.803 272.448 276.117 279.811	56.5488 56.9415 57.3342 57.7269 58.1196 58.5123 58.9050 59.2977
	153.938 156.700 159.485 162.296 165.130 167.990 170.874 173.782	43.9824 44.3751 44.7678 45.1605 45.5532 45.9459 46.3386 46.7313	19	283.529 287.272 291.040 294.832 298.648 302.489 306.355 310.245	59.6904 60.0831 60.4758 60.8685 61.2612 61.6539 62.0466 62.4393

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.				
20 শ্রেশ্বকারিশ্রের্লির বিশ্বের্লির বিশ্বর	314.160 318.099 322.063 326.051 330.064 334.102 338.164 342.250	62.8320 63.2247 63.6174 64.0101 64.4028 64.7955 65.1882 65.5809	25 To Adrigo deviction terio	490.875 495.796 500.742 505.712 510.706 515.726 520.769 525.838	78.5400 78.9327 79.3254 79.7181 80.1108 80.5035 80.8962 81.2889				
21	346.361 350.497 354.657 358.842 363.051 367.285 371.543 375.826	65.9736 66.3663 66.7590 67.1517 67.5444 67.9371 68.3298 68.7225	do decino decino de colo de co	530.930 536.048 541.190 546.356 551.547 556.763 562.003 567.267	81.6816 82.0743 82.4670 82.8597 83.2524 83.6451 84.0378 84.4305				
902 नायानीकारायानात्याम् वर्गकाराम्	380.134 384.466 388.322 393.203 397.609 402.038 406.494 410.973	69.1152 69.5079 69.9006 70.2933 70.6860 71.0787 71.4714 71.8641	27 Hond Aniponde volconi Anipo	572.557 577.870 583.209 588.571 593.959 599.371 604.807 610.268	84.8232 85.2159 85.6086 86.0013 86.3940 86.7867 87.1794 87.5721				
PCO priestojo priestojo objetojo	415.477 420.004 424.558 429.135 433.737 438.364 443.015 447.690	72.2568 72.6495 73.0422 73.4349 73.8276 74.2203 74.6130 75.0057	00 02 02	615.754 621.264 626.798 632.357 637.941 643.549 649.182 654.840	87.9648 88.3575 88.7502 89.1429 89.5356 89.9283 90.3210 90.7137				
A miles referencies referencies referencies referencies referencies	452.390 457.115 461.864 466.638 471.436 476.259 481.107 485.979	75.3984 75.7911 76.1838 76.5765 76.9692 77.3619 77.7546 78.1473	29 rejord environessenisonis enviro	660.521 666.228 671.959 677.714 683.494 689.299 695.128 700.982	91.1064 91.4991 91.8918 92.2845 92.6772 93.0699 93.4626 93.8553				

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
30	706.860	94.248	35	962.115	109.956
1	712.763	94.641	1 2	969.000	110.349
ì	718.690	95.033	1	975.909	110.741
3	724.642	95.426	30	982.842	111.134
1	730,618	95.819	1 2	989.800	111.527
5	736.619	96.212	5	996.783	111.919
3	742.645	96.604	3/4	1003.790	112.312
7 8	748.695	96.997	rico pi e cojco rico sejso coj e rico	1010.822	112.705
31	754.769	97.390	36	1017.878	113.098
à	760.869	97.782	1 8	1024.960	113.490
1	766.992.	98.175	1	1032.065	113.883
ā	773.140	98.568	38	1039.195	114.276
rajoo-distrucijoo sajest-jac	779.313	98.960		1046.349	114.668
. 5	785.510	99.353	5/8	1053.528	115.061
3	791.732	99.746	34	1060.732	115.454
78	797.979	100.138	78	1067.960	115.846
32	804.250	100.531	37	1075.213	116.239
18	810.545	100.924	1 8	1082.490	116.632
1	816.865	101.317	40 14 3 a	1089.792	117.025
3	823.210	101.709	38	1097.118	117.417
1/2	829.579	102.102	1 2	1104.469	117.810
do ridenio rigenio nidenia	835.972	102.495	-(cus)cos)-	1111.844	118.203
1	842.391	102.887	3	1119.244	118.595
78	848.833	103.280	78	1126.669	118.988
33	855.301	103.673	38	1134.118	119.381
18	861.792	104.065	ন্ধতা ন্ধুৰংকাতে ন্ধুংখ তোতে কান্ধাংশত	1141.591	119.773
1	868.309	104.458	4	1149.089	120.166
8	874.850	104.851	38	1156.612	120.559
2	881.415	105.244	2	1164.159	120.952
*5 00 m  41-14	888.005	105.636	8	1171.731	121.344
*	894.620	106.029	4	1179.327	121.737
र्ड	901.259	106.422	8	1186.948	122.130
34	907.922	106.814	39	1194.593	122.522
8	914.611	107.207	18 14	1202.263	122.915
. 4	921.323	107.600	4	1209.958	123.308
38	928.061	107.992	3 8	1217.677	123.700
2	934.822	108.385	2	1225.420	124.093
98	941.609	108.778	2/00 0	1233 188	124.486
40 44 300 42 500 34 7 10	948.420	109.171	1 245 80 33 447- 00	1240.981	124.879
8	955.255	109.563	8	1248.798	125.271

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference
40	1256.64	125.664	45	1590.43	141.372
1	1264.51	126.057	1 8	1599.28	141.765
ì	1272.40	126,449	î	1608.16	142.157
3	1280.31	126.842	#3je	1617.05	142,550
do rda color rda color cola	1288.25	127,235	1	1625.97	142.943
5	1296.22	127.627	1,200,000,14	1634.92	143.335
3	1304.21	128.020	3	1643.89	143.728
7	1312.22	128.413	7 8	1652.89	144.121
41	1320.26	128.806	46	1661.91	144,514
18	1328.32	129.198	1	1670.95	144.906
1	1336.41	129.591	1	1680.02	145,299
3	1344.52	129.984	3	1689.11	145,692
i	1352.66	130.376	1	1698.23	146.084
5	1360.82	130.769	5	1707.37	146,477
3	1369.00	131.162	3	1716.54	146.870
color de color de la color de	1377.21	131.554	78	1725.73	147.262
42	1385.45	131.947	47	1734.95	147.655
+	1393.70	132.340	1	1744.19	148.048
1	1401.99	132.733	1	1753.45	148.441
30	1410.30	133.125	3	1762.74	148.833
ž	1418.63	133.518	1	1772.06	149.226
5	1426.99	133.911	5	1781.40	149.619
e-ja asjanske asjes	1435.37	134.303	3	1790.76	150.011
78	1443.77	134.696	rest rest color dos un jos cojes rejo	1800.15	150.404
43	1452.20	135.089	48	1809.56	150.797
1	1460.66	135.481	· ·	1819.00	151.189
-los-l-amin	1469.14	135.874	181438	1828.46	151.582
3	1477.64	136.267	3	1837.95	151.975
1/2	1486.17	136.660	1	1847.46	152.368
5 8	1494.73	137.052	5/0	1856.99	152.760
	1503.30	137.445	-description rejes to the	1866.55	153.153
78	1511.91	137.838	78	1876.14	153.546
44	1520.53	138.230	49	1885.75	153.938
8	1529.19	138.623	18	1895.38	154.331
do 1-t-series	1537.86	139.016	1	1905.04	154.724
1	1546.56	139.408	oju	1914.72	155.116
1/2	1555.29	139.801	1 2	1924.43	155.509
5 8	.1564.04	140.194	58	1934.16	155.902
3 4	1572.81	140.587	ল(০০ ল্বিবাসে(০০ ল(মেস)ত স্ট্রিবান)	1943.91	156.295
7	1581.61	140.979	7	1953.69	156.687

Diameter.	Area.	Circumference.	Diameter.	Area.	· Circumference.	
50	1963.50	157.080	55	2375.83	172.788	
18	1973.33	157.473	1 8	2386.65	173.181	
81	1983.18	157.865		2397.48	173.573	
3	1993.06	158.258	400	2408.34	173.966	
color descripto color el en el ec	2002.97	158.651		2419.23	174.359	
2	2012.89	159.043	1210/00/01/4	2430.14	174.751	
8		159.436	8 3	2441.07	175.144	
4	2022.85			2452.03	175.537	
*	2032.82	159.829	7 8	2402.00	110.001	
51	2042.83	160.222	56	2463.01	175.930	
1	2052.85	160.614	18	2474.02	176.322	
1 1	2062.90	161.007	1	2485.05	176.715	
38	2072.98	161.400	3	2496.11	177.108	
	2083.08	161.792	1	2507.19	177.500	
5	2093.20	162.185	1200	2518.30	177.893	
3	2103.35	162.578	34	2529.43	178.286	
1(245)2000 47- 0	2113.52	162,970	7	2540.58	178,678	
	2110.00	100.010				
52	2123.72	163,363	57	2551.76	179.071	
1	2133.94	163.756	- A	2562.97	179.464	
Į.	2144.19	164,149	1	2574.20	179.857	
3	2154.46	164,541	3	2585.45	180.249	
i	2164.76	164.934	i	2596.73	180.642	
5	2175.08	165.327	5	2608.03	181.035	
3	2185.42	165.719	å	2619.36	181.427	
deD milde color milde color milde color	2195.79	166.112		2630.71	181.820	
53	2206.19	166,505	58	2642.09	182,213	
	2216.61	166.897	4	2653.49	182.605	
. 8	2227.05	167.290	8	2664.91	182.998	
4			4 3	2676.36	183.391	
8	2237.52	167.688	8			
ৰ্ক্তি স্কৃত্ত কাহাত কাহাত হয়	2248.01	168.076	-4-min -40-15-6-7-4	2687.84	183.784	
8	2258.53	168.468	8	2699.33	184.176	
34	2269.07	168.861	4	2710.86	184.569	
8	2279.64	169.254	78	2722.41	184.962	
54	2290.23	169.646	59	2733.98	185.354	
	2300.84	170.039	1	2745.57	185.747	
1	2311.48	170.432	1	2757.20	186,140	
27	2322.15	170.824	829	2768.84	186,532	
î	2332.83	171,217	1	2780.51	186.925	
5	2343.55	171.610	5	2792.21	187.318	
केंद्र न्यं कर्णात न्यंत्र कांद्र कांद्र कांद्र	2354.29	172.003	네.D 나는 4 작년 8 자연 나는 10 가는 4 자년	2803.93	187.711	
7	2365.05	172.395	7	2815.67	188,103	

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.	
60 শতি শুলি গুলি গুলি গুলি গুলি গুলি গুলি গুলি গ	2827.44 2839.23 2851.05 2862.89 2874.76 2886.65 2898.57 2910.51	188.496 188.889 189.281 189.674 190.067 190.459 190.852 191.245	CDdordenjodouble objet-jo	3318.31 3331.09 3343.89 3356.71 3369.56 3382.44 3395.33 3408.26	204.204 204.597 204.989 205.382 205.775 206.167 206.560 206.953	
61	2922.47 2934.46 2946.48 2958.52 2970.58 2982.67 2994.78 3006.92	191.638 192.030 192.423 192.816 193.208 193.601 193.994 194.386	CO -do-decio-devolocoles-io	3421.20 3434.17 3447.17 3460.19 3473.24 3486.30 3499.40 3512.52	207.346 207.738 208.131 208.524 208.916 209.309 209.702 210.094	
60 - de respondentes	3019.08 3031.26 3043.47 3055.71 3067.97 3080.25 3092.56 3104.89	194.779 195.172 195.565 195.957 196.350 196.743 197.135 197.528	67	3525.66 3538.83 3552.02 3565.24 3578.48 3591.74 3605.04 3618.35	210.487 210.880 211.273 211.665 212.058 212.451 212.843 213.236	
63 - desidentes desidentes estantes	3117.25 3129.64 3142.04 3154.47 3166.93 3179.41 3191.91 3204.44	197.921 198.313 198.706 199.099 199.492 199.884 200.277 200.670	68 14 saylor (1916) 167 (19	3631.69 3645.05 3658.44 3671.86 3685.29 3698.76 3712.24 3725.75	213.629 214.021 214.414 214.807 215.200 215.592 215.985 216.378	
64	3217.00 3229.58 3242.18 3254.81 3267.46 3280.14 3292.84 3305.56	201.062 201.455 201.848 202.240 202.633 203.026 203.419 203.811	TO Price price of the section of the	3739.29 3752.85 3766.43 3780.04 3793.68 3807.34 3821.02 3834.73	216.770 217.163 217.556 217.948 218.341 218.734 219.127 219.519	

Diameter.	Area,	Circumference.	Diameter.	Area.	Circumference.
70	3848.46	219.912	75	4417.87	235.620
10	3862.22	220.305		4432.61	236.013
8	3876.00	220.697	40 44 4 02/00 pm[03 15]00 05] 4 5-jo		
3			Til.	4447.38	236.405
38	3889.80	221.090	8	4462.16	236.798
1200000	3903.63	221.483	2	4476.98	237.191
8	3917.49	221.875	8	4491.81	237.583
34	3931.37	222.268	34	4506.67	237.976
7 8	3945.27	222.661	7 8	4521.56	238.369
71	3959.20	223.054	76	4536.47	238.762
1 1	3973.15	223.446	1 2	4551.41	239.154
î	3987.13	223,839	1	4566.36	239.547
3	4001.13	224.232	3	4581.35	239.940
3	4015.16	224.624	8	4596.36	240.332
2 5	4029.21	225.017	2 5	4611.39	240.725
년(0) pulpulation pulpulation polymer-je			H(00 Fd(+675)40 Fd(7415)40 F3)+6 F- cc		
4	4043.29	225.410	4	4626.45	241.118
8	4057.39	225.802	8	4641.53	241.510
72	4071.51	226.195	77	4656.64	241.903
1	4085.66	226.588	1	4671.77	242.296
1	4099.84	226,981	i	4686.92	242,689
3	4114.04	227.373	3	4702.10	243.081
8	4128.26	227.766	8	4717.31	243,474
2 5	4142.51	228.159	2 5	4732.54	243.867
8 3	4156.78	228.551	8 2	4747.79	244.259
न्दैक म्दैबार) o म्द्रिबार) o स्ट्रिबार			-(100 mily-8 00/00 mily-8 00/00 00/-8 0-/00		
ŧ	4171.08	228.944	8	4763.07	244.652
73 .	4185.40	229.337	78	4778.37	245.045
1	4199.74	229.729	1	4793.70	245.437
- 1	4214.11	230.122	1 1	4809.05	245.830
3	4228.51	230.515	800	4824.43	246.223
į.	4242.93	230,908	ì	4839.83	246.616
5	4257.37	231.300	5	4855.26	247.008
en ele color relación color de ele	4271.84	231.693	400 p44 0000 p404 00000 00 4 2-10	4870.71	247,401
力	4286.33	232.086	7	4886.18	247.794
	4200.00	000.000	8	4000.10	N21.102
74	4300.85	232.478	79	4901.68	248.186
1	4315.39	232.871	1	4917.21	248.579
8	4329.96	233.264	1	4932.75	248.972
	4344.55	233.656	3	4948.33	249.364
1	4359.17	234.049	8	4963.92	249.757
12 5	4373.81	234.442	2 5	4979.55	250.150
8	4388.47	234.835	8 3	4995.19	250.543
4			년 00 1세 세 약 (00 pulled 15) (00 05) 세 주   a		1
8	4403.16	235.227	8	5010.86	250.935

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
BO Tonger planta milet planta milet planta	5026.56 5042.28 5058.03 5073.79 5089.59 5105.41 5121.25 5137.12	251.328 251.721 252.113 252.506 252.899 253.291 253.684 254.077		5674.51 5691.22 5707.94 5724.69 5741.47 5758.27 5775.10 5791.94	267.036 267.429 267.821 268.214 268.607 268.999 269.392 269.785
81 Adaptive region and standard for the	5153.01 5168.93 5184.87 5200.83 5216.82 5232.84 5248.88 5264.94	254.470 254.862 255.255 255.648 256.040 256.433 256.826 257.218		5808.82 5825.72 5842.64 5859.59 5876.56 5893.55 5910.58 5927.62	270.178 270.570 270.963 271.356 271.748 272.141 272.534 272.926
00 1(60 rd 4400)00 rd(440)0000 447-18	5281.03 5297.14 5313.28 5329.44 5345.63 5361.84 5378.08 5394.34	257.611 258.004 258.397 258.789 259.182 259.575 259.967 260.360	87 100 14 1000 14 1000 11 41 100	5944.69 5961.79 5978.91 5996.05 6013.22 6030.41 6047.63 6064.87	273.319 273.712 274.105 274.497 274.890 275.283 275.675 276.068
Prisonal designation relativistics sold designation and designation relativistics and designation of the second se	5410.62 5426.93 5443.26 5459.62 5476.01 5492.41 5508.84 5525.30	260.753 261.145 261.538 261.931 262.324 262.716 263.109 263.502		6082.14 6099.43 6116.74 6134.08 6151.45 6168.84 6186.25 6203.69	276.461 276.853 277.246 277.638 278.032 278.424 278.817 279.210
84	5541.78 5558.29 5574.82 5591.37 5607.95 5624.56 5641.18 5657.84	263.894 264.287 264.680 265.072 265.465 265.858 266.251 266.643		6221.15 6238.64 6256.15 6273.69 6291.25 6308.84 6326.45 6344.08	279.602 279.995 280.388 280.780 281.173 281.566 281.959 282.351

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.	
90	6361.74	282.744	95	7088.24	298,452	
	6379.42	283,137		7106.90	298.845	
ન(ઝન) લાજોળ ન(જાડોણ જો લાગોલ	6397.13	283.529		7125.59	299.237	
3	6414.86	283.922	4 3	7144.31	299,630	
8	6432.62	284.315	8	7163.04	300.023	
2		284.707	2	7181.81	300.415	
8	6450.40		5			
4	6468.21	285.100	4	7200.60	300.808	
B	6486.04	285.493	8	7219.41	301.201	
91	6503.90	285.886	96	7238.25	301.594	
青	6521.78	286.278	18	7257.11	301.986	
1	6539.68	286.671	1	7275.99	302.379	
3	6557.61	287.064	3	7294.91	302.772	
i	6575.56	287.456	1	7313.84	303.164	
50	6593.54	287.849	5	7332.80	303.557	
3	6611.55	288.242	3	7351.79	303.950	
-(6-4-6-0)0(	6629.57	288.634	-(0) -(4-6-0) (0) -4(-4-0) (0) 00   4-5-100	7370.79	304.342	
92	6647.63	289.027	97	7389:83	304.735	
	6665.70	289.420		7408.89	305.128	
1 8	6683.80	289.813	1	7427.97	305.521	
4			4			
8	6701.93	290.205	8	7447.08	305.913	
2	6720.08	290.598	2	7466.21	306.306	
- 4 selector estator e	6738.25	290.991		7485.37	306.699	
4	6756.45	291.383	4	7504.55	307.091	
78	6774.68	291.776	7 8	7523.75	307.484	
93	6792.92	292.169	98	7542.98	307.877	
1	6811.20	292.562	1	7562.24	308.270	
101	6829.49	292.954	1	7581.52	308.662	
3	6847.82	293,347	3	7600.82	309.055	
1	6866.16	293.740	i	7620.15	309,448	
5	6884.53	294.132	5	7639.50	309.840	
8 3	6902.93	294.525	8 3	7658.88	310.233	
ত্তি শ্ৰেণ্ডত তাৰু শ্ৰ	6921.35	294.918		7678.28	310.626	
94	6939.79	295,310	. 99	7697.71	311.018	
1 2	6958.26	295.703		7717.16	311.411	
8	6976.76	296.096	8	7736.63	311.804	
3	6995.28	296.488	4 3	7756.13	312.196	
8			8			
2	7013.82	296.881	22	7775.66	312.589	
ojos o	7032.39	297.274	D C	7795.21	312.982	
+ 10 14 4 00 10 14 2 15 10 00 4 7 14	7050.98	297.667		7814.78	313.375	
8	7069.59	298.059	78	7834.38	313.767	
			100	7854.00	314.160	

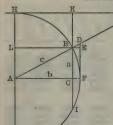
### LOGARITHMS OF NUMBERS, FROM 0 TO 1000.

No.	0	1	2	8	4	5	6	7	8	9
0	0	00000	30103	47712	60206	69897	77815	84510	90309	9542
10	000000	00432 04532	00860 04922	01284	01703 05690	02119 06070	02531	02938	03342	0374
12	07918	08279	08636	08991	09342	09691	10037	10380	10721	1105
18	11394 14613	11727 14922	12057 15229	12385 15534	12710 15836	13033 16137	13354 16435	13672 16732	18988 17026	1430 1731
15	17609	17898 20683	18184 20952	18469 21219	18752 21484	19033 21748	19312	19590 22272	10866	2014
16 17	20412 23045	23300	23553	23805	24055	24304	22011 24551	24797	22531 25042	2278 2528
18	25527	25768	26007	26245	26482	26717	26951	27184	27416	2764
19	27875	28103	28330	28556	28780	29003	29226	29447	29667	2988
20 21	30103	30320	30535 32634	30750 32838	30963	31175 33244	31387 33445	31597 33646	31806 33846	3201
22	34242	34439	34635	34830	35025	35218	35411	85608	35793	3404
23	36173 38021	36361 38202	36549 38382	36736 38561	36922 38739	37107 38917	37291 39094	37475 39270	37658 39445	3784 3965
25	39794	39967	40140	40312	40483	40654	40824	40993	41162	
98	41497	41664	41830	41996	42160	42325	42488	42651	42813	4297
27	43136	43297	43457	43616	43775	43933	44091	44248	44404	4450
28 29	44716 46240	44871 46389	45025 46538	45179 46687	45332 46835	45484 46982	45637 47129	45788 47276	45939 47422	4609 4756
80	47712	47857	48001	48144	48287	48430	48572	48714	48855	4899
31 82	49136 50515	49276 50651	49415 50786	49554 50920	49693 51055	49831 51188	49969 51322	50106 51455	50243	5037 5172
33	51851	51983	52114	52244	52375	52504	52634	52763	52892	5302
34	53148	53275	53403	53529	53656	53782	53908	54033	54158	5428
35 36	54407	54531	54654 55871	54777	54900 56110	55023 56229	55145	55267 56467	55388 56585	5550
37	55630 56820	55751 56937	57054	55991 57171	57287	57403	56348 57519	57634	57749	5670 5786
88	57978 50106	58093 59218	58206 59329	58320 59439	58433 59550	58546 59660	58659 59770	58771 59879	58883 59988	5899
41	60206	60314	60423	60531	61700	61805	61909	62014	61086	6222
42	62325	62428	62531	62634	62737	62839	62941	63043	63144	6324
43	63347 64345	63448	63548 64542	63649 64640	63749 64738	63849 64836	63949 64933	64048 65031	64147 65128	6424 6522
45	65321	65418	65514	65610	65706	65801	65896	65092	66087	6618
48	66276	66370	66464	66558	60652	68745	66839	86082	67025	6711
47	67210 68124	67302 68215	67394 68305	67486 68395	67578 68485	67669 68574	68664	67852 68753	67943 68842	6803
40	69020	69108	69197	69285	69373	69461	69548	69636	69723	6981
50	69897	80084	70070	70157	70243	70329	70415	70501	70586	7067
51 52	70757 71600	70842 71684	70927 71767	71012 71850	71096 71933	71181 72016	71265 72099	71349 72181	71433 72263	7151 7234
53	72428 73239	72509	72591	72673	72754 73560	72835 73640	72916	72997	73078 73878	7315

## LOGARITHMS OF NUMBERS, FROM 0 TO 1000

No.	0	1	2	8	4	Б	6	7	8	9
55	74036	74115	74194	74273	74351	74429	74507	74586	74663	74741
56	74819	74896	74974	75051	75128	75205	75282	75358	75435	75511
57	75587	75664	75740	75815	75891	75967	76042	76118	76193	76268
58	76343	76418	76492	76567	76641	76716	76790	76864	76938	77012
59	77085	77159	77232	77305	77379	77452	77525	77597	77670	77743
60	77815	77887	77960	78032	78104	78176	78247	78319	78390	78462
61	78533	78604	78675	78746	78817	78888	78958	79029	79099	79169
62	79239	79309	79379	79449	79518	79588	79657	79727	79796	79865
63	79934	80003	80072	80140	80209	80277	80346	80414	80482	80550
64	80618	80686	80754	80821	80889	80956	81023	81090	81158	81224
65	81291	81358	81425	81491	81558	81624	81690	81757	81829	81889
66	81954	82020	82086	82151	82217	82282	82347	82413	82478	82543
67	82607	82672	82737	82802	82866	82930	82995	83059	83123	83187
68	83251	83315	83378	83442	83506	83569	83632	83696	83759	83822
69	83885	83948	84011	84073	84136	84198	84261	84323	84386	84448
70	84510	84572	84634	84696	84757	84819	84880	84942	85063	85065
71	85126	85187	85248	85309	85370	85431	85491	85552	85612	85673
72	85733	85794	85854	85914	85974	86034	86094	86153	86213	86273
73	86332	86392	86451	86510	86570	86629	86688	86747	86806	86864
• 74	86923	86982	87040	87099	87157	87216	87274	87332	87390	87448
75	87506	87564	87622	87680	87737	87795	87852	87910	87967	88024
76	88081	88138	88196	88252	88309	88366	88423	88480	88536	88593
77	88649	88705	88762	88818	88874	88930	88986	89042	89098	89154
78	89209	89265	89321	89376	89432	89487	89542	89597	89653	89708
79	89763	89818	89873	89927	89982	90037	90091	90146	90200	90255
80	90309	90363	90417	90472	90526	90580	90634	90687	90741	90795
81	90849	90902	90956	91009	91062	91116	91169	91222	91275	91328
82	91381	91434	91487	91540	91593	91645	91698	91751	91803	91855
83	91908	91960	92012	92065	92117	92169	92221	92273	92324	92376
84	92428	92480	92531	92583	92634	92686	92737	92788	92840	92891
85	92942	92993	93044	93095	93146	93197	93247	93298	93349	93399
86	93450	93500	93551	93601	93651	93702	93752	93802	93852	93902
87	93952	94002	94052	94101	94151	94201	94250	94300	94349	94399
88	94448	94498	94547	94596	94645	94694	94743	94792	94841	94890
89	94939	94988	95036	95085	95134	95182	95231	95279	95328	95876
90	95424	95472	95521	95569	95617	95665	95713	95761	95809	95856 .
91	95904	95952	95999	96047	96095	96142	96190	96237	96284	96332
92	96379	96426	96473	96520	96567	96614	96661	96708	96755	96802
93	96848	96895	96942	96988	97035	97081	97128	97174	97220	97267
94	97313	97359	97405	97451	97497	97543	97589	97635	97681	97727
95	97772	97818	97864	97909	97955	98000	98046	98091	98137	98182
96	98227	98272	98318	98363	98408	98453	98498	98543	98588	98632
97	98677	98722	98767	98811	98856	98900	98945	98989	99034	99078
98	99123	99167	99211	99255	99800	99344	99388	99432	99476	99520
99	99564	99607	99651	99695	99739	99782	99826	99870	99913	09957

#### TRIGONOMETRIC FORMULAE. TRIGONOMETRIC FUNCTIONS.



Let A = angle BAC = arc BF. Let radius AF = AB = AH = 1.

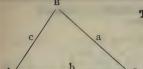
#### Then

 $\sin A = BC$ versin A = CF = BEcovers A = BK = HL  $\cos A = AC$ exsec A = BD tan A = DF  $\begin{array}{lll} \cot A & = HG & \operatorname{coexsec} A = BG \\ \sec A & = AD & \operatorname{chord} A & = BF \\ \operatorname{cosec} A = AG & \operatorname{chord} 2A = BI = 2BC \end{array}$ 

#### RIGHT-ANGLED TRIANGLES.

In the right-angled triangle ABC, Let side AB = c, side AC = b, and side BC = a; let angle ABC = B.

Then 
$$\sin A = \frac{a}{c} = \cos B$$
  $a = c \sin A = b \tan A$ 
 $\cos A = \frac{b}{c} = \sin B$   $b = c \cos A = a \cot A$ 
 $\tan A = \frac{a}{b} = \cot B$   $c = \frac{a}{\sin A} = \frac{b}{\cos A}$ 
 $\cot A = \frac{b}{a} = \tan B$   $a = c \cos B = b \cot B$ 
 $\sec A = \frac{c}{b} = \csc B$   $b = c \sin B = a \tan B$ 
 $\csc A = \frac{c}{a} = \sec B$   $c = \frac{a}{\cos B} = \frac{b}{\sin B}$ 
 $\cot A = \frac{c - b}{b} = \csc B$   $\cot B = a \cot B$ 
 $\cot A = \frac{c - b}{b} = \csc B$   $\cot B = a \cot B$ 
 $\cot A = \frac{c - b}{b} = \csc B$   $\cot B = a \cot B$ 
 $\cot A = \frac{c - b}{b} = \csc B$   $\cot B = a \cot B$ 
 $\cot A = \frac{c - b}{b} = \csc B$   $\cot B = a \cot B$ 
 $\cot A = \frac{c - b}{b} = \csc B$   $\cot B = a \cot B$ 
 $\cot A = \frac{c - b}{c \cos A} = \cot B$ 
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 $\cot A = \frac{c - b}{c \cos B} = \cot B$ 
 $\cot A = \frac{c - c \cos B}{c \cos B} = \cot B$ 
 $\cot A = \frac{c - c \cos B}{c \cos B} =$ 



# TRIGONOMETRIC FORMULÆ (Continued).

#### OBLIQUE TRIANGLES.

s =	1/2	(a+b+c)	
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A	ь	$s = \frac{1}{2}(a+b+c)$
KNOWN	REQUIRED	FORMULÆ
А, В, а	C, b	$C = 180^{\circ} - (A + B),  b = \frac{a}{\sin A} \cdot \sin B,$
	С	$c = \frac{a}{\sin A} \sin (A + B)$
A, a, b	B, C	$\sin B = \frac{\sin A}{a}$ . b, $C = 180^{\circ} - (A+B)$ ,
	С	$c = \frac{a}{\sin A} \cdot \sin C$
C, a, b		$\frac{1}{2}(A+B) = 90^{\circ} - \frac{1}{2}C$
	½ (A−B)	$\tan \frac{1}{2} (A - B) = \frac{a - b}{a + b} \tan \frac{1}{2} (A + B)$
-	А, В	$A = \frac{1}{2} (A+B) + \frac{1}{2} (A-B),$ $B = \frac{1}{2} (A+B) - \frac{1}{2} (A-B)$
F4 3	С	$c = (a+b) \frac{\cos \frac{1}{2} (A+B)}{\cos \frac{1}{2} (A-B)}$
	-	$= (a-b) \frac{\sin \frac{1}{2} (A+B)}{\sin \frac{1}{2} (A-B)}$
		$=\sqrt{a^2+b^2-2ab\cdot\cos C}$
	area	$area = \frac{1}{2}$ a b sin C.
a, b, c	A	$\sin \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{b c}}$
		$\cos \frac{1}{2} A = \sqrt{\frac{s (s-a)}{b c}}$
		$\tan \frac{1}{2} A = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}}$
	-	$\sin A = \frac{2\sqrt{s (s-a) (s-b) (s-c)}}{b c}$
		$vers A = \frac{2 (s-b) (s-c)}{b c}$
	area	$area = \sqrt{s(s-a)(s-b)(s-c)}$
A, B, C, a	area	$area = \frac{a^2 \sin B \cdot \sin C}{2 \sin A}$

# TRIGONOMETRIC FORMULÆ—(Continued).

$$\sin A = \frac{1}{\csc A} = \sqrt{1 - \cos^2 A} = \tan A \cos A$$

$$= 2 \sin \frac{1}{2} A \cos \frac{1}{2} A = \text{vers } A \cot \frac{1}{2} A$$

$$= \sqrt{\frac{1}{2}} \text{ vers } 2 A = \sqrt{\frac{1}{2}} (1 - \cos 2 A)$$

$$\cos A = \frac{1}{\sec A} = \sqrt{1 - \sin^2 A} = \cot A \sin A$$

$$= 1 - \text{vers } A = 2 \cos^2 \frac{1}{2} A - 1 = 1 - 2 \sin^2 \frac{1}{2} A$$

$$= \cos^2 \frac{1}{2} A - \sin^2 \frac{1}{2} A = \sqrt{\frac{1}{2} + \frac{1}{2} \cos 2 A}$$

$$\tan A = \frac{1}{\cot A} = \frac{\sin A}{\cos A} = \sqrt{\sec^2 A - 1}$$

$$= \sqrt{\frac{1}{\cos^2 A} - 1} = \frac{\sqrt{1 - \cos^2 A}}{\cos A} = \frac{\sin 2 A}{1 + \cos 2 A}$$

$$= \frac{1 - \cos 2 A}{\sin 2 A} = \frac{\text{vers } 2 A}{\sin 2 A} = \text{exsec A cot } \frac{1}{2} A$$

$$\cot A = \frac{1}{\tan A} = \frac{\cos A}{\sin A} = \sqrt{\csc^2 A - 1}$$

$$= \frac{\sin 2 A}{1 - \cos 2 A} = \frac{\sin 2 A}{\text{vers } 2 A} = \frac{1 + \cos 2 A}{\sin 2 A} = \frac{\tan \frac{1}{2} A}{\text{exsec } A}$$

vers A = 
$$1 - \cos A = \sin A \tan \frac{1}{2} A = 2 \sin^2 \frac{1}{2} A$$

exsec A = sec A-1 = tan A tan 
$$\frac{1}{2}$$
 A =  $\frac{\text{vers A}}{\cos A}$ 

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} = \sqrt{\frac{\operatorname{vers} A}{2}}$$

$$\cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\tan \frac{1}{2} A = \frac{\tan A}{1 + \sec A} = \csc A - \cot A = \frac{1 - \cos A}{\sin A} = \sqrt{\frac{1 - \cos A}{1 + \cos A}}$$

$$\cot \frac{1}{2} A = \frac{\sin A}{\operatorname{vers} A} = \frac{1 + \cos A}{\sin A} = \frac{1}{\operatorname{cosec} A - \cot A}$$

vers 
$$\frac{1}{2}$$
 A =  $\frac{\frac{1}{2} \text{ vers A}}{1 + \sqrt{1 - \frac{1}{2} \text{ vers A}}} = \frac{1 - \cos A}{2 + \sqrt{2} (1 + \cos A)}$ 

## TRIGONOMETRIC FORMULÆ—(Continued). GENERAL.

exsec 
$$\frac{1}{2}$$
 A =  $\frac{1 - \cos A}{(1 + \cos A) + \sqrt{2} (1 + \cos A)}$ 

$$\sin 2 A = 2 \sin A \cos A$$

$$\cos 2 A = 2 \cos^2 A - 1 = \cos^2 A - \sin^2 A = 1 - 2 \sin^2 A$$

$$\tan 2 A = \frac{2 \tan A}{1 - \tan^2 A}$$

$$\cot 2 A = \frac{\cot^2 A - 1}{2 \cot A}$$

$$\operatorname{exsec} 2 A = \frac{2 \tan^2 A}{1 - \tan^2 A}$$

$$\sin 3 A = 3 \sin A - 4 \sin^3 A$$

$$\cos 3 A = 4 \cos^3 A - 3 \cos A$$

$$\tan 3 A = \frac{3 \tan A - \tan^3 A}{1 - 3 \tan^2 A}$$

$$\sin 4 A = 4 \sin A \cos A - 8 \sin^3 A \cos A$$

$$\cos 4 A = 1 - 8 \cos^2 A + 8 \cos^4 A$$

$$\tan 4 A = \frac{4 \tan A - 4 \tan^3 A}{1 - 6 \tan^2 A + \tan^4 A}$$

$$\sin (A+B) = \sin A \cdot \cos B + \sin B \cdot \cos A$$

$$\sin (A-B) = \sin A \cdot \cos B - \sin B \cdot \cos A$$

$$cos(A+B) = cos A \cdot cos B - sin A \cdot sin B$$
  
 $cos(A-B) = cos A \cdot cos B + sin A \cdot sin B$ 

$$\sin A + \sin B = 2 \sin \frac{1}{2} (A + B) \cos \frac{1}{2} (A - B)$$

$$\sin A + \sin B = 2 \sin \frac{1}{2} (A + B) \cos \frac{1}{2} (A - B)$$
  
 $\sin A - \sin B = 2 \cos \frac{1}{2} (A + B) \sin \frac{1}{2} (A - B)$ 

$$\cos A + \cos B = 2 \cos \frac{1}{2} (A+B) \cos \frac{1}{2} (A-B) \cos B - \cos A = 2 \sin \frac{1}{2} (A+B) \sin \frac{1}{2} (A-B)$$

$$\sin^2 A - \sin^2 B = \cos^2 B - \cos^2 A = \sin (A+B) \sin (A-B)$$

$$\cos^2 A - \sin^2 B = \cos (A + B) \cos (A - B)$$

$$\tan A + \tan B = \frac{\sin (A+B)}{\cos A \cdot \cos B} \qquad \tan A - \tan B = \frac{\sin (A-B)}{\cos A \cdot \cos B}$$

FUNCTION.	QUADRANT SIGN.						
FUNCTION.	Ist	2nd	3rd	4th			
sine, cosecant, coexsecant	+	+	-	_			
cosine, secant, exsecant	+	_	-	+			
tangent, cotangent	+	_	+	-			
versed sine, coversed sine	+	+	+ 1	+			

0	,	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	,	8
0	10 20 30 40 50	.000000 .002909 .005818 .008727 .011635 .014544	Infinite. 343.77516 171.88831 114.59301 85.945609 68.757360	.000000 .002909 .005818 .008727 .011636 .014545	Infinite. 343.77371 171.88540 114.58865 85.939791 68.750087	1.00000 1.00000 1.00002 1.00004 1.00007 1.00011	1.000000 .99996 .999983 .999962 .999932 .999894	0 50 40 30 20 10	90
1	16 20 30 40 50	.017452 .020361 .023269 .026177 .029085 .031992	57.298688 49.114062 42.975713 38.201550 34.382316 31.257577	.017455 .020365 .023275 .026186 .029097 .032009	57.289962 49.103881 42.964077 38.188459 34.367771 31.241577	1.00015 1.00021 1.00027 1.00034 1.00042 1.00051	.999848 .999793 .999729 .299657 .999577 .999488	80 20 10	89
3	0 10 20 30 40 50	.034899 .037806 .040713 .043619 .046525 .049431	28.653708 26.450510 24.562123 22.925586 21.493676 20.230284	.034921 .037834 .040747 .043661 .046576 .049491	28.636253 26.431600 24.541758 22.903766 21.470401 20.205553	1.00061 1.00072 1.00083 1.00095 1.00108 1.00122	.999391 .999285 .999171 .999048 .998917 .998778	0 50 40 30 20 10	88
8	0 10 20 30 40 50	.052336 .055241 .058145 .061049 .063952 .066854	19.107323 18.102619 17.198434 16.380408 15.636793 14.957882	.052408 .055325 .058243 .061163 .064083 .067004	19.081137 18.074977 17.169337 16.349855 15.604784 14.924417	1.00137 1.00153 1.00169 1.00187 1.00205 1.00224	.998630 .998473 .998308 .998135 .997953 .997763	50 40 80 20 10	87
4	0 10 20 30 40 50	.069756 .072658 .075559 .078459 .081359 .084258	14.335587 13.763115 13.234717 12.745495 12.291252 11.868370	.069927 .072851 .075776 .078702 .081629 .084558	14.300666 13.726738 13.196888 12.706205 12.250505 11.826167	1.00244 1.00265 1.00287 1.00309 1.00333 1.00357	.997564 .997357 .997141 .996917 1996685 .996444	50 40 80 20 10	86
Б	0 10 20 30 40 50	.087156 .090053 .092950 .095846 .098741 .101635	11.473713 11.104549 10.758488 10.433431 10.127522 9.8391227	.087489 .090421 .093354 .096289 .099226 .102164	11.430052 11.059431 10.711913 10.385397 10.078031 9.7881732	1.00382 1.00408 1.00435 1.00463 1.00491 1.00521	.996195 .995937 .995671 .995396 .995113 .994822	0 50 40 80 20 10	85
6	10 20	.104528 .107421 .110313	9.5667722 9.3091699 9.0651512	.105104 .108046 .110990	9.5143645 9.2553035 9.0098261	1.00551 1.00582 1.00614	.994522 .994214 .993897	50 40	84
	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.	,	0

For functions from 83°-40' to 90° read from bottom of table upward.

0	,	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	,	0
6	30 40 50	.113203 .116093 .118982	8.8336715 8.6137901 8.4045586	.113936 .116883 .119833	8.7768874 8.5555468 8.3449558	1.00647 1.00681 1.00715	.993572 .993238 .992896	30 20 10	
7	0 10 20 30 40 50	.121869 .124 <b>7</b> 56 .127642 .130526 .133410 .136292	8.2055090 8.0156450 7.8344335 7.6612976 7.4957100 7.3371909	.122785 .125738 .128694 .131653 .134613 .137576	8.1443464 7.9530224 7.7703506 7.5957541 7.4287064 7.2687255	1.00751 1.00787 1.00825 1.00863 1.00902 1.00942	.992546 .992187 .991820 .991445 .991061 .990669	0 50 40 30 20 10	88
8	0 10 20 30 40 50	.139173 .142053 .144932 .147809 .150686 .153561	7.1852965 7.0396220 6.8997942 6.7654691 6.6363293 6.5120812	.140541 .143508 .146478 .149451 .152426 .155404	7.1153697 6.9682335 6.8269437 6.6911562 6.5605538 6.4348428	1.00983 1.01024 1.01067 1.01111 1.01155 1.01200	.990268 .989859 .989442 .989016 .988582 .988139	0 50 40 80 20 10	82
9	0 10 20 30 40 50	.156434 .159307 .162178 .165048 .167916 .170783	6.3924532 6.2771933 6.1660674 6.0588583 5.9553625 5.8553921	.158384 .161368 .164354 .167343 .170334 .173329	6.3137515 6.1970279 6.0844381 5.9757644 5.8708042 5.7693688	1.01247 1.01294 1.01342 1.01391 1.01440 1.01491	.987688 .987229 .986762 .986286 .985801 .985309	0 50 40 30 20 10	81
10	0 10 20 30 40 50	.173648 .176512 .179375 .182236 .185095 .187953	5.7587705 5.6653331 5.5749258 5.4874043 5.4026333 5.3204860	.176327 .179328 .182332 .185339 .188359 .191363	5.6712818 5.5763786 5.4845052 5.3955172 5.3092793 5.2256647	1.01543 1.01595 1.01649 1.01703 1.01758 1.01815	.984808 .984298 .983781 .983255 .982721 .982178	50 40 30 20 10	80
11	0 10 20 30 40 50	.190809 .193664 .196517 .199368 .202218 .205065	5.2408431 5.1635924 5.0886284 5.0158517 4.9451687 4.8764907	.194380 .197401 .200425 .203452 .206483 .209518	5.1445540 5.0658352 4.9894027 4.9151570 4.8430045 4.7728568	1.01872 1.01930 1.01989 1.02049 1.02110 1.02171	.981627 .981068 .980500 .979925 .979341 .978748	50 40 30 20 10	79
12	0 10 20 30 40 50	.207912 .210756 .213599 .216440 .219279 .222116	4.8097343 4.7448206 4.6816748 4.6202263 4.5604080 4.5021565	· .212557 .215599 .218645 .221695 .224748 .227806	4.7046301 4.6382457 4.5736287 4.5107085 4.4494181 4.3896940	1.02234 1.02298 1.02362 1.02428 1.02494 1.02562	.978148. .977539 .976921 .976296 .975662 .975020	50 40 30 20 10	78
0	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.	,	0

For functions from 77°-10' to 83°-30' read from bottom of table upward.

0	,	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	,	0
18	0 10 20 30 40 50	.224951 .227784 .230616 .233445 .236273 .239098	4.4454115 4.3901158 4.3362150 4.2836576 4.2323943 4.1823785	.230868 .233934 .237004 .240079 .243158 .246241	4.3314759 4.2747066 4.2193318 4.1652998 4.1125614 4.0610700	1.02630 1.02700 1.02770 1.02842 1.02914 1.02987	.974370 .973712 .973045 .972370 .971687 .970995	0 50 40 30 20 10	77
14	0 10 20 30 40 50	.241922 .244743 .247563 .250380 .253195 .256008	4.1335655 4.0859130 4.0393804 3.9939292 3.9495224 3.9061250	.249328 .252420 .255517 .258618 .261723 .264834	4.0107809 3.9616518 3.9136420 3.8667131 3.8208281 3.7759519	1.03061 1.03137 1.03213 1.03290 1.03368 1.03447	.970296 .969588 .968872 .968148 .967415	0 50 40 30 20 10	76
15	0 10 20 80 40 50	.258819 .261628 .264434 .267238 .270040 .272840	3.8637033 3.8222251 3.7816596 3.7419775 3.7031506 3.6651518	.267949 .271069 .274195 .277325 .280460 .283600	3.7320508 3.6890927 3.6470467 3.6058835 3.5655749 3.5260938	1.03528 1.03609 1.03691 1.03774 1.03858 1.03944	.965926 .965169 .964404 .963630 .962849 .962059	0 50 40 30 20 10	75
16	0 10 20 30 40 50	.275637 .278432 .281225 .284015 .286803 .289589	3.6279553 3.5915363 3.5558710 3.5209365 3.4867110 3.4531735	.286745 .289896 .293052 .296214 .299380 .302553	3.4874144 3.4495120 3.4123626 3.3759434 3.3402326 3.3052091	1.04030 1.04117 1.04206 1.04295 1.04385 1.04477	.961262 .960456 .959642 .958820 .957990 .957151	0 50 40 30 20 10	74
17	0 10 20 30 40 50	.292372 .295152 .297930 .300706 .303479 .306249	3.4203036 3.3880820 3.3564900 3.3255095 3.2951234 3.2653149	.305731 .308914 .312104 .315299 .318500 .321707	3.2708526 3.2371438 3.2040638 3.1715948 3.1397194 3.1084210	1.04569 1.04663 1.04757 1.04853 1.04950 1.05047	.956305 .955450 .954588 .953717 .952838 .951951	0 50 40 30 20 10	78
18	0 10 20 30 40 50	.309017 .311782 .314545 .317305 .320062 .322816	3.23606S0 3.2073673 3.1791978 3.1515453 3.1243959 3.0977363	.324920 .328139 .331364 .334595 .337833 .341077	3.0776835 3.0474915 3.0178301 2.9886850 2.9600422 2.9318885	1.05146 1.05246 1.05347 1.05449 1.05552 1.05657	.951057 .950154 .949243 .948324 .947397	0 50 40 30 20 10	72
19	0 10 20	.325568 .328317 .331063	3.0715535 3.0458352 3.0205693	.344328 .347585 .350848	2.9042109 2.8769970 2.8502349	1.05762 1.05869 1.05976	.945519 .944568 .943609	0 50 40	71
0	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.	,	0

For functions from 70°-40' to 77°-0' read from bottom of table upward.

0	2	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	,	0
19	30 40 50	.333807 .336547 .339285	2.9957443 2.9713490 2.9473724	.354119 .357396 .360680	2.8239129 2.7980198 2.7725448	1.06085 1.06195 1.06306	.942641 .941666 .940684	30 20 10	
20	10 20 30 40 50	.342020 .344752 .347481 .350207 .352931 .355651	2.9238044 2.9006346 2.8778532 2.8554510 2.8334185 2.8117471	.363970 .367268 .370573 .373885 .377204 .380530	2.7474774 2.7228076 2.6985254 2.6746215 2.6510867 2.6279121	1.06418 1.06531 1.06645 1.06761 1.06878 1.06995	.939693 .938694 .937687 .936672 .935650 .934619	0 50 40 30 20 10	70
21	10 20 30 40 50	.358368 .361082 .363793 .366501 .369206 .371908	2.7904281 2.7694532 2.7488144 2.7285038 2.7085139 2.6888374	.383864 .387205 .390554 .393911 .397275 .400647	2.6050891 2.5826094 2.5604649 2.5386479 2.5171507 2.4959661	1.07115 1.07235 1.07356 1.07479 1.07602 1.07727	.933580 .932534 .931480 .930418 .929348 .928270	50 40 30 20 10	69
22	10 20 20 40 50	.374607 .377302 .379994 .382683 .385369 .388052	2.6694672 2.6503962 2.6316180 2.6131259 2.5949137 2.5769753	.404026 .407414 .410810 .414214 .417626 .421046	2.4750869 2.4545061 2.4342172 2.4142136 2.3944889 2.3750372	1.07853 1.07981 1.08109 1.08239 1.08370 1.08503	.927184 1926090 1924989 .923880 .922762 .921638	50 40 50 20 10	68
28	0 10 20 30 40 50	.390731 .393407 .396080 .398749 .401415 .404078	2.5593047 2.5418961 2.5247440 2.5078428 2.4911874 2.4747726	.424475 .427912 .431358 .434812 .438276 .441748	2.3558524 2.3369287 2.3182606 2.2998425 2.2816693 2.2637357	1.08636 1.08771 1.08907 1.09044 1.09183 1.09323	.920505 .919364 .918216 .917060 .915896 .914725	50 40 30 20 10	67
24	10 20 30 40 50	.406737 .409392 .412045 .414693 .417338 .419980	2.4585933 2.4426448 2.4269222 2.4114210 2.3961367 2.3810650	.445229 .448719 .452218 .455726 .459244 .462771	2.2460368 2.2285676 2.2113234 2.1942997 2.1774920 2.1608958	1.09464 1.09606 1.09750 1.09895 1.10041 1.10189	.913545 .912358 .911164 .909961 .908751 .907533	50 40 30 20 10	66
25	0 10 20 30 40 50	.422618 .425253 .427884 .430511 .433135 .435755	2.3662016 2.3515424 2.3370833 2.3228205 2.3087501 2.2948685	.466308 .469854 .473410 .476976 .480551 .484137	2.1445069 2.1283213 2.1123348 2.0965436 2.0809438 2.0655318	1.10338 1.10488 1.10640 1.10793 1.10947 1.11103	.906308 .905075 .903834 .902585 .901329 .900065	50 40 30 20 10	65
0	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.	,	0

For functions from 64°-10' to 70°-30' read from bottom of table upward.

0	,	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	7	o
26	10 20 30 40 50	.438371 .440984 .443593 .446198 .448799 .451397	2.2811720 2.2676571 2.2543204 2.2411585 2.2281681 2.2153460	.487733 .491339 .494955 .498582 .502219 .505867	2.0503038 2.0352565 2.0203862 2.0056897 1.9911637 1.9768050	1.11260 1.11419 1.11579 1.11740 1.11903 1.12067	.898794 .897515 .896229 .894934 .893633 .892323	50 40 30 20 10	64
27	10 20 30 40 50	.453990 .456580 .459166 .461749 .464327 .466901	2.2026893 2.1901947 2.1778595 2.1656806 2.1536553 2.1417808	.509525 .513195 .516876 .520567 .524270 .527984	1.9626105 1.9485772 1.9347020 1.9209821 1.9074147 1-8939971	1.12233 1.12400 1.12568 1.12738 1.12910 1.13083	.891007 .889682 .888350 .887011 .885664 .884309	50 40 30 20 10	63
28	10 20 30 40 50	.469472 .472038 .474600 .477159 .479713 .482263	2.1300545 2.1184737 2.1070359 2.0957385 2.0845792 2.0735556	.531709 .535447 .539195 .542956 .546728 .550515	1.8807265 1.8676003 1.8546159 1.8417708 1.8290628 1.8164892	1.13257 1.13433 1.13610 1.13789 1.13970 1.14152	.882948 .881578 .880201 .878817 .877425 .876026	50 40 30 20 10	62
29	0 10 20 30 40 50	.484810 .487352 .489890 .492424 .494953 .497479	2.0626653 2.0519061 2.0412757 2.0307720 2.0203929 2.0101362	.554309 .558118 .561939 .565773 .569619 .573478	1.8040478 1.7917362 1.7795524 1.7674940 1.7555590 1.7437453	1.14335 1.14521 1.14707 1.14896 1.15085 1.15277	.874620 .873206 .871784 .870356 .868920 .867476	50 40 30 20 10	61
30	10 20 30 40 50	.500000 .502517 .505030 .507538 .510043 .512543	2.0000000 1.9899822 1.9800810 1.9702944 1.9606206 1.9510577	.577350 .581235 .585134 .589045 .592970 .596908	1.7320508 1.7204736 1.7090116 1.6976631 1.6864261 1.6752988	1.15470 1.15665 1.15861 1.16059 1.16259 1.16460	.866025 .864567 .863102 .861629 .860149 .858662	50 40 30 20 10	60
31	0 10 20 30 40 50	.515038 .517529 .520016 .522499 .524977 .527450	1.9416040 1.9322578 1.9230173 1.9138809 1.9048469 1.8959138	.600861 .604827 .608807 .612801 .616809 .620832	1.6642795 1.6533663 1.6425576 1.6318517 1.6212469 1.6107417	1.16663 1.16868 1.17075 1.17283 1.17493 1.17704	.857167 .855665 .854156 .852640 .851117 .849586	50 40 30 20 10	59
82	0 10 20	.529919 .532384 .534844	1.8870799 1.8783438 1.8697040	.624869 .628921 .632988	1.6003345 1.5900238 1.5798079	1.17918 1.18133 1.18350	.848048 .846503 .844951	0 50 40	58 57
10	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.	,	0

For functions from 57°-40' to 64°-0' read from bottom of table upward.

0	'	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	,	o
82	30 40 50	.537300 .539751 .542197	1.8611590 1.8527073 1.8443476	.637070 .641167 .645280	1.5696856 1.5596552 1.5497155	1.18569 1.18790 1.19012	.843391 .841825 .840251	30 20 10	
88	0 10 20 30 40 50	.544639 .547076 .549509 .551937 .554360 .556779	1.8360785 1.8278985 1.8198065 1.8118010 1.8038809 1.7960449	.649408 653551 .657710 .661886 .666077 .670285	1.5398650 1.5301025 1.5204261 1.5108352 1.5013282 1.4919039	1.19236 1.19463 1.19691 1.19920 1.20152 1.20386	.838671 .837083 .835488 .833886 .832277 .830661	50 40 30 20 10	57
34	0 10 20 30 40 50	.559193 .561602 .564007 .566406 .568801 .571191	1.7882916 1.7806201 1.7730290 1.7655173 1.7580837 1.7507273	.674509 .678749 .683007 .687281 .691573 .695881	1.4825610 1.4732983 1.4641147 1.4550090 1.4459801 1.4370268	1.20622 1.20859 1.21099 1.21341 1.21584 1.21830	.829038 .827407 .825770 .824126 .822475 .820817	50 40 30 20 10	50
35	0 10 20 80 40 50	.573576 .575957 .578332 .580703 .583069 .585429	1.7434468 1.7362413 1.7291096 1.7220508 1.7150639 1.7081478	.700208 .704552 .708913 .713293 .717691 .722108	1.4281480 1.4193427 1.4106098 1.4019483 1.3933571 1.3848355	1.22077 1.22327 1.22579 1.22833 1.23089 1.23347	.819152 .817480 .815801 .814116 .812423 .810723	50 40 30 20 10	51
36	0 10 20 30 40 50	.587785 .590136 .592482 .594823 .597159 .599489	1.7013016 1.6945244 1.6878151 1.6811730 1.6745970 1.6680864	.726543 .730996 .735469 .739961 .744472 .749003	1.3763810 1.3679959 1.3596764 1.3514224 1.3432331 1.3351075	1.23607 1.23869 1.24134 1.24400 1.24669 1.24940	.809017 .807304 .805584 .803857 .802123 .800383	50 40 30 20 10	54
37	0 10 20 80 40 50	.601815 .604136 .606451 .608761 .611067 .613367	1.6616401 1.6552575 1.6489376 1.6426796 1.6364828 1.6303462	.753554 .758125 .762716 .767327 .771959 .776612	1.3270448 1.3190441 1.3111046 1.3032254 1.2954057 1.2876447	1.25214 1.25489 1.25767 1.26047 1.26330 1.26615	.798636 .796882 .795121 .793353 .791579 .789798	50 40 30 20 10	5
38	10 20 30 40 50	.615661 .617951 .620235 .622515 .624789 .627057	1.6242692 1.6182510 1.6122908 1.6063879 1.6005416 1.5947511	.781286 .785981 .790698 .795436 .800196 .804979	1.2799416 1.2722957 1.2647062 1.2571723 1.2496933 1.2422685	1.26902 1 27191 1.27483 1 27778 1.28075 1.28374	.788011 .786217 .784416 .782608 .780794 .778973	50 40 30 20 10	5:
0	,	Cosine.	Secant,	Cotangent.	Tangent.	Cosecant.	Sina,	,	0

For functions from 51°-10' to 57°-30' read from bottom of table upward.

					1				
0	,	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	,	0
89	10 20 30 40 50	.629320 .631578 .633831 .636078 .638320 .640557	1.5890157 1.5833318 1.5777077 1.5721337 1.5666121 1.5611424	.809784 .814612 · .819463 .824836 .829234 .834155	1.2348972 1.2275786 1.2203121 1.2130970 1.2059327 1.1988184	1.28676 1.28980 1.29287 1.29597 1.29909 1.30223	.777146 .775312 .773472 .771625 .769771 .767911	0 50 40 30 20 10	51
40	0 10 20 30 40 50	.642788 .645013 .647233 .649448 .651657 .653861	1.5557238 1.5503558 1.5450378 1.5397690 1.5345491 1.5293773	.839100 .844069 .849062 .854081 .859124 .864193	1.1917536 1.1847376 1.1777698 1.1708496 1.1639763 1.1571495	1.30541 1.30861 1.31183 1.31509 1.31837 1.32168	.766044 .764171 .762292 .760406 .758514 .756615	0 50 40 80 20 10	50
41	0 10 20 30 40 50	.656059 .658252 .660439 .662620 .664796	1.5242531 1.5191759 1.5141452 1.5091605 1.5042211 1.4993267	.869287 .874407 .879553 .884725 .889924 .895151	1.1503684 1.1436326 1.1369414 1.1302944 1.1236909 1.1171305	1.32501 1.32838 1.33177 1.33519 1.33864 1.34212	.754710 .752798 .750880 .748956 .747025 .745088	0 50 40 30 20 10	49
42	0 10 20 30 40 50	.669131 .671289 .673443 .675590 .677732 .679868	1.4944765 1.4896703 1.4849073 1.4801872 1.4755095 1.4708736	.900404 .905685 .910994 .916331 · .921697 .927091	1.1106125 1.1041365 1.0977020 1.0913085 1.0849554 1.0786423	1.34563 1.34917 1.35274 1.35634 1.35997 1.36363	.743145 .741195 .739239 .737277 .735309 .733335	0 50 40 30 20 10	48
43	0 10 20 30 40 50	.681998 .684123 .686242 .688355 .690462 .692563	1.4662792 1.4617257 1.4572127 1.4527397 1.4483063 1.4439120	.932515 .937968 .943451 .948965 .954508 .960083	1.0723687 1.0661341 1.0599381 1.0537801 1.0476598 1.0415767	1.36733 1.37105 1.37481 1.37860 1.38242 1.38628	.731354 .729367 .727374 .725374 .723369 .721357	50 40 30 20 10	47
44	10 20 30 40 50	.694658 .696748 .698832 .700909 .702981 .705047	1.4395565 1.4352393 1.4309602 1.4267182 1.4225134 1.4183454	.965689 .971326 .976996 .982697 .988432 .994199	1.0355303 1.0295203 1.0235461 1.0176074 1.0117088 1.0058348	1.39016 1.39409 1.39804 1.40203 1.40606 1.41012	.719340 .717316 .715286 .713251 .711209 .709161	50 40 30 20 10	46
45	Ö	.707107	1.4142136	1.000000	1.0000000	1.41421	.707107	0	45
•	,	Cosine.	Seant.	Cotangent.	Tangent.	Cosecant.	Sine.	,	0

For functions from 45°-0' to 51°-0' read from bottom of table upward.

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
1.	1	1	1.0000000	1.0000000	1.000000000
2	4	8	1.4142136	1.2599210	.500000000
3	9	27	1.7320508	1.4422496	.333333333
4 .	16	04	2.0000000	1.5874011	.250000000
5	25	125	2.2360680	1.7099759	.200000000
6	36	216	2.4494897	1.8171206	.166666667
7	49	343	2.6457513	1.9129312	.142857143
8	64	512	2.8284271	2.0000000	.125000000
0	81	729	3.0000000	2.0800837	.1111111111
• 10	100	1000	3.1622777	2.1544347	.100000000
11	121	1331	3.3166248	2.2239801	.090909091
12	144	1728	3.4641016	2.2894286	.083333333
13	169	2197	3.6055513	2.3513347	.076923077
14	196	2744	3.7416574	2.4101422	.071428571
15	225	3375	3.8729833	2.4662121	.066666667
16	256	4096	4.0000000	2.5198421	.062500000
17	289	4913	4.1231056	2.5712816	.058823529.
18	324	5832	4.2426407	2.6207414	.05555556
19	361	6859	4.3588989	2.6684016	.052631579
20	400	8000	4.4721360	2.7144177	.050000000
21	441	9261	4.5825757	2.7589243	.047619048
22	484	10648	4.6904158	2.8020393	.045454545
23	529	12167	4.7958315	2.8438670	.043478261
24	576	13824	4.8989795	2.8844991	.041666667
25	625	15625	5.0000000	2.9240177	,0400000000
26	676	17576	5.0990195	2.9624960	.038461538
27	729	19683	5.1961524	3.0000000	.037037037
28	784	21952	5.2915026	3.0365889	.035714286
29	841	24389	5.3851648	3.0723168	.034482759
30	900	27000	5.4772256	3.1072325	.033333333
31	961	29791	5.5677644	3.1413806	.032258065
32	1024	32768	5.6568542	3.1748021	.031250000
33	1089	35937	5.7445626	3.2075343	.030303030
34	1156	39304	5.8309519	3.2396118	.029411765
35	1225	42875	5.9160798	3.2710663	.028571429
36	1296	46656	6.0000000	3.3019272	.027777778
37	1369	50653	6.0827625	3.3322218	.027027027
38	1444	54872	6.1644140	3.3619754	.026315789
39	1521	59319	6.2449980	3.3912114	.025641026
40	1600	64000	6.3245553	3.4199519	.025000000
41	1681	68921	6.4031242	3.4482172	.024390244
42	1764	74088	6.4807407	3.4760266	.023809524
43	1849	79507	6.5574385	3.5033981	023255814
44	1936	85184	6.6332496	3,5303483	.022727273
45	. 2025	91125	6.7082039	3,5568933	.02222222
46	2116	97336	6.7823300	3.5830479	.021739130
47	2209	103823	6.8556546	3.6088261	.021276596
48	2304	110592	6.9282032	3.6342411	.020833333
49	2401	117649	7.0000000	3.6593057	.020408163
50	2400	125000	7.0710678	3.6840314	.020000000
51	2601	132651	7.1414284	3,7084298	.019607843
52	2704	140608	7.2111026	3.7325111	.019230769
58	2809	148877	7.2801099	3.7562858	018867925
54	2916	157464	7.3484692	3.7797631	.018518519
55	3025	166375	7.4161985	3.8029525	.018181818
56	3136	175616	7.4833148	3.8258624	.017857143
57	3249	185193	7.5498344	3.8485011	.017543860
58	3364	195112	7.6157731	3.8708766	.017241379
50	3481	205379	7.6811457	3.8929965	.016949153

No.	Squares.	Cubes.	Square Roots.	Cube Roots,	Reciprocals.
60 61 62 63 64 65 67 67	3600 3721 3844 3969 4096 4225 4356 4489 4624	216000 226981 238328 250047 262144 274625 287496 300763 314432	7.7459667 7.8102497 7.8740079 7.9372539 8.0000000 8.0622577 8.1249384 8.1853528 8.2462113	3.9148676 3.9364972 3.9578915 3.9790571 4.0000000 4.0207256 4.0412401 4.0615480 4.0816551	.016666667 .016393443 .016129032 .015873016 .015625000 .015384615 .015151515 .014925373
70 71 72 73 74 75 76 77 78	4761 4900 5041 5184 5329 5476 5625 5776 5929 6084 6241	328509 343000 357911 373248 389017 405224 421875 438976 456533 474552 493039	8.3066239 8.3666003 8.4261498 8.4852814 8.5440037 8.6023253 8.6602540 8.7177979 8.7749644 8.8317609 8.8881944	4.1015661 4.1212853 4.1408178 4.1601676 4.1793390 4.1933364 4.2171633 4.2358236 4.2543210 4.2726586 4.2908404	.014492754 .014285714 .014084507 .013888889 .013698630 .013513514 .01333333 .013157895 .012987013 .012820513
80 81 82 83 84 85 86 87 88	6400 6561 6724 6889 7056 7225 7396 7599 7744 7921	512000 531441 551368 571787 592704 614125 636056 658503 681472 704969	8.9442719 9.0000000 9.0553851 9.1104336 9.1651514 9.2195445 9.2736185 9.3273791 9.3808315 9.4339811	4.3088695 4.3267487 4.3444815 4.3620707 4.3795191 4.3068296 4.4140049 4.4310476 4.4479602 4.4647451	.012500000 .012345679 .012195122 .012048193 .011904762 .011764706 .011627907 .011494253 .011363636 .011235955
90 91 92 93 94 95 96 97 98	8100 8281 8464 8649 8836 9025 9216 9409 9604 9801	729000 753571 778688 804357 830584 857375 884736 912673 941192 970299	9.4868330 9.5393920 9.5916630 9.6436508 9.6953597 9.7467943 9.7979590 9.8488578 9.8994949 9.9498744	4.4814047 4.4979414 4.5143574 - 4.5306549 4.5468359 4.5629026 4.5788570 4.5947009 4.6104363 4.6280650	.01111111 .010989011 .010869565 .010752688 .010638298 .010526316 .010416667 .010309278 .010204082
100 101 102 103 104 105 106 107 108 109	10000 10201 10404 10609 10816 11025 11236 11449 11664 11881	1000000 1030301 1061208 1092727 1124864 1157625 1191016 1225043 1259712 1295029	10.0000000 10.0498756 10.0995049 10.1488916 10.1980390 10.2469508 10.2956301 10.3440804 10.3923048	4.6415888 4.6570095 4.6723287 4.6875482 4.7026694 4.7176940 4.7326235 4.7474594 4.7622032 4.7768562	.01000000 .009900990 .009803922 .009708738 .009615385 .009523810 .009433902 .009345794 .009259259 .009174312
110 111 112 113 114 115 116 117 118 119	12100 12321 12544 12769 12996 13225 13456 13680 13924 14161	1331000 1367631 1404928 1442897 1481544 1520875 1560896 1601613 1643032 1685159	10.4880885 10.5356538 10.5350528 10.6301458 10.6770783 10.7238053 10.7703296 10.8166538 10.8627805 10.9087121	4.7914199 4.8058955 4.8202845 4.8345881 4.8488076 4.8629442 4.8769990 4.8909732 4.9048681 4.9186847	.009090900 .009009009 .009828571 .008849558 .008771930 .008695652 .008547009 .008474578 .008403361

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
120	14400	1728000	10.9544512	4.9324242	.008333333
121	14641	1771561	11.0000000	4.9460874	.008264463
122	14884	1815848	11.0453610	4.9596757	.008196721
123	15129	1860867	11.0905365	4.9731898	.008130081
124	15376	1906624	11.1355287	4.9866310	.008064516
125	15625	1953125	11.1803399	5.0000000	.008000000
126	15876	2000376	11.2249722	5.0132979	.007936508
127	16129	2048383	11.2694277	5.0265257	.007874016
128	16384	2097152	11.3137085	5.0396842	.007812500
129	16641	2146689	11.3578167	5.0527743	.007751938
130	16900	2197000	11.4017543	5.0657970	.007692308
131	17161	2248091	11.4455231	5.0787531	.007633588
132	17424	2299968	11.4891253	5.0916434	.007575758
133	17689	2352637	11.5325626	5.1044687	.007518797
134	17956	2406104	11.5758369	5.1172299	.007462687
135	18225	2460375	11.6189500	5.1299278	.007407407
136	18496	2515456	11.6619038	5.1425632	.007352941
137	18769	2571353	11.7046999	5.1551367	.007299270
138	19044	2628072	11.7473401	5.1676493	.007246377
139	19321	2685619	11.7898261	5.1801015	.007194245
140	19600	2744000	11.8321596	5.1924941	.007142857
141	19881	2803221	11.8743421	5.2048279	.007092199
142	20164	2863288	11.9163753	5.2171034	.007042254
143	20102	2924207	11.9582607	5.2293215	.006993007
144	20736	2985984	12.0000000	5.2414828	.006944444
145	21025	3048625	12.0415946	5.2535879	.006896552
146	21316	3112136	12.0830460	5.2656374	.006849315
147	21609	3176523	12.1243557	5.2776321	.006802721
148	21904	3241792	12.1655251	5.2895725	.006756757
149	22201	3307949	12.2065556	5.3014592	.006711409
	22500	3375000			
150 151	22801	3442951	12.2474487	5.3132928	.006666667
152	23104	3511808	12.2882057	5.3250740	.006622517
153	23409	3581577	12.3288280 12.3693169	5.3368033	.006578947
154	23716	3652264	12.4096736	5 3484812 5.3601084	.006535948
155	24025	3723875	12.4498996	5.3716854	.006451613
156	24336	3796416	12.4899960	5.3832126	.006410256
157	24649	3869893	12.5299641	5.3946907	.006369427
158	24964	3944312	12.5698051	5.4061202	.006329114
159	25281	4019679	12.6095202	5.4175015	.006289308
160	25600	4096000	12.6491106	5.4288352	
161	25921	4173281	12.6885775	5.4401218	.006250000
162	26244	4251528	12.7279221	5.4513618	.006172840
163	26569	4330747	12.7671453	5.4625556	.006134969
164	26896	4410944	12.8062485	5.4737037	.006097561
165	27225	4492125	12.8452326	5.4848066	.006060606
166	27556	4574296	12.8840987	5.4958647	.006024096
167	27889	4657463	12.9228480	5.5068784	.005988024
168	28224	4741632	12.9614814	5.5178484	.005952381
169	28561	4826809	13.0000000	5.5287748	.005917160
170	28900	4913000	13.0384048	5.5396583	.005882353
171	29241	5000211	13.0766968	5.5504991	.005847953
172	29584	5088448	13.1148770	5.5612978	.005813953
173	29929	5177717	13.1529464	5.5720546	.005780347
174	30276	5268024	13.1909060	5.5827702	.005747126
175	30625	5359375	13.2287566	5.5934447	.005714286
176	30976	5451776	13.2664992	5.6040787	.005681818
177	31329	5545233	13.3041347	5.6146724	.005649718
178	31684	5639752	13.3416641	5.6252263	.005617978
179	32041	5735339	13.3790882	5.6357408	1005586592

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
180	32400	5832000	13.4164079	5.6462162	.005555556
181	32761	5929741	13.4536240	5.6566528	.005524862
182	33124	6028568	13.4907376	5.6670511	.005494505
183	33489	6128487	13.5277493	5.6774114	.005464481
184	33856	6229504	13.5646600	5.6877340	.005434783
185	34225	6331625	13.6014705	5.6980192	.005405405
186	34596	6434856	13.6381817	5.7082675	.005376344
187	34969	6539203	13.6747943	5.7184791	.005347594
188	35344	6644672	13.7113092	5.7286543	.005319149
189	35721	6751269	13.7477271	5.7387936	.005291005
190	36100	6859000	13.7840488	5.7488971	.005263158
191	36481	6967871	13.8202750	5.7589652	.005235602
192	36864	7077888	13.8564065	5.7689982	.005208333
193	37249	7189057	13.8924440	5.7789966	.005181347
194	37636	7301384	13.9283883	5.7889604	.005154639
195	38025	7414875	13.9642400	5.7988900	.005128205
					.000120200
196	38416	7529536	14.0000000	5.8087857	.005102041
197	38809	7645373	14.0356688	5.8186479	.005076142
198	39204	7762392	14.0712473	5.8284767	.005050505
199	39601	7880599	14.1067360	5.8382725	.005025126
200	40000	8000000	14.1421356	5.8480355	.005000000
201	40401	8120601	14.1774469	5.8577660	.004975124
202	40804	8242408	14.2126704	5.8674643	.004950495
203	41209	8365427	14.2478068	5.8771307	.004926108
204	41616	8489664	14.2828569	5.8867653	.004901961
205	42025	8615125	14.3178211	5.8963685	.004878049
				5.9059406	.004854369
206	42436	8741816	14.3527001		
207	42849	8869743	14.3874946	5.9154817	.004830918
208	43264	8998912	14.4222051	5.9249921	.004807692
209	43681	9129329	14.4568323	5.9344721	.004784689
210	44100	9261000	14.4913767	5.9439220	.004761905
211	44521	9393931	14.5258390	5.9533418	.004739336
212	44944	9528128	14.5602198	5.9627320	.004716981
213	45369	9663597	14.5945195	5.9720926	.004694836
214	45796	9800344	14.6287388	5.9814240	.004672897
215	46225	9938375	14.6628783	5.9907264	.004651163
216		10077696	14.6969385	6.0000000	.004629630
	46656			6.0092450	.004608295
217	47089	10218313	14.7309199		
218	47524	10360232	14.7648231	6.0184617	.004587156
219	47961	10503459	14.7986486	6.0276502	.004566210
220	48400	10648000	14.8323970	6.0368107	.004545455
221	48841	10793861	14.8660687	6.0459435	.004524887
222	49284	10941048	14.8996644	6.0550489	.004504505
223	49729	11089567	14.9331845	6.0641270	.004484305
224	50176	11239424	14.9666295	6.0731779	.004464286
225	50625	11390625	15.0000000	6.0822020	.00444444
					.004424779
226	51076	11543176	15.0332964	6.0911994	.004424779
227	51529	11697083	15.0665192	6.1001702	
228	51984	11852352	15.0996689	6.1091147	.004385965
229	52441	12008989	15.1327460	6.1180332	.004366812
230	52900	12167000	15.1657509	6.1269257	.004347826
231	53361	12326391	15.1986842	6.1357924	.004329004
232	53824	12487168	15.2315462	6.1446337	.004310345
223	54289	12649337	15.2643375	6.1534495	.004291845
234	54756	12812904	15.2970585	6.1622401	.004273504
235	55225	12977875	15.3297097	6.1710058	.004255319
				6.1797466	.004237288
236	55696	13144256	15.3622915		
237	56169	13312053	15.3948043	6.1884628	.004219409
238	56644	13481272	15.4272486	6.1971544	.004201681
239	57121	13651919	15.4596248	6.2058218	.004184100

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
240	57600	13824000	15.4919334	6.2144650	.004166667
241	58081	13997521	15.5241747	6.2230843	.004149378
242	58564	14172488	15.5563492	6.2316797	.004132231
243	59049	14348907	15.5884573	6.2402515	.004115226
244	59536	14526784	15.6204994	6.2487998	.004098361
245	60025	14706125	15.6524758	6.2573248	.004081633
246	60516	14886936	15.6843871	6.2658266	.004065041
247	61009	15069223	15.7162336	6.2743054	.004048583
248	61504	15252992	15.7480157	6.2827613	.004032258
249	62001	15438249	15.7797338	6.2911946	.004016064
250	62500	15625000	15.8113883	6.2996053	.004000000
251	63001	15813251	15.8429795	6.3079935	.003984064
252	63504	16003008	15.8745079	6.3163596	.003968254
253	64009	16194277	15.9059737	6.3247035	.003952569
254	64516	16387064	15.9373775	6.3330256	.003937008
255	65025	16581375	15.9687194	6.3413257	.003921569
256	65536	16777216	16.0000000	6.3496042	.003906250
257	66049	16974593	16.0312195	6.3578611	.003891051
258	66564	17173512	16.0623784	6.3660968	.003875969
259	67081	17373979	16.0934769	6.3743111	.003861004
260	67600	17576000	16.1245155	6.3825043	.003846154
261	68121	17779581	16.1554944	6.3906765	.003831418
262	68644	17984728	16.1864141	6.3988279	.003816794
263	69169	18191447	16.2172747	6.4069585	.003802281
264	69696	18399744	16.2480768	6.4150687	.003787879
265	70225	18609625	16.2788206	6.4231583	.003773585
266	70756	18821096	16.3095064	6.4312276	.003759398
267	71289	19034163	16.3401346	6.4392767	.003745318
268	71824	19248832	16.3707055	6.4473057	.003731343
269	72361	19465109	16.4012195	6.4553148	.003717472
270	72900	19683000	16.4316767	6.4633041	.003703704
271	73441	19902511	16.4620776	6.4712736	.003690037
272	. 73984	20123648	16.4924225	6.4792236	.003676471
273	74529	20346417	16.5227116	6.4871541	.003663004
274	75076	20570824	16.5529454	6.4950653	.003649635
275	75625	20796875	16.5831240	6.5029572	.003636364
276	76176	21024576	16.6132477	6.5108300	.003623188
277	76729	21253933	16.6433170	6.5186839	.003610108
278	77284	21484952	16.6733320	6.5265189	.003597122
279	77841	21717639	16.7032931	6.5343351	.003584229
280	78400	21952000	16.7332005	6.5421326	.003571429
281	78961	22188041	16.7630546	6.5499116	003558719
282	79524	22425768	16.7928556	6.5576722	.003546099
283	80089	22665187	16.8226038	6.5654144	003533569
284	80656	22906304	16.8522995	6.5731385	.003521127
285	81225	23149125	16.8819430	6.5808443	.003508772
286	81796	23393656	16.9115345	6.5885323	.003496503
287	82369	23639903	16.9410743	6.5962023	.003484321
288	82944	23887872	16.9705627	6.6038545	.003472222
289	83521	24137569	17.0000000	6.6114890	.003460208
290	84100	24389000	17.0293864	6.6191060	.003448276
291	84681	24642171	17.0587221	6.6267054	.003436426
292	85264	24897088	17.0880075	6.6342874	.003424658
293	85849	25153757	17.1172428	6.6418522	.003412969
294	86436	25412184	17.1464282	6.6493998	.003401361
295	87025	25672375	17.1755640	6.6569302	.003389831
296	87616	25934336	17.2046505	6.6644437	.003378378
297	88209	26198073	17.2336879	6.6719403	.003367003
298	88804	26463592	17.2626765	6.6794200	.003355705
299	89401	26730899	17.2916165	6.6868831	.003344482

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
300 301 302 303 304 305	90000 90601 91204 91809 92416 93025	27000000 27270901 27543608 27818127 28094464 28372625	17.3205081 17.3493516 17.3781472 17.4068952 17.4355958 17.4642492	6.6943295 6.7017593 6.7091729 6.7165700 6.7239508 6.7313155	.003333333 .003322259 .003311258 .003300330 .003289474 .003278689
306 307 308 309	93636 94249 94864 95481	28652616 28934443 29218112 29503629	17.4928557 17.5214155 17.5499288 17.5783958	6.7386641 6.7459967 6.7533134 6.7606143	.003267974 .003257329 .003246753 .003236246
310 311 312 313 314 315 316 317 318 319	96100 96721 97344 97969 98596 90225 90856 100489 101124 101761	29791000 30080231 30371328 30664297 30959144 31255875 31554496 31855013 32157432 32461759	17.6068169 17.6351921 17.6635217 17.6918060 17.7200451 17.7482393 17.7763888 17.8044938 17.8325545 17.8605711	6.7678995 6.7751690 6.7824229 6.7896613 6.7968844 6.8040921 6.8112847 6.8184620 6.8256242 6.8327714	.003225806 .003215434 .003205128 .003194888 .003184713 .003174603 .003164557 .003154574 .003134796
320 321 322 323 324 325 326 327 328 329	102400 103041 103684 104329 104976 105625 106276 106929 107584 108241	32768000 33076161 33386248 33698267 34012224 34328125 34645976 34965783 35287552 35611289	17.885438 17.9164729 17.9443584 17.9722008 18.0000000 18.0277564 18.0554701 18.0831413 18.1107703 18.1383571	6.8399037 6.8470213 6.8541240 6.8612120 6.8682855 6.8763443 6.8823888 6.8894188 6.8964345 6.0034359	.003125000 .003115265 .003105590 .003095975 .003086420 .003076923 .003067485 .003048780 .003048780
330 331 332 333 334 335 356 337 338 338	108900 109561 110224 110889 111556 112225 112896 113569 114244 114921	35987000 36264691 36594368 36926037 37259704 37595375 37933056 38272753 38614472 28958219	18.1659021 18.1934054 18.2208672 18.2482876 18.2756669 18.3030052 18.3303028 18.3575598 18.3847763 18.4119526	6.9104232 6.9173964 6.9243556 6.9313008 6.9382321 6.9451496 B.U520533 6.9589434 6.9688198 6.9726826	.003030803 .003012148 .003012048 .003003003 .002994012 .002985075 .002976190 .002967359 .002958580 .002949853
340 341 842 343 844 845 346 347 348 349	115600 116281 116964 117649 118336 119025 119716 120409 121104 121801	39304000 39651821 40001688 40353607 40707584 41063625 41421736 41781923 42144192 42508549	18.4390889 18.4661853 18.4932420 18.5202592 18.5472370 18.5741758 18.6010752 18.6279360 18.6547581 18.6815417	6.9795321 6.9865851 6.9931906 7.0000000 7.0067962 7.0135791 7.0203490 7.0271058 7.0338497 7.0405806	.002941176 .002923551 .002923977 .002915452 .002906977 .002898551 .002890173 .002881844 .002873563
350 351 352 353 354 355 356 357 358 359	122500 123201 123904 124609 125316 126025 126736 127449 128164 128881	42875000 43243551 43614208 43986977 44361864 44738875 45118016 45499293 45882712 46268279	18.7082569 18.7349040 18.7616630 18.7882942 18.8148877 18.8414437 18.8679623 18.8944436 18.9208879 18.9472953	7.0472987 7.0540041 7.0606967 7.0673767 7.0740440 7.0806988 7.0873411 7.0939709 7.1005885 7.10071937	.002857143 .002849003 .002849009 .002832861 .002834859 .002816901 .002801120 .002793296

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
360	129600	46656000	18.9736660	7.1137866	.002777778
361	130321	47045881	19.0000000	7.1203674	.002770083
362	131044	47437928	19.0262976	7.1269360	.002762431
363	131769	47832147	19.0525589	7.1334925	.002754821
364	132496	48228544	19.0787840	7.1400370	.002747253
865	133225	48627125	19.1049732	7.1465695	.002739726
266	133956	49027896	19.1311265	7.1530901	.002732240
367	134689	49430863	19.1572441	7.1595988	.002732240
368	135424	49836032	19.1833261	7.1660957	.002724790
200		50243409			.002717391
	136161		19.2093727	7.1725809	
370	136900	50653000	19.2353841	7.1790544	.002702703
371	137641	51064811	19.2613603	7.1855162	.002695418
372	138384	51478848	19.2873015	7.1919663	.002688172
373	139129	51895117	19.3132079	7.1984050	.002680965
374	139876	52313624	19.3390796	7.2048322	.002673797
375	140625	52734375	19.3649167	7.2112479	.002666667
376	141376	53157376	19.3907194	7.2176522	.002659574
377	142129	53582633	19.4164878	7.2240450	.002652520
378	142884	54010152	19.4422221	7.2304268	.002645503
379	143641	54439939	19.4679223	7.2367972	.002638522
380	144400	54872000	19.4935887	7.2431565	.002631579
381	145161	55306341	19.5192213	7.2495045	.002624672
382	145924	55742968	19.5448203	7.2558415	.002617801
383	146689	56181887	19.5703858	7.2621675	.002610966
384	147456	56623104	19.5959179	7.2684824	.002604167
385	148225	57066625	19.6214169	7.2747864	.002597403
386	148996	57512456	19.6468827	7.2810794	.002590674
387	149769	57960603	19.6723156	7.2873617	.002583979
888	150544	58411072	19.6977156	7.2936330	.002577320
389	151321	58863869	19.7230829	7.2998936	.002570694
390	152100	59319000	19.7484177	7.3061436	.002564103
391	152881	59776471	19.7737199	7.3123828	.002557545
392	153664	60236288	19.7989899	7.3186114	.002551020
393	154449	60698457	19.8242276	7.3248295	.002544529
394	155236	61162984	19.8494332	7.3310369	.002538071
395	156025	61629875	19.8746069	7.3372339	.002531646
396	156816	62099136	19.8997487	7.3434205	.002525253
397	157609	62570773	19.9248588	7.3495966	.002518892
398	158404	63044792	19.9499373	7.3557624	.002512563
399	159201	63521199	19.9749844	7.3619178	.002506266
400	160000	64000000	20.0000000	7.3680630	.002500000
401	160801	64481201	20.0249844	7.3741979	.002493766
402	161604	64964808	20.0499377	7.3803227	.002487562
403	162409	65450827	20.0499577	7.3864373	.002487362
404					
	163216	65939264	20.0997512	7.3925418	.002475248
405	164025	66430125	20.1246118	7.3986363	.002469136
406	164836	66923416	20.1494417	7.4047206	.002463054
407	165649	67419143	20.1742410	7.4107950	.002457002
408	166464	67917312	20.1990099	7.4168595	.002450980
400	167281	68417929	20.2237484	7.4229142	.002444988
410	168100	68921000	20.2484567	7.4289589	.002439024
411	168921	69426531	20.2731349	7.4349938	.002433090
412	169744	69934528	20.2977831	7.4410189	.002427184
413	170569	70444997	20.3224014	7.4470342	.002421308
414	171396	70957944	20.3469899	7.4530399	.002421303
415	172225	71473375	20.3715488	7.4590359	.002413439
416	173056	71991296	20.3960781	7.4650223	.002409639
417	173889	72511713	20.4205779		
418	174724			7.4709991	.002398082
418		73034632	20.4450483	7.4769664	.002392344
419	175561	73560059	20.4694895	7.4829242	.002386635

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
420	176400	74088000	20,4939015	7.4888724	.002380952
421	177241	74618461	20.5182845	7.4948113	.002375297
422	178084	75151448	20.5426386	7.5007406	.002369668
423	178929	75686967	20.5669638	7.5066607	.002364066
424	179776	76225024	20.5912603	7.5125715	.002358491
425	180625	76765625	20.6155281	7.5184730	.002352941
426	181476	77308776	20.6397674	7.5243652	.002347418
427	182329	77854483	20.6639783	7.5302482	.002341920
428	183184	78402752	20.6881609	7.5361221	.002336449
429	184041	78953589	20.7123152	7.5419867	.002331002
430	184900	79507000	20.7364414	7.5478423	.002325581
431	185761	80062991	20.7605395	7.5536888	.002320186
432	186624	80621568	20.7846097	7.5595263	.002314815
400	187489	81182737	20.8086520	7.5653548	.002309469
434	188356	81746504	20.8326667	7.5711743	.002304147
435	189225	82312875	20.8566536	7.5769849	.002298851
436	190096	82881856	20.8806130	7.5827865	.002293578
437	190969	83453453	20.9045450	7.5885793	.002288330
438	191844	84027672	20.9284495	7.5943633	.002283108
430	192721	84604519	20.9523268	7.6001385	.002277904
440	193600	85184000	20.9761770	7.6059049	.0022727272
441	194481	85766121	21.0000000	7.6116626	.002267574
442	195364	86350888	21.0237960	7.6174116	.002262443
443	196249	86938307	21.0475652	7.6231519	.002257336
444	197136	87528384	21.0713075	7.6288837	.002252252
445	198025	88121125	21.0950231	7.6346067	.002247191
446	198916	88716536	21.1187121	7.6403213	.002242152
447	199809	89314623	21.1423745	7.6460272	.002237136
448	200704	89915392	21.1660105	7.6517247	.002232143
449	201601	90518849	21.1896201	7.6574138	.002227171
450	202500	91125000	21.2132034	7.6630943	.002222222
451	203401	91733851	21.2367606	7.6687665	.002217298
452	204304	92345408	21.2602916	7.6744303	.002212389
453	205209	92959677	21.2837967	7.6800857	.002207506
454	206116	93576664	21.3072758	7.6857328	.002202643
455	207025	94196375	21.3307290	7.6913717	.002197802
456	207936	94818816	21.3541565	7.6970023	.002192982
457	208849	95443993	21.3775583	7.7026246	.002188184
458	209764	96071912	21.4009346	7.7082388	.002183400
459	210681	96702579	21.4242853	7.7138448	.002178649
460	211600	97336000	21.4476106	7.7194426	.002173913
461	212521	97972181	21.4709106	7.7250325	.002169197
462	213444	98611128	21.4941853	7.7306141	.002164502
463	214369	99252847	21.5174348	7.7361877	.002159827
464	215296	99897344	21.5406592	7.7417532	.002155172
465	216225	100544625	21.5638587	7.7473109	.002150538
466	217156	101194696	21.5870331	7.7528606	.002145923
467	218089	101847563	21.6101828	7.7584023	.002141328
468	219024	102503232	21.6333077	7.7639361	.002136752
469	219961	103161709	21.6564078	7.7694620	.002132190
470	220900	103823000	21.6794834	7.7749801	.002127660
471	221841	104487111	21.7025344	7.7804904	.002123142
				7.7859928	.00212814
472	222784	105154048	21.7255610	7 701/1975	.00211416
473	223729	105823817	21.7485632	7.7914875	
474	224676	106496424	21.7715411	7.7969745	.002109705
475	225625	107171875	21.7944947	7.8024538	.002105263
476	226576	107850176	21.8174242	7.8079254	.002100840
477	227529	108531333	21.8403297	7.8133892	.002096436
478	228484	109215352	21.8632111	7.8188456	.002092050
479	229441	109902239	21.8860686	7.8242942	1002087688

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
480	230400	110592000	21.9089023	7.8297353	.002083333
481	231361	111284641	21.9317122	7.8351688	.002079002
482	232324	111980168	21.9544984	7.8405949	.002074689
483	233289	112678587	21.9772610	7.8460134	.002070393
484	234256	113379904	22.0000000	7.8514244	.002066116
485	235225	114084125	22.0227155	7.8568281	.002061856
486	236196	114791256	22.0454077	7.8622242	.002057613
487	237169	115501303	22.0680765	7.8676130	.002053388
488	238144	116214272	22.0907220	7.8729944	.002049180
489	239121	116930169	22.1133444	7.8783684	.002044990
490	240100	117649000	22.1359436	7.8837352	.002040816
491	241081	118370771	22.1585198	7.8890946	.002036660
492	242064	119095488	22.1810730	7.8944468	.002032520
493	243049	119823157	22.2036033	7.8997917	.002028398
494	244036	120553784	22.2261108	7.9051294	.002024291
495	245025	121287375	22.2485955	7.9104599	.002020202
496	246016	122023936	22.2710575	7.9157832	.002016129
497	247009	122763473	22.2934968	7.9210994	.002012072
498	248004	123505992	22.3159136	7.9264085	.002008032
499	249001	124251499	22.3383079	7.9317104	.002004008
500	250000	125000000	22.3606798	7.9370053	.002000000
501	251001	125751501	22.3830293	7.9422931	.001996008
502	252004	126506008	22.4053565	7.9475739	.001992032
503	258009	127263527	22.4276615	7.9528477	.001988072
504	254016	128024064	22.4499443	7.9581144	.001984127
505	255025	128787625	22.4722051	7.9633743	.001980198
506	256036	129554216	22.4944438	7.9686271	.001976285
507	257049	130323843	22.5166605	7.9738731	.001972387
508	258064	131096512	22.5388553	7.9791122	.001968504
509	259081	131872229	22.5610283	7.9843444	.001964637
510	260100	132651000	22.5831796	7.9895697	.001960784
511	261121	133432831	22.6053091	7.9947883	.001956947
512	262144	134217728	22.6274170	8.0000000	.001953125
513	263169	135005697	22.6495033	8.0052049	.001949318
514	264196	135796744	22.6715681	8.0104032	.001945525
515	265225	136590875	22.6936114	8.0155946	.001941748
516	266256	137388096	22.7156334	8.0207794	.001937984
517	267289	138188413	22.7376340	8.0259574	.001934236
518	268324	138991832	22.7596134	8.0311287	.001930502
519	269361	139798359	22.7815715	8.0362935	.001926782
520	270400	140608000	22.8035085	8.0414515	.001923077
521					.001923077
	271441	141420761	22.8254244	8.0466030	
522	272484	142236648	22.8473193	8.0517479	.001915709
523	273529	143055667	22.8691933	8.0568862	.001912046
524	274576	143877824	22.8910463	8.0620180	.001908397
625	275625	144703125	22.9128785	8.0671432	.001904762
526	276676	145531576	22.9346899	8.0722620	.001901141
527	277729	146363183	22.9564806	8.0773743	.001897533
528	278784	147197952	22.9782506	8.0824800	.001893939
529	279841	148035889	23.0000000	8.0875794	.001890359
530	280900	148877000	23.0217289	8.0926723	.001886792
531	281961	149721291	23.0434372	8.0977589	.001883239
532	283024	150568768	23.0651252	8.1028390	.001879699
533					.001876173
	284089	151419437	23.0867928	8.1079128	
534	285156	152273304	23.1084400	8.1129803	.001872659
535	286225	153130375	23.1300670	8.1180414	.001869159
536	287296	153990656	23.1516738	8.1230962	.001865672
537	288369	154854153	23.1732605	8.1281447	.001862197
538	289444	155720872	23.1948270	8.1331870	.001858736
539	290521	156590819	23.2163735	8.1382230	.001855288

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
540 541 542 543 544 545 546 547 548 549	291600 292681 293764 294849 295936 297025 298116 299209 300304	157464000 158340421 159220088 160103007 160989184 161878625 162771336 163667323 164566592	23.2379001 23.2594067 23.2809893 23.3023604 23.3238076 23.3452351 23.366429 23.3880311 23.4093998	8.1432529 8.1482765 8.1532939 8.1583051 8.1633102 8.1683092 8.1733020 8.1782888 8.1833695	.001851852 .001848429 .001845018 .001841621 .001838235 .001834862 .001831502 .001828154
550 551 552 553 554 555 556 557 557	301401 302500 303601 304704 305809 306916 308025 309136 310249 311364	165469149 166375009 167284151 168196608 169112377 170031464 170953875 171879616 172808693 173741112	23.4307490 23.4520788 23.4733892 23.4946802 23.5159520 23.5372046 23.5584380 23.5796522 23.6008474 23.6220236	8.1882441 8.1932127 8.1981753 8.2031319 8.2080825 8.2130271 8.2179657 8.2228985 8.2278254 8.2327463	.001821494 .001818182 .001814882 .001811594 .001805054 .001805054 .001795361 .001795332 .001792115
559 560 561 562 563 564 565 566 567 568	312481 313600 314721 315844 316969 318096 319225 320356 321489 322624 323761	174676879 175616000 176558481 177504328 178453547 179406144 180362125 181321496 182284263 183250432 184220009	23.6431808 23.6643191 23.6854386 23.7065392 23.7276210 23.7486842 23.7697286 23.8117618 23.8327506 23.8327506	8.2376614 8.2425706 8.2474740 8.2523715 8.2572633 8.2621492 8.2670294 8.2767726 8.2816355 8.2864928	.001788909 .001785714 .001782531 .001779359 .001776199 .0017769912 .001766784 .001763668 .00176757469
570 571 572 573 574 576 576 577 578	324900 326041 327184 328329 329476 330625 331776 332929 334084 335241	185193000 186169411 187149248 188132517 189119224 190109375 191102976 192100033 193100552 194104539	23.8746728 23.8956063 23.9165215 23.9374184 23.9582971 23.9791576 24.000000 24.0208243 24.0416306 24.0624188	8.2913444 8.2961903 8.3010304 8.3058651 8.3106941 8.3155175 8.320353 8.3251475 8.3299542 8.3347553	.001754386 .001751313 .001748252 .001742160 .001739130 .001739130 .001730104 .001730104
580 581 582 583 584 585 586 587 588 588 589	336400 337561 338724 339889 341056 342225 343396 344569 345744 346921	195112000 196122941 197137368 198155287 199176704 200201625 201230056 202262003 203297472 204336469	24.0831891 24.1039416 24.1246762 24.1453929 24.1660919 24.1867732 24.2074369 24.2280822 24.2487113 24.2693222	8.3395509 8.3443410 8.3491256 8.3539047 8.3586784 8.3634466 8.3682095 8.3729668 8.37777188 8.3824653	.001724138 .001721170 .001718213 .001715266 .001712329 .001709402 .001709402 .001709680 .001709680
590 591 592 593 594 595 596 597 598 599	348100 349281 350464 351649 352836 354025 355216 356409 357604 358801	205379000 206425071 207474688 208527857 209584584 210644875 211708736 212776173 213847192 214921799	24.2899156 24.3104916 24.3310501 24.3515913 24.3721152 24.3926218 24.4131112 24.4335834 24.4540385 24.4744765	8.3872065 8.3919423 8.3966729 8.4013981 8.4061180 8.4108326 8.4155419 8.4202460 8.4249448 8.4296383	.001694915 .001692047 .001689189 .001686341 .001683502 .001676752 .001677852 .001675042 .0016750442

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals
600	360000	216000000	24.4948974	8.4343267	.001666667
601	361201	217081801	24.5153013	8.4390098	.001663894
602	362404	218167208	24.5356883	8.4436877	.001661130
603	363609	219256227	24.5560583	8.4483605	.001658375
604	364816	220348864	24.5764115	8.4530281	.001655629
605	366025	221445125	24.5967478	8.4576906	.001652893
606	367236	222545016	24.6170673	8.4623479	.001650165
607	368449	223648543	24.6373700	8.4670001	.001647446
608	369664	224755712	24.6576560	8.4716471	.001644737
000	370881	225866529	24.6779254	8.4762892	.001642036
610	372100	226981000	24.6981781	8.4809261	.001639344
611	373321	228099131	24.7184142	8.4855579	.001636661
612	374544	229220928	24.7386338	8.4901848	.001633987
613	375769	230346397	24.7588368	8.4948065	.001631321
614	376996	231475544	24.7790234	8.4994233	.001628664
615	378225	232608375	24.7991935	8.5040350	.001626016
616	379456	233744896	24.8193473	8.5086417	.00162337
617	380689	234885113	24.8394847	8.5132435	.001620740
618	381924	236029032	24.8596058	8.5178403	.00161812
619	383161	237176659	24.8797106	8.5224321	.00161550
620	384400	238328000	24.8997992	8.5270189	.00161290
621	385641	239483061	24.9198716	8.5316009	.00161030
622	386884	240641848	24.9399278	8.5361780	.00160771
623	388129	241804367	24.9599679	8.5407501	.001605130
624	389376	242970624	24.9799920	8.5453173	.00160256
625	390625	244140625	25.0000000	8.5498797	.001600000
626	391876	245314376	25.0199920	8.5544372	.00159744
627	393129	246491883	25.0399681	8.5589899	.00159489
628	394384	247673152	25.0599282	8.5635377	.00159235
629	395641	248858189	25.0798724	8,5680807	.00158982
030	396900	250047000	25.0998008	8.5726189	.00158730
631	398161	251239591	25.1197134	8.5771523	.00158478
632	399424	252435968	25.1396102	8.5816809	.00158227
633	400689	253636137	25.1594913	8.5862047	.00157977
634	401956	254840104	25.1793566	8.5907238	.00157728
635	403225	256047875	25.1992063	8.5952380	.00157480
636	404498	257259456	25.2190404	8.5997476	.00157232
637	405769	258474853	25.2388589	8.6042525	.00156985
638	407044	259694072	25.2586619	8.6087526	.00156739
639	408321	260917119	25.2784493	8.6132480	.00156494
640	409600	262144000	25.2982213	8.6177388	.00156250
641	410881	263374721	25.3179778	8.6222248	.00156006
642	412164	264609288	25.3377189	8.6267063	.00155763
643	413449	265847707	25.3574447	8.6311830	.00155521
644	414736	267089984	25.3771551	8.6356551	.00155279
645	416025	268336125	25.3968502	8.6401226	.00155038
646				8.6445855	.00153058
647	417316 418609	· 269586136 270840023	25.4165301 25.4361947	8.6490437	.00154758
648				8.6534974	.00154321
	419904	272097792	25.4558441	8.6579465	.00154083
649	421201	273359449	25.4754784		1
850	422500	274625000	25.4950976	8.6623911	.00153846
651	423801	275894451	25.5147016	8.6668310	.00153609
652	425104	277167808	25.5342907	8.6712665	.00153374
653	426409	278445077	25.5538647	8.6756974	.00153139
654	427716	279726264	25.5734237	8.6801237	.00152905
655	429025	281011375	25.5929678	8.6845456	.00152671
656	430336	282300416	25.6124969	8.6889630	.00152439
657	431649	283593393	25.6320112	8.6933759	.00152207
658	432964	284890312	25.6515107	8.6977843	.00151975
659	434281	286191179	25.6709953	8.7021882	.00151745

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
660 661 662 663 664 665 666 667 668	435600 430921 438244 439569 440896 442225 443556 444889 446224 447561	287496000 288804781 290117528 291434247 292754944 294079625 295408296 296740963 298077632	25.6904652 25.7099203 25.7293607 25.7487864 25.7681975 25.8069758 25.8263431 25.8456960	8.7065877 8.7109827 8.7153734 8.7153734 8.7197596 8.7241414 8.7285187 8.7328918 8.7372604 8.7416246	.001515152 .001512859 .001510874 .001508296 .001506024 .001503759 .001501502 .001499250
670 671 672 673 674 675 676 677 678 679	447901 448900 450241 451584 452929 454276 455625 456976 458329 459684 461041	299418309 300763000 302111711 303464448 304821217 306182024 307546875 308915776 310288733 311665752 313046839	25.8650343 25.8843582 25.9036677 25.9229628 25.9422435 25.9615100 25.9807621 26.0000000 26.0192237 26.0384331 26.0576284	8.7459846 8.7503401 8.7546913 8.7590383 8.7633809 8.7677192 8.7720532 8.7780330 8.7807084 8.7850293 8.7893465	.001494768 .001492537 .001490313 .001488095 .001485884 .001483680 .001481481 .001479290 .001477105 .001474926
680 681 682 683 684 685 686 687 688	462400 463761 465124 466489 467856 469225 470596 471969 473344 474721	314432000 315821241 317214568 318611987 320013504 321419125 322828856 324242703 325660672 327082769	26.0768096 26.0959767 26.1151297 26.1342687 26.1533937 26.1725047 26.1916017 26.2106848 26.2297541 26.2488095	8.7936593 8.7979679 8.8022721 8.8065722 8.8108681 8.8151598 8.8194474 8.8237307 8.8280099 8.8322850	.001470588 .001468429 .001466276 .001461198 .001451985 .001457726 .001455604 .001453488 .001451379
690 691 692 693 694 695 696 697 698	476100 477481 478864 480249 481636 483025 484416 485809 487204 488601	329509000 329939371 331373888 332812557 334255384 335702375 337153536 338608873 340068392 341532099	26.2678511 26.2868789 26.3058929 26.3248932 26.3438797 26.3628527 26.3818119 26.4007576 26.4196896 26.4386081	8.8365559 8.8408227 8.8450854 8.8493440 8.8535985 8.8578489 8.863375 8.8705757 8.8705757	.001449275 .001447178 .001445001 .001443001 .00144302 .00143849 .001434720 .001432665 .001430615
700 701 702 703 704 705 706 707 708 709	490000 491401 492804 494200 495616 497025 498436 499849 501264 502681	34300000 344472101 345948408 347428927 348913664 350402625 351895816 353393243 354894912 356400829	26.4575131 26.4764046 26.4952826 26.5141472 26.5329983 26.5518361 26.5706605 26.5894716 26.6082694 26.6270539	8.8790400 8.8832661 8.8874882 8.8917063 8.8959204 8.9001304 8.9043366 8.9085387 8.9127369 8.9169311	.001428571 .001426534 .001424501 .001422475 .001420455 .001418440 .001416431 .001414427 .001412429
710 711 712 713 714 715 716 717 718 719	504100 505521 506944 508369 509796 511225 512656 514089 515524 516961	357911000 359425431 360944128 362467097 363994344 365525875 367061696 368601813 370146232 371694959	26.6458252 26.6645833 26.6833281 26.7020598 26.7207784 26.7394839 26.7581763 26.7768557 26.7955220 26.8141754	8.9211214 8.9253078 8.9294902 8.9336687 8.9378433 8.9420140 8.9503438 8.9503438 8.9545029 8.9586581	.001408451 .001406470 .001404494 .001402525 .001400560 .001398601 .001394700 .001394700 .001392758

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
720	518400	373248000	26.8328157	8.9628095	.001388889
721	519841	374805361	26.8514432	8.9669570	.001386963
722	521284	376367048	26.8700577	8.9711007	.001385042
722 723	522729	377933067	26.8886593	8.9752406	.001383126
724	524176	379503424	26.9072481	8.9793766	.001381215
725	525625	381078125	26.9258240	8.9835089	.001379310
726	527076	382657176	26.9443872	8.9876373	.001377410
727	528529	384240583	26.9629375	8.9917620	.001375516
728	529984	385828352	26.9814751	8.9958829	.001373626
729	531441	387420489	27.0000000	8:0000000	.001371742
730	532900	389017000	27.0185122	9.0041134	.001369863
731	534361	390617891	27.0370117	9.0082229	.001367989
732	535824	392223168	27.0554985	9.0123288	.001366120
733	537289	393832837	27.0739727	9.0164309	.001364256
734	538756	395446904	27.0924344	9.0205293	.001362398
735	540225	397065375	27.1108834	9.0246239	.001360544
736	541696	398688256	27.1293199	9.0287149	.001358696
737	543169	400315553	27.1477439	9.0328021	.001356852
738	544644	401947272	27.1661554	9.0368857	.001355014
739	546121	403583419	27.1845544	9.0409655	.001353180
740	547600	405224000	27.2029410	9.0450417	.001351351
741	549081	406869021	27.2213152	9.0491142	.001349528
742	550564	408518488	27.2396769	9.0531831	.001347709
743	552049	410172407	27.2580263	9.0572482	.001345895
744	553536	411830784	27.2763634	9.0613098	.001344086
745	555025	413493625	27.2946881	9.0653677	.001342282
746	556516	415160936	27.3130006	9.0694220	.001340483
747	558009	416832723	27.3313007	9.0734726	.001338688
748	559504	418508992	27.3495887	9.0775197	.001336898
749	561001	420189749	27.3678644	9.0815631	.001335113
750	502500	421875000	27.3861279	0.0850030	.001333333
751	564001	423564751	27.4043792	9.0896392	.001331558
752	565504	425259008	27.4226184	9.0936719	.001329787
753	567009	426957777	27.4408455	9.0977010	.001328021
754	568516	428661064	27.4590604	9.1017265	.001326260
755	570025	430368875	27.4772633	9.1057485	.001324503
756	571536	432081216	27.4954542	9.1097669	.001322751
757	573049	433798093	27 5136330	9.1137818	.001321004
758	574564	435519512	27.5317998	9.1177931	.001319261
759	576081	437245479	27.5499546	9.1218010	.001317523
760	577600	438976000	27.5680975	9.1258053	.001315789
761	579121	440711081	27.5862284	9.1298061	.001314060
762	580644	442450728	27.6043475	9.1338034	.001312336
763	582169	444194947	27.6224546	9.1377971	.001310616
764	583696	445943744	27.6405499	9.1417874	.001308901
765	585225	447697125	27.6586334	9.1457742	.001307190
766	586756	449455096	27.6767050	9.1497576	.001305483
767	588289	451217663	27.6947648	9.1537375	.001303781
768	589824	452984832	27.7128129	9.1577139	.001302083
769	591361	454756609	27.7308492	9.1616869	.001300390
770	592900	456533000	27.7488739	9.1656565	.001298701
771	594441	458314011	27.7668868	9.1696225	.001297017
772	595984	460099648	27.7848880	9.1735852	.001295337
773	597529	461889917	27.8028775	9.1775445	.001293661
774	599076	463684824	27.8208555	9.1815003	.001291990
775	600625	465484375	27.8388218	9.1854527	.001290323
776	602176	467288576	27.8567766	9.1894018	.001288660
777	603729	469097433	27.8747197	9.1933474	.001287001
778	605284	470910952	27.8926514	9.1972897	.001285347

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
780	608400	474552000	27.9284801	9.2051641	.001282051
781	609961	476379541	27.9463772	9.2090962	.001280410
782	611524	478211768	27.9642629	9.2130250	.001278772
783	613089	480048687	27.9821372	9.2169505	
784	614656				.001277139
		481890304	28.0000000	9.2208726	.001275510
785	616225	483736625	28.0178515	9.2247914	.001273885
786	617796	485587656	28.0356915	9.2287068	.001272265
787	619369	487443403	28.0535203	9.2326189	.001270648
788	620944	489303872	28.0713377	9.2365277	.001269036
789	622521	491169069	28,0891438	9.2404333	.001267427
790	624100	493039000			
			28.1069386	9.2443355	.001265823
791	625681	494913671	28.1247222	9.2482344	.001264223
792	627264	496793088	28.1424946	9.2521300	.001262626
793	628840	498677257	28.1602557	9.2560224	.001261034
794	630436	500566184	28.1780056	9.2599114	.001259446
795	632025	502459875	28.1957444	9.2637973	.001257862
796	633616	504358336	28.2134720	9.2676798	.001256281
797	635209	506261573	28.2311884	9.2715592	
798					.001254705
	636804	508169592	28.2488938	9.2754352	.001253133
799	638401	510082399	28.2665881	9.2793081	.001251564
800	640000	512000000	28.2842712	9.2831777	.001250000
801	641601	513922401	28.3019434	9.2870440	.001248439
802	643204	515849608	28.3196045	9.2909072	.001246883
803	644809				
804		517781627	28.3372546	9.2947671	.001245330
	646416	519718464	28.3548938	9.2986239	.001243781
805	648025	521660125	28.3725219	9.3024775	.001242236
806	649636	523606616	28.3901391	9.3063278	.001240695
807	651249	525557943	28.4077454	9.3101750	.001239157
808	652864	527514112	28.4253408	9.3140190	.001237624
809	654481	529475129	28.4429253	9.3178599	.001236094
810	656100	531441000	28.4604989	9.3216975	.001234568
811					
	657721	533411731	28.4780617	9.3255320	.001233046
812	659344	535387328	28.4956137	9.3293634	.001231527
813	660969	537367797	28.5131549	9.3331916	.001230012
814	662596	539353144	28.5306852	9.3370167	.001228501
815	664225	541343375	28.5482048	9.3408386	.001226994
816	665856	543338496	28.5657137	9.3446575	.001225490
817	667489	545338513	28.5832119	9.3484731	.001223990
818	669124	547343432	28.6006993	9.3522857	.001222494
819	670761	549353259	28.6181760	9.3560952	.001221001
820	672400	551368000	28.6356421	9.3599016	.001219512
821	674041	553387661	28.6530976	9.3637049	.001218027
822	675684	555412248	28.6705424	9.3675051	.001216545
823	677329	557441767	28.6879766	9.3713022	.001215067
824	678976	559476224	28.7054002	9.3750963	.001213592
825	680625	561515625	28.7228132	9.3788873	.001213332
826					
	682276	563559976	28.7402157	9.3826752	.001210654
827	683929	565609283	28.7576077	9.3864600	.001209190
828	685584	567663552	28.7749891	9.3902419	.001207729
829	687241	569722789	28.7923601	9.3940206	.001206273
830	688900	571787000	28.8097206	9.3977964	.001204819
831	690561	573856191			.001204318
832			28.8270706	9.4015691	
	692224	575930368	28.8444102	9.4053387	.001201923
833	693889	578009537	28.8617394	9.4091054	.001200480
834	695556	580093704	28.8790582	9.4128690	.001199041
835	697225	582182875	28.8963666	9.4166297	.001197605
836	698896	584277056	28.9136646	9.4203873	.001196172
837	700569	586376253	28.9309523	9.4241420	.001194743
838	702244	588480472	28.9482297	9.4278936	.001193317
	100022				PERMITTER

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
840	705600	592704000	28.9827535	9.4353880	.001190476
841	707281	594823321	29.0000000	9.4391307	.001189061
842	708964	596947688	29.0172363	9.4428704	.001187648
843	710649	599077107	29.0344623	9.4466072	.001186240
844	712336	601211584	29.0516781	9.4503410	.001184834
845	714025	603351125	29.0688837	9.4540719	.001183432
846	715716	605495736	29.0860791	9.4577999	.001182033
847	717409	607645423	29.1032644	9.4615249	.001180638
848	719104	609800192	29.1204396	9.4652470	.001179245
840	720801	611960049	29.1376046	9.4689661	
850	722500	614125000	29.1547595	9.4726824	.001176471
851	724201	616295051	29.1719043	9.4763957	.001175088
852	725904	618470208	29.1890390	9.4801061	.001173709
853	727609	620650477	29.2061637	9.4838136	.001172333
854	729316	622835864	29.2232784	9.4875182	.001170960
855	731025	625026375	29.2403830	9.4912200	.001169591
856	732736	627222016	29.2574777	9.4949188	.001168224
857	734449	629422793	29.2745623	9.4986147	.001166861
858	736164	631628712	29.2916370	9.5023078 9.5059980	.001165501
859	737881	633839779	29.3087018		
860	739600	636056000	29.3257566	9.5096854	.001162791
861	741321	638277381	29.3428015	9.5133699	.001161440
862	743044	640503928	29.3598365	9.5170515	.001160093
863	744769	642735647	29.3768616	9.5207303	.001158749
864	746496	644972544	29.3938769	9.5244063	.001157407
865	748225	647214625	29.4108823	9.5280794	.001156069
866	749956	649461896	29.4278779	9.5317497	.001154734
867	751689	651714363	29.4448637	9.5354172	.001153403
868	753424	653972032	29.4618397	9.5390818	.001152074
889	755161	656234909	29.4788059	9.5427437	
870	756900	658503000	29.4957624	9.5464027	.001149425
871	758641	660776311	29.5127091	9.5500589	.001148106
872	760384	663054848	29.5296461	9.5537123	.001146789
873	762129	C65338617	29.5465734	9.5573630	.001145475
874	763876	667627624	29.5634910	9.5610108	.001144165
875	765625	669921875	29.5803989	9.5646559	.001142657
876	767376	672221376	29.5972972	9.5682982 9.5719377	.001141353
877	769129	674526133 676836152	29.6141858 29.6310648	9.5755745	.001138952
878	770884		29.6479342	9.5792085	.001137656
879	772641	679151439			***************************************
880	774400	681472000	29.6647939	9.5828397	.001136364
881	776161	683797841	29.6816442	9.5864682	.001135074
882	777924	686128968	29.6984848	0.5900939	.001133787
883	779689	688465387	29.7153159	9.5937169	.001132503
884	781456	690807104	29.7321375	9.5973373 9.6009548	.001131222
885 880	783225 784996	693154125 695506456	29.7489496 29.7657521	9.6045696	.001128668
887	786769	697864103	29.7825452	9.6081817	.001127396
888	788544	700227072	29.7993289	9.6117911	.001126126
889	790321	702595369	29.8161030	9.6153977	.001124859
			29.8328678		.001123598
890 891	792100	704969000	29.8328678	9.6190017 9.6226030	.001123390
891	793881	707347971 709732288	29.8663690	9.6262016	.001121076
893	795664			9.6297975	.001119821
894	797449 799236	712121957 714516984	29.8831056 29.8998328	9.6333907	.001118568
895	801025	716917375	29 9165506	9.6369812	.001117318
896	802816	719323136	29.9332591	9.6405690	.001116071
897	804609	721734273	29.9499583	9.6441542	.001114827
898	806404	724150792	29.9666481	9.6477367	.001113586
899	808201	726572699	29.9833287	9,6513166	.001112347

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
900	810000	729000000	30.0000000	9.6548938	.001111111
901	811801	731432701	30.0166620	9.6584684	.001109878
902	813604	733870808	30.0333148	9.6620403	.001108647
903	815409	736314327	30.0499584	9.6656096	.001107420
904	817216	738763264	30.0665928	9.6691762	.001106195
905	819025	741217625	30.0832179	9.6727403	.001104972
906	820836	743677416	30.0998339	9.6763017	.001103753
907	822649	746142643	30.1164407	9.6798604	.001103733
908	824464	748613312	30.1330383	9.6834166	.001102330
909	826281	751089429	30.1496269	9.6869701	.001100110
910	828100	753571000	30.1662063	9.6905211	.001098901
911	829921	756058031	30.1827765	9.6940694	.001097695
912	831744	758550528	30.1993377	9.6976151	.001096491
913	833569	761048497	30.2158899	9.7011583	.001095290
914	835396	763551944	30.2324329	9.7046989	.001094092
915	837225	766060875	30.2489669	9.7082369	.001092896
918	839056	768575296	30.2654919	9.7117723	.001091703
917	840889	771095213	30.2820079	9.7153051	.001090513
918	842724	773620632	30.2985148	9.7188354	.001089325
919	844561	776151559	30.3150128	9.7223631	.001088139
920	846400	778688000	30.3315018	9.7258883	.001086957
921	848241	781229961	30.3479818	9.7294109	.001085776
922	850084	783777448	30.3644529	9.7329309	.001084599
923	851929	786330467	30.3809151	9.7364484	.001083424
924	853776	788889024	30.3973683	9 7399634	.001082251
925	855625	791453125	30.4138127	9.7434758	.001081081
926	857476	794022776	30.4302481	9.7469857	.001079914
927	859329	796597983	30.4466747	9,7504930	.001078749
928	861184	799178752	30.4630924	9.7539979	.001077586
929	863041	801765089	30.4795013	9.7575002	.001076426
930	864900	804357000			
931			30.4959014	9.7610001	.001075269
	866761	806954491	30.5122926	9.7644974	.001074114
932	868624	809557568	30.5286750	9.7679922	.001072961
933	870489	812166237	30.5450487	9.7714845	.001071811
934	872356	814780504	30.5614136	9.7749743	.001070664
935	874225	817400375	30.5777697	9.7784616	.001069519
936	876096	820025856	30.5941171	9.7819466	.001068376
937	877969	822656953	30.6104557	9.7854288	.001067236
938	879844	825293672	30.6267857	9.7889087	.001066098
939	881721	827936019	30.6431069	9.7923861	.001064963
940	883600	830584000	30.6594194	9.7958611	.001063830
941	885481	833237621	30.6757233	9.7993336	.001062699
942	887364	835896888	30.6920185	9.8028036	.001061571
943	889249	838561807	30.7083051	9.8062711	.001060445
944	891136	841232384	30.7245830		.001000443
				9.8097362	
945	893025	843908625	30.7408523	9.8131989	.001058201
946	894916	846590536	30.7571130	9.8166591	.001057082
947	896809	849278123	30.7733651	9.8201169	.001055966
948	898704	851971392	30.7896086	9.8235723	.001054852
949	900601	854670349	30.8058436	9.8270252	.001053741
950	902500	857375000	30.8220700	9.8304757	.001052632
951	904401	860085351	30.8382879	9.8339238	.001051525
952	906304	862801408	30.8544972	9.8373695	.001050420
953	908209	865523177	30.8706981	9.8408127	.001049318
954	910116	868250664	30.8868904	9.8442536	.001048218
955	912025	870983875	30.9030743	9.8476920	.001047120
956	913936	873722816	30.9192497	9.8511280	.001047120
957	915849	876467493	30.9354166	9.8545617	.001040025
958 959	917764	879217912 881974079	30.9515751	9.8579929 9.8614218	.001043841
	919681		30.9677251		

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
960	921600	884736000	30.9838668	9.8648483	.001041667
961	923521	887503681	31.0000000	9.8682724	.001040583
962	925444	890277128	31.0161248	9.8716941	.001039501
963	927369	893056347	31.0322413	9.8751135	.001038422
964	929296	895841344	31.0483494	9.8785305	.001037344
965	931225	898632125	31.0644491	9.8819451	.001036269
966	933156	901428696	31.0805405	9.8853574	.001035197
967	935089	904231063	31.0966236	9.8887673	.001034126
968	937024	907039232	31.1126984	9.8921749	.001033058
969	938961	909853209	31.1287648	9.8955801	.001031992
970	940900	912673000	31.1448230	9.8989830	.001030928
971	942841	915498611	31.1608729	9.9023835	.001029866
972	944784	918330048	31.1769145	9.9057817	.001028807
973	946729	921167317	31.1929479	9.9091776	.001027749
974	948676	924010424	31.2089731	9.9125712	.001026694
975 976	950625 952576	926859375 929714176	31.2249900 31.2409987	9.9159624	.001025641
977	954529	932574833	31.2569992	9.9193513 9.9227379	.001024590
978	956484	935441352	31.2729915	9.9261222	.001022495
979	958441	938313739	31.2889757	9.9295042	.001021450
980	960400		31.3049517	9,9328839	.001020408
981	962361	941192000 944076141	31.3209195	9.9362613	.001020408
082	964324	946966168	31.3368792	9.9396363	.001018330
983	966289	949862087	31.3528308	9.9430092	.001017294
984	968256	952763904	31.3687743	9.9463797	.001016260
985	970225	955671625	31.3847097	9.9497479	.001015228
986	972196	958585256	31.4006369	9.9531138	.001014199
987	974169	961504803	31.4165561	9.9564775	.001013171
988	976144	964430272	31.4324673	9.9598389	.001012146
989	978121	967361669	31.4483704	9.9631981	.001011122
990	980100	970299000	31.4642654	9.9665549	.001010101
991	982081	973242271	31.4801525	9.9699095	.001009082
992	984064	976191488	31.4960315	9.9732619	.001008065
993	986049	979146657	31.5119025	9.9766120	.001007049
994	988036	982107784	31.5277655	9.9799599	.001006036
995	990025	985074875	31.5436206	9.9833055	.001005025
996	992016	988047936	31.5594677	9.9866488	.001004016
997	994000 996004	991026973 994011992	31.5753068 31.5911380	9.9899900 9.9933289	.001003009
888	998001	997002999	31.6069613	9.9966656	.001002004
1000	1000000 1002001	1000000000 1003003001	31.6227766 31.6385840	10.0000000 10.0033322	.001000000
1002	1004004	1006012008	31.6543836	10.0066622	.0009980040
1002	1006009	1009027027	31.6701752	10.0099899	.0009970090
1004	1008016	1012048064	31.6859590	10.0133155	.0009960159
1005	1010025	1015075125	31.7017349	10.0166389	.0009950249
1006	1012036	1018108216	31.7175030	10.0199601	.0009940358
1007	1014049	1021147343	31.7332633	10.0232791	.0009930487
1008	1016064	1024192512	31.7490157	10.0265958	.0009920635
1009	1018081	1027243729	31.7647603	10.0299104	.0009910803
1010	1020100	1030301000	31.7804972	10.0332228	.0009900990
1011	1022121	1033364331	31.7962262	10.0365330	.0009891197
1012	1024144	1036433728	31.8119474	10.0398410	.0009881423
1013	1026169	1039509197	31.8276609	10.0431469	.0009871668
1014	1028196	1042590744	31.8433666	10.0464506	.0009861933
1015	1030225	1045678375	31.8590646	10.0497521	.0009852217
1016	1032256	1048772096	31.8747549	10.0530514	.0009842520
1017 1018	1034289 1036324	105 <b>1</b> 871913 1054977832	31.8904374	10.0563485	.0009832842
1018	1038361	1054977832	31.9061123 31.9217794	10.0596435 10.0629364	.0009823183
1019	1000001	1000000000	01.0211139	10.0028009	.0000010043

Fraction	0	1	2	3	4	5
0 1 64 3 32	.000000 .000244 .000977	1.00000 1.03149 1.06348	4.00000 4.06274 4.12598	9.00000 9.09399 9.18848	16.00000 16.12524 16.25098	25.00000 25.15649 25.31341
64	.002197	1.09595	4.18970	9.28345	16.37720	25.47098
8 16 64 3 7 32	006104	1.16235	4.31860	9.57591 9.47485 0.57129	16.63110 16.75879	25.7873
64	.011963	1.23071	4.44946	9.66821	16.65696	26.1057
9 1/8	.015625	1.26563	4.51563	9.76563 9.86353	17.01563 17.14478	26.3666
64 5 11 32 64 ··	.024414	1.33691 1.37329	4.64941 4.71704	9.96191 10.05079	17.27441 17.40454	26.5869 26.7482
13 16 64	.035166 .041260	1.41016 1.44751	4.78516	10.16016 10.26001	17.53516 17.68625	26.9101
15 32 64 ··	.047862 .054932	1.48535 1.52368	4.92285	10.36035 10.46118	17.79785 17.92993	27.235B 27.3986
17 1/4	.062500 .070557	1.56250	5.06250 5.13806	10.56250	18.06250 18.19556	27.5625 27.7268
64 9 19 32 64 ··	.079102	1.64160 1.68188	5.20410 5.27563	10.76860	18.32910 18.46313	27.8916 28.0568
2i 16 64 ii	1097656	1.72266 1.76392	5.34766 5.42017	10.97266 11.07642	18.59765 18.73267	28.2226 28.3889
64 ii 23 32 64 ··	.118164	1.80556 1.84790	5.49316 5.58665	11.18068 11.28540	18.86816 19.00415	28.5556
25 3/8 64 ii	.140625	1.89063	5.64063 5.71509	11.39063	19.14063 19.27759	28.8906
$\begin{array}{ccc}  & \overline{64} & \underline{13} \\  & \underline{27} & \overline{32} \\  & \underline{64} & \cdots \end{array}$	.165039	1.97754 2.02173	5.79004 5.86548	11.60254 11.70923	19.41504 19.55298	29.2275 29.2967
29 16 64 16	.191406	2.06641 2.11157	5.94141 6.01782	11.81641 11.92407	19.69141 19.83032	29.5664
64 <u>i5</u> 31 32 64 ··	.219727 .254619	2.15723 2.20337	6.09473 6.17212	19.03923 12.14087	19.96973 20.10962	29.9072 30.0783
33 1/2 64 iż	250000	2,25000	6.25000	12.25000	20.25000	30.2500
$\frac{64}{35}$ $\frac{17}{32}$	282227	2.34473	6.40723 6.48657	18.46973 12.58032	20.53223	30.5947
37 16 64 jà	1316406 1334229	2.44141 2.49048	6.56541	12.69141 12.80299	20.81641	30.9414
64 <u>i 9</u> 39 32 64 ··	352539 371338	2.54004 2.59009	6.72754 6.80884	12.91504 13.02759	21.10254 21.24634	31.2900 31.4650
4i 5/8	390625	2.64063	6.89063	13.14063 13.25416	21.39063	31.6406
64 21 43 32 64 ··	.430564 .451416	2.74316 2.79517	7.05566 7.13892	13.36816	21.68066 21.82642	31.9931 32.1701
45 16 16 23	472656	3.84766 2.90063	7.22266 7.30688	13.59766	21.97266 23.11938	32.3476
64 23 47 32 64 ··	.516602 .539307	2.95410 3.00806	7.39160 7.47681	13.82910	22.26660 22.41431	32.7641

Fraction	6	7	8	9	10	11
0 64 3 64 1 32 64	36.09000 36.18774 36.37598 35.56470	49.00000 49.21899 40.43848 49.65845	64.00000 64.25024 64.50098 64.75220	81.00000 81.28140 81.56348 81.54595	100.00000 100.31274 100.62598 100.93970	121.00000 121.34399 121.68846 122.03346
$\begin{array}{cccc} & & & \frac{1}{16} \\ \hline & 64 & & \frac{3}{3} \\ \hline & 7 & & & \\ \hline & 64 & & & \\ \end{array}$	36.75391 36.94360 37.13379 37.32446	49.87891 50.09985 50.32129 50.64321	65.00391 65.25610 65.60879 65.76196	82.12391 82.41235 82.69629 82.98071	101.25391 101.56860 101.88379 102.19946	122.37891 122.72486 123.07129 123.41821
9 64 11 64 32	37.51563 37.70728 37.89941 38.09204	50.76563 50.98853 51.21191 51.43579	66.01563 66.26978 66.53441 66.77954	83.26563 83.55103 83.85691 84.12329	102.51563 102.83228 103.14941 103.46704	123.76563 124.11353 124.46191 124.81079
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	38.28516 38.47876 38.67285 38.86743	51.66016 51.88501 52.11035 52.33618	67.03516 67.29126 67.54785 67.80493	84.41016 84.69751 84.98535 85.27368	103.78516 104.10376 104.42285 104.74243	125.16016 125.51001 125.86035 126.21118
17 64 19 32 64	39.06250 39.25806 39.45410 89.65063	52.56250 52.78931 53.01660 53.24438	68.06250 68.32056 68.57910 68.83813	85.56250 85.85181 86.14160 86.43188	105.06250 105.38306 105.70410 106.02563	126.56250 126.91431 127.26660 127.61938
2i 5 64 ii 23 32 64 ··	39.84766 40.04517 40.24316 40.44165	53.47266 53.70142 53.93066 54.16040	69.09766 69.35767 69.61816 69.87915	86.72266 87.01392 87.30566 87.59790	106.34766 106.67017 106.99316 107.31665	127.97266 128.32642 128.68066 129.03540
25 64 27 64 27 64	40.64063 40.84009 41.04004 41.24048	54.39063 54.62134 54.85254 55.08423	70.14063 70.40289 70.66504 70.92798	87.89063 88.18384 88.47754 88.77173	107.64063 107.96509 108.29004 108.61548	129.39063 129.74634 130.10254 130.45923
$\begin{array}{cccc}  & 7 \\  & 16 \\  & 64 \\  & 15 \\  & 32 \\  & 64 \\  & & & \\ \end{array}$	41.44141 41.64282 41.84473 43.04712	55.31641 55.54907 55.78223 56.01587	71.19141 71.45532 71.71973 71.98462	89.06641 89.36157 89.65723 89.95337	108.94141 109.26782 109.59473 109.92212	130.81641 131.17407 131.53223 131.89087
$\frac{33}{64}$ $\frac{1}{2}$ $\frac{35}{64}$ $\frac{17}{32}$ $\frac{35}{64}$	42.25000 42.45337 42.65723 42.86157	56.25000 56.48462 56.71973 56.95532	72.25000 72.51587 72.78222 73.04907	90.25000 90.54712 90.84473 91.14282	110.25000 110.57837 110.90723 111.23657	132.25000 132.60962 132.96973 133.33032
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	43.06641 43.27173 43.47754 43.68384	57.19141 57.42798 57.66504 57.90259	73.31641 73.58423 73.85254 74.12134	91.44141 91.74048 92.04004 92.34009	111.56641 111.89673 112.22754 112.55884	133.69141 134.05298 134.41504 134.77759
41 64 21 43 64	43.89063 44.09790 44.30566 44.51392	58.14063 58.37915 58.61816 58.85767	74.39063 74.66040 74.93066 75.20142	92.64063 92.94165 93.24316 93.54517	112.89063 113.22290 113.55566 113.88892	135.14063 135.50415 135.86816 136.23267
45 11 64 23 47 32	44.72266 44.93188 45.14160 45.35181	59.09766 59.33812 59.57910 59.82086	75.47266 75.74438 76.01660 76.28931	93.84766 94.15063 94.45410 94.75906	114,22266 114,55688 114,89160 115,22681	136.59766 136.96313 137.32910 137.69556

Fraction	0	1	2	8	4	5
49 64 51 34 64 25 32	.562500 .586182 .610352 .635010	3.06250 3.11743 3.17285 3.22576	7.56250 7.64868 7.73535 7.82251	14.06250 14.17993 14.29785 14.41626	22.56250 22.71118 22.86035 23.01001	33.0625 33.2424 33.4228 33.6037
\$3 16	1660156	3.20516	7,91016	14.53516	23.16016	33.7851
64 27	1685791	3.34204	7,99829	14.65454	23.31079	33.9670
85 32	1711914	3.39941	8,08691	14.77441	23.46191	34.1494
64	1738525	3.45728	8,17608	14.89478	23.61353	34.3322
\$7 7/8	.765625	3.51563	8.26563	15.01563	23.76563	34.5156
\$7 64 29	.793213	3.57446	8.35571	15.13698	23.91821	34.6994
\$9 32	.821289	3.63379	8.44629	15.25879	24.07129	34.8837
\$64	.849854	3.69360	8.53735	15.38110	24.22485	35.0686
61 15	.878906	3.75391	8.62891	15.50391	24.37891	35.2539
64 31	.908447	3.81470	8.72095	15.62720	24.53345	35.4397
63 32	.938477	3.87598	8.81348	15.75098	24.68848	35.6259
64 ··	.968994	3.93774	8.90649	15.87524	24.84399	35.8127
Fraction	12	13	14	15	16	17
0 1 32 1 3 16 32 16	144.0000 144.7510 145.5039 146.2588	169.0000 169.8135 170.6289 171.4463	196.0000 196.8760 197.7539 198.6338	225.0000 225.9385 226.8789 227.8213	256.0000 257.0010 258.0039 259.0088	289.000 290.063 291.128 292.196
··· 1/8	147.0156	173.2656	199.5156	228.7658	260.0156	293,265
32 ··· 3	147.7744	173.0869	200.3994	229.7119	261.0244	294,336
··· 36	148.5352	173.9102	201.2852	230.6602	262.0352	295,410
··· 16	149.2979	174.7354	202.1725	231.6104	263.0479	296,485
$\begin{array}{ccc}  & \frac{1}{4} \\  & \frac{9}{32} \\  & \frac{1}{16} \\  & \frac{1}{32} \\  & \ddots \\  & \dots \\  & \ddots \\  & \dots \\  $	150.0625	175.5625	203.0625	232.5625	264.0625	297.562
	150.8291	176.3916	203.9541	233.5166	265.0791	298.641
	151.5977	177.2227	204.8477	234.4727	266.0977	299.722
	152,3682	178.0557	205.7432	235.4307	267.1182	300.805
$\frac{13}{32}$ $\frac{3}{8}$ $\frac{15}{32}$ $\frac{7}{16}$ $\frac{15}{32}$	153.1406	178.8906	206.6406	236.3906	268.1406	301.890
	153.9150	179.7275	207.5400	237.3525	269.1650	302.977
	154.6914	180.5664	208.4414	238.3164	270.1914	304.066
	155.4697	181.4072	209.3447	239.2822	271.2197	305.157
$\begin{array}{ccc} \frac{\mathbf{i} \dot{7}}{32} & \frac{\mathbf{I}/2}{9} \\ \underline{\mathbf{i} \dot{9}} & \overline{16} \\ \underline{32} & \ddots & \\ \end{array}$	156.2500	182.2500	210.2500	240.2500	272.2500	306,250
	157.0322	183.0947	211.1572	241.2197	273.2822	307,344
	157.8164	183.9414	212.0664	242.1914	274.3164	308,441
	158.6035	184.7900	213.9775	243.1650	275.3525	309,540
21 5/8	159.3906	185.6406	213.8906	244.1406	276.3906	310.640
32 11	160.1807	186.4932	214.8057	245.1182	277.4307	311.743
23 16	160.9727	187.3477	215.7227	246.0977	278.4727	312.847
32	161.7666	188.2041	216.6416	247.0791	279.5166	313.954
$\frac{25}{32}$ $\frac{3}{16}$ $\frac{27}{32}$ $\frac{13}{16}$ $\frac{27}{32}$ $\frac{1}{16}$	162.5625	189.0625	217.5625	248.0625	280,5625	315.062
	163.3604	189.9229	218.4854	249.0479	281,6104	316.172
	164.1602	190.7852	219.4102	250.0352	282,6602	317.285
	164.9619	191.6494	220.3369	251.0244	283,7119	318.399
29 32 31 31 32 16	165.7656 166.5713 167.3789 168.1885	192.5156 193.3839 194.2539 195.1260	221.2656 222.1963 223.1289 224.0635	252.0156 253.0088 254.0039 255.0010	284.7656 285.8213 286.8789 287.9385	319.515 320.633 321.753 322.876

Fractio	n	6	7	8	9	10	11
	4	45.56250	60.06250	76.56250	95.06250	115.56250	138.06250
	5	45.77368	60.30493	76.83618 77.11035	95.36743 95.67285	115.89868	138.42993
	2	46.19751	60.79126	77.38501	95.97876	116.23535 116.57251	138.79785
64		40.19101	60.13120	11.30001	30.31010	110.01201	109.10020
22 1	3	46.41016	61,03516	77.66016	96,28516	116.91016	139,53516
		46.62329	61.27954	77.93579	96.59204	117.24829	139.90454
	7	46.83691	61.52441	78.21191	96.89941	117.58691	140.27441
		47.05103	61.76978	78.48853	97.20728	117.92603	140.64478
7	16					********	*** ****
	8	47.26568	62.01563	78.76563	97.51563	118.26563	141.01563
	9	47.48071	62.26196	79.04321 79.32129	97.82446 98.13379	118.60571 118.94629	141.38696 141.75879
	2	47.91235	62.75610	79.59985	98.44360	119.28735	142.13110
		21.01200	UM. 10020	13.03300	30.42000	113.20100	122.10110
:: 7	5	48.12891	63.00391	79.87891	98.75391	119.62891	142.50391
		48.34595	63.25220	80.15845	99.06470	119.97095	142.87720
	1 2	48.56348	63.50098	80.43848	99.37598	120.31348	143.25098
63 3		48.78149	63.75024	80.71899	99.68774	120.65649	143.62524
Fractio	n	18	19	20	21	22	23
	0	324,0000	361,0000	400.0000	441.0000	484.0000	529.0000
-	-	325,1260	362.1885	401.2510	442.3135	485.3760	530,4385
32	1 6	326.2539	363.3789	402,5039	443.6289	486.7539	531.8789
	6	327,3838	364.5713	403,7588	444.9463	488,1338	533.3213
1	8	328.5156	365.7656	405.0156	446.2656	489.5156	534.7656
5 7		329.6494	366.9619	406.2744	447.5869	490.8994	536.2119
7 1	3	330.7852	368.1602	407.5352	448.9102	492.2852	537.6602
32 .		331.9229	369.3604	408.7979	450.2354	493.6729	539.1104
. 1	4	333.0625	370.5625	410.0625	451,5625	495.0625	540.5625
		334.2041	371.7666	411.3291	452.8916	496.4541	542.0166
	5_	335,3477	872,9727	412,5977	454.2227	497.8477	543.4727
<u>ii</u> 1	. 6	336.4932	374.1807	413.8682	455.5557	499.2432	544.9307
	8	337.6406	375.3906	415.1406	456.8906	500.6406	546.3906
13 3	7 6	338.7900	376.6025	416.4150	458.2275	502.0400	547.8525
15 1 32 .	6	339.9414	377.8164	417.6914	459.5664	503.4414	549.8164
		341.0947	379.0322	418.9697	460.9072	504.8447	550.7822
1: 3	2	\$42,2500	380.2500	420.2500	462.2500	506.2500	552.2500
12	9	343.4072	381.4697	421.5322	463.5947	507.6572	553.7197
is I	6	344.5664	382.6914	422.8164	464.9414	509.0664	555.1914
32 .		345.7275	383.9150	424.1025	466.2900	510.4775	556.6650
5	18	346.8906	385,1406	425.3906	467.6406	511.8906	558.1406
		348.0557	386.3682	426.6807	468.9932	513.3057	559.6182
33 1	i 6	349.2227	387.5977	427.9727	470.3477	514.7227	561.0977
23 32		350.3916	388.8291	429.2666	471.7041	516.1416	562.5791
3,	4	351.5625	390,0625	430,5625	473.0625	517.5625	564.0625
		352.7354	391.2979	431.8604	474.4229	518.9854	565.5479
32 1	3	253.9102	392.5352	433.1602	475.7852	520.4102	567.0352
		255.0869	393.7744	434.4619	477.1494	521.8369	568.5244
67	1/8	356,2656	395,0156	435,7656	478.5156	523,2656	570,0156
		357.4463	396.2588	437.0713	479.8838	524.6963	571.5088
02 1	5	258.6289	397.5039	438.3789	481.2539	526.1289	573.0039
3i 1		359.8135	398.7510	439,6885			574.5010

******								
No.	0	1/8	1/4	3/8	1/2	5/8	3/4	7/8
24	576	582.0156	588.0625	594.1408	600.25	606.3906	612.5625	618.7656
25	625	631.2656	637.5625	643.8906	650.25	656.6406	663.0625	669.5156
26	676	682.5156	689.0625	695.6406	702.25	708.8906	715.5625	722.2656
27	729	735.7656	742.5625	749.3906	756.25	763.1406	770.0625	777.0156
28	784	791.0156	798.0625	805.1406	812.25	819.3906	826.5625	833,7656
29	841	848.2656	855.5625	862.8906	870.25	877.6406	885.0625	892.5156
30	900	907.5156	915.0625	922.6406	930.25	937.8906	945.5625	953.2656
31	961	968.7656	976.5625	984.3906	992.25	1000.1406	1008.0625	1016.0156
32	1024	1032.0156	1040.0625	1048.1406	1056.25	1064.3908	1072.5625	1080.7656
33	1089	1097.2656	1105.5625	1113.8906	1122.25	1130.6406	1139.0625	1147.5156
34	1156	1164.5156	1173.0625	1181.6406	1190.25	1198.8906	1207.5625	1216.2656
35	1225	1233.7656	1242.5625	1251.3908	1260.25	1269.1406	1278.0625	1287.0156
36	1296	1305.0156	1314.0625	1323.1406	1332.25	1341.3906	1350.5625	1359.7656
37	1369	1378.2656	1387.5625	1396.8906	1406.25	1415.6406	1425.0625	1434.6156
38	1444	1453.5156	1463.0625	1472.6406	1482.25	1491.8906	1501.5625	1511.2656
39 40	1521	1530.7656 1610.0156	1540.5625 1620.0625	1550.3906 1630.1406	1560.25	1570.1406 1650.3966	1580.0625 1660.5625	1590.0156 1670.7656
41	1681	1691.2656	1701.5625	1711.8906	1722.25	1732.6406	1743.0625	1753,5156
42	1764	1774.5156	1785.0625	1795.6406	1806.25	1816.8908	1827.5625	1838,2656
43	1849	1859.7656	1870.5625	1881.3906	1892.25	1903.1406	1914.0625	1925,0156
44	1936	1947.0156	1958.0625	1969.1406	1980.25	1991.3906	2002.5626	2013,7656
45	2025	2036.2656	2047.5625	2058.8906	2070.25	2081.6406	2093.0625	2104.5156
47	2209	2220.7656	2232.5625	2244.3906	2256.25	2268.1406	2280.0625	2292.0156
48	2304	2316.0156	2328.0625	2340.1406	2352.25	2364.3906	2376.5625	2388.7656
49	2401	2413.2656	2425.5625	2437.8906	2450.25	2462.6406	2475.0625	2487.5156
51	2500	2512.5156	2525.0625	2537.6406	2550.25	2562.8906	2575.5625	2588.2656
	2601	2613.7656	2626.5625	2639.3906	2652.25	2665.1406	2678.0625	2691.0156
52	2704	2717.0156	2730.0625	2743.1406	2756.25	2769.3906	2782.5625	2795.7656
53	2809	2822.2656	2835.5625	2848.8906	2862.25	2875.6406	2889.0625	2902.5156
54	2916	2929.5156	2943.0625	2956.6406	2970.25	2983.8906	2997.5625	3011.2656
55	3025	3038.7656	3052.5625	3066.3906	3080.25	3094.1406	3108.0625	3122.0156
56	3136	3150.0156	3164.0625	3178.1406	3192.25	3206.3906	3220.5625	3234.7656
57	3249	3263.2656	3277.5625	3291.8906	3306.25	3320.6406	3335.0625	3349.5156
58	3364	3378.5156	3393.0625	3407.6406	3422.25	3436,8906	3451.5625	3466.2656
59	3481	3495.7656	3510.5625	3525.3906	3540.25	3555,1406	3570.0625	3585.0156
60	3600	3615.0156	3630.0625	3645.1406	3660.25	3675,3906	3690.5625	3705.7656
61	3721	3736.2656	3751.5625	3766.8906	3782.25	3797.6406	3813.0625	3828.5156
62	3844	3859.5156	3875.0625	3890.6406	3906.25	3921.8906	3937.5625	3953.2656
63	3969	3984.7656	4000.5625	4016.3906	4032.25	4048.1406	4064.0625	4080.0156
64	4096	4112.0156	4128.0625	4144.1406	4160.25	4176.3906	4192.5625	4208.7656
65	4225	4241.2656	4257.5625	4273.8906	4290.25	4306.6406	4323.0625	4339.5156
66	4356	4372.5156	4389.0625	4405.6406	4422.25	4438.8906	4455.5625	4472.2656
67	4489	4505.7656	4522.5625	4539.3906	4556.25	4573.1406	4590.0625	4607.0156
68	4624	4641.0156	4658.0625	4675.1406	4692.25	4709.3906	4726.5625	4743.7656
69 70	4761	4778.2656 4917.5156	4795.5625 4935.0625	4812.6906 4952.6406	4830.25 4970.25	4847.6406 4987.8906	4865.0625 5005.5625	4882.5156

Fraction	0	1	2	3	4	5
1 0 32		1.000000	8.000000	27.00000	64.00000	125.00000
32	.04 30518	1.096710	8.380890	27.85257	65.51175	127.35843
$\frac{32}{3}$ $\frac{1}{16}$	.03 24414	1.199463	8.773682	28.72290	67.04712 68.60629	129.74634
32	.03 82397	1.308441	9.178558	29.61118	05.60629	132.16391
5 1/8 32 ··	.0019531	1.423828	9.595703	30.51758	70.18945	134.61133
32	.0038147	1.545807	10.025299	31.44229	71.79678 73.42847	137.08878
7 16	.0065918	1.674561 1.810272	10.467529	33.34738	75.08469	139.59644
82						
9 1/4	.0156250	1.953125	11.390625	34.32813	76.76563	144.70313
32 ··· ii 5 16	.0222473	2.103302	11.871857	35.32791	78.47147	147.30252
ii 16	.0305176	2.260986	12.366455	36.34692 37.38535	80.20239 81.95859	149.93286 152.59433
_	.0400103	M. 2200001	14.072000	31.00000	02.30003	102.05200
13 3/8	.0527344	2.599609	13.396484	38.44336	83.74023	155.28711
	.0670471	2.780914	13.932281	39.52115	85.54752	158.01138
15 16	.1029968	2.970459 3.168427	14.482178 15.046356	40.61890	87.38062 89.23972	160.76733 163.55515
32 1/2	.1250000	3.375000	15.625000	42.87500	91.12500	166.37500
			,			
17 32 · .	.1499329	3.590363	16.218292	44.05372	93.03665	169.22708
19 16 32 ··	.1779785	3.814697	16.826416	45.21313	94.97485	172.11157
32	.2093201	4.048187	17.449554	46.41342	96.93979	175.02866
31 5/8	.2441406	4.291016	18.087891	47.63477	98.93164	177.97852
	.2826233	4.543365	18.741608	48.87735	100.95059	180.96133
32 <u>ii</u> 23 16 32 ··	.3249512	4.805420	19.410889	50.14136	102.99683	183.97729
32	.3713074	5.077362	20.095917	51.42697	105.07053	187.02658
3 3/4	.4218750	5.369375	20.796876	52.73438	107.17188	190.10938
32 ;;	.4768372	5.651642	21.513947	54.06375	109.30106	193.22586
32 <u>i3</u> 27 16	.5363770	5.954346	22.247314	55.41528	111.45825	196.37622
	16006775	6.267670	22.997162	56.78915	113.64365	199.56064
. 20 7/8	.6699219	6.591797	23.763672	58.18555	115.85742	202.77930
32 16	.7442932	6.926910	24.547028	59.60464	118.09976	206.03238
31 16	8239746	7.273193	25.347412	61.04663	120.37085	209.32007
	.9091492	7.630829	26.168009	62.51169	122.67087	212.64255
Fraction	6	7	8	9	10	11
0	216.00000	343.00000	512.00000	729.0000	1000.0000	1331.0000
32 1	219.39261	347.61429	518.02347	736.6201	1009.4043	1342.3760
32 1	222.82056	352.26978	524.09399	744.2932	1018.8674	1353.8167
33	226.28403	356.96664	530.21176	752.0194	1028.3895	1365.3221
1/8	229.78320	361.70508	536.37695	759.7988	1037.9707	1376.8926
32 %	233.31827 236.88940	366.48526 371.30737	542.58975	767.6317	1047.6112	1388.5282
7 16	240,49680	376.17160	548.85034 555.15891	775.5183 783.4587	1057.3113 1067.0710	1400,2292
7/	244.14063	381.07813				1423.8281
9 1/4 32 5	247.82108	381.07813	561.51563 567.92068	791.4531	1076.8906	1423.8281
32 5 11 16	251.53833	391.01880	574.37427	807.6047	1096.7102	1447.6907
ii 16	255.29257	396.05331	580.87656	815.7623	1106.7105	1459.7213
2/	259.03398	401.13086	587,42773	823,9746	1116,7715	1471.8184
i3 38	262.91275	406.25162	594.02798	832.2418	1126.8932	1483.9821
15 16 32 ···	266.77905	411.41577	600.67749	840.5642	1137.0759	1496.2126
32	270.68307	416.62350	607.37643	848.9419	1147.3198	1508.5102

Fraction	6	7	В	9	10	11
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	274.62500 278.60501 282.62329 286.68002	421.87500 427.17044 432.51001 437.89389	614.12500 620.92337 627.77173 634.67026	857.3750 865.8638 874.4084 882.0091	1157.6250 1167.9917 1178.4202 1188.9105	1520.8750 1533.3073 1545.8069 1558.3774
2 <u>i</u> 5/8 32 <u>ii</u> 2 <u>3</u> 16 32 ··	290.77539 294.90958 299.08276 303.29514	443.32227 448.79532 454.31323 459.87619	641.61914 648.61856 655.66870 662.76974	891.6660 900.3793 909.1491 917.9758	1199.4629 1210.0775 1220.7546 1231.4943	1571.0098 1583.7133 1595.4851 1609.2254
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	307.54688 311.83817 316.16919 320.54013	465.48438 471.13797 476.83716 482.56212	669.92188 677.12527 684.38013 691.68661	926.8594 935.8001 944.7981 953.8536	1242.2969 1253.1624 1264.0911 1275.0831	1622.2344 1635.2122 1648.2590 1661.3751
29 7/8 32 15 31 16 32	824,95117 329,40250 333,89429 338,42673	488.37305 494.21011 500.09351 506.02341	699.04492 706.46523 713.91772 721.43259	962.9668 972.1378 981.3669 990.6543	1296.1387 1297.2580 1308.4412 1319.6884	1674.5505 1687.8156 1701.1404 1714.5351
Fraction	12	13	14	15	16	17
1 0 1 16 1/8 3 16 ··	1728.0000 1755.1409 1782.5645 1810.2722	2197.0000 2228.8401 2260.9863 2293.4402	2744.0000 2780.9143 2819.1582 2855.7332	3375.0000 3417.3635 3460.0801 3503.1511	4096.0000 4144.1877 4192.7520 4241.6941	4913.0000 4967.3870 5022.1738 5077.3621
5 1/4 16 3/8 16 ··	1838.2656 1866.5461 1895.1152 1923.9744	2326.2031 2359.2766 2393.6621 2426.3611	2893.6406 2931.8821 2970.4590 3009.3728	3545.5781 3590.3625 3634.5059 3679.0095	4291.0156 4340.7180 4390.5027 4441.2712	5132,9531 5188,9485 5245,3496 5302,1580
9 1/2 16 5/8 11 0 0 0 0	1953.1250 1982.5686 2012.3066 2042.3406	2460.3750 2494.7053 2529.3535 2564.3210	3048.6250 3088.2170 3128.1504 3168.4265	3723.8750 3769.1036 3814.6973 3860.6576	4492.1250 4543.3656 4594.9941 4647.0125	5359.3750 5417.0032 5475.0410 5533.4929
i3 3/4 16 7/8 15 16 ··	2072.6719 2103.3020 2134.2324 2165.4646	2599.6094 2635.2200 2671.1543 2707.4138	3209.0469 3250.0129 3291.3262 3332.9880	3906.9844 3953.6809 4000.7480 4048.1873	4699.4219 4752.2239 4805.4199 4869.0116	5592.3594 5651.6418 5711.3418 5771.4607
Fraction	18	19	20	21	22	23
0 16 16 3 16	5832.0000 5892.9612 5954.3457 6016.1550	6859,0000 6926,9104 6995,2676 7064,0730	8000.0000 8075.2346 8150.9395 8227.1160	9361.000 9343.934 9427.361 9511.284	10648.000 10739.608 10830.633 10922.577	12167.000 12266.457 12366.455 12466.995
5 1/4 16 3/8 7 16 ··	6078,3905 6141,0540 6204,1465 6267,6697	7133.3281 7203.0344 7273.1934 7343.8064	8303.7656 8380.8899 8458.4902 8636.5681	9595.703 9680.620 9766.037 9851.955	11015.141 11108.226 11201.834 11295.957	12568.078 12669.706 12771.881 12874.603
9 1/2 16 :: 11 5/8 16 ::	6331.6250 6396.0139 6460.8379 6526.0984	7414.8750 7486.4006 7558.3848 7630.8289	8615.1250 8694.1624 8773.6816 8853.6843	9938.375 10025.299 10112.729 10200.665	11390.625 11485.811 11581.525 11677.770	12977.875 13081.698 13186.072 13291.001
ii 3/4 16 7/8 ii 7/8	6591.7969 6657.9348 6724.5137 6791.5849	7703.7344 7777.1028 7850.9355 7925.2341	8934.1719 9015.1458 9096.6074 9178.5583	10289,109 10378,064 10467,529 10557,508	11774.547 11871.857 11969.701 12068.082	13396.484 ,13503.525 13609.123 13716.281

No.	0	1/8	1/4	3/8	1/2	5/8	3/4	3/8
24 25	13824 15625			14482.178 16338.725	14706.125 16581.375		15160.922 17073.859	
26 27	17576 19683	19957.643	20234.828	18347.521 20514.568	18609.625 20796.875	21081.760	19141.297 21369.234	19410.889 21659.311
28 29 30	21952 24389 27000	24705.736	25025.203	22845.865 25347.412 28025.209	23149.125 25672.375 28372.625	23455.057 26000.104 28722.900	23763.672 26330.609 29076.047	
31 32	29791 32768		33542.016	30885.256 33933.553	31255.875 34328.125	34725.744	32005.984 35126.422	35530.170
33 34 35	35937 39304 42875	36346,924 39739,096 43336,018	36759.953 40177.391 43800.328	37176.100 40618.896 44267.943	37595.375 41063.625 44738.875	41511.588	38443.359 41962.797 45690.734	42417.264
36 37	46656 50653	51168.111	47634.766 51686.703	48129.240 52208.787	48627.125 52734.375	49128.432 53263.479	49633.172 53796.109	54332.279
38 39 40	54872 59319 84000	59891.205	55962.141 60467.078 65207.516	56512.584 81046.631 65816.928	57066.625 61629.875 66430.125	57624.275 62216.822 67047.119	58185.547 62807.484 67667,922	
41 42 43	68921 74088 79507	*69553.299 74751.471 80202.393	70189.453 75418.891 80901.828	70829.475 76090.272 81605.318	71473.375 76765.625	72121,166 77444.963 83024,510	72772.859 78128.297	73428.467 78815.639
44 45	85184 91125	85912.065 91888.486	86644.266 92652.203	87380.615 93422.162	82312.875 88121.125 94196.375	88865.807 94974.854	83740.234 89614.672 95757.609	84460.061 90367.732 96544.654
		98131.658 104653.58 111458.25	98931.641 105488.58 112329.02	99735.959 106328.01 113204.30	100544.63 107171.87 114084.12	101357.65 108020.20 114968.49	102175.05 108872.98 115857.42	102996.83 109730.25 116750.92
49	117649	118551.67 125939.85	119458.95 126884.39	120370.85 127833.65	121287.37 128787.62	122208.54 129746.34	123134.36 130709.80	124064.84 131678.01
52	140608	133628.77 141624.44 149932.86	134611.33 142645.77 150993.70	135598.69 143671.99 152059.54	136590.87 144703.12 153130.37	137587.88 145739.18 154206.23	138589.73 146780.17 155287.11	139596.44 147826.11 156373.03
E4	157464	158560.03 167511.96	159661.14 168654.08	160767.33 169801.38	161878.62 170953.87	162995.03 172111.57	164116.55	165243.20 174442.62
57	185193	176794.63 186414.05 196376.22	177978.52 187640.45 197645.89	179167.68 188872.22 198921.02	180362.12 190109.37 200201.62	181561.87 191351.92 201487.71	182766.92 192599.86 202779.30	183977.29 193853.22 204076.39
		206687.14 217352.81	208000.83 218711.27	209320.07 220075.37	210644.87 221445.12	211975.26 222820.56	213311.23	214652.81 225588.48
62	238328	228379.24 239772.41 251538.33	229783.20 241222.64 253035.58	231192.91 242678.71 254538.76	232608.38 244140.63 256047.88	234029.60 245608.40 257562.95		236889.40 248561.58 260611.00
65	274625	263683.00 276212.42	265228.02 277805.95	266779.05 279405.60	268336.13 281011.38	269899.24 282623.29	271468.42 284241.36	273043.67 285865.59
68	300763 314432	289132.60 302449.52 316169.19	290775.39 304142.33 317912.77	292424.40 305841.44 319662.74	294079.63 307546.88 321419.13	295741.09 309258.63 323181.93	310976.73	299082.76 312701.19 326726.86
		330297.61 344840.78	332092.70 346688.14	333894.29 348542.08	335702.37 350402.61	337516.98 352269.77	339338.11	341165.78 356023.95

## **VALUES FOR COMBINATIONS OF** $\pi$ ( $\pi$ = 3.14159265359).

Combination.			Values for n.		
Combination.	1	2	3	4	5 .
nπ	3.141593	6.283185	9.424778	12.566371	15.707963
$\frac{n\pi}{4}$	.785398	1.570796	2.356194	3.141593	3.926991
<u>n</u> π	.523599	1.047196	1.570796	2.094395	2.617994
<u>nπ</u>	.392699	.785398	1.178097	1.570796	1.963495
<u>nπ</u> 16	196350	.392699	1589049	.785398	.981748
$\frac{n\pi}{32}$	1098175	.196350	.294524	.392699	.490874
<u>nπ</u> 64	.049087	1098175	.147262	196350	.245427
<u>π</u>	3.141593	1.570796	1.047198	1785398	.628319
π	.318310	1686620	1954930	1.273240	1.591549
TC - 000	.034907	.017453	.011636	.008727	.006981
n 90° n 90°	28.647890	57.295780	85.943670	114.59156	143.239450
π <sup>n</sup>	3.141593	9.869604	31.006277	97.409091	306.01979
1 72	318310	.101321	.032252	.010266	.003268
2/7	3.141593	1.772454	1.464592	1.331335	1.257274
1 V "	.318310	.564190	.682784	.751126	.795371
nπ <sup>2</sup>	9.869604	19.739209	29.608813	39.478418	49.348022
$\frac{n}{\pi^2}$	.101321	.202642	.303963	1405284	.506605
√nπ	1.772454	2.506628	3.069980	3.544908	3.963328
$\sqrt{\frac{n}{\pi}}$	.564190	.797885	.977205	1.128379	1.26156G
$n\sqrt{\pi}$ .	1.772454	3.544908	5.317362	7.089815	8.862269
$\sqrt{\pi}$	.564190	1.128379	1.692569	3.256785	9.820948
nπ <sup>3</sup>	31.006277	62.013553	93.018830	124.02511	155.03138
$\frac{n}{\pi^8}$	.032252	1064503	.096755	.129006	161258
$\sqrt[3]{n\pi}$	1.464592	1.845270	2.112469	2.324895	2.504417
$\sqrt[3]{\frac{n}{\pi}}$	.682784	.860254	.984745	1.086351	1.167544
$n\sqrt[3]{\pi}$	1.464592	2.929184	4.393776	5.858368	7.322959
n 3/T	.6827841	1.3655681	2.0483522	2.7311363	3.4129203
ηπ4	97.409091	104.81818	292.22727	389,63636	487.04545
π4	10102660	10205320	10307979	.0410639	0513299
√nπ	1.331335	1.563283	1.752136	1.882793	1.990811
$\sqrt[4]{\frac{n}{\pi}}$	.751126	.893244	.988537	1.062252	1.123195

## **VALUES FOR COMBINATIONS OF** $\pi$ ( $\pi$ = 3.14159265359).

	Combination.			
6	7	8	9	Combination.
18.849556	21.991149	25.132741	28.274334	ηπ
4.712389	5.497787	6.283165	7.088583	<u>a</u>
3.141593	3.665191	4.188790	4.712380	<u>nπ</u>
2.356194	2.748894	3.141593	3,534292	<u>n</u> π
1.178097	1.374447	1.570796	1.767146	nπ
.589049	1687223	1785898	.883573	<u>n</u> π
.294524	.343612	.392699	.441786	nπ 64
1523599	.44879)	1392699	.349068	T
1.909859	2.228169	2.546479	2.864789	<u>n</u>
.005818	.004987	.004363	1003879	T T
171.88738	200.53523	223.18312	257.84101	n 90°
961.38937	3020.1938	9488.5331	29809.108	π π <sup>a</sup>
.001040	.000331	.000103	.000034	1
1.210203	1.177664	1.153835	1.136635	T <sup>n</sup>
.826307	.849139	.866675	.880564	π 1
59.217626	69.087231	79.956835	88.826440	√π nπ²
.607926	.709247	.810563	.911883	n
4.341608	4.689471	5.013257	5.317362	$\sqrt{n\pi}$ $\pi^2$
1.381977	1.492705	1.595769	1,692569	$\sqrt{n}$
10.634723	12.407177	14.179631	15.952085	π π
		4.513517	5.077705	n √ π
3.385138	3.949327			$\sqrt{\pi}$
166.03766	217.04394	243.05021	279.05649	nπ <sup>3</sup>
.193509	.225761	.258013	.290264	
2.661340	2.801663	2.939184	3.046474	<sup>3</sup> nπ
1.240701	1.306189	1.365563	1.420248	$\sqrt[q]{\frac{n}{\pi}}$
8.787551	10.252143	11.716735	13.181327	$n\sqrt[3]{\pi}$
4.096704	4.779489	5.462273	6.145057	$\frac{1}{\sqrt[3]{\pi}}$
584.45455	681.86364	779.27273	876.68182	nπ.4
.061596	.071862	.082123	.092394	<u>n</u>
2.083653	2.165519	2.239030	3.305940	\$\sqrt{n\pi}
1.175575 .	1.221763	1.263237	1.300988	√ <u>n</u>

### MENSURATION.

#### LENGTH.

Circumference of circle = diameter  $\times$  3.1416.

Diameter of circle = circumference  $\times$  0.3183.

Side of square of equal periphery as circle = diameter  $\times 0.7854$ . Diameter of circle of equal periphery as square = side  $\times$  1.2732.

Side of an inscribed square = diameter of circle  $\times$  0.7071.

Diameter of circle circumscribed about square = side  $\times$  1.4142.

Circumference of circle whose diameter is 1=

 $\pi = 3.14159265$ 

$$\log \pi = 0.4971499$$

$$\sqrt{\pi} = 1.772454$$

$$\pi^{2} = 9.869604$$

$$r = \frac{c^{2}}{8v} + \frac{v}{2}$$

$$\sqrt{\frac{1}{\pi}} = 0.564190$$

$$v = \sqrt{r^{2} - (r + o - v)^{2}}$$

$$v = \sqrt{r^{2} - \frac{c^{2}}{4}} = \frac{c}{2} \tan \frac{A}{4} = 2r \sin^{2} \frac{A}{4} = r + o - \sqrt{r^{2} - x^{2}}$$

$$c = 2\sqrt{2vr - v^{2}} = 2r \sin \frac{A}{2}$$

Length of arc = 
$$\frac{\pi \text{ r A}^{\circ}}{180}$$
 = .0174533 r A°

Angle A° = 
$$\frac{180 \times arc}{\pi r}$$
 =  $\frac{57.29578 \times arc}{r}$ 

$$\cos \frac{A}{2} = \frac{c^2 - 4v^2}{c^2 + 4v^2}$$

For division of circle into n parts,  $c = 2r \sin \theta$ 

### MENSURATION-(Continued).

#### AREA

Triangle = base × half perpendicular height.

Parallelogram = base × perpendicular height.

Trapezoid = half the sum of the parallel sides × perpendicular height.

Trapezium, found by dividing into two triangles.

Circle = diameter squared  $\times$  0.7854; or, = circumference squared  $\times$  0.07958.

Sector of circle = length of arc × half radius.

Segment of circle = area of sector of equal radius - triangle when segment is less, and + triangle when segment is greater than the semicircle; also for flat segments very nearly =

$$\frac{4v}{3}\sqrt{0.388 \ v^2 + \frac{c^2}{4}}$$

Side of square of equal area as circle = diameter × 0.8862; also, = circumference × 0.2821.

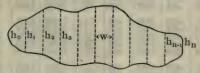
Diameter of circle of equal area as square = side × 1.1284.

Parabola = base × ½ height.

Ellipse = long diameter  $\times$  short diameter  $\times$  0.7854.

Regular polygon = sum of sides × half perpendicular distance from center to sides.

### APPROXIMATE AREA OF IRREGULAR FIGURE.



Divide figure into n strips by equidistant parallel ordinates, h<sub>0</sub>, h<sub>1</sub>, h<sub>2</sub>, etc.

Then by

Simpson's Rule, (n must be even)

Area = 
$$\frac{\mathbf{w}}{3}$$
[(h<sub>0</sub>+h<sub>n</sub>)+4(h<sub>1</sub>+h<sub>2</sub>+...h<sub>n-1</sub>)+2(h<sub>2</sub>+h<sub>4</sub>+...h<sub>n-2</sub>)]

Durand's Rule

Area = w[0.4  $(h_0+h_n)+1.1 (h_1+h_{n-1})+(h_2+h_3+...h_{n-2})]$ 

Trapezoidal Rule

Area =  $w \left[ \frac{1}{2} (h_0 + h_n) + (h_1 + h_2 + h_3 + \dots h_{n-1}) \right]$ 

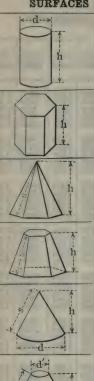
## RELATIONS IN CIRCULAR SEGMENTS

Central	Area	Chord	Height	Arc	Central	Area	Chord	Height	Arc
Degrees	Radius:	Radius	Radius	Radius	Degrees	Radius <sup>2</sup>	Radius	Radius	Radius
1	.0640	.017	.0440	.017	46	.04176	.781	.0795	.803
2 3	.0535	.035	.0315	.035	47	104448	.797	.0829	.820
3	.0412	.052	.0334	.052	48	.04731	.813	.0865	.838
4	.0428	.070	.0361	.070	49	.05025	.829	.0900	.855
5	.0455	.087	.0395	.087	50	.05331	.845	.0937	.873
6	.0496	.105	.0014	.105	51 52	.05649 .05978	.861	.1012	.890
7 8	.00023	.140	(0024	.140	53	.06319	892	.1012	1925
9	00033	.157	.0024	.157	54	06673	908	.1090	.942
10	.00044	.174	.0038	.175	55	07039	923	.1130	960
11	.00059	.192	.0046	192	56	.07417	1939	.1171	.977
13	00076	.209	0055	.227	57 58	07808	.954	.1212	1.012
14	.00121	.244	.0075	244	59	08629	1985	.1296	1.030
15	.00149	.261	.0086	.262	60	109059	1.000	.1340	1.047
16	.00181	.278	.0097	.279	61	.09502	1.015	.1384	1.065
17	.00217	.296	.0110	.297	62	.09958	1.030	1428	1.08
18	.00257	.313	.0123	.314	63	.10428	1.045	.1474	1.10
19	.00302	.330	.0137	.332	64	.10911	1.060	.1520	1.117
20	.00352	.347	.0152	.349	65	.11408	1.075	.1566	1.134
21	.00408	.364	.0167	.367	66	.11919	1.089	.1613	1.152
22	.00468	.382	.0184	.384	67 68	12982	1.104	.1661	1.169
24	.00535	.416	0219	.419	69	13535	1.133	.1710	1.204
25	.00686	.433	.0237	.436	70	.14102	1.147	11808	1.225
26	.00771	450	.0256	.454	71	.14683	1.161	1559	1.239
27	.00862	.467	.0276	.471	72	.15279	1.176	.1910	1.257
28	.00961	.484	.0297	489	73	15889	1.190	.1961	1.274
29	.01067	.501	.0319	.506	74	.16514	1.204	.2014	1.292
30	.01180	.518	.0341	.524	75	.17154	1.218	.2066	1.309
31	.01301	534	.0364	.541	76	.17808	1.231	.2120	1.326
32	.01429	.551	.0387	1559	77	.18477	1.245	.2174	1.344
33	01566	.568	.0412	576	78	.19160	1.259	2229	1.361
34 35	.01711	.601	.0437	.611	80	19859	1.286	2340	1.379
36	.02027	1618	.0489	.628	81	.21301	1.299	2396	1.414
37	.02198	635	.0517	.646	82	22045	1.312	2453	1.431
38	02378	651	.0545	.663	83	22804	1.325	.2510	1.449
39	.02568	.668	.0574	.681	84	23578	1.338	.2569	1.466
40	.02767	.684	10603	.698	85	.24367	1.351	2627	1.454
41	.02976	.700	0633	.716	86	.25171	1.364	2686	1.501
42	.03195	.717	.0664	.733	87	25990	1.377	.2746	1.518
43	.03425	.733	.0696	.750	88	26825	1.389	2807	1.536
44	.03664	.749	.0728	768	89	.27677	1.402	2867	1.553
45	.03915	765	.0761	.785	90	28540	1.414	2929	1.571

## RELATIONS IN CIRCULAR SEGMENTS

Central	Area	Chord	Height	Arc	Central	Area	Chord	Height	Arc
Angle		-		-	Angle	-	Radius	-	Radius
Degrees	Radius <sup>2</sup>	Radius	Radius	Radius	Degrees	Radius <sup>2</sup>	Kadius	Radius	Radius
7-									
91	.2942	1.427	.2991	1.588	136	.8395	1.854	.6254	2.374
92	.3032	1.439	.3053	1.606	137	.8545	1.861	.6335	2.391
93	.3123	1.451	.3116	1.623	138	.8697	1.867	.6416	2.409
94	.3215	1.463	.3180	1.641	139	.8850	1.873	.6498	2.426
95	.3309	1.475	.3244	1.658	140	19003	1.879	.6580	2.443
96	3405	1.486	.3309	1.676	141	.9158	1.885	.6662	2.461
97	3502	1.498	.3374	1.693	142	.9313	1.891	.6744	2.478
98	.3601	1.509	.3439	1.710	143	.9470	1.897	.6827	2,496
99	.3701	1.521	.3506	1.728	144	.9627	1.902	.6910	2.513
100	.3803	1.532	.3572	1.745	145	.9786	1.907	.6993	2.531
***	2000		19000	4 7700	***	.9945	4 049	.7076	2.548
101	.3906 .4010	1.543	.3639	1.763	146	1.0105	1.913	.7160	2.566
103	.4117	1.565	3775	1.798	148	1.0265	1.923	.7244	2.583
104	4224	1.576	3843	1.815	149	1.0427	1.927	7328	2.601
105	4333	1.587	.3912	1.833	150	1.0590	1.932	.7412	2.618
106	.4444	1.597	3982	1.850	151	1.0753	1.936	.7496	2.635
107	.4556	1.608	.4052	1.868	152	1.0917	1.941	.7581	2.653
108	4669	1.618	.4122	1.885	153	1.1082	1.945	.7666	2.670
109	.4784	1.628	.4193	1.902	154	1.1247	1.949	.7750	2.688
110	.4901	1.638	.4264	1.920	155	1.1413	1.953	.7836	2.705
111	.5019	1.648	4336	1.937	156	1.1580	1.956	.7921	2.723
112	.5138	1.658	.4408	1.955	157	1.1747	1.960	.8006	2.740
113	.5259	1.668	.4481	1.972	158	1.1915	1.963	.8092	2.758
114	.5381	1.677	.4554	1.990	159	1.2083	1.967	.8178	2.775
115	.5504	1.687	.4627	2.007	160	1.2252	1.970	.8264	2.793
440	Ecco	4.000	47701	0.005	101	1.2422	1.973	.8350	2.810
116	.5629	1.696	.4701	2.025	161	1.2592	1.975	.8436	2.827
118	.5883	1.714	4850	2,059	163	1.2763	1.978	8522	2.845
119	.6012	1.723	.4925	2.077	164	1.2933	1.981	18608	2.862
120	.6142	1.732	.5000	2.094	165	1.3105	1.983	.8695	2.880
121	.6273	1.741	.5076	2.112	166	1.3277	1.985	.8781	2.897
122	.6406	1.749	.5152	2.129	167	1.3449	1.987	.8868	2.915
123	.6540	1.758	5228	2.147	168	1.3621	1.989	.8955	2.932
125	6676	1.766	.5305	2.164	169 170	1.3967	1.991	.9042	2.967
120	.uora	1.112	.0300	2.102	110	1.3301	1.992	.oure	2.301
126	.6950	1.782	.5460	2.199	171	1.4140	1.994	9215	2.985
127	.7090	1.790	.5538	2.217	172	1.4314	1.995	.9302	3.002
128	.7230	1.798	.5616	2.234	173	1.4488	1.996	19390	3.019
129	.7372	1.805	.5695	2.251	174	1.4662	1.997	.9477	3.037
130	.7514	1.813	.5774	2.269	175	1.4836	1.998	9554	3.054
131	.7658	1.820	5853	2.286	176	1.5010	1.999	.9651	3.072
132	.7803	1.827	5933	2.304	177	1.5185	1.999	.9738	3.089
133	.7950	1.834	.6013	2.321	178	1.5359	2.000	9825	3.107
134	.8097	1.841	.6093	2.339	179	1.5533	2.000	.9913	3.124
135	.8245	1.848	.6173	2.356		1.5708		1.0000	3.142

### SURFACES AND VOLUMES OF SOLIDS.



h

#### CYLINDER

Convex Surface =  $\pi dh$ Total Surface =  $\pi dh + \frac{\pi d^2}{2}$ 

 $Volume = \frac{\pi}{4} d^2h$ 

Volume Cylinder, right or oblique area of section at right angles to sides X length of side.

#### PRISM

Lateral Surface =  $h \times Base$  Perimeter Total Surface = Lateral Surface +  $(2 \times Base$  Area) Volume =  $h \times Base$  Area

#### PYRAMID

Lateral Surface =  $\frac{8}{2}$  × Base Perimeter Total Surface = Lateral Surface + Base Area Volume =  $\frac{h}{3}$  × Base Area

Center of Gravity  $=\frac{h}{4}$ , above base

FRUSTUM OF PYRAMID

Lateral Surface = s(Top + Base Perimeters) + 2

If a = top area and A = base area,

Total Surface = Lateral Surface + (a+A)

Volume =  $h(a+A+\sqrt{aA})+3$ Center of Gravity =  $\frac{h}{4} \left( \frac{3a+A+2\sqrt{aA}}{a+A+\sqrt{aA}} \right)$ 

### CONE

Convex Surface =  $\frac{\pi}{2}$ ds =  $\frac{\pi d}{4} \sqrt{d^2 + 4h^2}$ Total Surface = Convex Surface +  $\frac{\pi d^2}{4}$ 

Volume =  $\frac{\pi}{12}$ d<sup>2</sup>h =  $\frac{\pi}{24}$ d<sup>2</sup>  $\sqrt{4s^2 - d^2}$ Center of Gravity above base =  $\frac{h}{12}$ 

#### FRUSTUM OF CONE

Convex Surface =  $\frac{\pi s}{2}$ (d+d') =  $\frac{\pi}{4}$ (d+d')  $\sqrt{4h^2+(d-d')^2}$ Total Surface =  $\frac{\pi s}{2}$ (d+d') +  $\frac{\pi}{4}$ (d2+d'2)

Volume =  $\frac{\pi h}{12} (d^2 + dd' + d'^2)$ 

Center of Gravity above base  $\frac{h(d^2+2dd'+3d'^2)}{4(d^2+dd'+d'^2)}$ 

### WEDGE

Surface = Sum of surfaces of bounding planes  $Volume = \frac{wh}{6}(l+m+n)$ 

#### SURFACES AND VOLUMES OF SOLIDS.



## SPHERE

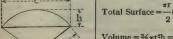




Side of an equal cube = diameter of sphere  $\times 0.806$ Length of an equal cylinder = diameter of sphere  $\times 0.6667$ 

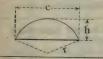
Center of Gravity of Half Sphere =3/8r above spherical center





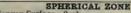
Total Surface = 
$$\frac{1}{2}(4h + c)$$
  
Volume =  $\frac{2}{3}\pi r^2h = \frac{2}{3}\pi r^2 \left(r - \sqrt{r^2 - \frac{c^2}{r^2}}\right)$ 

Center of Gravity = 3/4 above center of sphere



#### SPHERICAL SEGMENT

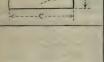
Spherical Surface =  $2\pi rh = \pi(c^2 + 4h^2) + 4$ Total Surface = Spherical Surface  $+(\pi c^2 + 4)$ Volume =  $\pi h^2(3r - h) + 3 = \pi h(3c^2 + 4h^2) + 24$ Center of gravity above base of segment  $=h(4r-h) \div 4(3r-h)$ 





Convex Surface = 
$$2\pi rh$$
  
Total Surface =  $2\pi rh + (c^2 + c'^2)$ 

Volume = 
$$\frac{\pi h}{24} (3c^2 + 3c'^2 + 4h^2)$$



### ELLIPSOID (I. Revolution about transverse axis)

Surface = 
$$2\pi r \left[ r + R \left( \frac{\sin^{-1}e}{e} \right) \right]$$

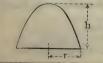
Volume =  $-\pi Rr^2$ 



### ELLIPSOID (II. Revolution about conjugate axis)

Surface = 
$$\pi \left[ 2R^2 + \frac{2.302r^2}{e} \log \left( \frac{1+e}{1-e} \right) \right]$$
Volume =  $\frac{2R^2}{e}$  Where  $e = \frac{R^2}{R^2 - r^2}$ 

Volume  $=-\pi R^2 r$ Where e =



### PARABOLOID

Convex Surface = 
$$\frac{\pi r}{6h^2} \left[ (r^2 + 4h^2)^{\frac{3}{2}} - r^3 \right]$$

Total Surface = Convex Surface +πr<sup>2</sup>

Center of Gravity =- above base

#### SURFACES AND VOLUMES OF SOLIDS

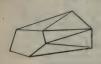


### CIRCULAR RING (TORUS)

D & R = Mean Diameter and Mean Radius.

respectively, of Ring
d & r=Mean Diameter and Mean Radius, respectively, of Section Surface =  $\pi^2 Dd = 4\pi^2 Rr$ 

 $Volume = 2\pi^2 Rr^2 = \frac{\pi^2}{2} Dd^2$ 

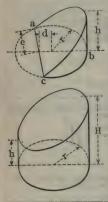


#### PRISMOID

End faces are in parallel planes.

Volume = -(A + A' + 4M), where

1 = perpendicular distance between ends A, A' = areas of endsM = area of mid section, parallel to ends



#### UNGULAS FROM RIGHT CIRCULAR CYLINDER

(As formed by cutting plane oblique to base)

Base, abc, less than semicircle;

Convex Surface  $=h(2re - (d \times length arc abc)) + (r - d)$ 

Volume= $h(\frac{2}{3}e^2-(d\times area base abc))+(r-d)$ 

II. Base, abc, = semicircle; Convex Surface = 2rh

Volume = 2/2 r2h III. Base, abc, greater than semicircle (figure): Convex Surface

 $=h(2re+(d \times length arc abc))+(r+d)$ Volume =  $h(\frac{2}{3}e^3 + (d \times area base abc)) + (r+d)$ 

Base, abc, = circle, oblique plane touching circumference.

Convex Surface = #rh Volume =  $\frac{1}{2}\pi r^2h$ Base, abc, = circle, oblique plane entirely above (figure). Convex Surface = 2 mr

 $\times \frac{1}{2}$  (h, minimum+H, maximum) Volume =  $\pi r^2 \times \frac{1}{2}$  (h, minimum +H, maximum)



#### ANY SOLID OF REVOLUTION

Let abcd represent the generating section about axis A-A of solid abef.

Let g at distance h from A-A be the center of gravity of abcd.

Let ao be the angular amount of generating revolution. Then

Total Surface of solid abef

 $=(2\pi h\alpha \div 360) \times perimeter abod$ Volume of solid abef =  $(2\pi h\alpha \div 360) \times area$  abcd For complete revolution  $(2\pi h\alpha + 360) = 2\pi h$ 

# MINUTES AND SECONDS EXPRESSED AS DECIMALS OF A DEGREE

Minutes	0	10	20	30	40	50			
0 1 2 3 4	.01667 .03333 .05000 .06667	.16667 .18333 .20000 .21667 .23333	.33333 .35000 .36667 .38333 .40000	.50000 .51667 .53333 .55000 .56667	.66667 .68333 .70000 .71667 .73333	.83338 .85000 .86667 .88333 .90000			
5 6 7 8 9	.08333 .10000 .11667 .13333 .15000	.25000 .26667 .28333 .30000 .31667	.41667 .43333 .45000 .46667 .48333	.58333 .60000 .61667 .63333 .65000	.75000 .76667 .78333 .80000 .81667	.91667 .93333 .95000 .96667 .98333			
Seconds	0	10	20	80	40	-50			
0 1 2 8 4	.00028 .00056 .00083 .00111	.00278 .00306 .00333 .00361 .00389	.00556 .00583 .00611 .00639 .00667	.00838 .00861 .00889 .00917 .00944	.01111 .01139 .01167 .01194 .01222	.01389 .01417 .01444 .01472 .01500			
5 6 7 8 9	.00189 .00167 .00194 .00222 .00250	.00417 .00444 .00472 .00500 .00528	.00694 .00722 .00750 .00778 .00806	.00972 .01000 .01028 .01056 .01083	.01250 .01278 .01306 .01333 .01361	.01528 .01556 .01583 .01611 .01689			

## DECIMALS OF A DEGREE EXPRESSED AS MINUTES OR SECONDS

Degree	.00 Min. (Sec.)	Min. (Sec.)	.20 Min. (Sec.)	Min. (Sec.)	.40 Min, (Sec.)
.00 .01 .02 .03 .04	.6( 36) 1.2( 72) 1.8(108) 2.4(144)	6.0 (360) 6.6 (396) 7.2 (432) 7.8 (468) 8.4 (504)	12.6 ( 756) 13.2 ( 792) 13.8 ( 828)	18.0 (1080) 18.6 (1116) 19.2 (1152) 19.8 (1188) 20.4 (1224)	24.6(1476) 25.2(1512) 25.8(1548)
.05 .06 .07 .08 .09	3.0(180) 3.6(216) 4.2(252) 4.8(288) 5.4(324)	9.0(540) 9.6(576) 10.2(612) 10.8(648) 11.4(684)	15.6(936) 16.2(972) 16.8(1008)	21.0(1260) 21.6(1296) 22.2(1332) 22.8(1368) 23.4(1404)	27.6 (1656) 28.2 (1692) 28.8 (1728)
Degree	Min. (Sec.)	Min. (Sec.)	Min. (Sec.)	Min. (Sec.)	.90 Min. (Sec.)
.00 .01 .02 .03 .04	30.6 (1836) 31.2 (1872) 31.8 (1908)	36.0 (2160) 36.6 (2196) 37.2 (2232) 37.8 (2268) 38.4 (2304)	42.6 (2556) 43.2 (2592) 43.8 (2628)	48.6 (2916) 49.2 (2952) 49.8 (2988)	54.6(3276) 55.2(3312) 55.8(3348)
.05 .06 .07 .08 .09	33.6 (2016) 34.2 (2052) 34.8 (2088)	39.0(2340) 39.6(2376) 40.2(2412) 40.8(2448) 41.4(2484)	45.6 (2736) 46.2 (2772) 46.8 (2808)	51.6(3096) 52.2(3132) 52.8(3168)	57.6 (3456) 58.2 (3492) 58.8 (3528)

### WEIGHTS AND MEASURES.

#### AVOIRDUPOIS WEIGHT.

United States and British.

Grains.	Drams,	Ounces.	Pounds.	Hundred- weight.	Gross Tons.
1, 27.34375 437.5 7000. 784000. 15680000.	.03657 1. 16. 256. 28672. 573440.	1002286 10625 1. 16. 1792. 35840.	.000143 .003906 .0025 1. 112. 2240.	.00000128 .00003488 .00055804 .0089286 1. 20.	.000000064 .000001744 .00002790 .0004464 .05

1 pound avoirdupois = 1.215278 pounds troy. 1 net ton = 2000 pounds = .892857 gross ton.

### TROY WEIGHT.

United States and British.

Grains.	Pennyweight.	Ounces.	Pounds.
1 24 480 5760	.041067 1. 20. 240.	.0020833 · .05 · .05 · .1. · .12.	.0001736 .0041667 .0833333

1 pound troy = .822857 pound avoirdupois. 175 ounces troy = 192 ounces avoirdupois.

### APOTHECARIES' WEIGHT.

United States and British.

Grains.	Scruples,	Drams.	Ounces.	Pounds.
1 20 60 480 5760	.05 1. 3. 24. 288.	.016667 [333333 1. 8. 96.	.0020833 .0416667 .125 1.	.000173611 .0034722 .0104167 .0833333 1.

The pound, ounce and grain are the same as in troy weight. The avoirdupois grain = troy grain = apothecaries' grain.

## WEIGHTS AND MEASURES—Continued.

#### United States and British.

Inches.	Feet.	Yards.	Rods.	Furlongs.	Miles.
1 12 36 198 7920 63360		.02778 .33333 1. 5.5 220. 1760.	.0050505 .0606061 .1818182 1. 40. 320.	.00012626 .00151515 .00454545 .025 1.	.00001578 .00018939 .00056818 .003125 .125

#### ROPE AND CABLE MEASURE.

- 1 inch = .111111 span = .013889 fathom = .0001157 cable's length.
- 1 span = 9 inches = .125 fathom = .00104167 cable's length.
- 1 fathom = 6 feet = 8 spans = 72 inches = .008333 cable's length.
- 1 cable's length = 120 fathoms = 720 feet = 960 spans = 8640 inches.

#### NAUTICAL MEASURE.

1 nautical mile, as adopted by the United States Coast and Geodetic Survey, equals the length of one minute of arc of a great circle of a sphere whose surface equals that of the earth = 6080.204 feet = 1.1516 statute miles.

1 league = 3 nautical miles = 18240.613 feet.

#### GUNTER'S CHAIN.

- 1 link = 7.92 inches = .01 chain = .000125 mile.
- 1 chain = 100 links = 66 feet = 4 rods = .0125 mile.
- 1 mile = 80 chains = 8000 links.

### SQUARE OR LAND MEASURE.

#### United States and British.

Square Inches.	Square Feet.	Square Yards.	Square Rods.	Acres.	Square Miles.
1 144 1296 39204 6272640	.006944 1. 9.0 272.25 43560. 27878400.	.0007716 .111111 1. 30.25 4840. 3097600.	.03306 1. 160. 102400.	.0002066 .00625 1. 640.	.00000977 .0015625 1.

- 1 square rood = 40 square rods.
- 1 acre = 4 square roods.
- 1 square acre = 208.71 feet square.

## WEIGHTS AND MEASURES-Continued.

#### CUBIC OR SOLID MEASURE.

#### United States and British.

- 1 cubic inch = .0005787 cubic foot = .000021433 cubic yard.
- 1 cubic foot = 1728 cubic inches = .03703704 cubic yard.
- 1 cubic yard = 27 cubic feet = 46656 cubic inches.
- 1 cord of wood = 128 cubic feet = 4 feet by 4 feet by 8 feet.
- $1~\rm perch$  of masonry =  $24.75~\rm cubic$  feet =  $16.5~\rm feet$  by 1.5 feet by 1 foot. It is usually taken as 25 cubic feet.

#### DRY MEASURE.

#### United States only.

Pints.	Quarts:	Gallons.	Pecks.	Bushels	Cubic Inches.
1 2 8 16 64	.50 1. 4. 8. 32.	.125 .25 1. 2. 8.	.0625 .125 .05 1.	.015625 .03125 .125 .25	33,6003125 67.200625 268.8025 537.605 2150.42

<sup>1</sup> heaped bushel = 1.25 struck bushel, and the cone must be not less than 6 inches high.

### LIQUID MEASURE.

#### United States only.

Gills.	Pints.	Quarts.	Gallons.	Barrels.	Cubic Inches.
1 4 8 32 1008	.25 1. 2. 8. 252.	.125 .5 1. 4. 126.	.03125 .125 .25 1. 31.5	.000992 .003968 .007937 .031746	7.21875 28.875 57.75 231. 7276.5

The British imperial gallon = 277.410 cubic inches or 10 pounds avoirdupois of pure water at  $62^{\circ}$  F. and barometer at 30 inches.

The British imperial gallon = 1.20091 United States gallons.

- 1 fluid drachm = 60 minims = .125 fluid ounce = .0078125 pint.
- 1 fluid ounce = 480 minims = 8 drachms = .0625 pint.

### WEIGHTS AND MEASURES-Concluded.

#### METRIC SYSTEM.

Measures of Length, Capacity and Weight.

LENGTH.	Kilometre.	Hecto- metre.	Decametre.	Metre.	Decimetre.	Centimetre.	Millimetre.
CAPACITY.	Kilolitre or Stere.	Hectolitre er Decistere.	Decalitre er Centistere.	Litre or Millistere.	Decilitre.	Centilitre.	Millilitre.
WRIGHT.	Kilo- gramme.	Hecto- gramme.	Deca- gramme.	Gramme,	Deci- gramme.	Centi- gramme.	Milli- gramme.
	1	10	100 10 1	1000 100 10 1 1 .01 .001	10000 1000 100 10 10 1 1 .1	100000 10000 1000 100 10 10 1	1000000 100000 10000 1000 100 100 10

1 myriametre = 10 kilometres = 10000 metres.

1 tonne = 1000 kilogrammes = 100 quintals = 10 myriagrammes. 1 gramme = weight of 1 cubic centimetre of distilled water at its maximum density at sea level in latitude of Paris and barometer at 760 millimetres.

1 litre = 1 cubic decimetre.

#### METRIC SYSTEM.

#### Square or Surface Measure.

Square Kilometre.	Square Hectometre or Hectare.	Square Decametre or Are.	Square Metre or Centiare.	Square Decimetre.	Square Centimetre.	Square Millimetre.
1	100 1 .01 .0001 .000001	10000 100 1 .01 .0001 .000001	1000000 10000 100 1 .01 .0001 1000001	1000000 10000 100 1 .01 .0001	1000000 10000 100 100 1	1000000 10000 100 1

1 square myriametre = 100 square kilometres = 100 000 000 square metres.

#### METRIC SYSTEM.

Cubic Measure.

Cubic Decametre.	Cubic Metre.	Cubic Decimetre.	Cubic Centimetre.	Cubic Millimetre.
.001 .000001 .00000001	1000 1 .001 .000001 .000000001	1000000 1000 1 .001 .000001	1000000000 1000000 1000 1000 1	100000000 100000 1000 1

1 cubic metre = 1 kilolitre = 1 stere.

# CUSTOMARY TO METRIC. Weights. See Page 590

No.	Grains	Troy Ounces	Avoirdupois Ounces	Avoirdupois Pounds to	Net Tons of 2000 Pounds	Gross Tons of 2240 Pound
	Milligrammes.	Grammes.	to Grammes.	Kilogrammes. Page 582	to Tonnes.	to Tonnes.
1 2	64.79892 129.59784	31.10348 62.20696	28.34953 56.69905	.45359 .90718	.90718 1.81437	1.01605
3	194.39675 259.19567	93.31044 124.41392	85.04858 113.39811	1.36078	2.72155 3.62874	3.04814
5	323.99459 388.79351	155.51740 186.62088	141.74763 170.09716	2.26796 2.72155	4.53592 5.44311	5.08024 6.09628
7 8 9	453.59243 518.39135 583.19026	217.72437 248.82785 279.93133	198.44669 226.79621 255.14574	3.17515 3.62874 4.08233	6.35029 7.25748 8.16466	7.11233 8.12838 9.14442

### 1 Avoirdupois Pound = 453.5924277 Grammes.

#### Linear Measure.

64ths of an	Inches	Foet	Yards	Statute Miles	Nautical Miles		
Inch to	to	to	to	to	to		
Millimetres.	Centimetres.	Metres.	Metres.	Kilometres.	Kilometres.		
Page 450	Page 568	Page 574					
.39688	2.54001	.304801	.914402	1,60935	1.85325		
.79375	5.08001	.609601	1.828804	3.21869	3.70650		
1.19063	7.62002	.914402	2.743205	4.82804	5.55975		
1.58750	10.16002	1.219202	3.657607	6.43739	7.41300		
1.98438	12.70003	1.524003	4.572009	8.04674	9.26625		
2.38125	15.24003	1.828804	5.486411	9.65608	11.11950		
2.77813	17.78004	2.133604	6.400813	11.26543	12.97275		
3.17501	20.32004	2.438405	7.315215	12.87478	14.82600		
3.57188	22.86005	2.743205	8.229616	14.48412	16.67925		
	Inch to Millimetres, Page 450  .39688 .79375 1.19063 1.58750 1.98438 2.38125 2.77813 3.17501	Inch to to Centimetres. Page 450 Page 568  .39688 2.54001 .79375 5.08001 1.19063 7.62002 1.98438 12.70003 2.38125 15.24003 2.77813 17.78004 3.17501 20.32004	Inch to         to           Millimetres.         Centimetres.           Page 450         Page 568           Page 574           .9868         2.54001           .9875         5.08001           .19063         7.62002           .914402           1.58750         10.16002           1.94848         12.70003           2.38125         15.24003           2.77813         17.78004           2.17360         24.38405	Inch to         to         to           Millimetres. Page 450         Centimetres. Page 568         Motres. Page 574           .39688         2.54001         .304801         .914402           .79375         5.08001         .609601         1.828804           1.19963         7.62002         .914402         2.743205           1.58750         10.16002         1.219202         3.657607           1.98438         12.70003         1.524003         4.572009           2.38125         15.24003         1.828804         5.48641           2.77813         17.78004         2.133604         6.400813           3.17501         20.32004         2.438405         7.315215	Inch to		

- 1 Nautical Mile = 1853.25 Metres.
- 1 Gunter's Chain = 20.1168 Metres.
- 1 Fathom = 1.829 Metres.

#### METRIC TO CUSTOMARY. Weights.

See Page 590

No.	Milligrammes	Grammes to	Grammes to Avoirdupois	Kilogrammes to Avoirdupois	Tonnes to Net Tons of	Tonnes to Gross Tons of
	Grains.	Troy Ounces.	Ounces.	Pounds, Page 586	2000 Pounds.	2240 Pounds.
1 2 3 4 5 6 7 8 9	.01543 .03086 .04630 .06173 .07716 .09259 .10803 .12346 .13889	.03215 .06430 .09645 .12860 .16075 .19290 .22506 .25721 .28936	.03527 .07055 .10582 .14110 .17637 .21164 .24692 .28219 .31747	2.20462 4.40924 6.61387 8.81849 11.02311 13.22773 15.43236 17.63698 19.84160	1.10231 2.20462 3.30693 4.40924 5.51156 6.61387 7.71618 8.81849 9.92080	.98421 1.96841 2.95262 3.93682 4.92103 5.90524 6.88944 7.87365 8.85785

1 Kilogramme = 15432.35639 Grains.

#### Linear Measure.

Ņo.	Millimetres to 64ths of an Inch.	Centimetres to Inches	Metres to Feet.	Metres to Yards.	Kilometres to Statute Miles.	Kilometres  to  Nantical Miles.
		Page 570	Page 578			
1 2 3 4 5 6 7 8 9	2.51968 5.03936 7.55904 10.07872 12.59840 15.11808 17.63776 20.15744 22.67712	.39370 .78740 1.18110 1.57480 1.96850 2.36220 2.75590 3.14960 3.54330	3.280833 6.561667 9.842500 13.123333 16.404167 19.685000 22.965833 26.246667 29.527500	1.093611 2.187222 3.280833 4.374444 5.468056 6.561667 7.655278 8.748889 9.842500	.62137 1.24274 1.86411 2.48548 3.10685 3.72822 4.34959 4.97096 5.59233	.53959 1.07919 1.61878 2.15837 2.69796 3.23756 3.77715 4.31674 4.85633

#### CUSTOMARY TO METRIC.

#### Square Measure.

No.	Square Inches to Square Centimetres.	Square Feet to Square Metres.	Square Yards to Square Metres.	Lo Lo Hectares.	Square Miles to Square Kilometres.
1 2	6.45163	.09290	.83613 1.67226	.40470	2.59000 5.18000
3	19.35488	.27871	2.50839	1.21409	7.77000
4.	25.80650 32.25813	.37161 .46452	3.34452 4.18065	1.61879 2.02349	10.35999 12.94999
6	38.70975	.55742	5.01679	2.42818	15.53999
7 8 9	45.16138 51.61300 58.06463	.65032 .74323 .83613	5.85292 6.68905 7.52518	2.83288 3.23758 3.64228	18.12999 20.71999 23.30999

<sup>1</sup> Square Statute Mile = 259.00 Hectares.

### Cubic Measure

No.	Oubic Inches to Cubic Centimetres.	Cubic Inches to Cubic Decimetres,	Cubic Feet to Cubic Metres.	Oubic Yards le Cubic Metres.
1 2 3 4 5 6 7 8 9	16.38716 32.77432 49.16148 65.54864 81.93580 98.32296 114.71013 131.09729 147.48445	.01639 .03277 .04916 .06555 .08194 .09832 .11471 .13110	.02832 .05663 .08495 .11327 .14159 .16990 .19822 .22654 .25485	.76456 1.52912 2.29968 3.05824 3.82280 4.58736 5.35192 6.11648 6.88104

#### METRIC TO CUSTOMARY.

#### Square Measure.

No.	Square Centi- metres to Square Inches.	Square Metres to Square Feet.	Square Metres to Square Yards.	Hectares to Acres.	Square Kilo- metres to Square Miles.
1	.15500	10.76387	1.19599	2.47104	.38610
2	.31000	21.52773	2.39197	4.94209	.77220
3	.46500	32.29160	3.58796	7.41313	1.15830
4	.62000	43.05547	4.78394	9.88418	1.54440
5	.77500	53.81934	5.97993	12.35522	1.93050
6	.93000	64.58320	7.17591	14.82626	2.31660
7	1.08500	75.34707	8.37190	17.29731	2.70270
8	1.24000	86.11094	9.56788	19.76835	3.08880
9	1.39500	96.87481	10.76387	22.23940	3.47490

1 Hectare = .003861 Square Statute Mile.

#### Cubic Measure

No.	Cubic Centimetres to Cubic Inches.	Cubic Decimetres to Cubic Inches,	Cubic Matres to Cubic Feet.	Cubic Metres to Cubic Yards.
1 2 3 4 5 6 7 8	.06102 .12205 .18307 .24409 .30512 .36614 .42716 .48819 .54921	61.02338 122.04676 183.07013 244.09351 305.11689 366.14027 427.16365 488.18702 549.21040	35.31445 70.62891 105.94336 141.25782 176.57227 211.88673 247.20118 282.51564 317.83009	1.30794 2.61589 3.92383 5.23177 6.53971 7.84766 9.15560 10.46354 11.77149

#### CUSTOMARY TO METRIC.

#### Capacity Measures.

No.	Liquid Quarts To Litres.	Gallons to Litres,	Gallons to Cubic Metres.	Bushels to Hectolitres,	Fluid Drackma to Millilitres or Cubic Centimetres.	Fluid Ounces to Millilitres or Cubic Centimetres.
1 2 3 4 5 6 7 8 9	.94636	3.78543	.00379	.35239	3.69671	29.57370
	1.89272	7.57087	.00757	.70479	7.39343	59.14741
	2.83908	11.35630	.01136	1.05718	11.09014	88.72111
	3.78543	15.14174	.01514	1.40957	14.78685	118.29482
	4.73179	18.92717	.01893	1.76196	18.48357	147.86852
	5.67815	22.71260	.02271	2.11436	22.18028	177.44222
	6.62451	26.49804	.02650	2.46675	25.87699	207.01593
	7.57087	30.28347	.03028	2.81914	29.57370	236.58963
	8.51723	34.06891	.03407	3.17154	33.27042	266.16334

#### Miscellaneous.

No.	Pounds per Lineal Foot to Kilogrammes per Lineal Metre.	Pounds per Square Inch to Kilogrammes per Square Centimetre.	Pounds per Square Foot to Kilogrammes per Square Metra.	Pounds per Cubis Foot to Kilogrammes per Cubic Metre.	Foot-Pounds to Kilogramme- Matres	United States Horsepower to Metric Horsepower.
1	1.48816	.07031	4.88241	16.01837	.13826	1.01387
2	2.97632	.14061	9.76482	32.03674	.27651	2.02775
3	4.46448	.21092	14.64723	48.05510	.41477	3.04162
4	5.95264	.28123	19.52963	64.07348	.55302	4.05549
õ	7.44081	.35153	24.41204	80.09185	.69128	5.06937
6	8.92897	.42184	29.29445	96.11021	.82953	6.08324
7	10.41713	.49215	34.17686	112.12858	.96779	7.09711
8	11.90529	.56245	39.05927	128.14695	1.10604	8.11098
9	13.39345	.63276	43,94168	144.16532	1.24430	9.12486

### METRIC TO CUSTOMARY.

Capacity Measures.

No.	Litres to Fluid Quarts.	Litres to Gallons.	Cubic Metres to Gallons.	Hectolitres to Bushels.	Millilitres or Cubic Centi- metres to Fluid Drachms.	Millilitres or Cubic Centi- metres to Fluid Ounces.
1 2 3	1.05668 2.11336 3.17005	.26417 .52834 .79251	264.17047 528.34093 792.51140	2.83774 5.67548 8.51323	.27051 .54102 .81153	.03381 .06763 .10144
4 5	4.22673	1.05668	1056.68187	11.35097	1.08204	.13526
6	5.28341 6.34009	1.32085	1320.85234	14.18871	1.62306	.20288
7 8 9	7.39677 8.45345 9.51014	1.84919 2.11336 2.37753	1849.19327 2113.36374 2377.53420	. 19.86420 22.70194 25.53968	1.89357 2.16408 2.43460	.23670 .27051 .30432

#### Miscellaneous.

No.	Kilogrammes per Lineal Metre to Pounds per Lineal Foot.	Kilogrammes per Square Centimetre to Pounds per Square Inch.	Kilogrammes per Square Metre to Pounds per Square Foot.	Kilogrammes per Cubic Metre to Pounds per Cubic Foot,	Kilogramme- Matres in Foot-Pounds.	Metric Horsepower to United States Horsepower.
1 2 3 4	.67197 1.34393 2.01590 2.68787	14.22340 28.44680 42.67020 56.89359	.20482 .40963 .61445 .81927 1.02408	.06243 .12486 .18728 .24971 .31214	7.23300 14.46600 21.69899 28.93199 36.16499	.98632 1.97264 2.95895 3.94527 4.93159
5 6 7 8 9	3.35984 4.03180 4.70377 5.37574 6.04770	71.11699 85.34039 99.56379 113.78719 128.01059	1.02408 1.22890 1.43372 1.63854 1.84335	.37457 .43700 .49943 .56185	50.10499 43.39799 50.63098 57.86398 65.09698	5.91791 6.90423 7.89054 8.87686

## EQUIVALENTS OF INCHES IN MILLIMETRES.

#### FRACTIONS OF AN INCH ADVANCING BY 32nds.

Page 450 shows values for each  $\frac{1}{14}$  to 1 inch. Conversion Factor: 1 inch=25,40005 millimetres.

	Inches		0"	1"	2"	3"	4"	5"
		0		25.400	50.800	76.200	101.600	127.000
32			.794	26.194	51.594	76.994	102.394	127.794
	16		1.588	26.988	52.388	77.788	103.188	128.588
$\frac{3}{32}$			2.381	27.781	53.181	78.581	103.981	129.382
		1/8		28.575			104.775	
32	4.			29.369			105.569	
	3 16			30.163			106.363	
7 32			5.556	30.956	56.356	81.756	107.156	132.557
		1/4		31.750			107.950	
32				32.544			108.744	
::	5 16			33.338			109.538	
11 32	• •		8.731	34.131	59.531	84.931	110.331	135.732
		3/8	9.525	34.925	60.325	85.725	111.125	136.525
$\frac{13}{32}$			10.319	35.719	61.119	86.519	111.919	137.319
	7 16		11.113	36.513	61.913	87.313	112.713	138.118
$\tfrac{15}{32}$			11.906	37.306	62.706	88.106	113.506	138.907
		1/2		38.100			114.300	
$\frac{17}{32}$				38.894			115.094	
	9 16		14.288	39.688	65.088	90.488	115.888	141.288
19 32			15.081	40.481	65.881	91.281	116.681	142.082
		5/8		41.275			117.475	
$\frac{21}{32}$	- 22			42.069			118.269	
	11/16			42.863			119.063	
32			18.256	43.656	69.056	94.456	119.856	145.257
		3/4	19.050	44.450	69.850	95.250	120.650	146.050
25 32				45.244			121.444	
	13			46.038			122.238	
$\frac{27}{32}$			21.431	46.831	72.231		123.031	
		7/8	22.225	47.625	73.025	98.425	123.825	149.225
29 32			23.019	48.419	73.819	99.219	124.619	150.019
	15		23.813	49.213	74.613	100.013	125.413	150.813
31			24.606	50.006	75.406	100.806	126.20€	151.607
			1					

12 Inches=304.8006 Millimetres.

## EQUIVALENTS OF INCHES IN MILLIMETRES.

Inches	6"	7"	8"	9"	10"	11"
0			203.200			
32			203.994			
16			204.788			
32	154.782	180.182	205.582	230.982	256.382	281.782
1/8	155.575	180.975	206.375	231.775	257.176	282.576
32	156.369	181.769	207.169	232.569	257.969	283.369
3	157.163	182.563	207.963	233.363	258.763	284.163
32	157.957	183.357	208.757	234.157	259.557	284.957
1/4	158.750	184.150	209.550	234.950	260.351	285.751
9	159.544	184.944	210.344	235.744	261.144	286.544
5	160.338	185.738	211.138	236.538	261.938	287.338
$\frac{11}{32}$	161.132	186.532	211.932	237.332	262.732	288.132
3/8	161.925	187.325	212.725	238.125	263.526	288.926
$\frac{13}{32}$			213.519			
. 7			214.313			
15 32 ·· ··			215.107			
½	165.100	190,500	215.900	241.300	266.701	292,101
17			216.694			
9 16			217.488			
19	167.482	192.882	218.282	243.682	269.082	294.482
5/8	168.275	193.675	219.075	244.475	269.876	295.276
$\frac{21}{32}$			219.869			
11 11			220.663			
$\frac{23}{32}$			221.457			
3/4	171.450	196.850	222.250	247 850	273.051	298.451
$\frac{25}{32}$ $\cdots$ $\frac{4}{3}$			223.044			
13			223.838			
27 32 ·· ··			224.632			
7/8	174 625	200 025	225,425	250 825	276 226	301 626
29			226.219			
15			227.013			
31 16			227.807			

Conversion Factor: 1 millimetre=.03937 inch.

Millimetres	0	100	200	300	400
0	.000	3.937	7.874	11.811	15.748
1	.039	3.976	7.913	11.850	15.788
2	.079	4.016	7.953	11.890	15.827
8	.118	4.055	7.992	11.929	15.866
4	.157	4.095	8.032	11.969	15.906
5	.197	4.134	8.071	12.008	15.945
6	.236	4.178	8.110	12.047	15.984
7	.276	4.213	8.150	12.087	16.024
8	.315	4.252	8.189	12.126	16.063
9	.354	4.291	8.228	12.165	16.103
10	.394	4.331	8.268	12.205	16.142
11	.433	4.370	8.307	12.244	16.181
12	.472	4.409	8.347	12.284	16.221
13	.512	4.449	8.386	12.323	16.260
14	.551	4.488	8.425	12.362	16.299
15	.591	4.528	8.465	12.402	16.339
16	.630	4.567	8.504	12.441	16.378
17	.669	4.606	8.543	12.480	16.417
18	.709	4.646	8.583	12.520	16.457
19	.748	4.685	8.622	12.559	16.496
20	.787	4.724	8.661	12.599	16.536
21	.827	4.764	8.701	12.638	16.575
22	.866	4.803	8.740	12.677	16.614
23	.906	4.843	8.780	12.717	16.654
24	.945	4.882	8.819	12.756	16.693
25	.984	4.921	8.858	12.795	16.782
26	1.024	4.961	8.898	12.835	16.772
27	1.063	5.000	8.937	12.874	16.811
28	1.102	5.039	8.976	12.913	16.851
29	1.142	5.079	9.016	12.953	16.890
30	1.181	5.118	9.055	12.992	16.929
31	1.220	5.158	9.095	13.032	16.969
32	1.260	5.197	9.134	13.071	17.008
33	1.299	5.236	9.173	13.110	17.047
34	1.339	5.276	9.213	13.150	17.087
85	1.378	5.315	9.252	13.189	17.126
36	1.417	5.354	9.291	13.228	17.166
37	1.457	5.394	9.331	13.268	17.205
38	1.496	5.433	9.370	13.307	17.244
39	1.535	5.472	9.410	13.347	17.284
40	1.575	5.512	9.449	13.386	17.323
41	1.614	5.551	9.488	13.425	17.362
42	1.654	5.591	9.528	13.465	17.402
48	1.693	5.630	9.567	13.504	17.441
44	1.732	5.669	9.606	13.548	17.480
45	1.772	5.709	9.646	13.583	17.520
46	1.811	5.748	9.685	13.622	17.559
47	1.850	5.787	9.724	13.662	17.599
48	1.890	5.827	9.764	13.701	17.638
49	1.929	5.866	9.803	13.740	17.677

-					
Millimetres	0	100	200	800	400
50	1.969	5.906	9.843	13.780	17.717
51	2.008	5.945	9.882	13.819	17.756
52	2.047	5.984	9.921	13.858	17.795
58	2.087	6.024	9.961	13.898	17.835
54	2.126	6.063	10.000	13.987	17.874
55	2.165	6.102	10.089	13.977	17.914
56	2.205	6.142	10.079	14.016	17.958
57	2.244	6.181	10.118	14.055	17.992
58	2.283	6.221	10.158	14.095	18.032
59	2.323	6.260	10.197	14.134	18.071
60	2.362	6.299	10.236	14.178	18.110
61	2.402	6.339	10.276	14.213	18.150
62	2.441	6.378	10.315	14.252	18.189
63	2.480	6.417	10.354	14.291	18.229
64	2.520	6.457	10.394	14.331	18.268
65	2.559	6.496	10.433	14.370	18.307
66	2.598	6.535	10.473	14.410	18.347
67	2.638	6.575	10.512	14.449	18.386
68	2.677	6.614	10.551	14.488	18.425
69	2.717	6.654	10.591	14.528	18.465
70	2.756	6.693	10.630	14.567	18.504
71	2.795	6.732	10.669	14.606	18.543
72	2.835	6.772	10.709	14.646	18.583
78	2.874	6.811	10.748	14.685	18.622
74	2.913	6.850	10.787	14.725	18.662
75	2.953	6.890	10.827	14.764	18.701
76	2.992	6.929	10.866	14.803	18.740
77	3.032	6.969	10.906	14.843	18.780
78	3.071	7.008	10.945	14.882	18.819
79	3.110	7.047	10.984	14.921	18.858
80	3.150	7.087	11.024	14.961	18.898
81	3.189	7.126	11.063	15.000	18.937
82	3.228	7.165	11.102	15.040	18.977
83	3.268	7.205	11.142	15.079	19.016
84	3.307	7.244	11.181	15.118	19.055
85	3.346	7.284	11.221	15.158	19.095
86	3.386	7.323	11.260	15.197	19.134
87	3.425	7.362	11.299	15.236	19.173
88	3.465	7.402	11.339	15.276	19.213
89	3.504	7.441	11.378	15.315	19.252
90	3.543	7.480	11.417	15.354	19.292
91	3.583	7.520	11.457	15.394	19.331
92	3.622	7.559	11.496	15.433	19.370
98	3.661	7.598	11.536	15.473	19.410
94	3.701	7.638	11.575	15.512	19.449
95	3.740	7.677	11.614	15.551	19.488
96	3.780	7.717	11.654	15.591	19.528
97	3.819	7.756	11.698	15.630	19.567
98	3.858	7.795	11.732	15.669	19.606
99	3.898	7.835	11.772	15.709	19.646

					-
Millimetres	500	600	700	800	900
0	19.685	23.622	27.559	31.496	35.433
1	19.725	23.662	27.599	31.536	35.478
2	19.764	23.701	27.638	31.575	35.512
3	19.803	23.740	27.677	31.614	35.552
4	19.843	23.780	27.717	31.654	35.591
56789	19.882	23.819	27.756	31.693	35.630
	19.921	23.858	27.796	31.733	35.670
	19.961	23.898	27.835	31.772	35.709
	20.000	23.937	27.874	31.811	35.748
	20.040	23.977	27.914	31.851	35.788
10	20.079	24.016	27.953	31.890	35.827
11	20.118	24.055	27.992	31.929	35.866
12	20.158	24.095	28.032	31.969	35.906
13	20.197	24.134	28.071	32.008	35.945
14	20.236	24.173	28.110	32.048	35.985
15	20.276	24.213	28.150	32.087	36.024
16	20.315	24.252	28.189	32.126	36.063
17	20.355	24.292	28.229	32.166	36.103
18	20.394	24.331	28.268	32.205	36.142
19	20.433	24.370	28.307	32.244	36.181
20	20.473	24.410	28.347	32.284	36.221
21	20.512	24.449	28.386	32.323	36.260
22	20.551	24.488	28.425	32.362	36.300
23	20.591	24.528	28.465	32.402	36.339
24	20.630	24.567	28.504	32.441	36.378
25	20.669	24.607	28.544	32.481	36.418
26	20.709	24.646	28.583	32.520	36.457
27	20.748	24.685	28.622	32.559	36.496
28	20.788	24.725	28.662	32.599	36.536
29	20.827	24.764	28.701	32.638	36.575
30	20.866	24.803	28.740	32.677	36.615
31	20.906	24.843	28.780	32.717	36.654
32	20.945	24.882	28.819	32.756	36.693
33	20.984	24.921	28.859	32.796	36.733
34	21.024	24.961	28.898	32.835	36.772
35	21.063	25.000	28.937	32.874	36.811
36	21.103	25.040	28.977	32.914	36.851
37	21.142	25.079	29.016	32.953	36.890
38	21.181	25.118	29.055	32.992	36.929
39	21.221	25.158	29.095	33.032	36.969
40	21.260	25.197	29.134	33.071	37.008
41	21.299	25.236	29.178	33.111	37.048
42	21.339	25.276	29.218	33.150	37.087
43	21.378	25.315	29.252	33.189	37.126
44	21.418	25.355	29.292	33.229	37.166
45	21.457	25.394	29.331	33.268	37.205
46	21.496	25.433	29.370	33.307	37.244
47	21.536	25.473	29.410	33.347	37.284
48	21.575	25.512	29.449	33.386	37.323
49	21.614	25.551	29.488	33.425	37.363

Millimetres	500	600	700	800	900
50	21.654	25.591	29.528	33.465	37.402
51	21.693	25.630	29.567	33.504	37.441
52	21.732	25.670	29.607	33.544	37.481
58	21.772	25.709	29.646	33.583	37.520
54	21.811	25.748	29.685	33.622	37.559
55	21.851	25.788	29.725	33.662	37.599
56	21.890	25.827	29.764	33.740	37.638
57	21.929	25.866	29.803	33.740	37.677
58	21.969	25.906	29.843	33.780	37.717
59	22.008	25.945	29.882	33.819	37.756
60	22.047	25.984	29.922	33.859	37.796
61	22.087	26.024	29.961	38.898	37.835
62	22.126	26.063	30.000	33.937	37.874
63	22.166	26.103	30.040	38.977	37.914
64	22.205	26.142	80.079	34.016	37.953
65	22.244	26.181	30.118	34.055	37.992
66	22.284	26.221	30.158	34.095	38.032
67	22.323	26.260	30.197	34.134	38.071
68	22.362	26.299	30.236	34.174	38.111
69	22.402	26.339	30.276	34.213	38.150
70	22.441	26.378	30.315	34.252	38.189
71	22.481	26.418	30.355	34.292	38.229
72	22.520	26.457	30.394	34.331	38.268
78	22.559	26.496	30.433	34.370	38.307
74	22.569	26.536	30.473	34.410	38.347
75	22.638	26.575	30.512	34.449	38.386
76	22.677	26.614	30.551	34.488	38.426
77	22.717	26.654	30.591	34.528	38.465
78	22.756	26.693	30.630	34.567	38.504
79	22.795	26.733	30.670	34.607	38.544
80	22.835	26.772	30.709	34.646	38.583
81	22.874	26.811	30.748	34.685	38.622
82	22.914	26.851	30.788	34.725	38.662
83	22.953	26.890	30.827	34.764	38.701
84	22.992	26.929	30.866	34.803	38.741
85	23.032	26.969	30.906	34.843	38.780
86	23.071	27.008	30.945	34.882	38.819
87	23.110	27.047	30.985	34.922	38.859
88	23.150	27.087	31.024	34.961	38.898
89	23.189	27.126	31.063	35.000	38.937
90	28.229	27.166	31.103	35.040	38.977
91	23.268	27.205	31.142	85.079	39.016
92	23.307	27.244	31.181	85.118	39.055
93	23.347	27.284	31.221	85.158	39.095
94	23.385	27.328	31.260	85.197	39.134
95	23.424	27.362	31.299	35.237	39.174
96	23.464	27.402	31.339	35.276	39.213
97	23.503	27.441	31.378	35.315	39.252
98	23.543	27.481	31.418	35.355	39.292
99	23.582	27.520	31.457	35.394	39.331

Conversion Factor: 1 foot = 0.3048006096 metre.

Feet	0	100	200	300	400
0		30.48006	60.96012	91.44018	121.92024
1	.30490	30.78486	61.26493	91.74498	132.22504
2	.60960	31.08966	61.56972	92.04978	132.52985
3	.91440	31.39446	61.87452	92.35458	122.83465
4	1.21920	31.69926	62.17932	92.65939	123.13945
5	1.52400	32.00406	62.48413	92.96419	123.44425
6	1.82880	32.30886	62.78893	93.26899	123.74905
7	2.13360	32.61367	63.09373	93.57379	124.05385
8	2.43840	32.91347	63.39853	93.87859	124.35865
9	2.74321	33.22327	63.70333	94.18339	124.66345
10	3.04801	33.52807	64.00813	94.48819	124.96825
11	3.35281	23.83287	64.31293	94.79299	125.27308
12	3.65761	34.13767	64.61773	95.09779	125.57780
13	2.96241	24.44247	64.92253	95.40259	125.88265
14	4.26721	34.74727	65.22733	95.70739	126.18740
15	4.57201	25.05207	65.53213	96.01219	126,49225
16	4.87681	35,35687	65.83693	96.31699	126.79705
17	5.18161	35.66167	66.14173	96,62179	127.10185
18	5.48641	25.96647	66.44653	96.92659	127.40665
19	5.79121	36.27127	66.75133	97.23139	127.71146
00	0.00004	20 52202	07.05040	05 50000	400 0400
20	6.09601	26.57607	67.05613	97.53620	128.01620
22	6.40081	37.18567	67.36093	97.84100	128.62586
23	7.01041	37.49047	67.97054	98.45060	128.93066
24	7.31521	27.79528	68.27534	98.75540	129.23546
25	7.62002	38.10008	68.53014	99.06020	129.54026
26	7.92482	38.40488	68.88494	99.36500	129.84506
28	8.53442	38.70968	69.18974 69.49454	99.97460	130.45466
29	8.83922	29.31928	69.79934	100.27940	130.75946
	0.14400				404 00400
30	9.14402	39.62408	70.10414	100.58420	131.06426
32	9.75362	39.92683 40.23368	70.40894	101.19380	131.67386
33	10.05842	40.53848	71.01854	101.49860	131.97860
34	10.36322	40.84328	71.32334	101.80340	132.28346
35	10.66802	41.14808	71.62814	102.10820	132.58827
36	10.97282	41.45288	71.93294	102.41300	132.89307
37	11.27762	41.75768	72.23774	102.71781	133.19787
38	11.58242	42.06248	72.54255	103.02261	133.80747
23	11.00122	. 42.30120	12.02120	-	133.00121
40	12.19202	42.67209	73.15215	103.63221	134.11227
41	12.49682	42.97689	73.45695	103.93701	134.41707
42	12.80163	43.28169	73.76175	104.24181	134.72187
43	13.10643	43.68649	74.06655	104.54661	135.02667
44	13.41123	43.89129	74.37135	104.85141	135.33147
45	13.71603	44.19609	74.67615	105.15621	135.63627
46	14.02083	44.50089	74.98095	105.46101	135.94107
47	14.32563	44.80569	75.28575	105.76581	136.24587
48	14.63043	45.11049	75.59055	106.07061	136.55067
4.5	14.93523	45.41529	75.89535	106.37541	136.85547

1 inch=.02540 metre. 2 inches=.05080 metre. 3 inches=.07620 metre.

Feet	0	100	200	800	400
50	15.24003	45.72009	76.20015	106.68021	137.16027
51	15.54483	46.02489	76.50495	106.98501	137.46507
52 53	16.84963	46.63449	76.80975 77.11455	107.28981	137.76988 138.07468
54	16.45923	46.98929	77.41935	107.89942	138.37948
55	16.76403	47.24409	77.72416	108.20422	138.68428
56	17.06833	47.54890 47.85370	78.02896	108.50902 108.81382	138.98908 139.29388
57	17.37363	48 15850	78.33376 78.63855	109.11862	139.59868
59	17.98324	48.45330	78.94336	109.42342	139.90348
50	18.28804	48.76810	79.24816	109.72822	140.20828
61	18.59284	49.07290	79.55396	110.03302 110.33782	140.51308 140.81788
62	18.89764	49.68250	79.85776 80.16256	110.64262	141.12268
64	19.50724	49.98730	80.46736	110.94742	141.42748
65	19.81204	50.29210	80.77216	111.25222	141.73228
66	20.11684	50.59690	81.07696	111.55702	142.03708
68	20.42164	50.90170 51.20650	81.38176 81.68656	111.86182 112.16662	142.34188
69	21.03124	51.51130	81.99136	112.47142	142.95149
70	21.33604	51.81610	82.29616	112.77623	143.25629
71	21.64084	52.12090	82.60097	113.08103	143.56109
72	21.94564	52.42570 52.73051	82.90577 83.21057	113.38583 113.69063	143.86589 144.17069
74	22.55525	53.03531	83.51537	113.99543	144.47549
75	22.86005	53.34011	83.82017	114.30023	144.78029
76	23.16485	53.64491	84.12497	114.60503	145.08509
77	23.46965	53.94971 54.25451	84.42977 84.73457	114.90983 115.21463	145.38989 145.69469
79	24.07925	54.55931	85.03937	115.51943	145.99949
80	24.38405	54.86411	. 85.34417	115.82423	146.30429
81	24.68885	55.16891	85.64897	116.12903	146.60909
82	24.99365 25.29845	55.47371 55.77851	85.95377 86.25857	116.43383 116.73863	146.91389 147.21869
84	25.60325	56.08331	86.56337	117.04343	147.52350
85	25.90805	56.38811	86.86817	117.34823	147.82830
86	26.21285	56.69291	87.17297	117.65304	148.13310
88	26.51765	56.99771 57.30251	87.47777 87.78258	117.95784 118.26264	148.43790
89	27.12725	57.60732	88.08738	118.56744	149.04750
90	27.43205	57.91212	88.39218	118.87224	149.35230
91	27.73686	58.21692	88.69698	119.17704	149.65710
92	28.04166 28.34646	58.52172 58.82652	89.00178 89.30668	119.48184 119.78664	149.96190 150.26670
94	28.65126	59.13132	89.61138	120.09144	150.57150
95	28.95606	59.43612	89.91618	120.39624	150.87630
96	29.26086	59.74092	90.22098	120.70104	151.18110
97	29.56566	60.04572 60.35052	90.52578 90.83058	121.00584 121.31064	151.48590 151.79070
99	30.17526	60.65532	91.13538	121.61544	152,09550

<sup>4</sup> inches=.10160 metre. 5 inches=.12700 metre. 6 inches=.15240 metre.

(Continued)

Peet			(	-ontinucu)		
1   152.70511   153.46597   13.7062   244.4509   274.2355   215.00991   153.46997   214.37062   244.45099   274.2315   275.23496   275.2	Feet	500	600	700	800	900
1         1 52,70511         183,18517         213,66523         244,15829         274,6255           2         153,31471         183,79477         214,27483         244,76489         275,23495           4         153,61951         184,09957         214,67963         245,05969         275,23495           5         158,92431         184,0957         214,67963         245,06929         275,13495           6         154,22911         184,70917         215,18923         245,66929         276,14935           7         194,53391         185,0397         215,49403         245,79409         276,46418           8         164,38371         185,31877         215,79832         246,58369         277,06375           10         185,44831         185,2287         216,10363         246,58369         277,76375           12         166,05791         186,8377         217,01303         247,4909         277,77316           13         156,36271         186,8477         217,32283         247,80290         277,97816           14         156,697231         187,45237         217,93244         248,10770         278,58776           15         166,97231         187,45237         217,3244         248,10770	0	152,40030	182.88007	213.36043	243.84049	274.32055
153.0991	1	152.70511	183.18517	213.66523		
3         153.34471         183.79477         214.27483         244.76489         275.23495           5         163.69431         184.09957         214.57968         225.05969         275.23495           6         164.22911         184.70917         215.18923         245.66929         276.14935           7         164.53991         185.01977         215.18923         245.6929         276.14935           8         164.83871         185.62357         216.10363         246.58369         277.05375           9         165.14351         185.62357         216.10363         246.58369         277.05375           10         165.44351         185.62357         216.10363         246.58369         277.76375           11         165.75311         186.23377         216.71323         247.19329         277.67365           12         166.66751         187.14757         217.62764         248.10770         278.58776           14         166.66751         187.14757         217.62764         248.10770         278.58776           15         166.97231         187.45237         217.93244         248.10770         278.58776           16         167.27711         187.56596         188.06196         218.24740	2	153.00991	183.46997-			
5         163.92431         184.40437         214.88443         245.6649         275.84456           6         164.22911         184.70917         215.18923         245.66929         276.14935           7         164.53391         185.01977         215.78823         245.74699         276.14845           8         164.83871         185.31877         216.10363         246.58369         277.06375           9         165.14351         185.62357         216.10363         246.58369         277.06375           10         185.46351         185.82377         216.10363         247.19329         277.67355           11         185.75311         186.83777         217.01803         247.19329         277.67356           12         186.66791         186.84277         217.32283         247.19329         277.97816           13         186.86791         186.84477         217.32284         248.10770         278.58776           15         186.97231         187.45237         217.93244         248.10770         278.58776           15         186.97231         187.45237         217.93244         248.10770         278.58776           15         186.97231         187.45237         217.93244         248.10770	3	153.31471				
6         154.29911         184.70917         215.18923         245.6929         276.14835           7         154.53911         185.01397         215.48403         245.97409         276.46415           8         164.83871         185.31877         215.78883         246.27889         277.76875           10         155.44831         185.92837         216.10363         246.58359         277.05375           11         185.75311         186.28317         216.71323         247.19329         277.76735           12         186.36771         186.8377         217.01803         247.49909         277.97816           13         186.36271         186.84977         217.32283         247.80290         277.97816           14         156.66751         187.14757         217.62764         248.10770         278.58776           15         166.97231         187.45237         217.93244         248.11570         278.58776           15         156.97231         187.45237         217.93244         248.10770         278.58776           15         156.97231         187.45237         217.93244         248.10770         278.58276           16         157.27711         187.75718         218.34974         249.92210 <th>4</th> <th>153.61951</th> <th>184.00957</th> <th>214.57963</th> <th>245.05969</th> <th>275.53975</th>	4	153.61951	184.00957	214.57963	245.05969	275.53975
7         164.53391         185.01397         215.49408         245.97409         276.46415           8         164.83871         185.01397         215.7883         246.27889         276.76891           10         165.44351         185.62357         216.10363         246.58369         277.06375           10         165.44351         186.82317         216.10363         246.88849         277.36856           11         165.75311         186.23317         216.71323         247.19329         277.6738           12         186.65791         186.83797         217.01803         247.49099         277.97816           13         186.36271         186.84277         217.32283         247.80290         278.2296           14         186.66751         187.14757         217.62764         248.10770         278.89276           15         166.97231         187.45237         217.93244         248.41250         278.89256           16         187.27711         187.75718         218.23724         248.71730         279.19736           16         187.28711         187.65237         218.35464         249.02210         279.50216           17         187.58192         188.06195         218.54204         249.02210 <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>						
8         164.83871         185.31877         215.78833         226.27889         277.06375           10         185.44351         185.62367         216.10363         226.58369         277.06375           11         185.75311         186.23317         216.40843         247.19329         277.6736           12         186.05791         186.83797         217.01803         247.19329         277.6736           13         186.36271         186.84377         217.32283         247.19329         277.6736           14         186.66751         187.14757         217.63264         248.10770         278.58276           15         186.97231         187.45237         217.93244         248.10770         278.58776           15         186.97231         187.45237         217.93244         248.10770         278.58776           16         187.27711         187.75718         218.354244         249.02210         279.50216           18         187.88672         188.36678         218.84584         249.322690         279.50216           21         185.4012         188.897638         219.45644         249.93250         280.41656           21         185.80112         189.28118         219.76124         250.24130<						
155.14351						
10 165.4631 185.92837 216.40843 246.88849 277.36856 11 165.75311 186.23317 216.71323 247.19329 277.67336 122 156.05791 186.23377 217.01803 247.49809 277.97316 13 156.36271 186.84277 217.32283 247.80250 278.28296 13 156.66751 187.14757 217.62764 248.10770 278.58776 15 166.97321 187.75718 218.23724 248.10770 278.58776 16 157.27711 187.75718 218.23724 248.10770 279.19735 17 187.58192 188.36195 218.54204 249.02210 279.50216 187.85672 188.36578 218.84568 249.32290 279.80696 19 158.19152 188.56716 219.15164 249.56170 280.11176 200 158.49632 189.25118 219.76124 250.24130 280.712136 21 158.80112 189.25118 219.76124 250.24130 280.72136 22 159.10592 189.56598 220.05604 250.54610 281.02616 23 159.41072 189.89078 220.27084 250.85090 281.3396 24 169.71852 190.19558 220.67564 251.15670 281.63576 26 160.32612 190.80618 21.28524 250.24130 282.24556 26 160.32612 190.80618 21.28524 250.24130 282.24556 26 160.32612 190.80618 21.28524 250.24130 282.255017 286.6663 281.24666 281.44678 281.44678 221.89484 252.37490 282.85497 286.6663 219.14676 221.85624 250.256670 281.63576 281.63576 281.63578 219.171958 222.18964 252.37490 282.85497 281.61.8952 191.71958 222.18964 252.37490 282.85497 281.61.8952 191.71958 222.18964 252.37490 282.85497 281.61.8952 191.71958 222.18964 252.37490 282.85497 281.61.8952 191.71958 222.18964 252.67971 283.15977 361.61.84912 192.32918 222.80455 253.28931 283.75937 361.61.84912 192.32918 222.80455 253.28931 283.75937 361.63.67733 193.65519 224.33325 254.81331 285.52937 37.166.6233 193.64539 222.5455 255.42291 283.59937 39.164.87633 193.65519 224.33325 254.81331 285.52937 39.164.87633 193.65519 224.58395 255.42291 285.50297 285.656337 194.46279 225.55245 256.32371 286.81737 286.6673 195.96679 226.66685 256.94691 287.42697 285.56991 284.58973 194.6279 225.55245 256.32571 285.52937 39.164.87633 195.67799 225.55245 256.32571 285.52937 39.164.87633 195.67799 225.55245 256.32571 285.52937 39.164.87633 195.6799 226.66685 256.94691 287.42697 285.66991 287.43697 225.56698 256.92691 287.43697 285.66698 287.75669 285.6						
11         155.75311         166.23317         216.71323         247.19329         277.67336           12         166.05791         186.33797         217.01803         247.49809         277.97816           13         166.66751         187.14757         217.32283         247.80290         278.28296           15         166.97321         187.46237         217.93244         248.1070         278.58776           16         187.27711         187.75718         218.23724         248.1250         279.19736           17         187.58192         188.36678         218.84584         249.02210         279.50216           18         187.86872         188.36678         218.84584         249.32690         279.50216           18         185.80158         219.15164         249.02610         279.50216           21         158.1012         188.87158         219.15164         249.93650         280.41656           21         158.90112         189.28118         219.76124         250.24130         280.41656           21         158.9012         189.89768         220.27084         250.85090         281.3366           23         159.41072         189.89978         220.27084         250.85090         281.3066	9	100.14301	100.02007	216.10363	240.08309	277.06370
12         156.05791         166.53797         217.01803         247.48909         277.97816           13         166.66751         186.84277         217.32283         247.80250         278.28267           15         166.66751         187.14757         217.32283         247.80250         278.28296           16         187.27711         187.75718         218.32724         248.11250         279.89256           16         187.27711         187.75718         218.34204         249.02210         279.50210           18         187.88672         188.36678         218.84584         249.02210         279.50216           20         168.49632         188.36678         218.84584         249.63170         280.1176           21         183.80112         189.28118         219.76124         250.24130         280.72136           22         189.1052         189.28118         219.76124         250.54610         281.02616           23         159.41072         189.89078         220.37084         250.54610         281.02616           24         169.71852         190.15083         220.98044         251.46050         281.94056           25         160.02032         190.5003         220.98044         251.76560 </th <th></th> <th>155.44831</th> <th>185.92837</th> <th>216.40843</th> <th>246.88849</th> <th>277.36855</th>		155.44831	185.92837	216.40843	246.88849	277.36855
13         166.36271         186.34477         217.32283         247.80250         278.28296           14         166.66751         187.14767         217.62764         248.10770         278.28296           15         166.66731         187.4767         217.92244         248.10770         278.28296           16         187.27711         187.75718         218.23724         248.17730         279.19736           17         187.58192         188.06198         218.54204         249.02210         279.50216           18         187.88672         188.36678         218.84684         249.32260         279.8069           19         168.1952         188.97638         219.45644         249.93650         280.41656           21         188.8012         189.28118         219.76124         250.24130         280.72136           22         159.10592         189.56598         220.06504         250.54610         281.02616           23         159.41072         189.89078         220.37084         250.85090         281.33656           25         160.032512         190.50033         220.95044         251.4560         281.94056           26         160.32512         190.80616         221.28524         251.75530 <th></th> <th>155.75311</th> <th>186.23317</th> <th>216.71323</th> <th>247.19329</th> <th>277.67336</th>		155.75311	186.23317	216.71323	247.19329	277.67336
14         156,66751         187,14757         217,62764         248,10770         278,58775           15         166,97331         187,45237         217,93244         248,11250         278,89256           16         187,27711         187,75718         218,33724         248,11250         279,19736           17         187,58192         188,06198         218,54204         249,02210         279,50216           18         187,86872         188,36678         218,45644         249,32800         279,80696           20         166,49632         188,97688         219,45644         249,93250         280,41656           21         183,80112         189,28118         219,76124         250,24130         280,73136           22         189,1092         189,38978         220,06604         250,54610         281,03696           24         189,71652         190,15558         220,07684         250,54610         281,3396           25         160,02032         190,50038         220,98044         251,46050         281,3396           25         160,62992         191,1095         221,59044         252,07010         282,55017           26         160,39372         191,11958         222,1944         252,49451 <th></th> <th>156.05791</th> <th>186.53797</th> <th>217.01803</th> <th>247.49809</th> <th>277.97816</th>		156.05791	186.53797	217.01803	247.49809	277.97816
15         166.97231         187.45237         217.93244         248.41250         278.89256           16         187.27711         187.75718         213.23724         243.71730         279.19736           17         187.58192         188.06188         218.54204         249.02210         279.80696           18         187.88672         188.36678         218.84684         249.02210         279.80696           18         168.19152         188.37168         219.15164         249.03690         279.80696           20         168.49632         188.97638         219.45644         249.93650         280.11176           21         183.80112         189.28118         219.76124         250.24130         280.72136           22         159.1092         183.89078         220.05604         250.54510         280.72136           23         159.41072         183.89078         220.37084         251.56509         281.3366           24         169.71852         190.19558         220.67564         251.46050         281.43576           25         160.032512         190.80618         221.28524         251.76500         281.94056           26         160.93472         191.14478         221.89484         252.37490			186.84277	217.32283	247.80290	278.28296
16         187,27711         187,75718         218,23724         248,71730         279,19736           17         187,58192         188,06198         218,24204         249,02210         279,50266           18         167,8872         188,36678         218,84684         249,32690         279,80696           19         168,19152         188,97638         219,15164         249,63170         280,11176           20         168,49632         188,97638         219,76124         250,24130         280,72136           21         158,80112         189,28116         219,76124         250,24130         280,72136           22         159,1092         189,58598         220,06504         250,54610         281,02616           23         159,41072         189,89078         220,37084         250,85090         281,33966           24         169,71852         190,19558         220,67664         251,15670         281,63576           25         160,039512         190,80618         21,28524         251,75530         282,24556           27         160,62992         191,10995         221,59004         252,07010         282,55017           28         160,93472         191,41476         221,89464         252,37490<	14	156.66751	187.14757	217.62764	248.10770	278.58776
16         187,27711         187,5718         213,23724         243,71730         279,19736           17         187,58192         188,06188         218,54204         249,02210         279,50216           18         187,58192         188,36678         218,84684         249,02210         279,80696           18         168,19152         188,37158         219,15164         249,63170         280,11176           20         168,49632         188,97638         219,45644         249,93650         280,72135           21         183,80112         189,28118         219,76124         250,24139         280,72136           22         189,1092         183,89078         220,06504         250,56509         281,3066           24         169,41072         189,89078         220,37084         251,56509         281,3066           25         160,02032         190,19558         220,67564         251,46050         281,4056           26         160,32512         190,80618         221,28504         251,46050         281,4056           27         160,62992         191,10995         221,28904         252,470710         282,55017           28         161,5432         192,02435         222,19964         252,07971	15	156.97231	187 45237	217 93244	248 41250	278 89256
17         187,58192         188,06198         218,54204         249,0210         279,50216           18         187,88672         188,36678         218,24504         249,23290         279,50216           19         186,19152         188,67168         219,15164         249,23290         280,11176           20         186,49632         188,97688         219,45644         249,93550         280,41656           21         188,8012         189,28118         219,76124         250,24130         280,72136           22         189,10592         189,89078         220,06604         250,54610         281,0366           24         189,71652         190,1958         220,07664         250,56610         281,0366           24         189,71652         190,1958         220,07664         250,56610         281,3396           25         160,02032         190,5003         20,98044         251,46050         281,4356           26         160,38512         190,80618         221,28044         251,46050         281,5456           27         160,6292         191,11998         221,59044         252,47971         282,55617           28         161,3352         191,14476         221,6446         252,98461	16					
18         167.88672         188.36678         218.84684         249.32690         279.80696           19         156.19152         188.67158         219.15164         249.63170         280.11176           20         168.49682         188.97688         219.45644         249.93550         280.41656           21         188.3012         189.28118         219.76124         250.24130         280.72136           22         189.10592         189.88578         220.07664         250.5509         281.3366           23         189.41072         189.8978         220.37084         250.5509         281.3266           24         169.71852         190.19558         220.67564         251.15670         281.63576           25         160.02032         190.5003         220.38044         251.46050         281.94056           26         160.32512         190.80618         221.28524         251.75300         282.24536           27         160.62992         191.10998         221.59044         252.07010         282.55017           28         161.5492         192.02438         222.19964         252.07971         283.15977           30         161.54921         192.02438         222.90925         35.28931	17					
18         168.19152         188.67158         219.15164         249.63170         280.11176           20         168.49632         188.97638         219.45644         249.93550         280.41656           21         188.80112         189.28118         219.76124         249.93550         280.41656           22         189.1032         189.58598         220.06504         250.54610         281.02616           23         189.41072         189.89078         220.37084         250.85090         281.33096           24         189.71852         190.19588         220.67564         250.565090         281.33096           25         160.02032         190.50038         220.28044         251.46050         281.94056           26         160.32512         190.80818         221.28524         251.76530         282.24536           27         160.62992         191.1098         221.59044         252.47010         282.255017           28         160.38512         191.71956         222.19964         252.47971         283.16871           30         161.54432         192.02438         222.50445         252.98451         283.46457           31         161.84912         192.32918         222.50445         253.2893	18	157.88672				
21         188,80112         189,28118         219,76124         250,24130         280,72136           22         189,1052         189,8558         220,06604         250,54610         281,02616           23         169,41072         189,89078         220,37084         250,5690         281,3396           24         169,71652         190,19558         220,67664         251,16570         281,63576           25         160,02032         190,50638         221,28524         251,76530         282,24536           27         160,62992         191,10998         221,28904         252,07010         282,255017           28         160,93472         191,44476         221,89484         252,37490         282,85597           29         161,38952         191,71958         222,19964         252,07971         283,15977           30         161,54432         192,02435         222,19964         252,67971         283,15977           31         161,84912         192,20358         223,50925         53,28931         283,46457           32         162,16872         192,0335         233,1405         253,59411         284,07417           33         162,46872         192,93879         233,1405         253,59411	19	158.19152	188.67158	219.15164		
21         188,80112         189,28118         219,76124         250,24130         280,72136           22         189,1052         189,8558         220,06604         250,54610         281,02616           23         169,41072         189,89078         220,37084         250,5690         281,3396           24         169,71652         190,19558         220,67664         251,16570         281,63576           25         160,02032         190,50638         221,28524         251,76530         282,24536           27         160,62992         191,10998         221,28904         252,07010         282,255017           28         160,93472         191,44476         221,89484         252,37490         282,85597           29         161,38952         191,71958         222,19964         252,07971         283,15977           30         161,54432         192,02435         222,19964         252,67971         283,15977           31         161,84912         192,20358         223,50925         53,28931         283,46457           32         162,16872         192,0335         233,1405         253,59411         284,07417           33         162,46872         192,93879         233,1405         253,59411	20	158.49632	188 97638	219 45644	249 93650	280 41656
22         189,10892         189,58598         220,05604         250,54610         281,02616           23         189,41072         189,89078         220,37084         250,85090         281,33096           24         169,71852         190,19858         220,37084         251,16570         281,63576           25         160,02032         190,50038         221,28824         251,76330         282,24536           26         160,32512         190,80818         221,28824         251,76330         282,24536           27         160,63932         191,10998         221,59044         252,07010         282,55617           28         160,338472         191,41478         221,89484         252,47971         282,85497           29         161,38952         191,71958         222,19964         252,98451         283,46457           31         161,84912         192,02438         222,50446         252,98451         283,76937           32         162,15392         192,63399         223,11406         253,89811         284,37897           33         162,46872         192,93879         223,71365         254,20371         284,68377           34         162,76553         193,85319         224,02845         254,808						
23         169,41072         189,89078         220,37084         250,85090         281,33096           24         169,71852         190,19558         220,67564         251,15670         281,33096           25         160,02032         190,50033         220,28044         251,46050         281,94056           26         160,32612         190,80618         221,28524         251,75330         282,24536           27         160,62992         191,1095         221,59064         252,77490         282,85497           28         160,33472         191,41476         221,89484         252,37490         282,85497           29         161,34952         192,71758         222,19964         252,298451         283,76937           30         161,54432         192,32918         222,50445         252,298451         283,76937           31         161,84912         192,32918         222,50445         252,38831         283,76937           32         162,1532         192,93879         223,41835         253,28931         283,76937           34         162,76533         193,54839         223,14265         253,28981         284,7893           35         163,66833         193,54839         223,41836         254,2031<	22	159.10592				
24         169.71552         190.19558         220.67564         251.15670         281.63576           25         160.02032         190.50033         220.38044         251.46050         281.94056           27         160.62992         191.10995         221.59004         252.07010         282.55017           28         160.93472         191.41476         221.89484         252.37490         282.85497           29         161.83952         191.71958         222.19964         252.67971         283.15977           30         161.54432         192.02435         322.50445         252.98451         283.46457           31         161.84912         192.02435         322.50445         252.98451         283.46457           32         162.16339         192.63393         223.11406         253.59411         284.76937           34         162.76553         193.28359         223.11406         253.89891         284.37897           35         163.06633         193.54839         224.02845         254.50851         284.98857           36         163.37313         193.85319         224.02845         254.50851         285.90297           35         163.67793         194.46279         224.02845         254.5085	23	159.41072				
26         180.328512         190.80818         221.28524         251.76530         282.24536           27         160.63932         191.10998         221.59044         252.07010         282.55017           28         160.93472         191.14978         221.59064         252.07071         283.25017           29         161.84952         191.71958         222.19964         252.67971         283.46977           30         161.84912         192.02438         222.80925         253.28931         283.46457           31         162.45872         192.63399         223.11405         253.59411         283.46457           32         162.45872         192.93879         223.41835         253.89891         284.07417           34         162.45872         193.54839         223.72365         254.20371         284.68377           35         163.05833         193.54839         224.02845         254.50851         284.98857           36         163.37313         193.85319         224.63806         255.14813         285.2937           37         163.67793         194.46779         224.63806         255.14813         285.59817           38         165.98273         194.46779         224.63806         255.1331	24	169.71552	190.19558			
26         160.32812         190.80618         221.28524         251.75630         282.24536           27         160.62932         191.10998         221.59064         252.07010         282.55017           28         160.93472         191.41476         221.89484         252.67971         282.85497           29         161.84912         192.02438         222.19964         252.67971         283.46457           31         161.84912         192.32918         222.80925         253.28931         283.76937           32         162.15392         192.63399         223.11406         253.59411         284.07417           33         162.45672         192.93879         223.41836         253.89891         284.07417           34         162.76353         193.24359         223.72365         254.20371         284.68377           35         163.06633         193.54839         224.02845         254.50851         284.98857           36         163.37313         193.85319         224.33925         254.81331         285.2937           37         163.67793         194.16799         224.63806         255.11811         285.59817           38         163.98273         194.46279         224.63806         255.1291<	25	160.02032	190.50038	220.98044	251.46050	281 94056
37         160.62992         191.10995         221.59004         252.07010         282.55617           28         160.93472         191.41476         221.89484         252.37490         322.85617           29         161.23952         191.71958         222.19964         252.67971         283.16977           30         161.54432         192.02435         222.80925         253.28931         283.46457           31         161.84912         192.02435         222.80925         253.28931         283.76937           32         162.16392         192.63399         223.11405         233.59411         284.07417           33         162.46872         192.93879         223.41886         253.89891         284.37897           34         162.76553         193.85319         224.02845         254.50851         284.98857           36         163.37313         193.65319         224.02845         254.50851         284.98857           37         163.67793         194.46279         224.02845         254.50851         285.90297           38         163.98273         194.46279         225.524765         255.72771         285.20777           40         164.89713         195.37719         225.55245         256.032	26					
28         160.93472         191.41476         221.89484         252.37490         282.85497           29         161.3952         191.71958         222.19964         252.67971         283.15977           30         161.8432         192.02435         222.50445         252.98451         283.46457           31         161.84912         192.3916         222.80925         253.28931         283.76937           32         162.15392         192.6339         223.11405         253.59411         284.07417           33         162.45672         192.92879         223.41835         253.89891         284.37897           34         162.76553         193.24359         223.72365         254.20371         284.63377           35         163.37813         193.85819         224.02245         254.50851         284.98857           36         163.37813         193.85819         224.02245         255.42391         285.29337           37         163.67793         194.15799         224.62805         255.11811         285.29337           38         164.28753         194.76759         225.24766         255.72771         286.50277           40         164.289233         195.0739         225.55245         256.33731 <th>27</th> <th></th> <th></th> <th></th> <th></th> <th></th>	27					
50         161.54432         192.02435         222.50445         252.98451         283.46457           31         161.84912         192.32918         222.80925         253.28931         283.76937           32         162.15392         192.63399         223.11405         253.59411         284.07417           33         162.46672         192.92879         223.41835         253.89891         284.37897           34         162.76553         193.24359         223.72365         254.20371         284.63377           35         163.06633         193.54839         224.02245         254.50851         284.98857           36         163.37313         193.85819         224.02245         254.50851         284.98857           37         163.67733         194.15799         224.62805         255.1811         285.29337           38         164.28753         194.76759         225.24766         255.72771         285.02777           40         164.289733         195.07239         225.55245         256.03231         286.51277           41         164.29233         195.07239         225.55245         256.33731         286.81237           42         165.20193         195.68199         226.16205         256.4221		160.93472	191.41478	221.89484	252.37490	282.85497
S1         161.84912         192.32918         222.80925         553.28931         283.76937           32         169.15392         192.3399         223.1406         253.59411         284.07417           33         162.46872         192.93879         223.41886         253.89891         284.37897           34         162.76553         193.24359         223.73266         254.2031         284.68377           35         163.6683         193.54839         224.02845         284.50851         284.98857           36         163.37313         193.85319         224.03245         254.81331         285.2937           37         163.67793         194.16799         224.4285         255.42311         285.5817           38         163.98273         194.6775         224.94285         255.42291         285.9277           39         164.28753         194.76759         225.55245         256.03251         286.20777           40         164.59233         195.07739         225.55245         256.03251         286.51257           41         164.39713         195.37719         225.85725         256.33731         286.51257           42         165.20133         195.68199         226.1200         256.94591	29	161.23952	191.71958	222.19964		
32         169,15392         192,63399         223,11405         253,59411         284,07417           33         162,46872         192,93879         223,41835         253,8981         284,37897           34         162,76353         193,24353         223,72365         254,20371         284,68377           35         163,06833         193,65319         224,02845         254,8031         285,29337           37         163,6773         194,46279         224,94285         255,1811         285,90297           38         163,98273         194,46279         224,94285         255,42291         285,90297           40         164,89713         195,07239         225,56245         256,03251         286,51257           41         164,89713         195,37719         225,56245         256,03251         286,51257           42         165,20139         195,68199         226,16205         256,64211         287,12217           43         185,50673         195,98679         226,46885         256,94691         287,42297           45         166,11633         196,89139         226,77165         257,26171         287,72174           45         166,11633         196,89139         226,77165         257,56132 <th>50</th> <td>161.54432</td> <td>192.02438</td> <td>222.50445</td> <td>252.98451</td> <td>283,46457</td>	50	161.54432	192.02438	222.50445	252.98451	283,46457
38         162,46672         192,93879         223,41835         253,88991         284,37897           34         162,76553         193,24359         223,72365         254,20371         284,68377           35         163,06633         193,54839         224,02245         254,50851         284,98857           36         163,37313         193,85319         224,63805         255,1831         285,2937           37         163,6773         194,16799         224,62805         255,1831         285,2937           38         164,28753         194,76759         224,94285         255,42291         285,90297           40         164,59233         195,07329         255,55245         256,03251         286,21777           41         164,89713         195,37719         225,85725         256,33731         286,81737           42         165,2013         195,68199         226,46695         256,94691         287,4221           43         165,50673         195,95679         226,46695         256,94691         287,4221           44         165,1633         195,8939         227,07645         257,2652         288,3656           45         166,4213         196,9019         227,36506         258,47632		161.84912	192.32918	222.80925	253.28931	283.76937
34         162.76353         193.24359         223.72365         254.20371         284.68377           35         163.06633         193.54839         224.02845         254.50851         224.98857           36         163.37313         193.85319         224.33925         254.81331         285.29317           37         163.67793         194.16799         224.63806         255.11811         285.59817           38         163.98273         194.46279         224.94285         255.42291         285.90297           39         164.38753         194.67679         225.24766         255.72771         285.90297           40         164.89713         195.37719         225.85725         256.03251         286.51257           41         164.89713         195.68199         226.16205         256.64211         287.1227           43         165.50673         195.98679         226.46685         256.94291         287.42697           44         166.81163         196.29159         226.77165         257.25171         287.73178           45         166.11633         196.89539         227.07645         257.86133         288.34133           47         166.73592         197.20599         227.68506         258.47692				223.11405	253.59411	284.07417
35         163.06633         193.54839         224.02845         254.50851         284.98857           36         163.37313         193.65319         224.33325         254.81331         285.2937           37         163.67793         194.16799         224.62856         255.1811         285.2931           38         163.98273         194.46279         224.94285         255.4291         285.90297           39         164.28763         194.76759         225.24765         255.72771         285.2077           40         164.89713         195.07239         225.56245         256.03251         286.81737           41         164.89713         195.07239         225.56545         256.03251         286.81737           42         165.20193         195.07879         226.16205         256.64211         287.12217           43         165.50673         195.96879         226.46695         256.34331         287.12217           44         165.81163         196.39159         227.07645         257.56522         288.0656           46         166.4213         196.9019         227.37.38125         257.86132         288.3656           47         166.703073         197.51030         227.93086         258.47092 <th></th> <th></th> <th></th> <th></th> <th>253.89891</th> <th>284.37897</th>					253.89891	284.37897
36         163,37813         193,85319         224,33925         254,81331         285,29837           37         163,67793         194,16799         224,68205         255,1811         285,59817           38         163,98273         194,46279         224,94285         255,42291         285,99297           39         164,28753         194,76759         225,24766         255,72771         286,2077           40         164,59233         195,07239         225,55245         256,03251         286,51257           41         164,89713         195,37719         225,85725         256,33731         286,81737           42         165,30193         195,68199         226,16205         256,46211         287,12217           43         165,50673         195,68199         226,77166         257,26171         287,73178           44         165,50673         195,39159         226,77166         257,26171         287,73178           45         166,11633         196,39159         227,07645         257,56552         288,36568           46         166,4213         196,99119         237,38126         257,86132         288,36184           47         166,703073         197,51030         237,99086         258,47092<	34	162.76353	193.24359	223.72365	254.20371	284.68377
36         163.37313         193.65319         224.33325         254.81331         285.2937           37         163.67793         194.16799         224.63805         255.11811         285.5931           38         163.98373         194.46279         224.94285         255.42291         285.90297           39         164.28763         194.76769         225.24766         255.72771         286.2077           40         164.59233         195.07239         225.55245         256.03251         286.51257           41         164.89713         195.37719         225.85725         256.33731         286.81737           42         165.20193         195.68199         226.16205         256.46211         287.12217           43         165.50673         195.99579         226.46693         256.34591         287.43214           44         165.81163         196.39159         227.07645         257.56522         288.06568           46         166.4213         196.99119         237.38125         257.86132         288.36368           47         166.703073         197.51030         237.39086         258.47092         288.66618           48         1616.703073         197.51030         237.38086         258.47092		163.06833	193.54839	224.02845	254.50851	284.98857
37         163.67793         194.16799         224.63805         255.11811         285.59817           38         163.98273         194.46279         224.94285         255.42291         285.90297           39         164.8763         194.76759         225.24765         255.72771         286.20777           40         164.89713         195.37719         225.55245         256.03251         286.51257           41         164.89713         195.37719         225.85725         256.34271         287.1217           43         165.50633         195.96679         226.46695         256.64211         287.1227           43         165.81163         196.39159         226.77165         257.25171         287.7378           45         166.11633         198.89539         227.07645         257.56522         288.03658           46         166.42113         196.90119         237.38125         257.86133         288.34138           47         166.73892         197.20899         227.66806         258.47092         288.66618           48         167.03073         197.51030         237.39086         258.47092         288.96618					254.81331	285.29337
39         164.28753         194.76759         225.24765         255.72771         286.20777           40         164.59323         195.07239         225.55245         256.03251         286.51257           41         164.89713         195.03719         225.85725         256.33731         286.81737           42         165.20193         195.68195         226.16205         256.64211         287.12217           43         165.80163         195.98679         226.46695         256.725171         287.42697           44         165.81163         196.29159         226.77165         257.25171         287.7378           45         166.1633         198.89539         227.07645         257.86132         288.34138           47         166.73392         197.20599         227.68506         258.16512         288.64618           48         167.03073         197.51030         237.39086         258.47092         288.9658						285.59817
40 164.59233 195.07239 225.55245 256.03251 286.51257 41 164.89713 195.37719 225.85725 256.32731 286.81737 42 165.20193 195.68199 226.16205 256.64211 287.12217 43 185.50673 195.08679 226.46695 256.94691 287.42697 44 165.31153 196.20159 226.77165 257.25171 287.73178 45 166.11633 195.89539 227.07645 257.55652 288.03658 46 166.42113 196.90119 227.38125 257.85132 288.34138 47 166.72592 197.20599 227.68506 258.16512 288.64618 48 167.03073 197.51030 227.93086 258.47092 288.96508						
41         164.89713         195.37719         225.85725         256.33731         286.81737           42         185.2013         195.68199         226.16205         256.64211         287.12217           43         185.50673         195.99679         226.46695         256.24691         287.42697           44         165.81163         196.29159         226.77165         257.26171         287.73178           45         166.11633         195.89539         227.07645         257.56552         288.03658           46         166.42113         196.99119         237.38125         257.56522         288.3438           47         166.72892         197.20599         227.66806         258.16612         288.64618           48         167.03073         197.51030         237.39086         258.47092         288.969618	39	164.28753	194.76759	225.24765	255.72771	286.20777
41         164.89713         195.37719         225.85725         256.32731         286.81757           42         165.20193         195.68199         226.16205         256.64211         287.12217           43         185.50673         195.08679         226.46695         256.94691         287.42697           44         165.31153         196.20169         226.77165         257.25171         287.73178           45         166.11633         198.89539         227.07645         257.55652         288.03658           46         166.42113         196.90119         227.38125         257.86132         288.34132           47         166.72592         197.20599         227.66506         258.45612         288.66618           48         167.03073         197.51030         227.39086         258.47092         288.96968	40	164.59233	195.07239	225.55245	256.03251	286,51257
42         165.20193         195.68199         226.16205         256.64211         287.12217           43         165.50673         195.98579         226.46695         256.94691         287.42697           44         165.81153         196.29159         226.77165         257.25171         287.72178           45         166.41633         195.89539         227.07645         257.55652         238.03658           46         166.42113         196.90119         237.38125         257.86132         288.34138           47         166.73593         197.20599         227.68506         258.16612         288.54618           48         167.03073         197.51030         227.93086         258.47092         288.96998		164.89713		225.85725		
44         165.81153         196.29169         226.77165         257.25171         287.73178           45         166.11633         196.89539         227.07645         257.55652         288.08658           46         166.42113         196.90119         227.38125         257.85132         288.34138           47         166.73592         197.20599         227.68506         258.16512         288.64618           48         167.03073         197.51030         227.93086         258.47092         288.96998			195.68199		256.64211	
45 166.11633 198.89539 227.07645 257.55652 288.03658 46 166.42113 196.90119 237.38125 257.86133 288.34138 47 166.73592 197.20599 227.66506 258.15612 288.64618 48 167.03073 197.51030 237.39086 258.47092 288.56618					256.94691	287.42697
46 166.42113 196.90119 297.38125 257.86133 288.34138 47 166.73592 197.20599 227.66506 258.16612 288.64618 48 167.03073 197.51030 227.93086 258.47092 288.56618	44	165.81153	196.29159	226.77165	257.25171	267.73178
46 166 4213 196 90119 237.38125 257.86132 288.34138 47 166 73593 197.30599 227.68506 258.16612 288.64618 48 167.03073 197.51030 227.39086 258.47092 288.96098		166.11633	198.89839	227.07645	257.55552	288.03658
48 167.03073 197.51030 227.99086 258.47092 288.95098	46	166.42113	196.90119	227.38125		
						288.64618
49   167.33553   197.81560   228.29566   258.77572   289.25578						288.95098
	49	167.33553	197.81560	228.29566	258.77572	289.25578

7 inches=.17780 metre. 8 inches=.20320 metre. 9 inches=.22860 metre.

(Continued)

Feet	500	600	700	800	900
50	167.64034	198.12040	228,60046	259.08052	289.56058
51	167.94514	198.42520	228.90526	259.38532	289.86538
52	168.24994	198.73000	229.21006	259.69012	290.17018
53	168.55474	199.03480	229.51486	259.99492	290.47498
54	168.85954	199.33960	229.81966	260.29972	290.77978
55	169.16434	199.64440	230.12446	260.60452	291.08458
56	169.46914	199.94920	230.42926	260.90932	291.38938
57	169.77394 170.07874	200.25400	230.73406 231.03886	261.21412 261.51892	291.69418 291.99898
58 59	170.38354	200.86360	231.34366	261.82372	292.30378
60	170.68834	201.16840	231.64846	262.12852	292,60859
61	170.99314	201.47320	231.95326	262,43332	292,91339
62	171.29794	201.77800	232.25806	262,73813	293,21819
63	171.60274	202,08280	232,56287	263,04293	293,52299
64	171.90754	202.38760	232.86767	263.34773	293.82779
65	172.21234	202.69241	233.17247	263.65253	294.13259
66	172.51715	202.99721	233.47727	263.95733	294.43739
67	172.82195	203.30201	233.78207	264.26213	294.74219
68	173.12675	203.60681	234.08687	264.56693	295.04699
69	173.43155	203.91161	234.39167	264.87173	295.35179
70	173.73635	204.21641	234.69647	265.17653	295.65659
71	174.04115	204.52121	235.00127	265.48133	295.96139
72	174.34595	204.82601	235.30607	265.78613	296.26619
73	174.65075 174.95555	205.13081 205.43561	235.61087 235.91567	266.09093 266.39573	296.57099 296.87579
75	175.26035	205.74041	236.22047	266.70053	297.18059
76	175.56515	206.04521	236.52527	267.00533	297.48539
77 78	175.86995	206.35001 206.65481	236.83007	267.31013 267.61494	297.79020
79	176.47955	206.95961	237.43967	267.91974	298.39980
80	176.78435	207.26441	237.74448	263.22454	298.70460
81	177.08915	207.56922	238.04928	268.52934	299.00940
82	177.39395	207.87402	238.35408	268.83414	299.31420
83	177.69876	208.17882	238.65888	269.13894	299.61900
84	178.00356	208.48362	238.96368	269.44374	299.92380
85	178.30836	208.78842	239.26848	269.74854	300.22860
86	178.61316	209.09322	239.57328	270.05334	300.53340
87	178.91796	209.39802	239.87808	270.35814	300.83820
88 89	179.22276 179.52756	209.70282	240.18288 240.48768	270.66294	301.14300 301.44780
90	179.83236	210.31242	240.79248	271.27254	301.75260
91	180.13716	210.61722	241.09723	271.57734 271.88214	302.05740
92	180.44196 180.74676	211.22682	241.70688	272.18694	302,36220
94	181.05156	211.53162	242.01168	272.49174	302.97181
95	181.35636	211.83642	242.31648	272.79655	303 27661
96	181.66116	212.14122	242.62129	273.10135	303.58141
97	181.96596	212.44602	242.92609	273.40615	303.88621
98	182,27076	212.75083	243.23089	273.71095	304.19101
99	182.57557	213.05563	243.53569	274.01575	304.49581

10 inches = .25400 metre. 11 inches = .27940 metre. 12 inches = .30480 metre.

Conversion factor: 1 metre=3.280833333 feet.

Metres	0	100	200	300	400
0		328.08333	656.16667	984.25000	1.312.33333
1	3.28083	331.36417	659.44750	987.53083	1,315.61417
2	6.56167	334.64500	662.72833	990.81167	1,318.89500
3	9.84250	337.92583	666.00917	994.09250	1,322.17583
- 4	13.12333	341.20667	669.29000	997.37333	1,325.45667
5	16.40417	344.48750	672.57083	1.000.65417	1,328.73750
6	19.68500	347.76833	675.85167	1.003.93500	1.332.01833
7	22.96583	351.04917	679.13250	1.007.21583	1,335.29917
8	26.24667	354.33000	682.41333	1,010.49667	1,338.58000
9	29.52750	357.61083	685.69417	1,013.77750	1,341.86083
10	32.80833	360.89167	688.97500	1,017.05833	1.345.14167
11	36.08917	364.17250	692.25583	1,020.33917	1,348.42250
12	39.37000	367.45333	695.53667	1,023.62000	1,351.70333
13	43.65083	370.73417	698.81750	1,026.90083	1.354.98417
14	45.93167	374.01500	702.09833	1,030.18167	1,358.26500
15	49.21250	377.29583	705.37917	1,033.46250	1.361.54583
16	52,49333	380.57667	708.66000	1.036.74333	1.364.82667
17	55.77417	383.85750	711.94083	1,040.02417	1,368.10750
18	59.05500	387.13833	715.22167	1,043.30500	1.371.38833
19	62.33583	390.41917	718.50250	1,046.58583	1,374.66917
20	65.61667	393,70000	721.78333	1.049.86667	1,377.95000
21	68.89750	396.98083	725.06417	1.053.14750	1.381.23083
22	72.17833	400.26167	728.34500	1.056.42833	1,384.51167
23	75.45917	403.54250	731.62583	1,059.70917	1,387,79250
24	78.74000	406.82333	734.90667	1,062.99000	1,391.07333
25	82.02083	410.10417	738.18750	1.066.27083	1.394.35417
26	85.30167	413.38500	741.46833	1.069.55167	1,397.63500
27	88.58250	416.66583	744.74917	1,072.83250	1,400.91583
28	91.86333	419.94667	748.03000	1,076.11333	1,404.19667
29	95.14417	423:22750	751.31083	1,079.39417	1,407.47750
30	98.42500	426.50833	754.59167	1.082.67500	1.410.75833
31	101.70583	429.78917	757.87250	1.085.95583	1.414.03917
32	104.98667	433.07000	761.15333	1,039.23667	1,417.32000
33	108.26750	436.35083	764.43417	1.092.51750	1,420,60083
34	111.54833	439.63167	767.71500	1,095.79833	1,423.88167
35	114.82917	442,91250	770.99583	1.099.07917	1.427.16250
36	118.11000	445.19333	774.27667	1.102.36000	1,430,44333
37	121.39083	449.47417	777.55750	1,105,64083	1,433.72417
38	124.67167	452.75500	780.83833	1,108,92167	1,437.00500
39	127.95250	456.03583	784.11917	1,112.20250	1,440.28583
40	131.23333	459.31567	787.40000	1.115.48333	1,443.56667
41	134.51417	462.59750	790.68083	1,118.76417	1,446.84750
42	137.79500	465.87833	793.96167	1,122,04500	1,450.12833
43	141.07583	469.15917	797.24250	1,125,32583	1,453,40917
44	144.35667	472.44000	800.52333	1,128.60667	1,456.69000
45	147.63750	475.72083	803.80417	1.131.88750	1,459,97083
46	150.91833	479.00167	807.08500	1,135.16833	1,463,25167
47	154.19917	482.28250	810.36583	1,138.44917	1,466.53250
48	157.48000	485.56333	813.64667	1,141.73000	1,469.81333
49	160.76083	488.84417	816.92750	1.145.01083	1,473.09417

Metres	0	100	- 200	300	400
50	164.04167	492,12500	820.20833	1,148.29167	1,476,37500
51	167.32250	495,40583	823.45917	1,151.57250	1,479.65583
52	170.60333	498.68667	826.77000	1,154.85333	1,482.93667
53	173.88417	501.96750	830.05083	1,158.13417	1,486.21750
54	177.16500	505.24833	833.33167	1,161.41500	1,489.49833
55	180,44583	508.52917	836.61250	1,164.69583	1,492.77917
56	183.72667	511.81000	839.89333	1,167.97667	1,496.06000
57	187.00750	515.09083	843.17417	1,171.25750	1,499.34083
58	190.28833	518.37167	846.45500	1,174.53833	1,502.62167
59	193.56917	521.65250	849.73583	1,177.81917	1,505.90250
60	196.85000	524.93333	853.01667	1,181.10000	1,509.18333
61	200.13083	528.21417	856.29750	1,184.38083	1,512.46417
62	203.41167	531.49500	859.57833	1,187.66167	1,515.74500
63	206.69250	534.77583	862.85917 868.14000	1,190.94250	1,522.30667
64	209.97333	538.05667	859.14000	1,194.22333	1,022.30001
65	213.25417	541.33750	869.42083	1,197.50417	1.525.58750
66	216.53500	544.61833	872.70167	1,200.78500	1,528.86833
67	219.81583	547.89917	875.98250	1,204.06583	1,532.14917
68	223.09667	551.18000	879.26333	1,207.34667	1,535.43000
69	226.37750	554.46083	882.54417	1,210.62750	1,538.71083
70	229.65833	557.74167	885.82500	1,213.90833	1,541.99167
71	232.93917	561.02250	889.10583	1,217.18917	1,545.27250
72	236.22000	564.30333	892.38667	1,220.47000	1,548.55333
73	239.50083	567.58417	895.66750	1,223.75083	1,551.83417
74	242.78167	570.86500	898.94833	1,227.03167	1,555.11500
75	246.06250	574.14583	902.22917	1,230.31250	1,558.39583
76	249.34333	577.42667	905.51000	1,233.59333	1,561.67667
77	252.62417	580.70750	908.79083	1,236.87417	1,564.95750
78	255.90500	583.98833	912.07167	1,240.15500	1,568.23833
79	259.18583	587.26917	915.35250	1,243.43583	1,571.51917
80	262.46667	590.55000	918.63333	1,246.71667	1,574.80000
81	265.74750	593.83083	921.91417	1,249.99750	1,578.09083
82	269.02833	597.11167	925.19500	1,253.27833	1,581.36167
83	272.30917	600.39250	928.47583	1,256.55917	1,584.64250
84	275.59000	603.67333	931.75667	1,259.84000	1,587.92333
85	278.87083	606.95417	935.03750	1,263.12083	1,591.20417
86	282.15167	610.23500	938.31833	1,286.40167	1,594.48500
87	285.43250	613.51583	941.59917	1,269.68250	1,597.76583
88	288.71333	616.79667	944.88000	1,272.96333	1,601.04667
89	291.99417	620.07750	948.16083	1,276.24417	1,604.32750
90	295.27500	623.35833	951.44167	1,279.52500	1,607.60833
91	298.55583	626.63917	954.72250	1,282.80583	1,610.88917
92	301.83667	629.92000	958.00333	1,286.08667	1,614.17000
93	305.11750 308.39833	633.20083 636.48167	961.28417 964.56500	1,289.36750	1,617.45083 1,620.73167
95	311.67917	639.76250	967.84563	1,295.92917	1,624.01250
96	314.96000	643.04333 646.32417	971.12667 974.40750	1,299.21000	1,627.29333
98	318.24083 321.52167	649.60500	977.68833	1,302,49083	1,633.85500
99	324.80250	652.88583	980.96917	1.309.05250	1,637,13583

	(Continued)						
Metres	500	600	700	800	900		
0	1,640.41667	1,968.50000	2,296.58333	2,624.66667	2,952.75000		
1	1,643.69750	1,971.78083	2,299.86417	2,627.94750	2,956.03083		
2	1,646.97833	1,975.06167	2,303.14500	2,631.22833	2,959.31167		
3	1,650.25917	1,978.34250	2,306.42583	2,634.50917	2,962.59250		
4	1,653.54000	1,981.62333	2,309.70667	2,637.79000	2,965.87333		
_							
5	1,656.82083	1,984.90417	2,312.98750	2,641.07083	2,969.15417		
6	1,660.10167	1,988.13500	2,316.26833	2,644.35167	2,972.43500		
7	1,663.38250	1,991.46533	2,319.54917	2,647.63250	2,975.71583		
8	1,666.66333	1,994.74667	2,322.83000	2,650.91333	2,978.99667		
9	1,669.94417	1,998.02750	2,326.11083	2,654.19417	2,982.27750		
10	1,673.22500	2.001.30833	2,329.39167	2,657,47500	2,985.55833		
11	1,676.50583	2,004.58917	2,332,67250	2,660.75583	2,988.83917		
12	1,679.78667	2,007.87000	2,335.95333	2,664.03667	2,992.12000		
13	1,683.06750	2,011.15083	2,339.23417	2,667.31750	2,995,40083		
14	1,686.34833	2,014.43167	2,342,51500	2,670.59833	2,998.68167		
	2,000.02000	2,012.20101	2,022.01000	2,010.03003	2,550.00201		
15	1,689.62917	2,017.71250	2,345.79583	2,673.87917	3,001.96250		
16	1,692.91000	2.020.99333	2.349.07667	2,677.16000	3,005.24333		
17	1,696.19083	2,024.27417	2,352.35750	2,680.44083	3,008.52417		
18	1,699,47167	2,027.55500	2,355.63833	2,683.72167	3.011.80500		
19	1,702.75250	2,030.83583	2,358.91917	2,687.00250	3,015.08583		
20	1,706.03333	0 004 11007	0 200 00000	2,690,28333	3.018.36667		
21	1,709.31417	2,034.11667	2,362.20000		3,021.64750		
		2,037.39750	2,365.48083	2,693.56417			
22	1,712.59500	2,040.67833	2,368.76167	2,696.84500	3,024.92833		
24	1,715.87583 1,719.15667	2,043.95917 2,047.24000	2,372.04250 2,375.32333	2,700.12583 2,703.40667	3,028.20917 3,031.49000		
					2000		
25	1,722.43750	2,050.52083	2,378.60417	2,706.68750	3,034.77083		
26	1,725.71833	2,053.80167	2,381.88500	2,709.96833	3,038.05167		
27	1,728.99917	2,057.08250	2,385.16583	2,713.24917	3,041.33250		
28	1,732.28000	2,060.36333	2,388.44667	2,716.53000	3,044.61333		
29	1,735.56083	2,063.64417	2,391.72750	2,719.81083	3,047.89417		
30	1.738.84167	2,066.92500	2,395.00833	2,723,09167	3,051,17500		
31	1,742.12250	2,070.20583	2,398.28917	2,726.37250	3,054.45583		
32	1,745.40333	2,073.48667	2,401.57000	2,729.65333	3,057.73667		
33	1.748.68417	2,076.76750	2,404.85083	2,732.93417	3,061.01750		
34	1,751.96500	2,080.04833	2,408.13167	2,736.21500	3,064.29833		
			,	Marie Contract	Maria and a second		
35	1,755.24583	2,083.32917	2,411.41250	2,739.49583	3,067.57917		
36	1,758.52667	2,086.61000	2,414.69333	2,742.77667	3,070.86000		
37	1,761.80750	2,089.89083	2,417.97417	2,746.05750	3,074.14083		
38	1,765.08833	2,093.17167	2,421.25500	2,749.33833	3,077.42167		
39	1,768.36917	2,096.45250	2,424.53583	2,752.61917	3,080.70250		
40	1,771.65000	2,099.73333	2,427.81667	2,755.90000	3,083.98333		
41	1,774.93083	2,103.01417	2,431.09750	2,759.18083	3,087.26417		
42	1,778.21167	2,106.29500	2,434.37833	2,762.46167	3,090.54500		
43	1,781.49250	2,109.57583	2,437.65917	2,765.74250	3,093.82583		
44	1,784.77333	2,112.85667	2,440.94000	2,769.02333	3,097.10667		
45	1,788.05417	2,116.13750	2,444.22083	2,772.30417	3,100.38750		
46	1,791.33500	2,119.41833	2,447.50167	2,775.58500	3,103.66833		
47	1,794.61583	2,122.69917	2,450.78250	2,778.86583	3,106.94917		
48	1,797.89667	2,125.98000	2,454.06333	2,782.14667	3,110.23000		
49	1,801.17750	2,129.26083	2,457.34417	2,785.42750	3,113.51083		

Metres	500	600	700	800	900
50	1,804.45833	2,132.54167	2,460.62500	2,788.70833	3,116.79167
51	1,807.73917	2,135.82250	2,463.90583	2,791.98917	3,120.07250
					3.123.35333
52	1,811.02000	2,139.10333	2,467.18667	2,795.27000	
53	1,814.30083	2,142.38417	2,470.46750	2,798.55083	3,126.63417
54	1,817.58167	2,145.66500	2,473.74833	2,301.83167	3,129.91500
55	1,820.86250	2,148.94583	2,477.02917	2,805.11250	3,133.19583
56	1,824.14333	2,152.22667	2,480.31000	2,808.39333	3,136.47667
57	1,827.42417	2,155.50750	2,483.59083	2,811.67417	3,139.75750
58	1,830.70500	2,158.78833	2,486.87167	2,814.95500	3,143.03833
59	1,833.98583	2,162.06917	2,490.15250	2,818.23583	3,146.31917
60	1,837.26667	2,165.35000	2,493.43333	2,821.51667	3,149.60000
61	1.840.54750	2.168.63083	2,496.71417	2.824.79750	3,152,88083
62	1.843.82833	2,171,91167	2,499.99500	2,828.07833	3,156.16167
63	1,847.10917	2,175.19250	2,503.27583	2,831.35917	3,159,44250
64		2,178.47333	2,506.55667	2,834.64000	3,162.72333
04	1,850.39000	2,110.21333	2,000.00001	2,032.02000	3,102.12330
65	1,853.67083	2,181.75417	2,509.83750	2,837.92083	3,166.00417
66	1.856.95167	2,185.03500	2,513.11833	2,841.20167	3,169.28500
67	1,860.23250	2,188.31583	2,516.39917	2,844.48250	3.172.56583
68	1,863.51333	2,191.59667	2,519.68000	2,847.76333	3.175.8466
69	1,866.79417	2,194.87750	2,522.96083	2,851.04417	3,179.1275
02	1,000.13111	2,151.01100	2,022.50000	2,002.0222	0,210.2210.
70	1,870.07500	2,198.15833	2,526.24167	2,854.32500	3,182.4083
71	1,873.35583	2,201.43917	2,529.52250	2,857.60583	3,185.6891
72	1,876.63667	2,204.72000	2,532.80333	2.860.88667	3.188.97000
73	1,879.91750	2,208.00083	2,536.08417	2,864.16750	3.192.25083
74	1,883.19833	2,211.28167	2,539.36500	2,867.44833	3,195.5316
75	1,886.47917	2,214.56250	2,542.64583	2,870,72917	3,198.8125
76	1,889.76000	2,217.84333	2,545,92667	2,874.01000	3,202.0933
77	1,893.04083	2,221.12417	2,549.20750	2.877.29083	3,205,3741
78		2,224.40500	2,552.48833	2,880.57167	3,208.6550
	1,896.32167			2,883.85250	
79	1,899.60250	2,227.68583	2,555.76917	2,003.00200	3,211.9358
80	1,902.88333	2,230.96667	2,559.05000	2,887.13333	3,215.21667
81	1,906.16417	2,234.24750	2,562.33083	2,890.41417	3,218.4975
82	1,909.44500	2,237.52833	2,565.61167	2,893.69500	3,221.7783
83	1,912.72583	2,240.80917	2,568.89250	2,896.97583	3,225.0591
84	1,916.00667	2,244.09000	2,572.17333	2,900.25667	3,228.3400
85	1,919.28750	2,247.37083	2.575.45417	2.903.53750	3.231.6208
86	1,922,56833	2,250.65167	2,578.73500	2,906.81833	3.234.9016
87	1.925.84917	2,253.93250	2,582.01583	2,910.09917	3,238.1825
88	1,929.13000	2,257.21333	2,585.29667	2,913.38000	3,241.4633
89	1,932.41083	2,260.49417	2,588.57750	2,916.66083	3,244.7441
	4 005 00405	0.000 77500	0 504 05000	0.010.04107	2 040 0070
90	1,935.69167	2,263.77500 2,267.05583	2,591.85833 2,595.13917	2,919.94167	3,248.0250
	1,942,25333	2,270.33667	2,598.42000	2,926.50333	3,254.5866
92			2,601.70083	2,929.78417	3,257.8675
93	1,945.53417	2,273.61750 2,276.89833	2,604.98167	2,933.06500	3,261.1483
	-,-				
95	1,952.09583	2,280.17917	2,608.26250	2,936.34583	3,264.4291
96	1,955.37667	2,283.46000	2,611.54333	2,939.62667	3,267.7100
97	1,958.65750	2,286.74083	2,614.82417	2,942.90750	3,270.9908
	1,961.93833	2,290.02167	2,618 10500	2,946.18833	3,274.2716
98	1,965.21917	2,293.30250	2,621.38583	2,949.46917	3,277.5525

Conversion Factor: 1 avoirdupois pound=0.4535924277 kilogram.

Pounds	0	100	200	800	400
0 1 2 3	.90718 1.36078	45.35924 45.81284 45.26643 46.72002	90.71849 91.17208 91.62567 92.07926	136.07773 136.53132 136.98491 137.43851	181,43697 181,89056 182,34416 182,79775
4	1.81437	47.17361	92.53286	137.89210	183.25134
5	2.26796	47.62720	92.98645	138.34569	183.70493
6	2.72155	48.08080	93.44004	138.79928	184.15853
7	3.17515	48.53439	93.89363	139.26288	184.61212
8	3.62874	48.98798	94.34722	139.70647	185.06571
9 10 11 12 13	4.08233 4.53592 4.98952 5.44311 5.89670 6.35029	49.44157 49.89517 50.34876 50.80235 51.25594	94.80082 95.25441 95.70800 96.16159 96.61519	140.16006 140.61365 141.06725 141.52084 141.97443 142.42802	185.51930 185.97290 186.42649 186.83008 187.33367
15 16 17 18	6.80389 7.25748 7.71107 8.16466 8.61826	51.70954 52.16313 52.61672 53.07031 53.52391 53.97750	97.06878 97.52237 97.97596 98.42956 98.88315 99.33674	142.42803 142.88161 143.33521 143.78880 144.24239 144.69598	187.78727 188.24086 188.69445 189.14804 189.60163 190.05523
20	9.07185	54.43109	99.79033	145.14958	190.50882
21	9.52544	54.88468	100.24393	145.60317	190.96241
22	9.97903	55.33828	100.69752	146.05676	191.41600
23	10.43263	55.79187	101.15111	146.51035	191.86960
24	10.88622	56.24546	101.60470	146.96395	192.32319
25	11.33981	56.69905	102.05830	147.41754	192.77678
26	11.79340	57.15265	102.51189	147.87113	193.23037
27	12.24700	57.60624	102.96548	148.32472	193.68397
28	12.70059	58.05983	103.41907	148.77832	194.13756
29	13.15418	58.51342	103.87267	149.23191	194.59115
30	13.60777	58.96702	104.32626	149.68550	195.04474
31	14.06137	59.42061	104.77985	150.13909	195.49834
32	14.51496	59.87420	105.23344	150.59269	195.95193
33	14.96855	60.32779	105.68704	151.04628	196.40552
34	15.42214	60.78139	106.14063	151.49987	196.85911
35	15.87573	61.23498	106.59422	151.95346	197.31271
36	16.32933	61.68857	107.04781	152.40706	197.76630
37	16.78292	62.14216	107.50141	152.86065	198.21989
38	17.23651	62.59576	107.95500	153.31424	198.67348
39	17.69010	63.04935	108.40859	153.76783	199.12708
40	18.14370	63.50294	108.86218	154.22143	199.58067
41	18.59729	63.95653	109.31578	154.67502	200.03426
42	19.05088	64.41012	109.76937	155.12861	200.48785
43	19.50447	64.86372	110.22296	155.58220	200.94145
44	19.95807	65.31731	110.67655	156.03580	201.39504
45 46 47 48	20.41166 20.86525 21.31884 21.77244 22.22603	65.77090 66.22449 66.67809 67.13168 67.58527	111.13014 111.58374 112.03733 112.49092 112.94451	156.48939 156.94298 157.39657 157.85016 158.30376	201.84863 202.30222 202.75682 203.20941 203.66300

1 oz.=.028350 kg. 2 oz.=.056699 kg. 3 oz.=.085049 kg. 4 oz.=.113398 kg.

(Continued)

Pounds	0	100	200	800	400
50 51	22.67962 23.13321	68.02886 68.49246	113.39811 113.85170	158.75735 159.21094	204.11659 204.57018
52	23.58681	68.94605	114.30529	159.66453	205.02378
53	24.04040	69.39964	114.75888	160.11813	205.47737
54	24.49399	69.85323	115.21248	160.57172	205.93096
55	24.94758	70.30683	115.66607	161.02531	206.38455
56	25.40118 25.85477	70.76042	116.11966 116.57325	161.47890 161.93250	206.83815 207.29174
58	26.30836	71.66760	117.02685	162.38609	207.74533
59	26.76195	72.12120	117.48044	162.83968	208.19892
60	27.21555	72.57479	117.93403	163.29327	208.65252
61	27.66914 28.12273	73.02838 73.48197	118.38762 118.84122	163.74687 164.20046	209.10611 209.55970
63	28.57632	73.93557	119.29481	164.65405	210.01329
64	29.02992	74.38916	119.74840	165.10764	210.46689
65	29.48351	74.84275	120.20199	165.56124	210.92048
66	29.93710	75.29634	120.65559	166.01483	211.37407
67	30.39069	75.74994	121.10918 121.56277	166.46842 166.92201	211.82766 212.28126
69	31.29788	76.20353 76.65712	122.01636	167.37561	212.73485
70	31.75147	77.11071	122,46996	167.82920	213.18844
71	82.20506	77.56431	122.92355	168.28279	213.64203
72	32.65865	78.01790	123.37714	168.73638	214.09563
73	33.11225	78.47149 78.92509	123.83073 124.28433	169.18998 169.64357	214.54922 215.00261
75	33.56584 34.01943	79.37867	124.73792	170.09716	215.45640
76	34.47302	79.83227	125.19151	170.55075	215.91000
77	34.92662	80.28586	125.64510	171.00435	216.36359
78	35.38021	80.73945	126.09869	171.45794	216.81718
79	35.83380	81.19304	126.55229	171.91153	217.27077
80	36.28739 36.74099	81.64664 82.10023	127.00588 127.45947	172.36512 172.81871	217.72437 218.17796
82	37.19458	82.55382	127.91306	173.27231	218.63155
83	37.64817	83.00741	128.36666	173.72590	219.08514
84	38.10176	83.46101	128.82025	174.17949	219.53874
85	38.55536	83.91460	129.27384	174.63308	219.99233
86 87	39.00895	84.36819	129.72743	175.08668	220.44592
88	39.46254 39.91613	84.82178 85.27538	130.18103 130.63462	175.54027 175.99386	220.89951 221.35310
89	40.36973	85.72897	131.08821	176.44745	221.80670
90	40.82332	86.18256	131.54180	176.90105	222.26029
91	41.27691	86.63615	131.99540	177.35464	222.71388
92	41.73050	87.08975	132.44899	177.80823	223.16747
94	42.18410 42.63769	87.54334 87.99693	132.90258 133.35617	178.26182 178.71542	223.62107 224.07466
95	43.09138	88.45052	133.80977	179.16901	224.52825
96	43.54487	88.90412	134.26336	179.62260	224.98184
97	43.99847	89.35771	134.71695	180.07619	225.43544
98	44.45206	89.81130	135.17054	180.52979	225.88903
שע	44.90565	90.26489	135.62414	180.98338	226.34262

5 oz.=.141748 kg. 6 oz.=.170097 kg. 7 oz.=.198447 kg. 8 oz.=.226796 kg.

(Continued)

	(Continued)							
Pounds	500	600	700	800	900			
0 1 2 3	226.79621 227.24981 227.70340 228.15699 228.61056	272.15546 272.60905 273.06264 273.51623 273.96983	317.51470 317.96829 318.42183 318.87548 319.32907	362.87394 363.32753 363.78113 364.23472 364.68831	408.23318 408.68678 409.14037 409.59396 410.04755			
5 6 7 8	223.06418 229.51777 229.97136 230.42495 230.87855	274.42342 274.87701 275.33060 275.78420 276.23779	319.78266 320.23625 320.68985 321.14344 321.69703	365.14190 365.59550 366.04909 366.50268 366.95627	410.50115 410.95474 411.40833 411.86192 412.31552			
10 11 12 13 14	231.33214 231.78573 232.23932 232.69292 233.14651	276.69138 277.14497 277.59857 278.05216 278.50575	322.05062 322.50422 322.95781 323.41140 323.86499	367.40987 367.86346 368.31705 368.77064 369.22424	412.76911 413.22270 413.67629 414.12989 414.58348			
15 16 17 18 19	233.60010 234.05369 234.50729 234.96088 235.41447	278.95934 279.41294 279.86653 280.32012 280.77371	324.31859 324.77218 325.22577 325.67936 326.13296	369.67783 370.13142 370.58501 371.03861 371.49220	415.03707 415.49066 415.94426 416.39765 416.85144			
20 21 22 23 24 25	235.86806 236.32165 236.77525 237.22884 237.68243 238.13502	281.22731 281.68090 282.13449 282.58808 283.04167 283.49527	326.58655 327.04014 327.49373 327.94733 328.40092 328.85451	371.94579 372.39938 372.85298 373.30657 373.76016 374.21375	417.30503 417.75863 418.21222 418.66581 419.11940			
26 27 28 29	238.58962 239.04321 239.49680 239.95039 240.40399	283.94886 284.40245 284.85604 285.30964 285.76323	329.30810 329.76169 330.21529 330.66888 331.12247	374.66735 375.12094 375.57453 376.02812 376.48171	419.57300 420.02659 420.48018 420.93377 421.38737 421.84096			
31 32 33 34 35	240.85758 241.31117 241.76476 242.21836 242.67195	286.21682 286.67041 287.12401 287.57760 268.03119	331.57606 332.02966 332.48325 332.93684 333.39043	376.93531 377.38890 377.84249 378.29608 378.74968	422.29455 422.74814 423.20174 423.65533 424.10892			
36 37 38 39 40	243.12554 243.57913 244.03273 244.48632 244.93991	288.48478 288.93838 289.39197 289.84556 290.29915	333.84403 334.29762 334.75121 235.20480 335.65840	379.20327 379.65686 380.11045 380.56405 381.01764	424.56251 425.01610 425.46970 425.92329 426.37688			
41 42 43 44	245.39350 245.84710 246.30069 246.75428 247.20787	290.75275 291.20634 291.65993 292.11352 292.56712	336.11199 336.56558 337.01917 337.47277 337.92636	381.47123 381.92482 382.37842 382.83201 383.28560	426.83047 427.28407 427.73766 428.19125 428.64484			
46 47 48 49	247.66147 248.11506 248.56865 249.02224	293.02071 293.47430 293.92789 294.38149	338.37995 338.83354 339.28714 339.74073	383.73919 384.19279 384.64638 385.09997	429.09844 429.55203 430.00562 430.45921			

9 oz. = .255146 kg. 10 oz. = .283495 kg. 11 oz. = .311845 kg. 12 oz. = .340194 kg.

(Continued)

Pounds	500	600	700	800	900
50	249.47584	294.83508	340.19432	385.55356	430.91281
51	249.92943	295.28867	340.64791	386.00716	431.36640
52	250.38302	295.74226	341.10151	386.46075	431.81999
53	250.83661	296.19586	341.55510	386.91434	432.27358
54	251.29020	296.64945	342.00869	387.36793	432.72718
55	251.74380	297.10304	342.46228	387.82153	433.18077
56	252.19739	297.55663	342.91588	388.27512	433.63436
57	252.65098	298.01022	343.36947	388.72871	434.08795
58 59	253.10457 253.55817	298.46382 298.91741	343.82305 344.27665	389.18230 389.63590	434.54155
60	254.01176	299.37100	344.73025	390.08949	435.44873
61	254.46535	299.82459	345.18384	390.54308	435,90232
62	254.91894	300.27819	345.63743	390.99667	436.35592
63	255.37254	300.73178	346.09102	391.45027	436.80951
64	255.82613	301.18537	346.54461	391.90386	437.26310
65	256.27972	301.63896	346.99821	392.35745	437.71669
66	256.73331	302.09256	347.45180	392.81104	438.17029
67	257.18691	302.54615	347.90539	393.26463	438.62388
68	257.64050 258.09409	302.99974	348.35898 348.81259	393.71823 394.17182	439.07747
70	258.54768 259.00128	303.90693 304.36052	349.26617 349.71976	394.62541	439.98465
72	259.45487	304.81411	350.17335	395.53260	440.89184
73	259.90846	305.26770	350.62695	395.98619	441.34543
74	260.36205	305.72130	351.08054	396.43978	441.79902
75	260.81565	306.17489	351.53413	396.89337	442.25262
76	261.26924	306.62848	351.98772	397.34697	442.70621
77	261.72283	307.08207	352.44132	397.80056	443.15980
78	262.17642	307.53567	352.89491	398.25415	443.61339
79	262.63002	307.98926	353.34850	398.70774	444.06699
80	263.08361	308.44285	353.80203	399.16134	444.52058
81	263.53720	308.89644	354.25569	399.61493	444.97417
82	263.99079 264.44439	309.35004	354.70928 355.16287	400.06852 400.52211	445.42776 445.88136
84	264.89798	310.25722	355.61646	400.97571	446.33495
85	265.35157	310.71081	356.07006	401.42930	446.78854
86	265.80516	311.16441	356.52365	401.88289	447.24213
87	266.25876	311.61800	356.97724	402.33648	447.69573
88	266.71235	312.07159	357.43083	402,79008	448.14932
89	267.16594	312.52518	357.88443	403.24367	448.60291
90	267.61953	312.97878	358.33802	403.69726	449.05650
91	268.07312	313.43237	358.79161	404.15085	449.51010
92	268.52672	313.88696	359.24520	404.60445	449.96369
93	268.98031 269.43390	314.33955 314.79314	359.69880 360.15239	405.05804 405.51163	450.41728 450.87087
95	269.43390	315.24674	360.15239	405.96522	451.32447
96	270.34109	315.24674	361.05957	405.96522	451.32447
97	270.79468	316.15392	361.51316	406.87241	452.23165
98	271.24827	316.60751	361.96676	407.32600	452.68524
99	271.70186	317.06111	362,42035	407.77959	453.13884

13oz.=.368544 kg. 14 oz.=.396893 kg. 15 oz.=.425243 kg. 16 oz.=.453593 kg.

Conversion factor: 1 kilogram = 2.204622341 avoirdupois pounds.

Kilos	0	100	200	300	400
O		220.4622	440.9245	661.3867	881.8489
1	2.2046	222.6669	443.1291	663.5913	884.0536
2	4.4092	224.8715	445.3337	665.7959	886.2582
3	6.6139	227.0761	447.5383	668,0006	888.4628
4	8.8185	229.2807	. 449.7430	670.2052	890.6674
5	11.0231	231.4853	451.9476	672.4098	892.8720
6	13.2277	233.6900	454.1522	674.6144	895.0767
7	15.4324	235.8946	456.3568	676.8191	897.2813
8	17.6370	238.0992	458.5614	679.0237	899.4859
9	19.8416	240.3038	460.7661	681.2283	901.6905
10	22.0462	242.5085	462.9707	683.4329	903.8952
11	24.2508	244.7131	465.1753	665.6375	906.0998
12	26.4555	246.9177	467.3799	687.8422	908.3044
13	28.6601	249.1223	469.5846	690.0468	910.5090
14	30.8647	251.3269	471.7892	692.2514	912.7136
15	33.0693	253.5316	473.9938	694.4560	914.9183
16	35.2740	255.7362	476.1984	696.6607	917.1229
17	37.4786	257.9408	478.4030	698.8653	919.3275
18	39.6832	260.1454	480.6077	701.0699	921.5321
19	41.8878	262.3501	482.8123	703.2745	923.7368
20	44.0924	264.5547	485.0169	705.4791	925.9414
21	46.2971	266.7593	487.2215	707.6838	928.1460
22	48.5017	268.9639	489.4262	709.8884	930:3506
23	50.7063	271.1685	491.6308	712.0930	932.5553
24	52.9109	273.3732	493.8354	714.2976	934.7599
25	55.1156	275.5778	496.0400	716.5023	936.9645
26	57.3202	277.7824	498.2446	718.7069	939.1691
27	59.5248	279.9870	500.4493	720.9115	941.3737
28	61.7294	282.1917	502.6539	723.1161	943.5784
29	63.9340	284.3963	504.8585	725.3208	945.7830
30	66.1387	286.6009	507.0631	727.5254	947.9876
31	68.3433	288.8055	509.2678	729.7300	950.1922
32	70.5479	291.0101	511.4724	731.9346	952.3969
33	72.7525	293.2148	513.6770	734.1392	954.6015
34	74.9572	295.4194	515.8816	736.3439	956.8061
35	77.1618	297.6240	518.0863	738.5485	959.0107
36	79.3664	299.8286	520.2909	740.7531	961.2153
37	81.5710	302.0333	522.4955	742.9577	963.4200
38	83.7756	304.2379	524.7001	745.1624	965.6246
39	85.9803	306.4425	526.9047	747.3670	967.8292
40	88.1849	308.6471	529.1094	749.5716	970.0338
41	90.3895	310.8518	531.3140	751.7762	972.2386
42	92.5941	313.0564	533.5186	753.9808	974.4431
43	94.7988	315.2610	585.7232	756.1855	. 976.6477
44	97.0034	317.4656	537.9279	758.3901	978.8523
45	99.2080	319.6702	540.1325	760.5947	981.0569
46	101.4126	321.8749	542.3371	762.7993	983.2616
47	103.6173	324.0795	544.5417	765.0040	985.4662
48	105.8219	326.2841	546.7463	767.2086	987,6708

Kilos	0	100	200	300	400
50	110.2311	330.6934	551.1556	771.6178	992,080
51	112.4357	332.8980	553.3602	773.8224	994.284
51	114.6404	335.1026	555.5648	776.0271	996.4893
53	116.8450	337.3072	557.7695	778.2317	998.6939
	119.0496		559,9741	780.4363	
54	119.0296	339.5118	999.9141	100.2303	1,000.898
55	121.2542	341.7165	562.1787	782.6409	1,003.103
56	123.4589	343.9211	564.3833	784.8456	1,005.307
57	125.6635	346.1257	566.5879	787.0502	1,007.512
58	127.8681	848.3303	568.7926	789.2548	1,009.717
59	130.0727	850.5350	570.9972	791.4594	1,011.921
60	133,3773	352,7396	573.2018	793.5640	1,014.126
61	134.4820	354.9442	575.4064	795.8687	1.016.330
62	136.6866	357.1488	577.6111	798.0733	1,018.535
					1,020.740
63	138.8912	359.3534	579.8157	800.2779	
64	141.0958	361.5581	582.0203	802.4825	1,022.944
65	143.3005	363.7627	584.2249	804.6872	1,025.149
66	145.5051	265.9673	586.4295	806.8918	1,027.354
67	147.7097	368.1719	588.6342	809.0964	1,029.558
68	149.9143	370.3766	590.8388	811.3010	1.031.763
69	152.1189	371.5812	593.0434	813.5056	1,033.967
70	154.3236	374.7858	595,2480	815,7103	1.036.172
71	156.5282	376.9904	597.4527	817.9149	1,038.377
- 72	158.7328	379.1950	599.6573	820.1195	1.040.581
73	160.9374	381.3997	601.8619	822.3241	1,042.786
74	163.1421	383.6043	604.0665	824.5288	1,044.991
75	165.3467	385.8089	606.2711	826.7334	1,047.195
76	167.5513	388.0135	608.4758	828.9380	1,049.400
77	169.7559	390.2182	610.6804	831.1426	1.051.604
78	171.9605	392.4328	612.8850	833,3472	1,053.809
79	174.1652	394.6274	615.0896	835.5519	1,056.014
80	176.3698	396.8320	617.2943	837.7565	1.058.218
81	178.5744	399.0366	619.4989	839.9611	1,060.423
82	180.7790	401.2413	621.7035	842.1657	1,062.628
83	182.9837	403.4459	623.9081	844.3704	1,064.832
84	185.1883	405.6505	626.1127	846.5750	1,067.037
85	187.3929	407.8551	628.3174	848.7796	1,069.241
86	189.5975	410.0598	630.5220	850.9842	1,071.446
87	191.8021	412.2644	632.7266	853.1888	1,073.651
88	194.0068	414.4690	634.9312	855,3935	1.075.855
89	196.2114	416.6736	637.1359	857.5981	1,078.060
90	198.4160	418.8782	639,3405	859.8027	1,080.264
91	200,6206	421.0829	641.5451	862.0073	1.082.469
92	202.8253	423.2875	643.7497	864.2120	1,084.674
					1,086.878
93	205.0299	425.4921 427.6967	645.9543 648.1590	868.4166 868.6212	1,089.083
32	201,2340	1000.142	020.1030	000.0212	2,003.003
95	209.4391	429.9014	650.3636	870.8258	1,091.288
96	211.6437	432.1060	652.5682	873.0304	1,093.492
97	213.8484	434.3106	654.7728	875.2351	1,095.697
98	216.0530	436.5152	656.9775	877.4397	1,097.901
99	218.2576	438,7198	659.1821	879.6443	1.100.106

(Continued)					
Kilos	500	600	700	800	900
0	1.102.3112	1.322.7734	1,543,2356	1,763.6979	1.984.1601
1	1,104.5158	1,324.9780	1,545.4403	1,765.9025	1,986.3647
2	1,106.7204	1,327.1826	1,547.6449	1,768.1071	1,988.5694
3	1,108.9250	1,329.3873	1,549.8495	1,770.3117	1,990.7740
, 4	1,111.1297	1,331.5919	1,552.0541	1,172.5164	1,992.9786
1 5	1,113.3343	1,333,7965	1.554.2588	1,774,7210	1.995.1832
: 6	1,115.5389	1,336.0011	1,556.4634	1,776.9256	1,997.3878
7	1,117.7435	1,338.2058	1,558.6680	1,779.1302	1,999.5925
8	1,119.9481	1,340.4104	1,560.8726	1,781.3349	2,001.7971
9	1,122.1528	1,342.6150	1,563.0772	1,783.5395	2,004.0017
10	1,124.3574	1,344.8196	1,565.2819	1,785.7441	2,006.2063
11	1,126.5620	1,347.0243	1,567.4865	1,787.9487	2,008.4110
12	1,128.7666	1,349.2289	1,569.6911	1,790.1533	2,010.6156
13	1,130.9713	1,351.4335	1,571.8957	1,792.3580	2,012.8202
14	1,133.1759	1,353.6381	1,574.1004	1,794.5626	2,015.0248
15	1,135.3805	1,355.8427	1,576.3050	1,796.7672	2,017.2294
16	1,137.5851	1,358.0474	1,578.5096	1,798.9718	2,019.4341
17	1,139.7898	1,360.2520	1,580.7142	1,801.1765	2,021.6387
18	1,141.9944	1,362.4566	1,582.9188	1,803.3811	2,023.8433
19	1,144.1990	1,364.6612	1,585.1235	1,805.5857	2,026.0479
20	1,146.4036	1,366.8659	1,587.3281	1,807.7903	2,028.2526
13.1	1,148.6082	1,369.0705	1,589.5327	1,809.9949	2,030.4572
22	1,150.8129	1,371.2751	1,591.7373	1,812.1996	2,032.6618
23	1,153.0175	1,373.4797	1,593.9420	1,814.4042	2,034.8664
24	1,155.2221	1,375.6843	1,596.1466	1,816.6088	2,037.0710
25	1,157.4267	1,377.8890	1,598.3512	1,818.8134	2,039.2757
26	1,159.6314	1,380.0936	1,600.5558	1,821.0181	2,041.4803
27	1,161.8360	1,382.2982	1,602.7604	1,823.2227	2,043.6849
28 29	1,164.0406 1,166.2452	1,384.5028	1,604.9651	1,825.4273	2,045.8895 2,048.0942
23	1,100.2402	1,380.1010	1,007.1031	1,021.0313	2,010.0312
30	1,168.4498	1,388.9121	1,609.3743	1,829.8365	2,050.2988
31	1,170.6545	1,391.1167	1,611.5789	1,832.0412	2,052.5034
39	1,172.8591	1,393.3213	1,613.7836	1,834.2458	2,054.7080
33	1,175.0637 1,177.2683	1,395.5259 1,397.7306	1,615.9882 1,618.1928	1,836.4504 1,838.6550	2,056.9126 2,059.1173
35	1,179.4730	1,399.9352	1,620.3974	1,840.8597	2,061.3219
36	1,181.6776	1,402.1398	1,622.6020	1,843.0643	2,063.5265
37	1,183.8822	1,404.3444	1,624.8067	1,845.2689	2,065.7311
39	1,186.0868	1,406.5491	1,627.0113	1,847.4735 1,849.6781	2,067.9358 2,070.1404
20	2,100.2314	1,200.1001	1,023.2103	1,013.0101	
40	1,190.4961	1,410.9583	1,631.4205	1,851.8828	2,072.3450
41	1,192.7007	1,413.1629	1,633.6252	1,854.0874	2,074.5496
43	1,194.9053	1,415.3675 1,417.5722	1,635.8298	1,856.2920	2,076.7542 2,078.9589
44	1,199.3146	1,419.7768	1,640.2390	1,860.7013	2,081.1635
46	1,201.5192	1,421.9814	1,642.4436	1,862.9059 1,865.1105	2,083.3681
47	1,205.9284	1,426.3907	1,646.8529	1,867.3151	2.087.7774
4.8	1,208.1330	1,428.5953	1.649.0575	1.869.5197	2,089.9820
49	1,210.3377	1,430.7999	1,651.2621	1,871.7244	2,092.1866

(Continued)					
Kilos	500	600	700	800	900
50	1,212.5423	1.433.0045	1.653.4668	1,873,9290	2,094,3912
51	1,214,7469	1,435,2091	1,655,6714	1.876.1336	2,096.5958
52	1,216.9515	1,437.4138	1,657.8760	1,878.3382	2,098.8005
53	1,219.1562	1,439.6184	1,660.0806	1,880.5429	2,101.0051
54	1,221.3608	1,441.8230	1,662.2852	1,882.7475	2,103.2097
55	1,223.5654	1,444.0276	1,664.4899	1.884.9521	2,105,4143
56	1,225.7700	1,446.2323	1,666.6945	1,887.1567	2,107.6190
57	1,227.9746	1,448.4369	1,668.8991	1,889.3613	2,109.8236
58	1,230.1793	1,450.6415	1,671.1037	1,891.5660	2,112.0282
59	1,232.3839	1,452.8461	1,673.3084	1,893.7706	2,114.2328
60	1,234.5885	1,455.0507	1,675.5130	1,895.9752	2,116.4374
61	1,236.7931	1,457.2554	1,677.7176	1,898.1798	2,118.6421
62	1,238.9978	1,459.4600	1,679.9222	1,900.3845	2,120.8467
68	1,241.2024	1,461.6646	1,682.1268	1,902.5891	2,123.0513
64	1,243.4070	1,463.8692	1,684.3315	1,904.7937	2,125.2559
65	1,245.6116	1,466.0739	1,686.5361	1,906.9983	2,127.4606
66	1,247.8162	1,468.2785	1,688.7407	1,909.2029	2,129.6652
67	1,250.0209	1,470.4831	1,690.9453	1,911.4076	2,131.8698
68	1,252.2255	1,472.6877 1,474.8923	1,693.1500 1,695.3546	1,913.6122 1,915.8168	2,134.0744 2,136.2790
43	1,203.2001	1,212.0520	1,000.3010	1,310.0100	2,130.2130
70	1,256.6347	1,477.0970	1,697.5592	1,918.0214	2,138.4837
71	1,258.8394	1,479.3016	1,699.7638	1,920.2261	2,140.6883
72	1,261.0440	1,481.5062	1,701.9684	1,922.4307	2,142.8929
73	1,263.2486	1,483.7108	1,704.1731	1,924.6353	2,145.0975
72	1,265.4532	1,485.9155	1,706.3777	1,926.8399	2,147.3022
75	1,267.6578	1,488.1201	1,708.5823	1,929.0445	2,149.5068
76	1,269.8625	1,490.3247	1,710.7869	1,931.2492	2,151.7114
77	1,272.0671	1,492.5293	1,712.9916	1,933.4538	2,153.9160
78 79	1,274.2717	1,494.7339	1,715.1962 1,717.4008	1,935.6584 1,937.8630	2,156.1206 2,158,3253
13	1,210.2103	1,230.3300	1,111.2000	1,331.0030	A,100.3203
80	1,278.6810	1,499.1432	1,719.6054	1,940.0677	2,160.5299
81	1,280.8856	1,501.3478	1,721.8100	1,942.2723	2,162.7345
82 83	1,283.0902	1,503.5524	1,724.0147 1,726.2193	1,944.4769	2,164.9391
84	1,285.2948	1,505.7571 1,507.9617	1,728.4239	1,946.6815 1,948.8861	2,167.1438 2,169,3484
	1,201.1002	2,001.0021	2,120.2200	2,020.0001	
85	1,289.7041	1,510.1663	1,730.6285	1,951.0908	2,171.5530
86	1,291.9087	1,512.3709	1,732.8332	1,953.2954	2,173.7576
87	1,294.1133	1,514.5755	1,735.0378	1,955.5000	2,175.9623
88 89	1,296.3179 1,298.5226	1,516.7802 1,518.9848	1,737.2424	1,957.7046	2,178.1669 2,180.3715
	1,200.0220	1,010.3010	1,133.2210	1,505.5050	2,100.0110
90	1,300.7272	1,521.1894	1,741.6516	1,962.1139	2,182.5761
91	1,302.9318	1,523.3940	1,743.8563	1,964.3185	2,184.7807
92	1,305.1364 1,307.3410	1,525.5987	1,746.0609 1,748.2655	1,966.5231 1,968.7278	2,186.9854 2,189.1900
94	1,309.5457	1,530.0079	1,750.4701	1,970.9324	2,191.3946
95 96	1,311.7503	1,532.2125	1,752.6748	1,973.1370	2,193.5992
97	1,313.9549 1,316.1595	1,534.4171 1,536.6218	1,754.8794 1,757.0840	1,975.3416	2,195.8039 2,198.0085
98	1,318.3642	1,538.8264	1,759.2886	1.979.7509	2,200.2131
99	1,320.5688	1,541.0310	1,761.4933	1,981.9555	2,202.4177
	,	, _,	_,	_,	,

### COMPARISON OF THE VARIOUS TONS AND POUNDS IN USE IN THE UNITED STATES.

(See Pages 562, 563, 582, 586)

		(occ z ages	002, 000, 002,	000)	
Troy Pounds	Avoirdupois Pounds	Kilograms	Short Tons	Long Tons	Metric Tons
1 2 3 4	1.645 71 2.468 57 3.291 43	.373 24 .746 48 1.119 73 1.492 97	.000 411 43 .000 822 86 .001 234 29 .001 645 71	.000 367 35 .000 734 69 .001 102 04 .001 469 39	.000 373 24 .000 746 48 .001 119 73 .001 492 97
5678	4.114 29	1.866 21	.002 057 14	.001 836 73	.001 866 21
	4.937 14	2.239 45	.002 468 57	.002 204 08	.002 239 45
	5.760 00	2.612 69	.602 880 00	.002 571 43	.002 612 69
9	6.582 86	2.985 93	.003 291 43	.002 938 78	.002 985 93
	7.405 71	3.359 18	.003 702 86	.003 306 12	.003 359 18
1.215 28 2.430 56 3.645 83 4.861 11	1 2 3 4	.453 59 .907 18 1.360 78 1.814 37	.0010 .0015 .0030	.000 446 43 .000 892 86 .001 339 29 .001 785 71	.000 453 59 .000 907 18 .001 360 78 .001 814 37
6.076 39	56789	2.267 96	.0025	.002 232 14	.002 267 96
7.291 67		2.721 55	.0030	.002 678 57	.002 721 55
8.506 94		3.175 15	.0035	.003 125 00	.003 175 15
9.722 22		3.628 74	.0040	.003 571 43	.003 628 74
10.937 50		4.082 33	.0045	.004 017 86	.004 082 33
2.679 23 5.358 46 8.037 69 10.716 91	2.204 62 4.409 24 6.613 87 8.818 49	1 2 3 4	.001 102 31 .002 204 62 .003 306 93 .004 409 24	.000 984 21 .001 968 41 .002 952 62 .003 936 83	.001 1003 1003
13.937 50	11.023 11	56789	.005 511 56	.004 921 03	1005
16.075 37	13.227 73		.006 613 87	.005 905 24	1006
18.754 60	15.432 36		.007 716 18	.006 889 44	1007
21.433 83	17.636 98		.008 818 49	.007 873 65	1008
24.113 06	19.841 60		.009 920 80	.008 857 86	1009
2430.56	2000	907.18	1	.892 87	.907 18
4861.11	4000	1814.37	2	1.785 71	1.814 37
7291.67	6000	2721.55	3	2.678 57	2.721 55
9722.22	8000	3628.74	4	3.571 43	3.628 74
12 152.78	10 000	4535.92	5	4.464 29	4.535 92
14 583.33	12 000	5443.11	6	5.357 14	5.443 11
17 013.89	14 000	6350.29	7	6.250 00	6.350 29
19 444.44	16 000	7257.48	8	7.142 86	7.257 48
21 875.00	18 000	8164.66	9	8.035 71	8.164 66
2722.22	2240	1016.05	1.12	1	1.016 05
5444.44	4480	2032.09	2.24	2	2.032 09
8166.67	6720	3048.14	3.36	3	3.048 14
10 888.89	8960	4064.19	4.48	4	4.064 19
13 611.11 16 333.33 19 055.56 21 777.78 24 500.00	11 200 13 440 15 680 17 920 20 160	5080.24 6096.28 7112.32 8128.38 9144.42	5.60 6.72 7.84 5.96 10.08	5 6 7 8	5.080 24 6.096 28 7.112 32 8.128 38 9.144 42
2679.23	2204.62	1000	1.102 31	.984 21	1 2 3
5358.46	4409.24	2000	2.204 62	1.968 41	
8037.69	6613.87	3000	3.306 93	2.952 62	
10 716.91	8818.49	4000	4.409 24	3.936 83	
13 937.50	11 023.11	5000	5.511 56	4.921 03	5
16 075.37	13 227.73	6000	6.613 87	5.905 24	6
18 754.60	15 432.36	7000	7.716 18	6.889 44	7
21 433.83	17 636.98	8000	8.818 49	7.873 65	8
24 113.06	19 841.60	9000	9.920 80	8.857 86	9

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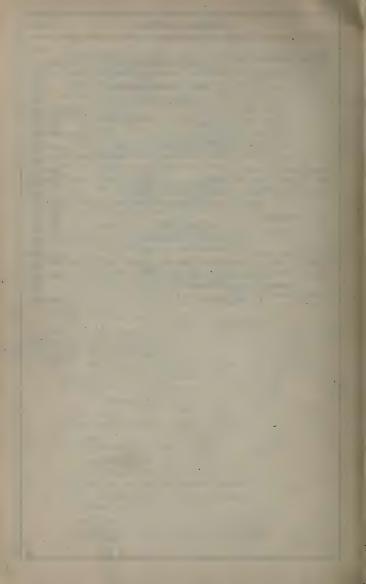
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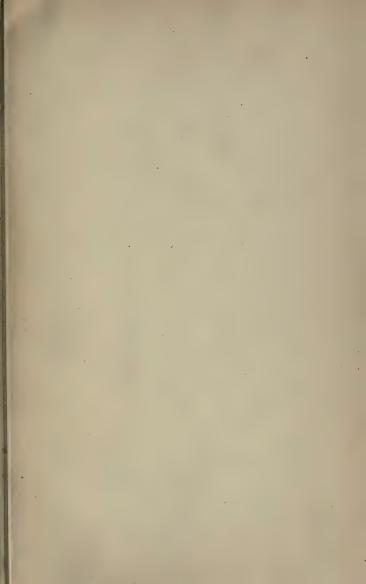
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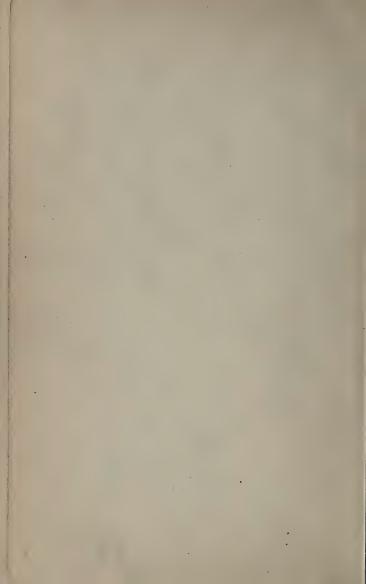
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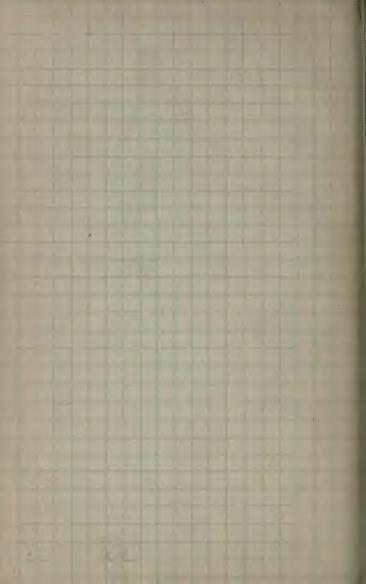














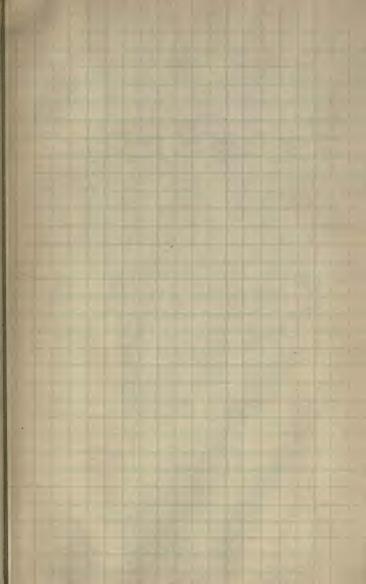


















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